

LONGHORN ARMY AMMUNITION PLANT

KARNACK, TEXAS

ADMINISTRATIVE RECORD

VOLUME 1 of 5

1989

**Bate Stamp Numbers
001910 - 002088**

Prepared for:

**Department of the Army
Longhorn Army Ammunition Plant
Marshall, Texas 75671-1059**

1995

**LONGHORN ARMY AMMUNITION PLANT
KARNACK, TEXAS
ADMINISTRATIVE RECORD - CHRONOLOGICAL INDEX**

VOLUME 1 of 5

1989

- A. Title: Final Report - Phase I RCRA Facility Investigation (RFI)
Active Burning Ground and Unlined Evaporation Pond
Volume 1 - Text**
- Site(s): LHAAP-18 & LHAAP-24 Burning Ground / Washout Pond & Evaporation Pond**
Location: Longhorn Army Ammunition Plant, Marshall, Texas
Agency: U.S. Army Corps Of Engineers, Fort Worth District
Author(s): U.S. Army Corps Of Engineers, Fort Worth District
Recipient: U.S. Army Corps Of Engineers, Huntsville Division
Date: July, 1989
Bate Stamp: 001910 - 002056
- B. Title: Final Report - Phase I RCRA Facility Investigation (RFI)
Active Burning Ground and Unlined Evaporation Pond
Volume 2 - Sheet Drawings**
- Group(s): 2 (Partial)**
Site(s): LHAAP-18 & LHAAP-24 Burning Ground / Washout Pond & Evaporation Pond
Location: Longhorn Army Ammunition Plant, Marshall, Texas
Agency: U.S. Army Corps Of Engineers, Fort Worth District
Author(s): U.S. Army Corps Of Engineers, Fort Worth District
Recipient: U.S. Army Corps Of Engineers, Huntsville Division
Date: July, 1989
Bate Stamp: 002057 - 002088

July 12, 1995

RCRA FACILITY INVESTIGATION

-FOR-

ACTIVE BURNING GROUND

-AND-

UNLINED SEWAGE TREATMENT PLANT

PAGE 1

LONGHORN ARMY AMMUNITION PLANT
KARLECK, TEXAS

VOLUME 1

-PREPARED FOR-

U.S. ARMY ENGINEER DIVISION, HUNTSVILLE
CORPS OF ENGINEERS
HUNTSVILLE, ALABAMA

-PREPARED BY-

U.S. ARMY ENGINEER DISTRICT, FORT WORTH
CORPS OF ENGINEERS
FORT WORTH, TEXAS

JULY 1969

EXECUTIVE SUMMARY

The U.S. Army Corps of Engineers (USACE), Huntsville Division, is contracting on behalf of Longhorn Army Ammunition Plant (LHAAP) to assess ground-water contamination beneath the Active Burning Ground (ABG) area of the installation and to investigate all past solid waste management units at the site that may be contributing to the contaminant plume. The work is being performed as a RCRA facility investigation (RFI) under the authority of the Resource Conservation and Recovery Act (RCRA) of 1976 as modified by the Hazardous and Solid Waste Amendments of 1984. This report documents Phase I of the RFI as it was performed by the USACE, Fort Worth District, for the ABG area and for the unlined evaporation pond (UEP), a surface impoundment located within the bounds of the ABG that was closed as a RCRA interim status unit in 1985. This work was performed between May 1987 and September 1988.

The ABG has been used since 1955 for the treatment, storage, and disposal of solid and liquid explosive, pyrotechnic, and combustible solvent wastes by open burning, incineration, evaporation, and burial. Historical waste management units include open burning pits, the UEP, stockpiles of solvent soaked sawdust, and suspected burial pits. Current waste management activities consist of disposing of explosive and explosive-contaminated wastes by burning and are not suspected to be contributing to the ground-water contamination problem beneath the site.

There have been three ground-water contamination investigations performed at the ABG since the potential for ground-water contamination from operation of the UEP was first recognized in 1981. The results of these studies indicated that ground-water beneath the ABG was contaminated with high concentrations of volatile organic compounds (VOCs) and elevated concentrations of barium. However, the results also showed that another source besides the UEP was contributing to ground-water contamination beneath the western portion of the ABG.

Geotechnical investigations for the Phase I RFI consisted of performing a soil gas survey to assist in siting shallow soil borings and additional monitoring wells, drilling and sampling 47 shallow soil borings to verify contaminant source locations, drilling and geophysically logging four deep test borings to define stratigraphy across the site, installing 12 shallow and 3 intermediate depth monitoring wells, slug testing all 15 newly installed wells, and performing one round of water sampling for the 15 new and 10 existing wells at the site. Results of these investigations are presented below.

Ground water beneath the ABG is contaminated with VOCs and elevated concentrations of chlorides, nitrates, and metals. The two most prevalent and highly concentrated contaminants are trichloroethene and methylene chloride, occurring at concentrations as high as 1,400,000 ug/l for TCE and in excess of 17,000,000 ug/l for methylene

chloride. Chlorides, nitrates, and the metals barium, cadmium, chromium, mercury, and lead were detected at concentrations exceeding Texas Department of Health drinking water standards.

Two sources were verified as contributing to the VOC contamination at the ABG. These are the UEP and remnants of sawdust pits located around the foundation of the air curtain destructor (ACD). A potential third source is a line of 18 burn pits located in the middle of the burn trench area. No sources have yet been investigated for the other contaminants detected.

For the most part, contamination is confined to a shallow zone of the aquifer underlying the ABG area. Significantly lower concentrations of VOC contaminants were detected in the next lower ground-water zone. Ground water in the shallow zone occurs under unconfined conditions. Regional flow is towards Harrison Bayou, about $\frac{1}{4}$ mile to the west and north of the ABG, and towards Caddo Lake, about 1 mile to the north of the ABG. However, the direction of flow across the ABG area varies due to a ground-water mound occurring beneath the site. The horizontal hydraulic gradient is extremely low both regionally and at the ABG. Current data are insufficient to determine the vertical hydraulic gradient. The average horizontal velocity for the shallow ground water monitored by the 12 newly installed wells is approximately 1.5 feet per year.

Most of the ABG site, including the identified source areas, is situated on the outcrop of the Wilcox Group, a highly interbedded

discontinuous series of clays, sands, and silts. The Harrison Bayou floodplain crosses the western corner of the site. The ABG area is situated over the regional Cypress aquifer, the base of which is defined by the contact between the Wilcox and underlying Midway Groups. A confining bed defining the shallow contaminated zone appears to be continuous within the Wilcox across most of the ABG area, but disappears at the floodplain boundary. Contamination has been identified beyond this point, indicating that Wilcox and floodplain materials are hydraulically connected. Because contamination extends laterally beyond the extent of the confining bed into the floodplain, and because it extends vertically beneath the confining bed into at least the intermediate zone of the aquifer, the base of the uppermost aquifer is defined as the base of the Cypress aquifer, which occurs as deep as 150 feet in the ABG area. Vertical plume definition will require monitoring to this depth.

The contaminant plume has not moved significantly over the past 30 years, extending about 200 feet past the fenced boundary of the ABG in the downgradient directions of the UEP, ACD, and row of 18 burn pits. Closure of the UEP removed the source of contamination for that unit. Although construction of the ACD removed much of the source material in the sawdust pits, some material remains within the water table and continues to contribute to ground-water contamination along the western portion of the site. It appears that any source materials in the burn pits have been removed. There

appears to be no immediate threat to surface waters or public water supplies at this time.

Recommendations at this time are to finish defining all possible contaminant sources within the ABG area as well as any others that may be contributing to ground-water contamination beneath the site; to finish characterizing the contaminant plume with respect to hydraulic and chemical properties; to finish defining the horizontal and vertical extent of the contaminant plume; and to investigate whether ground-water contamination has reached the surface waters in the immediate area.

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VOLUME 5

QA/QC Final Report

I.0 INTRODUCTION.

1.1 Scope. The U.S. Army Corps of Engineers (USACE), Fort Worth District, was tasked by the USACE, Huntsville Division, in March 1987 to continue ground-water quality assessment investigations at the Active Burning Ground (ABG) area of Longhorn Army Ammunition Plant (LHAAP) for the purpose of determining the source of organic contamination detected in the ground water underlying the western corner of the site. This report documents all Phase I efforts as required by the scope of work, contained in Appendix A. Phase I was modified several times due to evidence found and results obtained during the course of this investigation. This report addresses all Phase I tasking and these modifications.

1.2 Authority. The work described in this report was performed under the authority of the Resource Conservation and Recovery Act (RCRA) of 1976 as modified by the Hazardous and Solid Waste Amendments (HSWA) of 1984. The work was performed by the USACE, Fort Worth District, for the USACE, Huntsville Division, following the scope of work contained in Appendix A. Huntsville Division, in accordance with its Memorandum of Understanding with the U.S. Army Armament, Munitions, and Chemical Command (AMCCOM), prepared the scope of work on behalf of LHAAP.

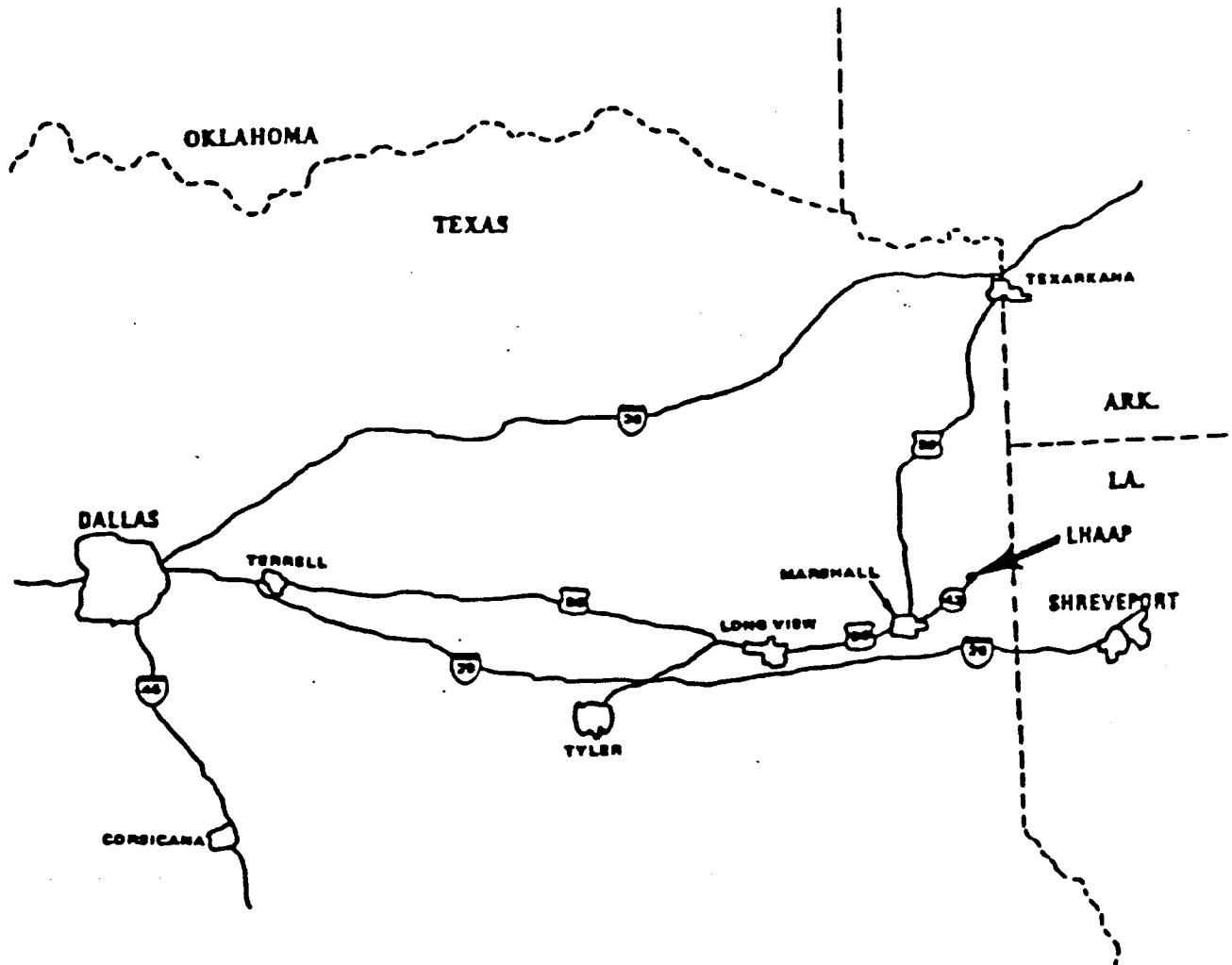
2.0 BACKGROUND INFORMATION.

2.1 General. Longhorn Army Ammunition Plant is a government-owned, contractor-operated industrial installation under the jurisdiction of the U.S. Army Armament, Munitions, and Chemical Command with the primary mission to load, assemble, and pack pyrotechnics, illuminating/signal ammunition, and solid rocket propellant motors. The Longhorn Division of Morton Thiokol, Inc., is the current operating contractor.

2.2 Location. Longhorn Army Ammunition Plant is located in Harrison County, Texas, approximately 14 miles northeast of Marshall, Texas, and approximately 40 miles west of Shreveport, Louisiana. The small communities of Karnack and Uncertain, Texas, lie along the western and northern boundaries of LHAAP, respectively. The installation occupies 8,493 acres between State Highway 43 and the western shore of Caddo Lake. A location map is shown on Figure 1.

2.3 Active Burning Ground. The ABG is located in the southeast quadrant of LHAAP, as shown on Figure 2. It is a 34.5-acre fenced, secured area that has been in operation since 1955. The area has been used for the treatment, storage, and disposal of solid and liquid explosive, pyrotechnic, and combustible solvent wastes by open burning, incineration, evaporation, and burial. Historical waste management units include open burning pits, an unlined evaporation pond (UEP), stockpiles of solvent soaked sawdust, and suspected burial pits.

Since the closure of the UEP, all ABG waste management activities



3

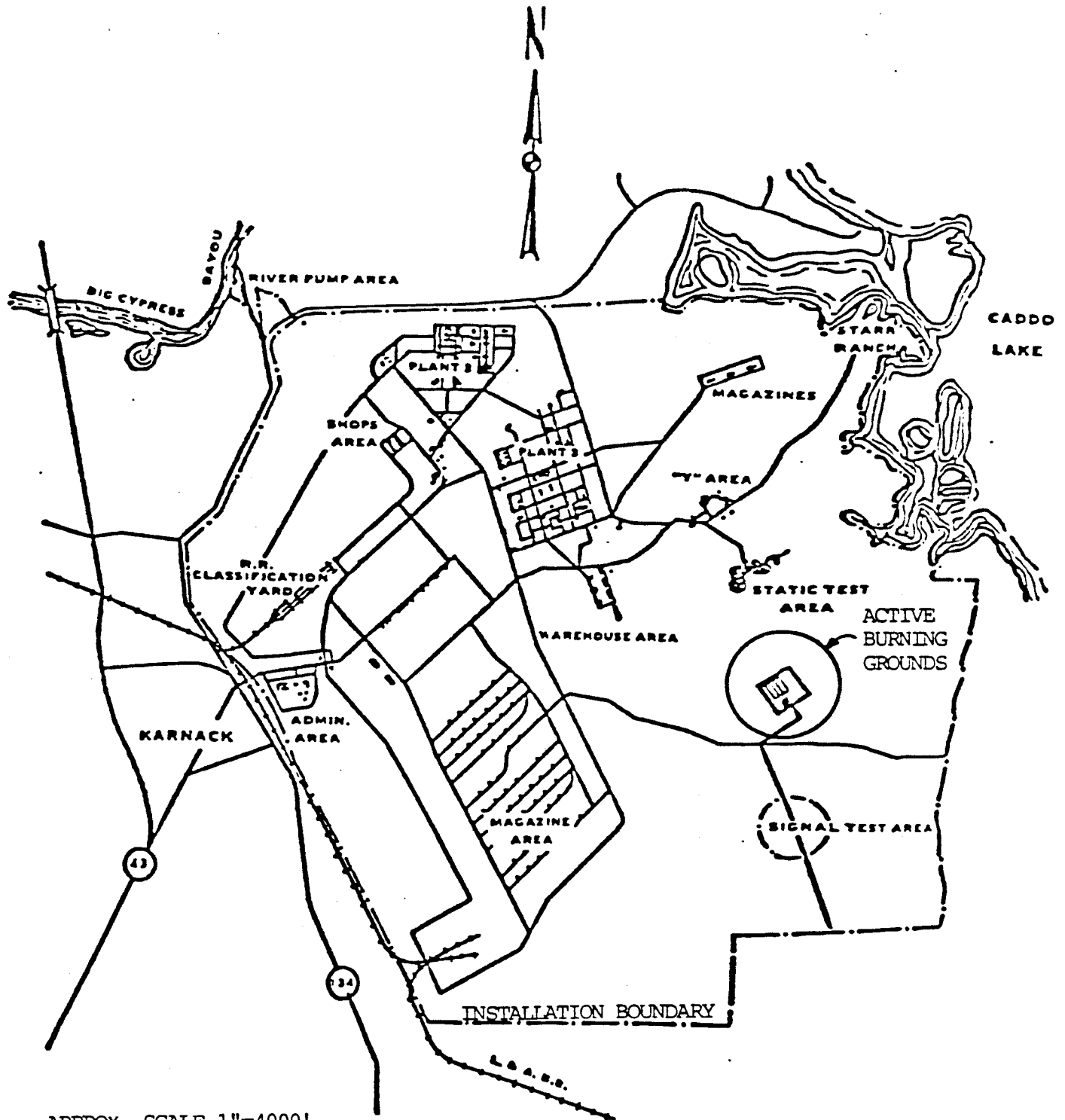


Figure 2. Location Map for Active Burning Grounds.

have been restricted to disposing of explosive and explosive-contaminated wastes by burning. Disposal of these wastes is currently performed using an air curtain destructor (ACD), three open burning cages, and two open burning pans. There is also a washout pad with a covered concrete sump servicing these operations. Two other contained sumps are located at the ACD. Locations of these facilities, as well as the location of the closed UEP, are shown on Figure 3. These ongoing waste management activities are addressed under LHAAP's RCRA Part B and are not suspected to be contributing to any ground-water contamination problem beneath the site.

2.4 Unlined Evaporation Pond. The UEP, located in the northern corner of the ABG, was constructed in 1963. It was originally used as a holding pond to store explosive wastes resulting from the washout of rocket motor casings. However, in 1973 the pond also began receiving wash water containing solvent residues and solids collected from LHAAP operations involving pyrotechnic material preparation and mixing. Wastes received by the UEP contained significant concentrations of several metallic cations such as aluminum, arsenic, barium, cadmium, chromium, iron, lead, magnesium, sodium, strontium, and zinc; nonmetallic anions such as nitrate/nitrite and phosphates; and organic solvents including trichloroethene (TCE), trichloroethane, acetone, ethyl alcohol, methyl ethyl ketone, methylene chloride, and toluene. Sawdust soaked with methylene chloride and other solvents that were used to clean and scour mixers used for mixing illuminants were also

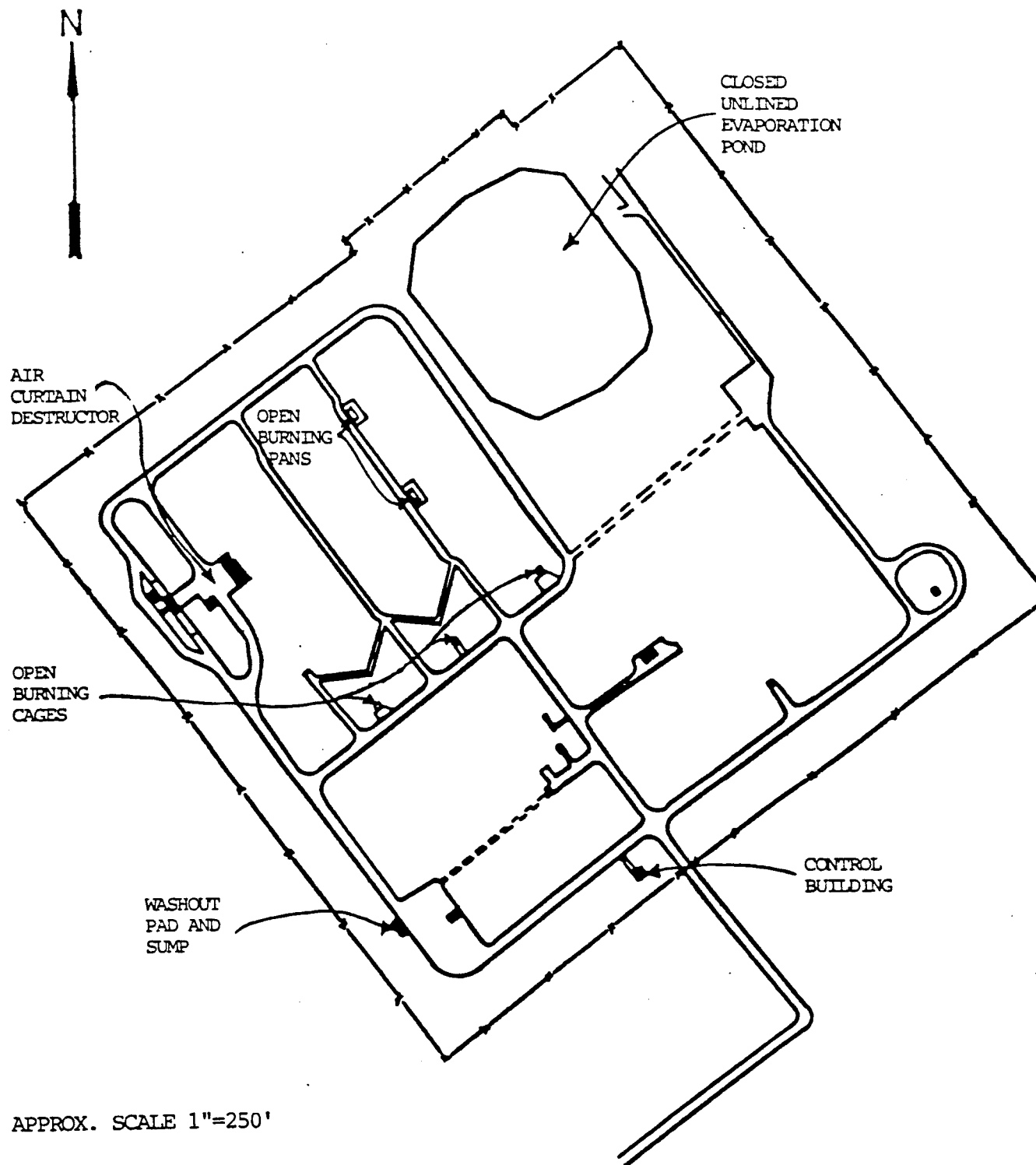


Figure 3. Current Features of Active Burning Grounds.

stockpiled along the southern berms of the UEP.

By 1983, the Army had completed two preliminary studies which indicated that ground water in the ABG area was contaminated with metallic and organic compounds. These studies are documented in the following reports:

- o Ground-Water Quality Assessment Plan, Hazardous Waste Special Study No. 32-26-0252-83, USAEHA, 28 March - 1 April 1983.

- o Longhorn Army Ammunition Plant Contamination Survey, Morton Thiokol Report No. 16651, prepared by Environmental Protection Systems, Inc., for USATHAMA, Contract No. DAAA09-78-C-3004, June 1984.

As part of the USAEHA study, 13 monitoring wells were installed at the UEP in 1980. Five of these wells (BH-3, BH-4, BH-7, BH-11, and BH-22) still exist at the site. The others were plugged as part of the closure of the UEP in 1985. The USATHAMA contamination survey resulted in the installation of 10 wells (101, 102, 109, 120, 123, 124, 125, 126, 129, and 130) within and around the ABG in 1982. All of these wells still exist, and except for wells 126 and 130, continue to be sampled quarterly by LHAAP. Well locations for these two studies are shown on Sheet 1. Analytical results for the two most prevalent hazardous constituents detected in these wells - methylene chloride and TCE - are summarized on Tables 1 and 2, respectively.

Because operation of the UEP appeared to be responsible for contaminating the ground water at the ABG, the Army ceased operation of the UEP in 1984 and began formal closure activities for the unit as an interim status surface impoundment following RCRA regulations. In 1985, all liquid, sludge, and soil contaminated with barium and

TABLE 1. METHYLENE CHLORIDE CONCENTRATIONS (ug/l) FROM PREVIOUS GROUND-WATER INVESTIGATIONS AND SAMPLING EVENTS

Well No.	USA/EHA ^a	USACE ^b		USEPA ^c	IHAAP ^d USACE ^e	USACE ^e	IHAAP ^d																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
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ND = Not detected or detected below calibration limits.

^aGround-Water Quality Assessment Plan, Hazardous Waste Special Study No. 32-26-0252-83, USAEHA, 28 March - 1 April 1983, as referenced in Groundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, USACE, 15 March 1985

^bGroundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, USACE, 15 March 1985

^cEPA Groundwater Monitoring Evaluation, Longhorn Army Ammunition Plant (IHAAP), Marshall, Texas, USEPA, 13 January 1986

^dIHAAP quarterly monitoring program

^eGroundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, Addendum, USACE, 8 May 1986

^fPlugged as part of UEP closure 1984-85.

001929

TABLE 2. TRICHLOROETHENE CONCENTRATIONS (ug/l) FROM PREVIOUS GROUND-WATER INVESTIGATIONS AND SAMPLING EVENTS

Well No.	USAEHA ^a	USACE ^b		USEPA ^c	LHAAP ^d USACE ^e	USACE ^e	LHAAP ^d								
		7/84	9/84				5/86	9/86	12/86	3/87	7/87	9/87	1/88		
BH-1 ^f															
BH-2 ^f	198	ND	1,100												
BH-3	30	8,400	6,200												
BH-4	140	ND	500												
BH-5 ^f	39,200	480													
BH-6 ^f	14,000	52,000	120,000												
BH-7		ND	1,600												
BH-8 ^f		ND	250												
BH-10 ^f		ND	ND												
BH-11		140,000	160,000												
BH-22		ND	1,100												
101					ND		ND	ND	ND	ND	ND	ND	ND	ND	ND
102					ND		ND	ND	ND	ND	ND	ND	ND	ND	ND
109		ND	ND		110		110	110	45	140	33	160	120		
120		12,000	27,000		29,000		20,000	37,000	22,000	195,000	27,000	50,000	23,000		
123		ND	ND		ND		ND	ND	ND	29	ND	4	ND		
124		ND	ND		ND		5	ND	ND	15	ND	ND	28		
125		ND	ND		4		ND	ND	ND	ND	ND	22	ND		
126		ND	ND												
129		11,000	18,000		7,400	ND	3,300	13,000	5,100	5,590	3,500	9,300	4,300		
130															
C-1			ND	ND											
C-2			4,700			ND									
C-3			1,300			ND									
C-4			ND	ND											
C-5			2,500	ND											
C-6															
C-7															
C-8															
C-9						ND									
C-10						ND									
Field Blank		ND	ND			ND									
Field Blank		ND	ND			ND									
Trip Blank		ND	ND			ND									

ND = Not detected or detected below calibration limits.

^aGround-Water Quality Assessment Plan, Hazardous Waste Special Study No. 32-26-0252-83, USAEHA, 28 March - 1 April 1983, as referenced in Groundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, USACE, 15 March 1985

^bGroundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, USACE, 15 March 1985

^cEPA Groundwater Monitoring Evaluation, Longhorn Army Ammunition Plant (LHAAP), Marshall, Texas, USEPA, 13 January 1986

^dLHAAP quarterly monitoring program

^eGroundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, Addendum, USACE, 8 May 1986

^fplugged as part of UEP closure 1984-85.

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exhibiting high COD values, were removed from the pond and were disposed in accordance with EPA regulations. The pond was then backfilled and capped. The Texas Water Commission (TWC) certified in March 1986 that the UEP was clean closed. The unit was replaced with an industrial wastewater treatment facility located elsewhere on LHAAP.

Upon closure of the UEP, LHAAP began a quarterly monitoring program for eight of the remaining wells in the ABG area. Analytical results from this ongoing program are summarized on Tables 1 and 2 for the two most prevalent hazardous constituents detected, which are methylene chloride and TCE, respectively. The Army also implemented a Ground-Water Quality Assessment (GWQA) for contamination caused by past operation of the UEP. The consulting engineering firm Camp Dresser & McKee, Inc. (CDM) performed the GWQA under contract to the USACE, Huntsville Division. Results of this GWQA are contained in the following two documents:

- o Groundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, prepared by Camp Dresser & McKee, Inc. (CDM), for USACE, Huntsville Division, Contract No. DAC87-830-C-0091, March 15, 1985.

- o Addendum to Groundwater Quality Assessment, Longhorn Army Ammunition Plant, Marshall, Texas: Groundwater Contamination Related to Seepage from an Unlined Evaporation Pond, prepared by CDM for USACE, Huntsville Division, Contract No. DAC87-830-C-0091, May 8, 1986.

Camp Dresser & McKee, Inc., concluded that the UEP was a secondary source, but not the primary source, of ground-water contamination within the ABG area. During CDM's investigation, organic contamination

measured in wells monitoring the UEP unexpectedly decreased to nearly detectable and undetectable concentrations. Laboratory error was ruled out as an explanation for the sudden decrease when the laboratory results were duplicated during subsequent samplings performed by CDM, EPA, and USAEHA. These analyses are shown on Tables 1 and 2. Although several theories were posed to explain this disappearance of ground-water contamination around the UEP, none were satisfactory or could be proven.

Camp Dresser & McKee, Inc., also concluded that the primary source of organics contamination that continues to be detected in wells in the western corner of the ABG is not the UEP, but a source located west of the pond. A major source of inorganic contamination, primarily barium, appears to be located south of the UEP beyond the ABG boundary. Due to contract limitations, these sources were not able to be determined by CDM.

In response to the CDM conclusions, the Army developed a proposal for continued ground-water monitoring and assessment efforts at the ABG. This document, prepared by USACE, Huntsville Division, titled "U.S. Army Proposal for Additional Groundwater Monitoring at the Closed Unlined Evaporation Pond (UEP), Longhorn Army Ammunition Plant (LHAAP), Marshall, Texas," was submitted by LHAAP to the TWC in April 1987. The Army's proposal consisted of a three-phase program, summarized as follows:

- o Implement a Compliance Monitoring Program at the Point of

Compliance of the UEP in order to demonstrate that the UEP is no longer a source of ground-water contamination. This will include the installation and quarterly sampling of six new wells.

- o Implement a Corrective Action Monitoring Program downgradient of the UEP in order to demonstrate that contaminants in the ground water resulting from operation of the UEP are not present in significant concentrations. This will include the quarterly sampling of four existing wells in addition to the six new wells.

- o Continue Ground-Water Quality Assessment investigations in the ABG area in order to determine the source of inorganic contaminants south of the ABG and organic contamination from within the ABG.

In March 1987, Huntsville Division tasked Fort Worth District with the scope of work contained in Appendix A to perform a GWQA investigation at the ABG as described in the Army's proposal to TWC. Included in this scope of work was the installation and one-time sampling of the six compliance monitoring wells at the UEP. Fort Worth District installed these wells, designated as MW-1 through MW-6 on Sheet 1, in August and September 1987. Longhorn AAP incorporated the wells into their quarterly sampling program in May 1988. The installation and sampling of these wells by Fort Worth District have been incorporated into this investigation because the UEP, which received waste after 26 July 1982, meets the definition of a solid waste management unit as it is stated in 31 TAC 335.156(a)(2).

3.0 GEOLOGIC SETTING.

3.1 Regional. Longhorn Army Ammunition Plant is situated on an outcrop of the Wilcox Group, which crops out over a large part of the eastern half of Harrison County, as shown on Figure 4. The Wilcox has a maximum thickness of 700 feet, and consists mostly of fine to medium grained sands interbedded with a considerable amount of clay and seams of lignite. Although sand beds up to 50 feet thick are present locally, individual beds are generally lenticular, with lenses of clay, sand, and silt pinching out or grading into each other over very short distances, making correlation difficult.

The Wilcox has been identified by the Texas Water Development Board in Report 27, "Ground-Water Resources of Harrison County, Texas", as the basal unit of the regional Cypress aquifer. The Cypress aquifer outcrops over most of Harrison County and is comprised of, in ascending order, the Wilcox Group, the Carrizo Sand, the Reklaw Formation, and the Queen City Sand. All units are believed to be hydraulically connected. A brief description of each of these units is provided on Figure 5. These units dip to the northwest into the East Texas syncline, while the ground surface generally dips gently to the southeast.

The availability of ground water in Harrison County is largely dependent on the hydrologic characteristics of the units comprising the Cypress aquifer. The Wilcox Group, outcropping in the area of LHAAP, yields small (<50 gpm) to moderate (50-500 gpm) quantities

System	Series	Group	Unit	Approximate maximum thickness (feet)	Character of rocks	Water-bearing properties
Quaternary	Recent and Pleistocene		Alluvium and terrace deposits (undivided)	50	Predominantly clay, silt, and fine sand. Terrace material locally fine to coarse sand.	Yields small quantities of water to a few wells
Tertiary	Eocene	Claiborne	Sparta Sand	25	Fine sand and sandy clay. Limonitic ironstone seams common in outcrop area.	Do.
			Wichita Greensand	50	Fine to medium sand, glauconitic and quartzitic, laminar to cross-bedded. Limonitic ironstone seams and concretions common in outcrop area.	Do.
			Queen City Sand	200	Very fine to medium sand, quartzitic, interbedded with silt and clay, laminar to cross-bedded. Contains minor amounts of lignite. Limonitic ironstone seams common in outcrop area.	Cypress aquifer
			Reklav Formation	100	Clay and fine sand, glauconitic and quartzitic, mostly laminar but locally cross-bedded. Locally contains marine fossils. Limonitic ironstone seams common in outcrop area.	
			Carrizo Sand	100	Fine to medium sand interbedded with silt and clay. Laminar to cross-bedded. Limonitic ironstone seams common in outcrop area.	
		Wilcox		700	Fine to medium sand interbedded with considerable amounts of clay. Commonly contains seams of lignite. Limonitic ironstone seams common in outcrop area.	
	Paleocene	Midway		900	Predominantly marine clay; becomes silty in upper part.	Not known to yield fresh water in Harrison County.

Source: Texas Water Development Board Report 27,
Ground-Water Resources of Harrison County,
Texas, August 1966

Figure 5. Geologic Units of Harrison County, Texas.

of fresh water to wells throughout the county. As the basal unit of the Cypress aquifer, the Wilcox is also considered as the base of fresh water in the area, conformably overlying the Midway Group, a predominantly calcareous clay that does not yield water but tends to serve as a relatively impermeable basement to the overlying waterbearing Wilcox. The base of the Wilcox, as does the base of overlying units, slopes westward, ranging from el. 193 feet above mean sea level (msl) in the east central part of the county to more than 750 feet below msl in the northwest corner of the county. A geologic section depicting the regional slope is shown on Figure 6. Contoured elevations approximating the base of the Wilcox are shown on Figure 7. In the vicinity of LHAAP, and specifically in the area of the ABG, this bottom elevation of the Wilcox shows to be around el. 50.

3.2 Active Burning Grounds. The ABG is located in the southeast quadrant of LHAAP, slightly west of the crest of a small topographic divide between Harrison Bayou and Saunders Branch, the two principal drainage basins for the southern part of the installation. The ABG is located approximately $\frac{1}{4}$ mile east of Harrison Bayou, which drains the site, and approximately 1 mile southwest of Caddo Lake, into which Harrison Bayou flows. The location of the ABG with respect to geology, topography, and surface features is shown on Figure 8.

Most of the fenced area of the ABG is on Wilcox materials. However, there appears to be a contact between the primary materials of the

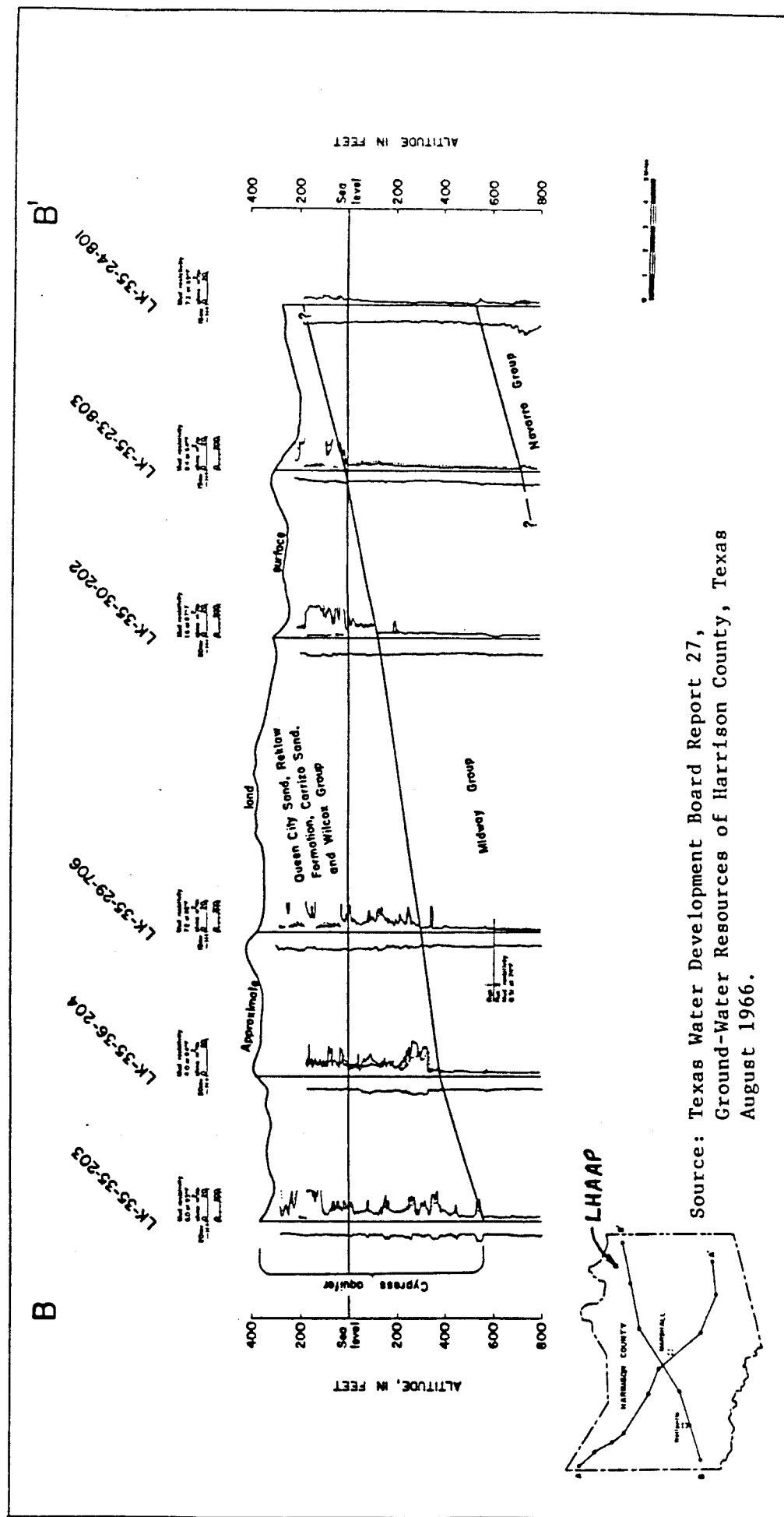
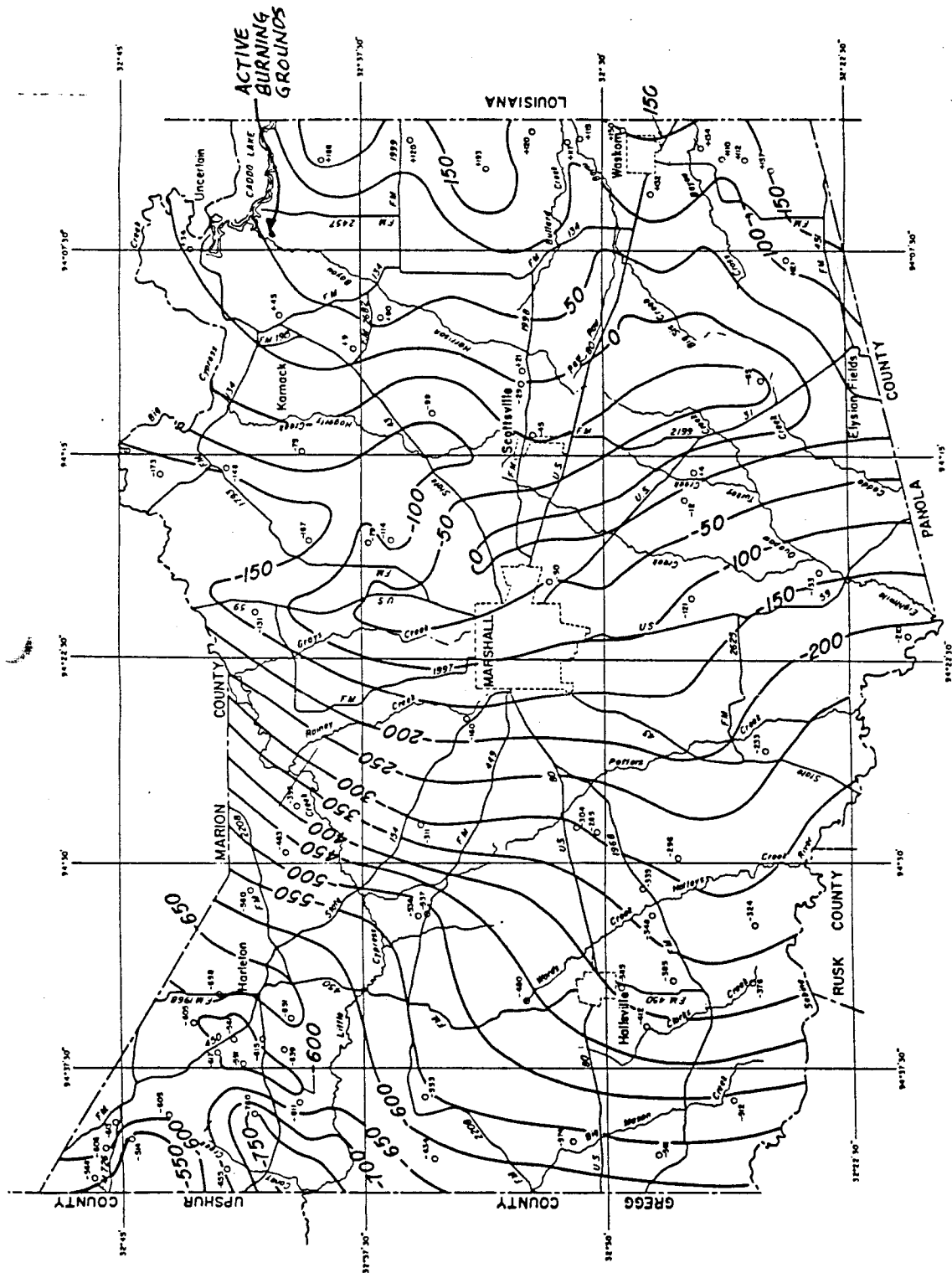


Figure 6. Geologic Section Across Harrison County, Texas.



EXPLANATION

--- 400 ---

Structure Contour
Drawn at the base of the Cypress aquifer
Contour interval 50 feet
Datum is mean sea level

NOTE: The contours also represent the
approximate altitude of the base of the
the Wilcox Group

Source: Texas Water Development Board Report 27,
Ground-Water Resources of Harrison County, Texas,
August 1966.

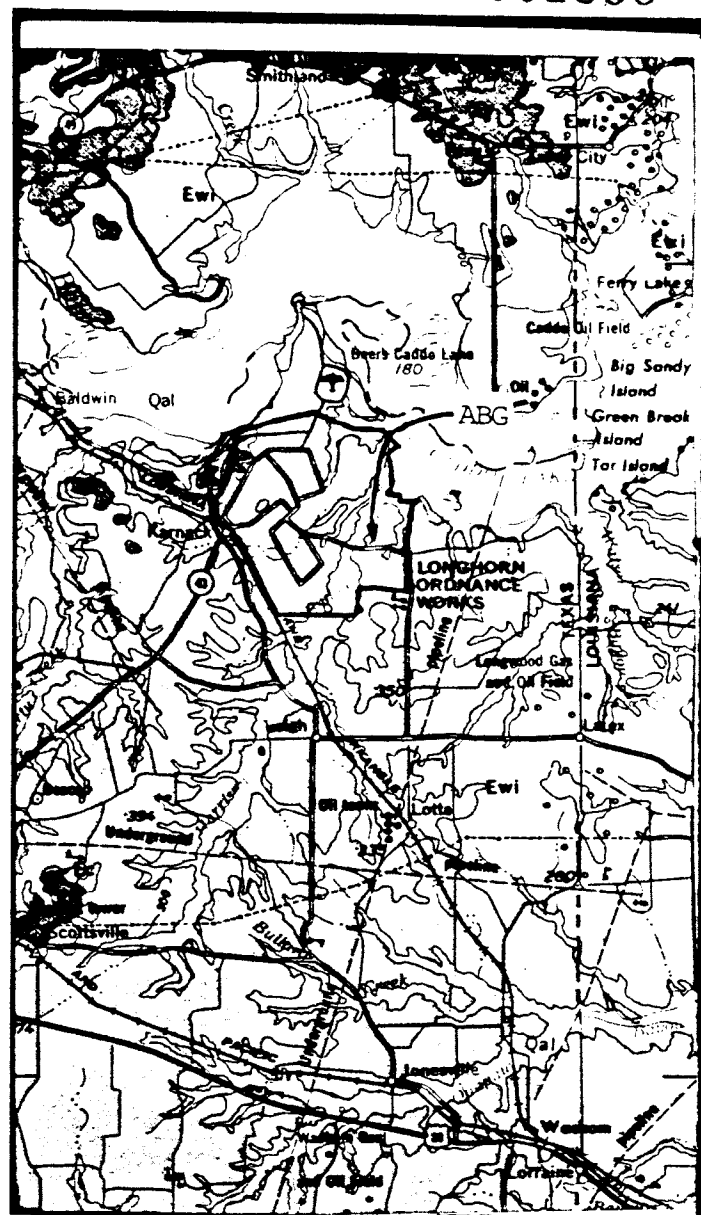
0 1 2 3 4 5 Miles

Figure 7. Approximate Elevation of Base of Cypress Aquifer,







Contour interval 10 feet. Not to scale.

Source: USGS Potters Point Quadrangle,
7.5 minute series, 1978.



LEGEND

	
Alluvium	Carrizo Sand
	
Reklaw Formation	Wilcox Group undivided

Contour interval 100 feet. Scale 1:250,000

Source: Bureau of Economic Geology,
Geologic Atlas of Texas,
Tyler Sheet, 1965.

Figure 3. Geology and Topography of the ABC Area.

Wilcox and Recent alluvium deposited by Harrison Bayou running somewhere across the western corner of the site. This contact appears to approximate both el. 180 shown on Figure 8, and the 100-year floodplain elevation for Harrison Bayou, shown on Sheet 1.

3.3 Water Supplies. There are no water supply wells on LHAAP. Well 602, shown on Figure 9, was constructed on the installation in 1942 as a standby well and is no longer in use. The installation obtains its water supply from Big Cypress Bayou at a pump station located approximately 1 mile northwest of LHAAP. The city of Marshall, Texas, also obtains its water supply from Big Cypress Bayou at a pump station located upstream of LHAAP's.

There are two public supply wells still in use in the area. One, well number 502 on Figure 9, is located in and owned by Caddo Lake State Park. It is completed to a depth of 315 feet (el. -5) and has been in use since 1935. The other public supply well, well number 801 on Figure 9, is owned by the Karnack Water Supply Corporation and services the town of Karnack. It is located approximately $\frac{1}{2}$ mile southeast of town. The well is 430 feet deep (el. -165), and the pump is set at a depth of 200 feet (el. 65). It has been in use since 1942. Two other public water supply wells are shown near LHAAP on Figure 9. These wells, numbers 504 and 902, are owned by the Karnack School and the George Washington Carver School, and are used as standby wells only. Well 504 is 265 feet deep (el. 0) and well 902 is 105 feet deep (el. 135).

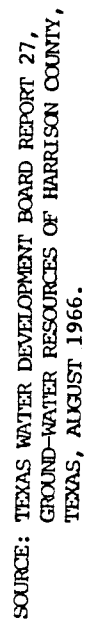


Figure 9. Water Supply Well Location Map, Harrison County, Texas

All other wells in the area of LHAAP are used for stock and domestic purposes. These wells are typically around 250 feet deep, bottoming at approximate el. 0. Well 402, a domestic supply well, is the closest well to the ABG, but due to insufficient supply, is no longer used. The next nearest well to the ABG is well 701, located approximately 2 miles southeast of the ABG. It is a 36-foot deep hand dug well used for domestic purposes.

Caddo Lake, which borders the northeastern edge of LHAAP, is created by Caddo Dam on Big Cypress Bayou in Caddo Parrish, Louisiana. The original dam was constructed in 1914 for local navigation purposes and was reconstructed in 1971. The lake provides the municipal water supply for Oil City, Louisiana, and for Mooringsport, Louisiana. Cooling water is also withdrawn from the lake by a steam-electric power plant located near Mooringsport.

Based on these various types of water supplies for the area around LHAAP, ground-water contamination originating at the ABG would pose the biggest threat to Caddo Lake by either discharging directly into Harrison Bayou upstream of the lake or by discharging directly into the lake itself. Ground-water contamination from the ABG poses little to no threat to any of the area's supply wells unless contamination has reached the base of the Cypress aquifer, in which case discharge to surface waters downdip of the site would be bypassed, threatening wells located northwest of the site and constructed at the base of the Cypress aquifer. The two most likely threatened wells in this

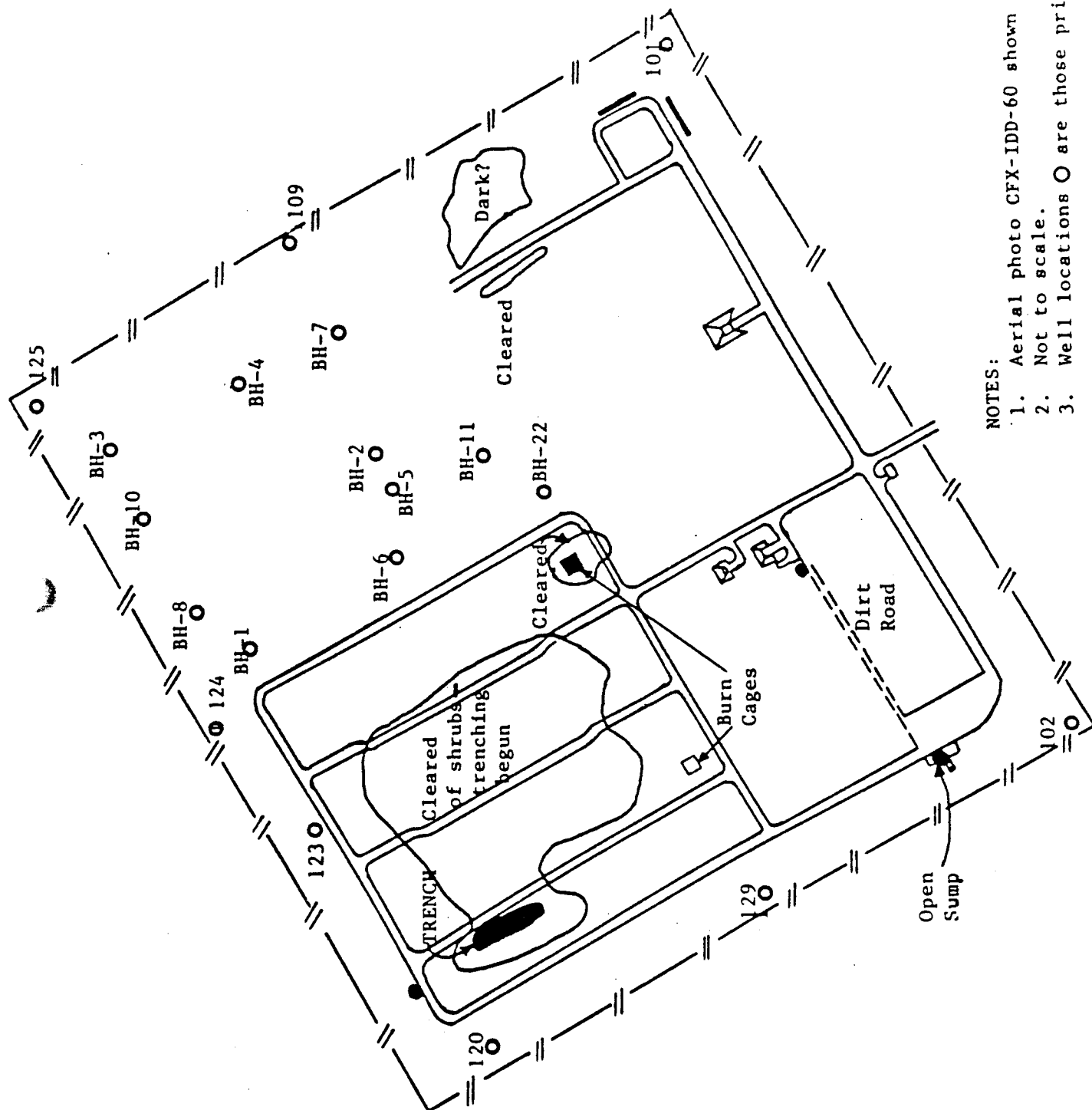
case are public supply well 502 in Caddo Lake State Park and domestic supply well 503. Both wells are located approximately 4 miles from the ABG.

4.0 INVESTIGATION FOR CONTAMINANT SOURCES.

4.1 Records Search. Aerial photos of the ABG taken in 1954, 1963, 1970, 1978, 1980, and 1985 were reviewed in an attempt to identify possible sources, specifically trenches, that may be causing the ground-water contamination underlying the western corner of the site. Aerial photos taken in 1963 and 1970, shown on Figures 10 through 13, showed possibly three trenches located directly upgradient of the contaminated well 120. The aerial photos showed these trenches to be located immediately beneath where the ACD is now situated. The USACE, Fort Worth District, administered the design and construction of the ACD (Contract No. DACA63-78-B-0010), which was built in 1979 and began operation in 1980. Survey data of the site gathered by the Fort Worth District in 1976 noted the existence of the two westernmost trenches, shown in the aerial photos, as "wastewater ponds." Soil borings drilled by the Fort Worth District in 1976 as part of the foundation design analysis identified a "muck" layer varying from 1.3 to 4.6 feet in thickness occurring from approximate elevations 173.9 to 178.5 in borings 3A-769, 6D-770, and 8A-771, situated between the two westernmost trenches shown in the photos. A fourth boring, 8A-772, did not encounter any "muck" material. These four boring locations are shown on Figure 14. The geologic logs are shown on Sheet 3. The as-builts for the destructor show this "muck" layer was removed during construction, but only to the lateral extent of the ACD foundation. The third easternmost trench, visible in both



Figure 10. Aerial Photo (CFX-IDD-60) of Active Burning Grounds,
LHAAP, 4-30-63.



NOTES:

1. Aerial photo CFX-IDD-60 shown on Figure 10.
2. Not to scale.
3. Well locations O are those prior to 1987.

Figure 11. Sketch of Active Burning Ground Features from
Aerial Photo CFX-IDD-60, 4-30-63.

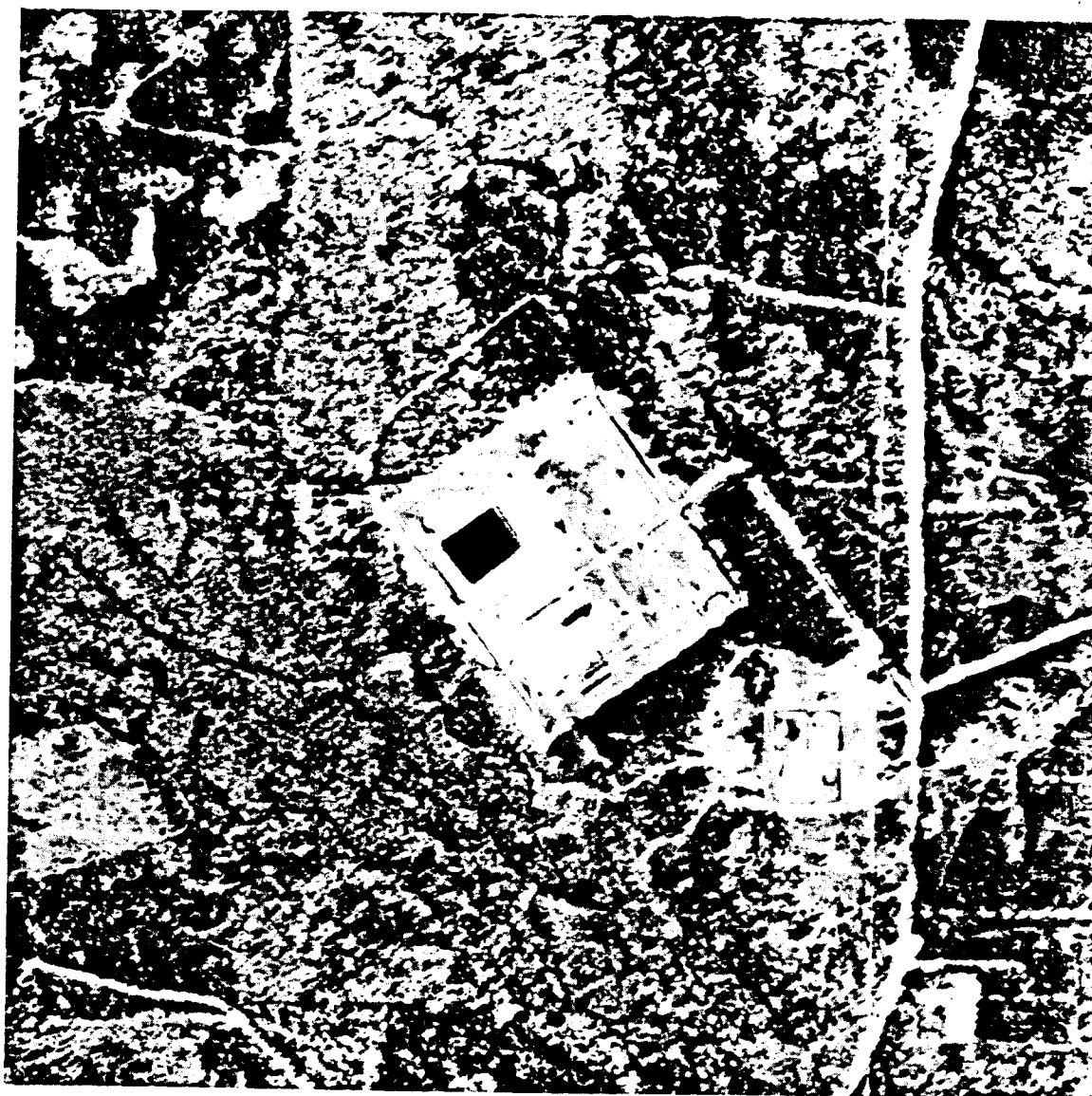


Figure 12. Aerial Photo (CFX-ILL-60) of Active Burning Grounds, LHAAP, 1-30-70.

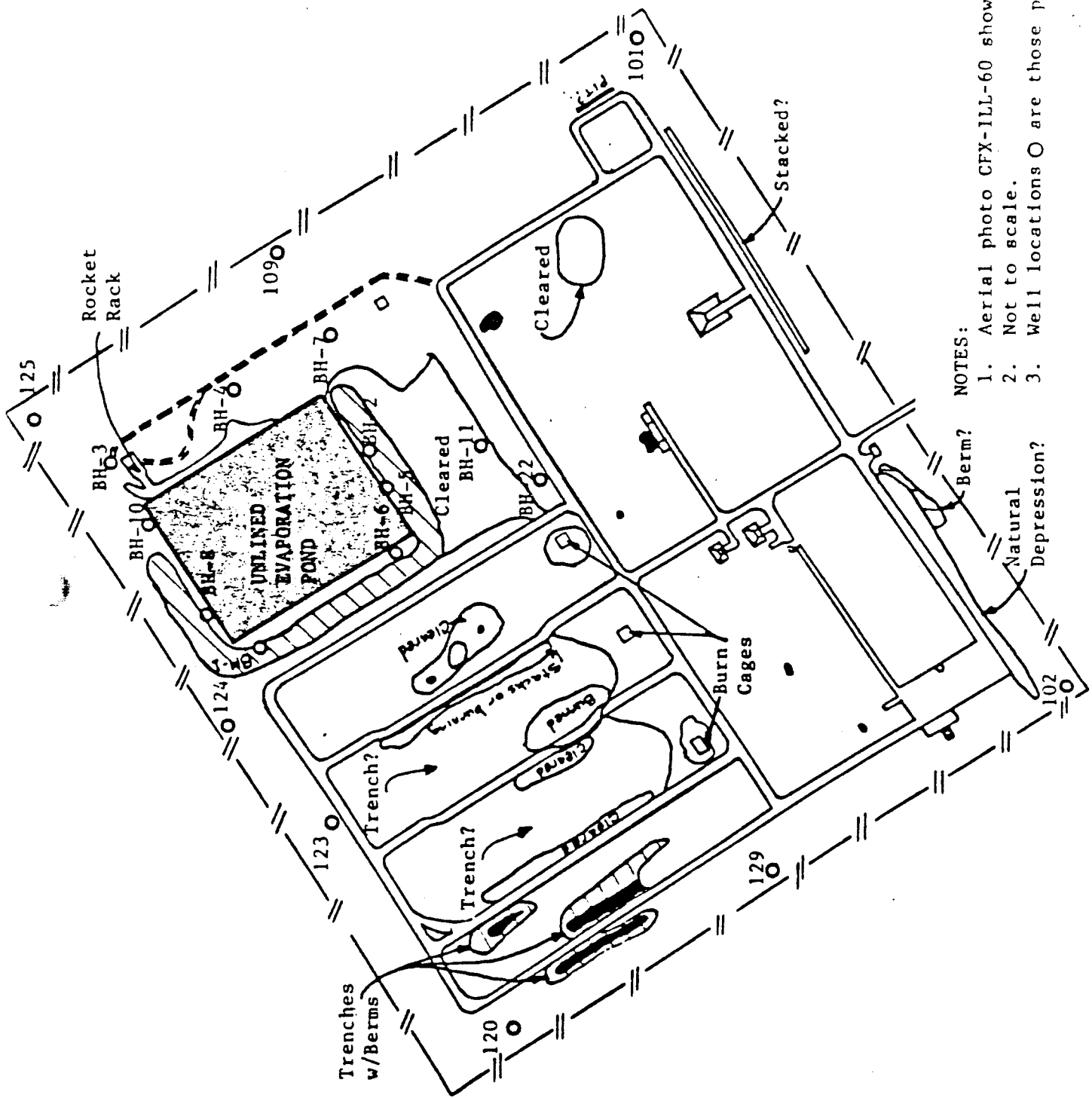


Figure 13. Sketch of Active Burning Ground Features from Aerial Photo CFX-III-60. 1-30-70

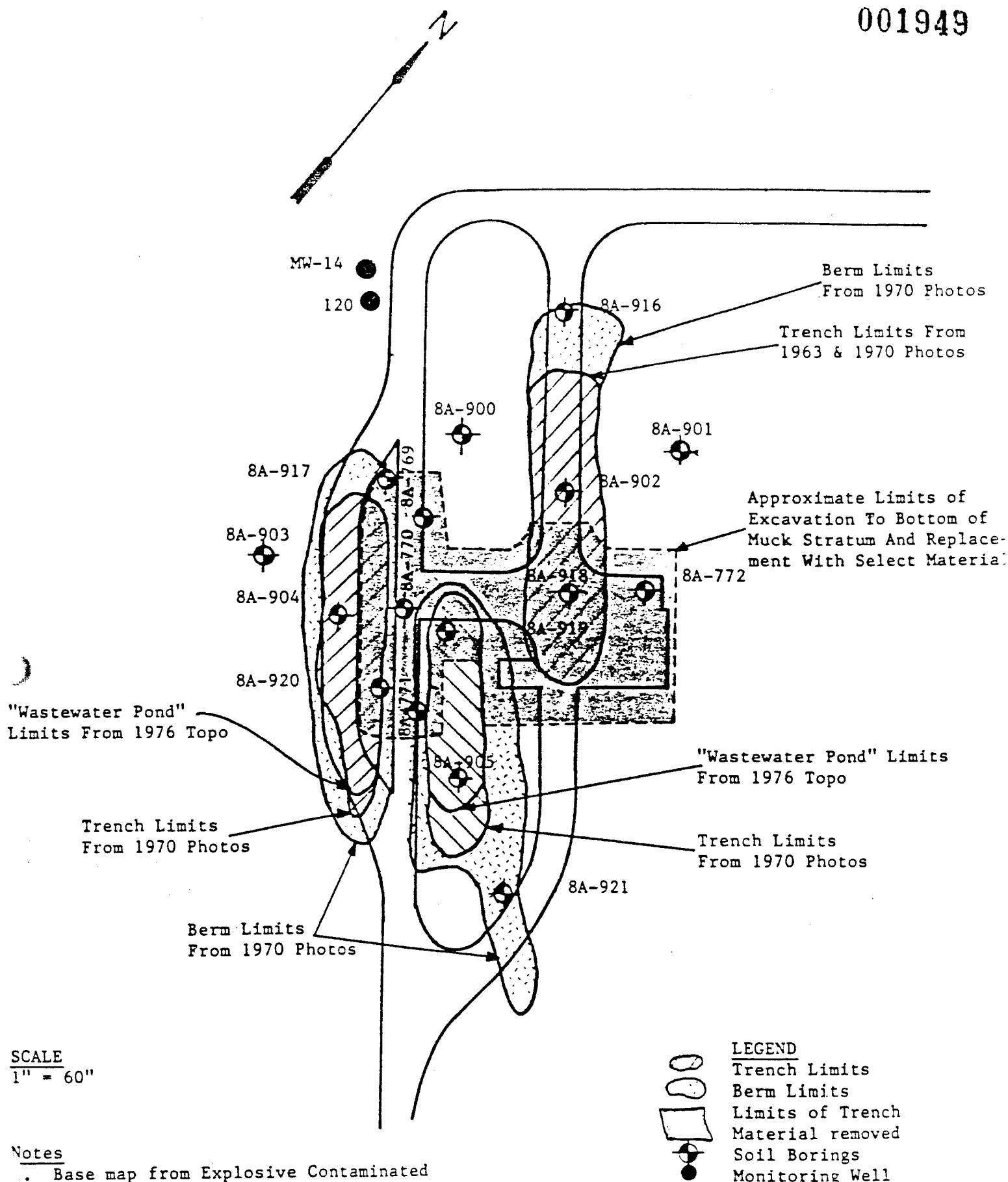


Figure 14. Trench Detail Beneath Air Curtain Destructor.

aerial photos, is not referenced in the survey data or on the as-builts for the project. This is the oldest of the three trenches, and it may have been buried prior to construction of the ACD. Figure 14 depicts the locations of the three trenches identified in the aerial photos as they relate to the as-builts for the ACD.

Existence of these trenches was further confirmed during a site visit to LHAAP in May 1987 by interviewing two longtime Morton Thiokol, Inc., employees familiar with past operations at the site. They indicated these trenches were used for the disposal of sawdust soaked with methylene chloride and other solvents. These materials were used to clean and scour mixers used for mixing illuminants, as documented in USAEHA Hazardous Waste Special Study No. 39-26-0215-83. The employees said that the trenches were approximately 3 to 4 feet deep and extended along the road to facilitate disposal. Periodically, the trenches were cleaned out and the contents ultimately disposed in the old landfill at LHAAP.

4.2 Geophysical Investigation. Prior to confirmation of the exact location of these trenches, plans were made to conduct a geophysical survey in the western corner of the ABG to assist in locating any buried trenches or pits suspected to be the source of contamination for well 120. The USACE Waterways Experiment Station (WES) recommended an electromagnetic (EM) survey to yield the most data by not only locating buried trenches, but possibly assisting in defining the extent of the contaminant plume. However, after visiting the site and seeing

the latest evidence indicating the trenches were most likely located beneath the ACD, WES determined that an EM survey would not be productive because the furnace structure and topographic relief would cause too much interference, making reliable interpretation of any geophysical data difficult. Therefore, geophysical survey plans were abandoned and were replaced with plans to conduct a soil gas survey, to be followed by a soil sampling program, to verify the locations of the trenches and any other source materials at the ABG.

4.3 Soil Gas Survey. A soil gas survey was performed at the site by Tracer Research Corporation from Tucson, Arizona, under contract to Fort Worth District, the week of 28 September 1987. The methodology and sampling, analytical, and quality assurance/quality control procedures are detailed in the Tracer Research final report, contained in Appendix B. It was originally anticipated that methylene chloride and TCE would be the two VOCs monitored. However, after the first day of monitoring for both of these VOCs in the vicinity of well 120 where it was known there were high concentrations of both compounds in the ground water, methylene chloride was not detected. Trichloroethene showed up well, however, and appeared to correspond with expected concentration trends in that area. Since ground-water data had shown a reasonably good correlation between methylene chloride and TCE concentrations (see Tables 1 and 2), and because TCE is a VOC more suited to soil gas sampling, the remainder of the survey was spent monitoring only TCE in the soil gas.

Soil gas analyses were performed on-site to allow for tailoring the sampling scheme as the survey progressed. A total of 60 locations were sampled at an approximate depth of 6 feet in the order that they are numbered. These sample locations, the concentrations of TCE detected, and the contoured concentrations of TCE detected are shown on Sheet 4. Contoured concentrations showed five "hot" spots centered at locations SG-07 (TCE = 6,500 ug/l), SG-12 (TCE = 290 ug/l), SG-53 (TCE = 1 ug/l), SG-15 (TCE = 4 ug/l), and SG-39 (TCE = 430 ug/l). The significance of the "hot" spots occurring at locations SG-07, SG-12, and SG-53 was most likely due to them being situated hydraulically downgradient from the trenches beneath the ACD. High concentrations in the vicinity of SG-15, however, were most likely due to another source other than the trenches because available ground-water data, shown on Sheet 1, indicated this location to be upgradient from the ACD. High soil gas concentrations in the vicinity of SG-39 were unexpected. One possible source for these high concentrations could be an abandoned demolition pit shown on an old LHAAP utility map in the area of SG-42. A change in vegetation and a hummocky ground surface that appears to be backfilled material corresponds to a cleared area shown on the 1970 aerial photo (Figures 12 and 13). However, sampling location SG-42, situated in the center of this area, did not yield a high soil gas concentration. Another possible source for the high TCE detected at SG-39 may be the activity associated with the cleared area shown at this location on the 1963

aerial photo (Figures 10 and 11). The configuration of this area on the photo suggests a trench adjacent to the road that was possibly used for disposal.

Three contours showing no detection of TCE in the soil gas were derived from the data obtained at the ABG. One of these contours runs east-west across the southern corner of the site, possibly supporting available ground-water and soil boring data that indicated monitoring wells situated south of the ABG are hydraulically upgradient of the site. The other two detection contours surround the UEP, with relatively low soil gas concentrations detected within these contours. Low concentrations beneath the UEP, known to have been a source for VOC contamination in the past, could either be due to a greater thickness of clay (about 10-15 feet) overlying the ground water than was encountered in the western corner of the ABG, which would tend to prevent high VOC concentrations from reaching the ground surface, or they could reflect a depletion in the source of the VOCs that resulted from closure of the UEP. Soil and ground-water sampling would verify one condition or the other.

4.4 Shallow Soil Sampling. A total of 47 shallow soil borings, designated 8A-896 through 8A-921 and 8A-926 through 8A-946, were drilled and sampled during this investigation for the purpose of locating VOC sources of ground-water contamination. Soil boring locations are shown on Sheet 5.

4.4.1 Field Investigation Procedures. Drilling and sampling were

performed by a Fort Worth District drill crew and geologist following a standard set of procedures. All borings were drilled with a Failing 1500 drill rig. All downhole equipment was steam cleaned prior to drilling each boring. All borings were drilled dry using an 8-inch diameter solid stem flight auger, and were backfilled with a neat cement bentonite grout after a 24-hour water level was obtained.

Safety procedures for all field investigations were designed for handling soils and water contaminated with methylene chloride and TCE. Procedures were detailed on each drill request provided to the driller and geologist. All field personnel had received 40 hours of training in personal protection and safety procedures for hazardous waste management operations. Rubber gloves were worn during periods of prolonged skin contact, and the breathing space around the drill rig was monitored using Drager gas detector tubes for methylene chloride and TCE. Gas detector readings were made for each VOC at least every 10 feet of boring advancement. Field personnel were instructed to shut down operations and leave the area if an average concentration of methylene chloride exceeded 500 ppm over an 8-hour period or an average concentration of TCE exceeded 100 ppm over an 8-hour period.

Two types of soil samples were taken in each boring. Soil samples to be analyzed for the soil classification characteristics grain size distribution, Atterberg limits, and moisture content were taken every foot for the first 10 feet, then every 5 feet or change of material for the remainder of the boring. However, none of the samples taken

was ever analyzed because the depths sampled were too shallow to provide useful data for correlation purposes. Soil samples to be analyzed for the chemical concentrations of total metals, explosives, and VOCs were usually taken at an estimated minimum and maximum burial depth for each area of the ABG investigated. These depths were typically 4 and 8 feet, but varied in many of the borings. All soil samples were taken from the flight auger using stainless steel tools.

Prior to taking chemical soil samples, the auger and any handheld tools coming in contact with the sample were washed with a mild detergent, then rinsed with distilled water. Clean, disposable rubber gloves were worn when chemical soil samples were taken. A single chemical soil sample consisted of two 1-liter jar samples. Each jar was filled completely with soil and sealed tightly with a teflon-lined screw lid. One jar was labeled for metals testing. The other jar was labeled for VOCs and explosives testing. Jar labels were filled out in indelible ink, then sealed completely with clear tape when affixed to the jar. Labeled jars were stored inverted on ice until delivered by Fort Worth District personnel to the USACE, Southwestern Division Laboratory (SWDL) in Dallas, Texas. Chain of custody forms were filled out and accompanied all chemical soils to SWDL. All samples were delivered to SWDL within 48 hours of being taken.

4.4.2 ABG Area - First Round Sampling. The data obtained from the soil gas survey, in conjunction with the information obtained from the aerial photos and construction drawings for the ACD, were used

TABLE 3. SHALLOW SOIL BORING DEPTHS AND LOCATION JUSTIFICATIONS

Boring No.	Depth To Be Drilled	Location Justification (TCE Concentration)
8A-896	15 ft	Hot spot SG-12 (290 ug/l).
8A-897	15 ft	High TCE concentration SG-13 (50 ug/l).
8A-898	15 ft	Between hot spots SG-07 (6,500 ug/l) and SG-12 (290 ug/l).
8A-899	15 ft	High TCE concentration SG-55 (45 ug/l).
8A-900	15 ft	High TCE concentration SG-20 (17 ug/l). Vicinity of trenches.
8A-901	15 ft	High TCE concentration SG-18 (2 ug/l). Adjacent to old road where possible dumping occurred.
8A-902	25 ft	Above trench.
8A-903	15 ft	Hot spot SG-07 (6,500 ug/l).
8A-904	15 ft	Above trench.
8A-905	15 ft	Above trench.
8A-906	15 ft	Vicinity of hot spot SG-15 (4 ug/l).
8A-907	15 ft	Hot spot SG-15 (4 ug/l).
8A-908	15 ft	Vicinity of hot spot SG-15 (4 ug/l). Adjacent to old road where possible dumping occurred.
8A-909	15 ft	High TCE concentration SG-40 (1 ug/l). Subsurface data.
8A-910	15 ft	High TCE concentration SG-49 (4 ug/l). Subsurface data.
8A-911	15 ft	Hot spot SG-39 (430 ug/l).
8A-912	15 ft	Demolition pits location.
8A-913	15 ft	Vicinity of demolition pits and hot spot SG-39 (430 ug/l). Subsurface data.
8A-914	15 ft	Subsurface data.
8A-915	15 ft	Subsurface data.

NOTE:

For soil gas sampling locations, see Sheet 4.

For soil boring locations, see Sheet 5.

to site 20 shallow soil borings, designated 8A-896 through 8A-915, at the locations shown on Sheet 5. These borings were sited at these locations in an attempt to locate contaminant sources and to obtain additional subsurface data to be used for siting additional monitoring wells at the ABG. All borings were drilled 15 feet deep, with the exception of 8A-902, located on top of the ACD foundation, which was drilled 25 feet deep in order to penetrate the foundation fill material and still drill 15 feet into in situ soils. Boring depths and justification for their locations are shown on Table 3.

Soil samples to be analyzed for total metals, explosives, and VOC concentrations were taken at 4- and 8-foot depths in each boring except 8A-902, which was sampled after 10 feet of fill had been penetrated. A copy of the drill request detailing decontamination, sampling, sample preservation, sample handling, and safety procedures is provided as Appendix C.

Fifteen of the borings were drilled from 18 March to 4 April 1988. The remaining five borings - 8A-896, 8A-897, 8A-899, 8A-910, and 8A-915 - were drilled from 10-11 May 1988 after wet ground conditions had improved sufficiently to allow the drill rig access to the site. Geologic logs for borings 8A-896 through 8A-915 are shown on Sheets 6 through 10.

A total of 40 soil samples were taken and analyzed for VOCs, total metals, and explosives. All samples were delivered to the SWDL in Dallas, Texas. Volatile organics and explosives analyses were performed

by Southwest Laboratory of Oklahoma in Tulsa, Oklahoma, under contract to the SWDL. Metals analyses were performed by the SWDL. The quality assurance/quality control plan for soil sampling and laboratory analyses was prepared by SWDL and is provided as Appendix D. Any variations to sample handling procedures as they are described in this plan were due to site specific conditions and were approved by SWDL before implementation by Fort Worth District personnel. All sample handling procedures followed by Fort Worth field personnel are described in this report.

Analytical results from these 40 soil samples are summarized on Table 4. Volatile organic compounds were detected at concentrations >20 ug/kg in all borings except 8A-906, 8A-909, 8A-910, 8A-912, 8A-913, 8A-914, and 8A-915. The most prevalent VOCs identified were TCE, 1,2-dichloroethene (total), methylene chloride, and 1,1-dichloroethene. Trichloroethene was detected in all borings where VOCs were found, with the exception of boring 8A-914, in which the only VOC detected was methylene chloride. The distribution of these TCE concentrations is shown on Sheet 5 and correspond well with the soil gas survey data. In most cases, VOC concentrations increased with depth. The highest VOC concentrations were detected around and downgradient from the ACD, with the most variety of VOCs occurring where trench materials were actually encountered in borings 8A-902, 8A-904, and 8A-905. Strong odors were frequently noted in the ground water and soil samples.

TABLE 4. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-896 THROUGH 8A-921

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
8A-896 ^c	4.0	ND	Trichloroethene 81	ND
	8.0	ND	1,2 Dichloroethane 24 Trichloroethene 1,400	ND
8A-897	4.0	31	Trichloroethene 19	ND
	8.0	ND	1,2 Dichloroethene (total) 10 1,2-Dichloroethane 31 Trichloroethene 550	ND
8A-898	4.0	ND	Methylene Chloride 1,050 1,2-Dichloroethene 90	ND
	8.0	ND	Methylene Chloride 123,090 1,2-Dichloroethene (total) 2,130 Trichloroethene 40,660	ND
8A-899	4.0	110	Trichloroethene 69	ND
	8.0	ND	1,2-Dichloroethene (total) 85 Trichloroethene 2,840	ND
8A-900	4.0	22	1,2 Dichloroethene (total) 17 Trichloroethene 567	ND
	8.0	ND	Vinyl Chloride 78 1,1-Dichloroethene 92 1,1-Dichloroethane 28 1,2-Dichloroethene (total) 1,636 1,2-Dichloroethane 157 Trichloroethene 2,172 Tetrachloroethene 8	ND
	8.0 Duplicate		1,2-Dichloroethene 1,974 Trichloroethene 4,860	

TABLE 4. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-896 THROUGH 8A-921 (cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
8A-901	4.0	20	1,2-Dichloroethene (total) 8	ND
			Trichloroethene 9	
	8.0	ND	1,2-Dichloroethene (total) 74	ND
			Trichloroethene 331	
8A-902	14.0 ^d	1,500	1,1-Dichloroethene 750	Tetryl 26.6 TNT 5.7
			1,1-Dichloroethane 2,539	
			1,2-Dichloroethene (total) 153,300	
			Trichloroethene 46,910	
			Tetrachloroethene 2,410	
			Toluene 2,450	
	18.0	ND	Methylene Chloride 30,335	ND
			1,1-Dichloroethene 133	
			1,1-Dichloroethane 110	
			Trichloroethene 42,180	
			1,1,2-Trichloroethane 830	
			4-Methyl-2-Pentanone 698	
			Tetrachloroethene 1,110	
			Toluene 380	
8A-903 ^c	4.0	100	1,2-Dichloroethene (total) 16	ND
			Trichloroethene 220	
	8.0	26	1,2-Dichloroethene (total) 144	ND
			Trichloroethene 2,079	
8A-904	4.0 ^d	120	Vinly Chloride 51	ND
			Acetone 40	
			1,1-Dichloroethene 6	
			1,2-Dichloroethene (total) 3,628	
			Trichloroethene 86	
	4.0 Duplicate		1,2-Dichloroethene (total) 8,395	
			Chloroform 7	
			Trichloroethene 226	

TABLE 4. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-896 THROUGH 8A-921 (cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
8A-904	8.0	87	Methylene Chloride 59	ND
			1,2-Dichloroethene 69	
			Trichloroethene 88	
			Styrene 17	
8A-905	4.0 ^d	1,000	1,2-Dichloroethene (total) 39,840	Tetryl 17.4
			Trichloroethene 78,870	
			Ethylbenzene 10,665	
	8.0	290	1,2-Dichloroethene (total) 14,645	Tetryl 9.5
			Trichloroethene 21,880	
			Ethylbenzene 1,390	
			Styrene 16,660	
8A-906	4.0	56	ND	ND
	8.0	63	ND	ND
8A-907 ^c	4.0	71	Trichloroethene 14	ND
	8.0	130	Trichloroethene 103	ND
8A-908	4.0	82	Trichloroethene 14	ND
	8.0	93	Trichloroethene 270	ND
8A-909	4.0	160	Trichloroethene 16	ND
	8.0	420	ND	ND
8A-910	4.0	290	Trichloroethene 15	ND
	8.0	150	ND	ND
8A-911 ^c	4.0	70	1,2-Dichloroethene (total) 1,219	ND
			Trichloroethene 2,279	

TABLE 4. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-896 THROUGH 8A-921 (cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
8A-911	8.0	120	Methylene Chloride 4,318 1,1-Dichloroethene 14 1,2-Dichloroethene (total) 194 Chloroform 5 Trichloroethene 3,228	ND
8A-912	0.0-1.0	200	e	ND
	1.0-2.0	47	e	ND
	4.0	57	ND	ND
	8.0	49	ND	ND
8A-913	4.0	69	ND	ND
	8.0	62	ND	ND
8A-914	4.0	66	Methylene Chloride 8	ND
	8.0	120	ND	ND
8A-915	4.0	120	ND	ND
	8.0	190	ND	ND

ND = Not detected or detected below calibration limits.

^aAnalyses performed by USACE Southwestern Division Laboratory. Calibration limit for Ba was 20 mg/kg.

^bAnalyses performed by Southwest Laboratory of Oklahoma, under contract to USACE Southwestern Division Laboratory. Calibration limits for specific VOCs are contained in Appendix E. Explosive cpds analyzed and respective calibration limits were HMX (1.6 ug/g), RDX (1.8 ug/g), tetryl (5.5 ug/g), TNT (0.8 ug/g), and 2,4 DNT (0.8 ug/g).

^c"Hot" spot from soil gas survey.

^dTrench material encountered.

^eAnalysis not performed.

Complete analytical results are contained in Appendix E.

However, no measurable amounts of VOCs were detected in the breathing space of the work area except in soil boring 8A-905, which briefly yielded a TCE concentration of 30-40 ppm when 10 feet had been drilled.

Explosives were detected in only two borings, 8A-902 and 8A-905, both of which contained trench material. Explosives identified were tetryl (26.6 ug/g) and TNT (5.7 ug/g) at 14 feet in 8A-902, and only tetryl at both 4 feet (17.4 ug/g) and 8 feet (9.5 ug/g) in 8A-905. These sample locations also showed the highest concentrations of total barium, with 1500 mg/kg occurring at 4 and 8 feet, respectively, in 8A-905. Complete laboratory results for these soil samples are contained in Appendix E. The quality assurance for these results is discussed in Volume 5.

4.4.3 Air Curtain Destructor Sampling. Prior to completing these 20 shallow soil borings and receiving laboratory results, six additional soil borings were added to the shallow soil sampling program after trench material was actually encountered in borings 8A-902, 8A-904, and 8A-905 around the ACD. The purpose of siting these additional borings was to determine how much trench material was actually removed during construction of the ACD and the extent of any material still remaining. These six borings, designated 8A-916 through 8A-921, were drilled and sampled by Fort Worth District personnel from 12-17 May 1988 at the locations shown on Sheet 5. Figure 14 shows how these boring locations relate to the construction as-builts that show the extent of "muck" removal and to the aerial photos that show the original extent of the trenches.

Each boring was drilled to approximate elevation 165. Borings were drilled dry using an 8-inch diameter solid stem flight auger. Three different depths were sampled in each boring for explosives and VOCs analyses. Sampling depths were designated at the approximate elevations for the top of the trenches (el 176), for the bottom of the trenches (el 172), and for approximately 6 feet below the bottom of the trenches (el 166) to see how far contamination had migrated downward. A copy of the drill request detailing decontamination, sampling, sample preservation, sample handling, and safety procedures is provided as Appendix F. Geologic logs for borings 8A-916 through 8A-921 are shown on Sheets 11 and 12.

A total of 18 soil samples were taken for chemical analysis. The results of these analyses are summarized on Table 5. It was originally intended that these samples would be analyzed for VOCs and explosives by East Texas Testing Laboratory, Inc., in Longview, Texas, under contract to Morton Thiokol, Inc., for performing soil analyses. Problems with the testing laboratory, however, resulted in transferring the samples to Ana-Lab Corp., in Kilgore, Texas, under contract to Morton Thiokol, Inc., to perform water analyses. Although not requested, East Texas Testing Laboratory, Inc., performed EP toxicity analyses for metals on all 18 samples. None of the samples exceeded the EP toxicity limits specified in 40 CFR 261.24. Volatile organics and explosive analyses were performed by Ana-Lab Corp. It is important to note that units for concentrations were incorrectly

TABLE 5. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES 001963
FROM SHALLOW SOIL BORINGS 8A-916 THROUGH 8A-921

Boring No.	Sample Depth (ft)	EP Toxic Metals ^a (kg/l)	VOCs ^b (ug/l)	Explosives ^b (mg/l)
8A-916	9.0 ^c	Ba 4.1 Pb 0.09	Benzene 7 Trichloroethene 7	ND
	14.0	Ba 0.22	1,1,1-Trichloroethane 13 1,2-Dichloroethene 89 Trichloroethene 1,800	ND
	20.0	Ba 0.11 Cd 0.01	1,2-Dichloroethane 65 Benzene 7 Methylene Chloride 61 Trichloroethene 640	ND
8A-917	2.0	Ba 0.23	Methylene Chloride 230 Trichloroethene 330	ND
	6.0	Ba 0.22	1,1,1-Trichloroethane 47,000 1,1-Dichloroethane 40 1,1-Dichloroethene 350 Benzene 90 Ethyl Benzene 900 Methylene Chloride 7,200 Tetrachloroethene 1,000 Toluene 10,000 1,2-Dichloroethene 360 Trichloroethene 1,000,000 Xylenes 890	ND
	12.0	Ba 0.23 Cd 0.01 Cr 0.02	1,1,1-Trichloroethane 650 1,1-Dichloroethene 40 1,2-Dichloroethane 130 Methylene Chloride 11,000 Tetrachloroethene 70 1,2-Dichloroethene 1,050 Trichloroethene 24,000	ND
8A-918	16.0	Ba 0.06 Cd 0.01	Methylene Chloride 820 1,2-Dichloroethene 500 Trichloroethene 770	ND
	18.4	Ba 6.1 Cr 0.68	1,1-Dichloroethane 45 1,1-Dichloroethene 40	ND

TABLE 5. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SEALLOW SOIL BORINGS 8A-916 THROUGH 8A-921 (cont'd)

001966

Boring No.	Sample Depth (ft)	EP Toxic Metals ^a (mg/l)	VOCs ^b (ug/l)	Explosives ^b (mg/l)
8A-918	18.4		1,2-Dichloroethane 340 Ethyl Benzene 100 Methylene Chloride 200 Tetrachloroethene 160 Toluene 30 1,2-Dichloroethene 6,600 Trichloroethene 550 Xylenes 1,200	
	26.0	Ba 0.15	1,1-Dichloroethene 16 1,2-Dichloroethane 880 Benzene 1,200 Methylene Chloride 2,200 Trichloroethene 1,300	ND
8A-919	18.0	Ba 0.40	Trichloroethene 36	ND
	22.0	Ba 0.48	Chloroform 10 Methylene Chloride 880 1,2-Dichloroethene 170 Trichloroethene 1,200	ND
	28.0	Ba 0.12	Methylene Chloride 29,000 Trichloroethene 1,700	ND
8A-920	3.0	Ba 0.11	Methylene Chloride 510 Trichloroethene 33	ND
	7.0	Ba 0.06	Benzene 8	ND
	13.0	As 0.02 Ba 0.73 Cd 0.01 Cr 0.48 Pb 0.06 Se 0.01	1,2-Dichloroethene 140 Trichloroethene 160	ND
8A-921	12.0	As 0.01 Ba 0.29	2-Chloroethylvinyl, ether 9 Trichloroethene 8	ND
	16.0	Ba 0.17 Cd 0.02	ND	ND
	22.0	Ba 0.22	Methylene Chloride 200 Trichloroethene 210	ND

TABLE 5. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-916 THROUGH 8A-921 (cont'd)

ND = Not detected or detected below calibration limits.

^aAnalyses performed by East Texas Testing Laboratory, Inc., under contract to Morton Thiokol, Inc.

^bAnalyses performed by Ana-Lab Corp., under contract to Morton Thiokol, Inc. Note that VOC analyses were performed after shelf life of samples were exceeded. Calibration limits for specific VOCs are contained in Appendix G. Explosive cpds analyzed and respective calibration limits were RDX (0.01 mg/l), HMX (0.01 mg/l), tetryl (0.3 mg/l), 2,4 DNT (0.01 mg/l), 2,6 DNT (0.01 mg/l), and 2,4,6 TNT (0.01 mg/l). Units are those reported by Ana-Lab Corp., possibly reflecting extraction concentrations only.

^cTrench material encountered.

Complete analytical results are contained in Appendix G.

and inexplicably reported as mg/l, possibly reflecting extraction concentrations only. No explosives were detected. It is also important to note that the VOC analyses were performed after the shelf life for VOCs was exceeded. In spite of the reliability of these test results, VOC concentrations were very high, even though no trench material was evident except in boring 8A-916, where traces of material were found at 9 feet. The maximum concentration of TCE reported was 1,000,000 ug/l at 6 feet in 8A-917. The least amount of contamination was found in boring 8A-921, sited on the trench berm limits as determined from the aerial photos. Few VOCs were detected at the upper sampling depths in 8A-921; however, methylene chloride and TCE were detected at 200 ug/l and 210 ug/l, respectively, at 22 feet. Complete analytical results provided to Fort Worth District by Morton Thiokol, Inc., are contained in Appendix G.

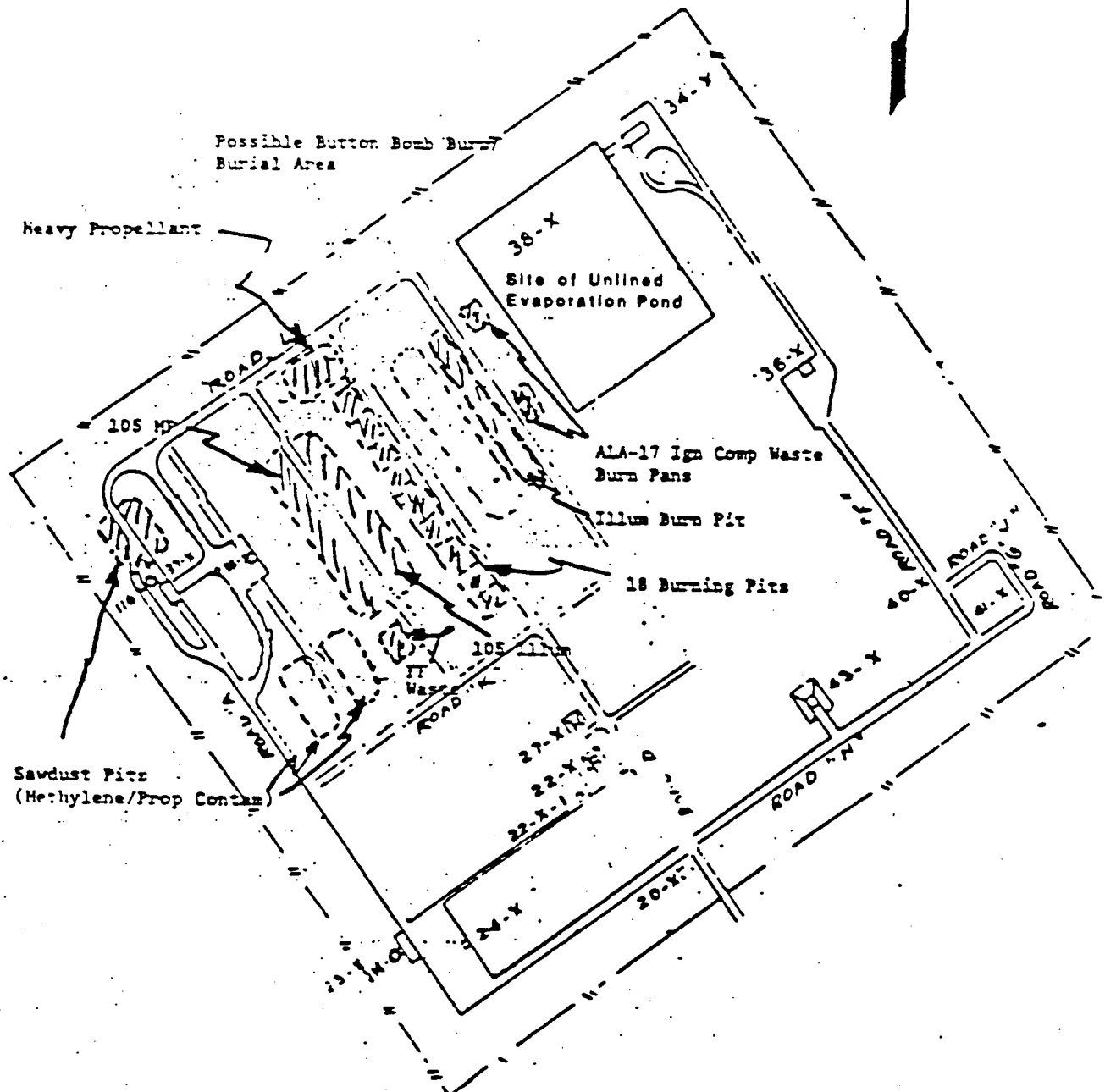
4.4.4 ABG Area - Second Round Sampling. In September 1987, Fort Worth District installed six monitoring wells, MW-1 through MW-6, at the Point of Compliance around the UEP as required by the scope of work for this investigation. Details of these installations are discussed in Section 5.0 of this report. On 7 May 1988, Morton Thiokol, Inc., sampled these wells as part of LHAAP's quarterly monitoring program. The samples were analyzed by Ana-Lab Corp., under contract to Morton Thiokol, Inc. The analytical results for MW-1 through MW-6 were provided to Fort Worth District by Morton Thiokol, Inc., and are contained in Appendix H. Four of the six wells showed concentrations

of methylene chloride ranging from 300 ug/l to 2,900,000 ug/l. All six of the wells showed concentrations of TCE ranging from 70 ug/l to 60,000 ug/l. These extremely high concentrations of methylene chloride and TCE indicated that ground-water contamination was still present around the UEP.

In order to investigate whether any other sources besides the past operation of the UEP was contributing to the contamination around the pond, 21 additional soil borings, designated 8A-926 through 8A-946, were added to the shallow soil boring program. The borings were sited comparing suspect areas identified in aerial photos with suspect areas identified on the map shown on Figure 15, which shows past solid waste management operations at the ABG as determined by the USAEHA in "Ground-Water Contamination Survey No. 38-26-0851-88, 18-22 May 1987." Borings 8A-926 through 8A-934 were sited at 60-foot intervals along the southwestern and southeastern edges of the UEP cap for the purpose of locating any remaining methylene chloride soaked sawdust that was stockpiled along the berms of the UEP during its operation. Borings 8A-935 through 8A-937 were sited along a suspected trench identified in 1980 aerial photos at a location coinciding with the "Illum Burn Pit" shown on Figure 15. The remaining nine borings were sited at 50-foot intervals along a suspect area identified as "Stacks or Burning" in the 1970 aerial photo sketch shown on Figure 13, which coincides with the line of "18 Burning Pits" shown on Figure 15. Boring locations are shown on Sheet 5.

BURNING GROUND #3
LHAAP-18

APPROXIMATE SCALE: 1 inch = 200 feet



Source: Ground-Water Contamination Survey No.
38-26-0851-88, LHAAP, Marshall, TX,
USAEHA, 18-22 May 1987.

Figure 15. Past Solid Waste Management Units at the ABG.

All 21 soil borings were drilled and sampled from 15-18 August 1988. Each boring was drilled 10 feet deep. Samples to be analyzed for total barium and VOC concentrations were taken at 4 and 10 feet depths in each boring. A copy of the drill request detailing decontamination, sampling, sample preservation, sample handling, and safety procedures is provided as Appendix I. Geologic logs for borings 8A-926 through 8A-946 are shown on Sheets 12 through 17.

A total of 42 soil samples were analyzed for total barium and VOC concentrations. Total barium was selected as an indicator parameter for pyrotechnic wastes. All samples were delivered by Fort Worth District personnel to the SWDL in Dallas, Texas. Volatile organics analyses were performed by Southwest Laboratory of Oklahoma in Tulsa, Oklahoma, under contract to the SWDL. Total barium analyses were performed by the SWDL.

Analytical results for these 42 soil samples are summarized on Table 6. Only the VOCs detected and quantified are shown because many VOCs were tentatively identified at estimated concentrations below detection limits. The tentatively identified and unknown compounds are shown in the complete laboratory results contained in Appendix J.

Volatile organic compounds were detected at concentrations >20 ug/kg in 11 of the 21 borings drilled. These contaminated soil borings are shown on Sheet 5. Of the nine borings sampled around the capped UEP, only borings 8A-930, 8A-931, and 8A-932 detected VOCs. These three locations are closest to the ramp area of the pond. Only trace

TABLE 6 SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-926 THROUGH 8A-946

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)
8A-926	4.0	92	ND
	10.0	190	ND
8A-927	4.0	97	ND
	10.0	110	ND
8A-928	4.0	56	ND
	10.0	110	Acetone ^c 21
8A-929	4.0	50	ND
	10.0	83	ND
8A-930	4.0	60	
	10.0	59	1,1- Dichloroethene 6 Trichloroethene 8
8A-931	4.0	32	Acetone ^c 14
			1,2-Dichloroethene (total) 9
			Trichloroethene 91
	10.0	96	1,1-Dichloroethene 49
			1,1-Dichloroethane 19
			1,2-Dichloroethene (total) 57
			1,1,1-Trichloroethane 13
			Trichloroethene 920E
10.0 Duplicate			Tetrachloroethene 64
			1,2-Dichloroethene 35
			Trichloroethene 520B
			Tetrachloroethene 44
8A-932	4.0	52	Trichloroethene 8
	10.0	75	ND

TABLE 6 SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-926 THROUGH 8A-946 (cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)
8A-933	4.0	79	ND
	10.0	78	ND
8A-934	4.0	120	ND
	10.0	130	ND
8A-935	4.0	61	ND
	10.0	85	1,1-Dichloroethene 57
8A-936	4.0	32	ND
	10.0	85	ND
8A-937	4.0	36	1,1,1-Trichloroethane 31 Tetrachloroethene 13
	10	60	1,1-Dichloroethene 14
8A-938	4.0	81	ND
	10.0	26	ND
8A-939	4.0	86	Trichloroethene 650E
	4.0 Duplicate		Trichloroethene 85B
	4.0 Duplicate		Trichloroethene 33B
	10.0	72	Trichloroethene 2500BE
8A-940	4.0	51	Methylene Chloride 22,000 Acetone 33,000 1,2-Dichloroethene (total) 14,000 1,2-Dichloroethane 4,600 Trichloroethene 430,000E Tetrachloroethene 4,500 Toluene 34,000 Ethylbenzene 2,900

TABLE 6. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-926 THROUGH 8A-946(cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)
8A-940	10.0	68	Methylene Chloride 420,000E Acetone 20,000 Chloroform 3,200B 1,2-Dichloroethane 120,000E 1,1,1-Trichloroethane 2,200 Trichloroethene 150,000E Tetrachloroethene 16,000 Toluene 6,700 Ethylbenzene 18,000 Xylene (total) 6,100 1,2-Dichlorobenzene 9,300
8A-941	4.0	67	Trichloroethene 90B
	10.0	140	Acetone ^c 46
	10.0 Duplicate		ND
8A-942	4.0	85	Toluene 690 Ethylbenzene 3,300E Xylene (total) 830
	10.0	170	Acetone ^c 150 1,2-Dichloroethene (total) 140 Trichloroethene 46B Toluene 8 Ethylbenzene 28
8A-943	4.0	28	Acetone ^c 18
	10.0	100	1,2-Dichloroethene (total) 18 Trichloroethene 19B
8A-944	4.0	29	Acetone 9,900 Ethylbenzene 1,100 Styrene 2,100 Xylene (total) 3,000

TABLE 6. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM SHALLOW SOIL BORINGS 8A-926 THROUGH 8A-946 (cont'd)

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)
8A-944	10.0	140	Methylene Chloride 4,500 Carbon Disulfide 13,000 Trichloroethene 3,800 Ethylbenzene 7,200 Styrene 35,000
8A-945	4.0	16	Methylene Chloride 310 Acetone 1,900E Trichloroethene 54 Tetrachloroethene 110 Ethylbenzene 70 Styrene 480 Xylene (total) 610
	4.0 Duplicate		Acetone 4,700
	10.0	43	Methylene Chloride 16,000 Trichloroethene 1,700
8A-946	4.0	62	ND
	10.0	98	ND

ND = Not detected or detected below calibration limits.

E = Concentration exceeded calibration limits.

B = Possible laboratory blank contamination.

^aAnalyses performed by USACE Southwestern Division Laboratory.
Calibration limit for Ba was 1.0 mg/kg.

^bAnalyses performed by Southwest Laboratory of Oklahoma, under contract to USACE Southwestern Division Laboratory. Calibration limits for specific VOCs are contained in Appendix J.

^cAcetone is common laboratory contaminant, with normal allowable level five times detection limit reported.

Complete analytical results are contained in Appendix J.

(<20 ug/kg) concentrations of solvent-type compounds were detected, except in boring 8A-931, where the concentration of TCE exceeded 920 ug/kg at the 10-foot depth. This concentration is questionable, however, because the method blank run with the duplicate analysis showed possible laboratory blank contamination. No physical evidence of sawdust was found and no methylene chloride was detected in any of these borings, suggesting that if any remnants of stockpiled sawdust do exist, they are most likely under the capped area of the UEP.

Two of the three borings drilled at the "Illum Burn Pit" location showed very low concentrations of VOCs. These two borings were 8A-935 and 8A-937. No physical evidence of the pits was noted. However, boring 8A-937 showed many unidentified compounds detected below calibration limits.

The remaining nine borings drilled along the line of "18 Burning Pits" showed the highest concentrations and most varied VOCs detected of the 21 soil borings. All of the borings except 8A-938, 8A-939, and 8A-946 showed backfill material ranging from 0.4 foot thick in 8A-945 up to 6.1 feet thick in 8A-944. Weak to strong odors were noted in all of the borings except 8A-938 and 8A-939. All borings except 8A-938 and 8A-946 showed VOCs present; however, only 4 borings had VOC concentrations >20 ug/kg. Boring 8A-940 had the highest concentrations of VOCs, with methylene chloride exceeding 420,000 ug/kg and TCE exceeding 430,000 ug/kg. Many types of hydrocarbons were also detected in 8A-940, some at concentrations as high as 34,000

ug/kg for toluene, and some unidentified at concentrations estimated as high as 110,000 ug/kg, shown in Appendix J. Borings 8A-942, 8A-944, and 8A-945 showed the same varied range of VOCs and hydrocarbons, with concentrations somewhat less than those detected in 8A-940. Total barium concentrations did not exceed 190 mg/kg, and did not exhibit any pattern with the concentrations of VOCs detected in any of the 21 borings. The quality assurance of these test results is discussed in Volume 5.

4.4.5 Summary. Based on these contaminant source investigations, there is a second source at the ABG, besides the past operation of the UEP, that is contributing to the ground-water contamination beneath the site. This source consists of the remnants of three trenches and their berms that are buried around the foundation of the ACD in the western corner of the ABG. Trench remnants encountered from approximate el. 175-177 in borings 8A-902 and 8A-905 consisted of solvent soaked straw, wood shavings, and sawdust in a fill binding material. Trench berm materials were encountered from approximate el. 173-177 in borings 8A-904 and 8A-916 and consisted of traces of these trench materials and other foreign matter. These locations correspond to the original location and extent of the trenches shown in the aerial photos. Because these four borings were the only borings that encountered physical evidence of trench material, it appears safe to assume that the trenches remaining under the foundation of the ACD were removed to the limits of "muck" excavation shown on the construction as-builts, leaving the trench remnants beyond the

foundation, as shown on Figure 16, as a likely source for ground-water contamination observed in this area.

Three subsurface profiles through this corner of the ABG are shown on Sheet 18 for the purpose of portraying the extent of remnant trench materials and the subsurface conditions where these remnants occur. Free water was encountered at various depths during the drilling in this area, and any attempts to get a 24-hour water level were fruitless because the borings would not stay open overnight. A 3-inch diameter PVC pipe was finally placed in 8A-921 to obtain a 24-hour water level. The ground-water elevation obtained was 177. In most cases, a strong sharp odor was observed in the ground water when it was encountered beneath the ACD. However, no odor was noted in the ground water moving away from the site except in the direction of boring 8A-896, which was a "hot" spot from the soil gas survey.

A potential third contaminant source was identified along the line of "18 Burning Pits" shown on Figure 15. Although no physical evidence of burned materials was encountered while drilling borings 8A-938 through 8A-946 along this line of pits, fill material was identified, as well as high concentrations of VOCs and hydrocarbons. The total depth of each of these borings was 10 feet, and no ground water was encountered. However, since the principal recharge to the ground water in this area is infiltration, soil contaminated from past operation of these pits definitely poses the threat of being carried into the ground water underlying the site.

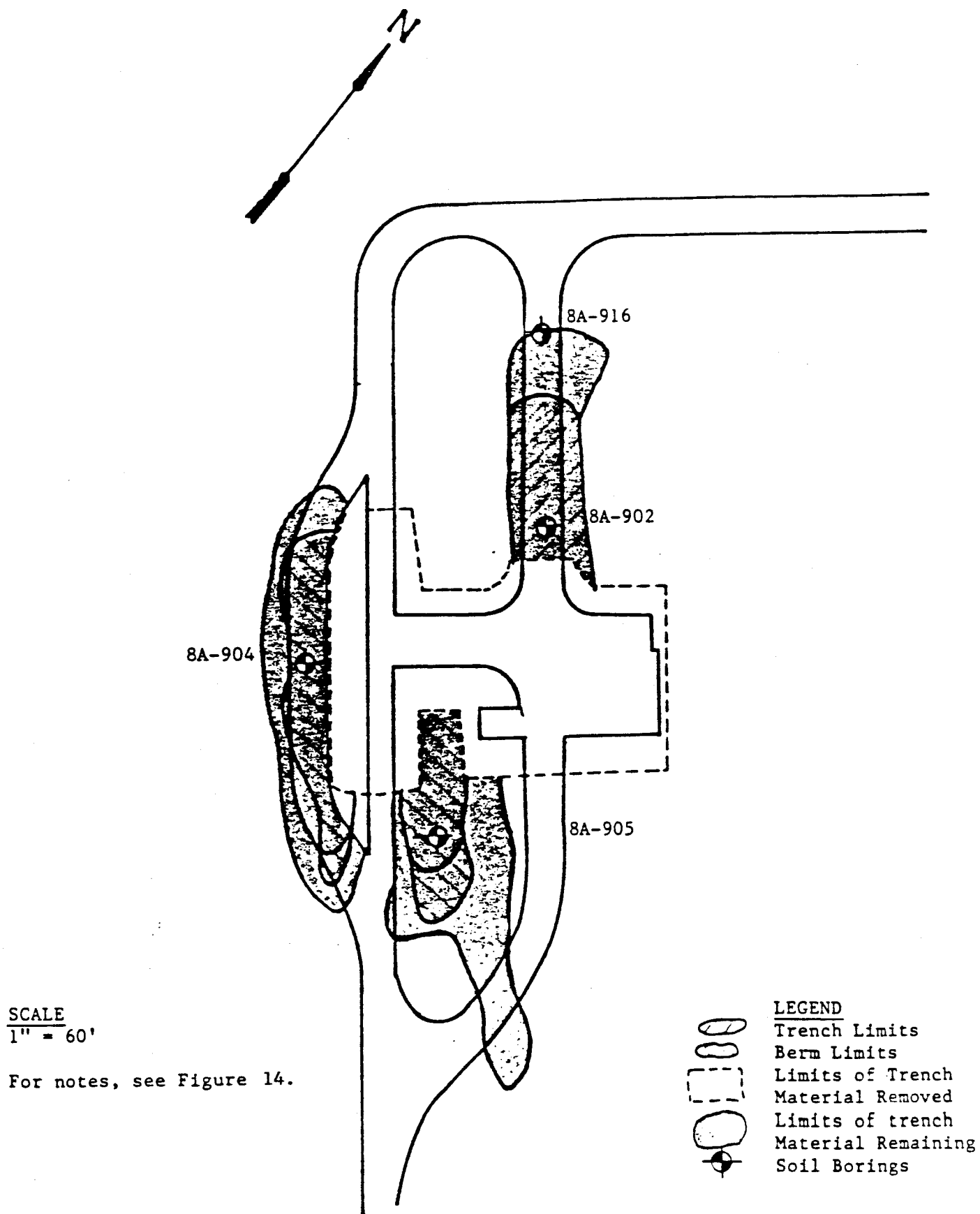


Figure 16. Extent of Contaminant Source Material.

A possible fourth source that could be contributing to ground-water contamination south of the UEP is a suspected trench location adjacent to the west side of the road east of boring 8A-911, suggested by the 1963 aerial photos. High concentrations of VOCs found in soil samples from 8A-911 suggest possible past activity nearby. However the abandoned demolition pit, located immediately south of 8A-911 at boring location 8A-912, which was suspected as a source prior to soil sampling, proved to be an unlikely source after soil samples taken in boring 8A-912 showed no VOCs detected. Soil samples taken for soil classification analyses from the top 2 feet of the boring were later selected for chemical analysis when the geologic log indicated black carbon matter was encountered while drilling. No VOC analyses were performed because the samples had exceeded the shelf life for VOCs. However, the samples were analyzed for total metals and explosives. The maximum concentration for barium detected was 200 mg/kg. No explosives were detected. These results do not eliminate this as a possible source area for VOCs, but because no odor was noted in the samples taken from 8A-912, and soil gas data showed a relatively low concentration of TCE, it appears unlikely that the abandoned demolition pit is a VOC source.

5.0 GROUND-WATER MONITORING.

5.1 Water Level Data. Three rounds of water levels were made at the ABG during the course of this investigation. The first round of measurements was made from 7-8 July 1987 for the 25 existing wells at the ABG. Depth to water and depth to the bottom of the well were measured from the top of the PVC well casing in all wells except C-10, where the depths were measured from the top of the protective casing. Measurements were made from these reference points to use the survey data already provided in the CDM reports. However, a comparison of recorded stick-up measurements for the well casings to the stick-up measurements made in the field showed several discrepancies that made the survey data and actual reference points questionable. For several wells (e.g., 101, 102, 125, and 129) it was found that the surveyed elevation for the top of PVC casing was actually the surveyed elevation for the outer protective casing. Recorded stick-ups for the top of PVC on other wells (e.g., 124) were noted as differing from field measurements as much as 1 foot or more. Also, the PVC pipe was cut at an angle or damaged on some wells (e.g., C-2, C-4, and C-10), and in other wells the top of PVC was far enough below the top of the protective casing to make it awkward to take accurate water level measurements consistently.

Because of these discrepancies, the water level elevations determined from the measurements made 7-8 July 1987 became questionable. Previous hydrologic data show a very low hydraulic gradient across

the ABG, which makes survey control very critical when plotting a piezometric surface to assist in determining future well locations. Therefore, the water level data obtained in July 1987 were considered bad data and are not presented.

The second round of water level measurements was made from 20-22 April 1988 for the 25 existing wells and the 6 newly installed Compliance Monitoring wells, MW-1 through MW-6. Depth to water in each well was measured from the recently surveyed notched well casing using a Slope Indicator Company Model 51453 water level indicator. The tip of the indicator was thoroughly washed with a mild detergent, then rinsed with distilled water prior to lowering it in each well. Depths to water were recorded to the nearest 0.1 foot and are shown on Table 7. Water level elevations were determined using the most recent Fort Worth District survey data compiled earlier in the month. Contoured elevations of the ground-water surface are presented on Sheet 19.

A third round of water levels was taken on 31 August 1988 for all existing and all newly installed wells except MW-13, which had not yet been installed. Depths were measured in the same manner as during the second round of water level readings and were recorded to the nearest 0.01 foot. Water level readings are shown on Table 7. Although wells MW-7 through MW-15 had not been surveyed yet, the inner well casings had been set level to allow for an accurate measurement from any edge. Water level elevations were determined

TABLE 7. WATER LEVEL DATA

WELL NO.	MEASURING POINT		20-22 APRIL 1988		31 AUGUST 1988	
	NOTCHED CASING	ELEVATION (FT-MSL)	DEPTH (FT)	ELEVATION (FT-MSL)	DEPTH (FT)	ELEVATION (FT-MSL)
BH-3	Well	196.30	21.5	174.8	24.26	172.04
BH-4	Well	197.44	23.0	174.4	24.75	172.69
BH-7	Well	197.24	23.1	174.1	24.27	172.97
BH-11	Well	199.03	25.3	173.7	27.18	171.85
BH-22	Well	199.25	24.3	175.0	25.49	173.76
101	Prot. ^a	197.51	7.0	190.5	9.65	187.86
102	Prot.	194.55	18.5	176.0	20.25	174.30
109	Prot.	197.11	23.6	173.5	24.59	172.52
120	Prot.	183.28	8.4	174.8	11.53	171.75
123	Prot	186.33	11.1	175.2	12.66	173.67
124	Prot.	186.39	10.7	175.7	12.68	173.71
125	Prot.	196.35	21.9	174.4	25.08	171.27
126	Prot.	199.41	26.2	173.2	28.00	171.41
129	Prot.	197.13	21.7	175.4	23.63	173.50
130	Prot.	177.80	5.4	172.4	7.20 ^b	170.60
C-1	Prot.	193.80	20.5	173.3	22.79	171.01
C-2	Prot.	176.03	2.8	173.2	6.13	169.90
C-3	Prot.	196.41	23.1	173.3	25.85	170.56
C-4	Prot.	194.74	21.3	173.4	24.49	170.25
C-5	Prot.	180.77	9.4	171.4	12.90	167.87
C-6	Prot.	192.34	22.3	170.0	25.27	167.07
C-7	Prot.	196.72	23.1	173.6	26.07	170.65
C-8	Prot.	192.56	19.1	173.5	21.33	171.23
C-9	Well	202.66	29.9	172.8	31.04	171.62
C-10	Prot.	202.04	28.1	173.9	30.35	171.69
MW-1	Well	199.24	23.8	175.4	25.30	173.94
MW-2	Well	197.00	22.2	174.8	26.66	170.34
MW-3	Well	196.51	23.3	173.2	25.37	171.14
MW-4	Well	197.31	22.6	174.7	25.19	172.12
MW-5	Well	195.21	21.1	174.1	24.34	170.87
MW-6	Well	192.18	18.6	173.6	21.62	170.56
MW-7	Well	188.56	-c	-	15.51	173.05
MW-8	Well	186.85	-c	-	13.90	172.95
MW-9	Well	184.78	-c	-	11.83	172.95
MW-10	Well	177.99	-c	-	8.50	169.49
MW-11	Well	177.65	-c	-	7.39	170.26
MW-12	Well	178.37	-c	-	8.12	170.25
MW-13	Well	176.72	-c	-	-c	-
MW-14	Well	182.99	-c	-	12.48	170.51
MW-15	Well	197.32	-c	-	26.56	170.76

^aProt. = Protective casing^bRecorded 12 Aug 89^cWell not installed

upon completion of the final round of surveying in September 1988. Contoured water level elevations for the 31 August 1988 readings are shown on Sheet 20.

5.2 Survey Data. Surveying was performed by Fort Worth District survey personnel at three different times. The first survey data were gathered in April 1988 to establish X,Y coordinates and elevations for all 25 existing wells at the ABG and for the 6 newly installed wells MW-1 through MW-6. At this time, a permanent reference mark for taking water level measurements was established on each well by notching the casing with the highest stick-up, painting the notch to make it visible, then surveying this mark to establish a reference elevation for taking all future water level measurements. A second round of surveying was performed in May 1988 to survey and stake eight proposed well locations (MW-7 through MW-14) and four stratigraphic test boring locations (3F-922 through 3F-925). The final round of surveying was performed in September 1988 after all new wells (MW-7 through MW-15) were installed. Coordinates were established to at least the nearest 0.01 foot and are referenced to the State Plane Coordinate System. All elevations were determined to at least the nearest 0.01 foot and are referenced to the National Geodetic Vertical Datum (NGVD) of 1929. Elevations were determined for the reference mark notched on each well casing. For those wells surrounded by a concrete pad (BH-3, BH-4, BH-7, BH-11, BH-22, and C-1 through C-10), "ground" elevations were surveyed for the top of the pad. For wells

MW-1 through MW-15, "ground" elevations were surveyed for the survey marker installed in the concrete pad. For all other wells, "ground" elevation was surveyed for the actual ground surface adjacent to the well. Survey data for all of the ABG monitoring wells and the four stratigraphic test borings are provided in Appendix K.

5.3 Monitoring Well Installation Procedures. A total of 15 monitoring wells were installed during this assessment. Twelve of these wells, designated MW-1 through MW-12, were screened at the base of the suspected uppermost saturated zone underlying the ABG area. The other three wells, designated MW-13, MW-14, and MW-15, were installed about 10 feet away from wells C-2, 120, and MW-2, respectively, and were screened in the next deeper saturated zone at each of these locations. Well locations are shown on Sheet 21.

All drilling, sampling, and well installations were performed by a Fort Worth District drill crew and geologist following a standard set of procedures. All borings were drilled with a Failing 1500 drill rig. All downhole equipment was steam cleaned prior to drilling each boring. Borings MW-1 through MW-12 were drilled dry using a 10-inch diameter solid stem flight auger. Borings MW-13 through MW-15 were drilled dry to the depth where casing was set and grouted to seal off the upper saturated zone. The remainder of these borings was augered until the borings began to cave. Each was then completed using a 9-7/8-inch diameter rockbit and a pure bentonite drill mud mixed with nonchlorinated water obtained from the ABG water supply.

Deep wells were completed using a 7-7/8-inch diameter rockbit.

Two types of soil samples were taken in each well boring. Soil samples to be analyzed for the soil classification characteristics grain size distribution, Atterberg limits, and moisture content were taken every foot for the first 10 feet, then once every 5 feet or change of material for the remainder of each boring. Soil samples for chemical analysis were taken at 2- and 10-foot depths in each boring. These samples were analyzed for total metals, explosives, and VOCs, and were taken in the same manner as those chemical samples obtained from the shallow soil borings described earlier.

Upon completion of drilling and sampling, each shallow monitoring well was constructed in accordance with the monitoring well construction detail shown on Figure 17. Deeper wells were constructed in accordance with the detail shown on Figure 18. All well materials were 4-inch I.D. Type 304 stainless steel with flush threaded joints. Well screens were 5 feet long and pre-slotted at a 0.010 inch slot size. The well materials were steam cleaned prior to installation. A manufactured silica sand with a standard sieve size range of 20 to 40 (0.33 to 0.165 inches) was used as a gravel pack, which was placed from the bottom of the boring to 2 feet above the top of the well screen. A 2-foot bentonite seal was placed above the gravel pack, and the remainder of the boring was grouted to the ground surface.

Safety procedures for monitoring well installations were the same as those previously described for the shallow soil sampling program

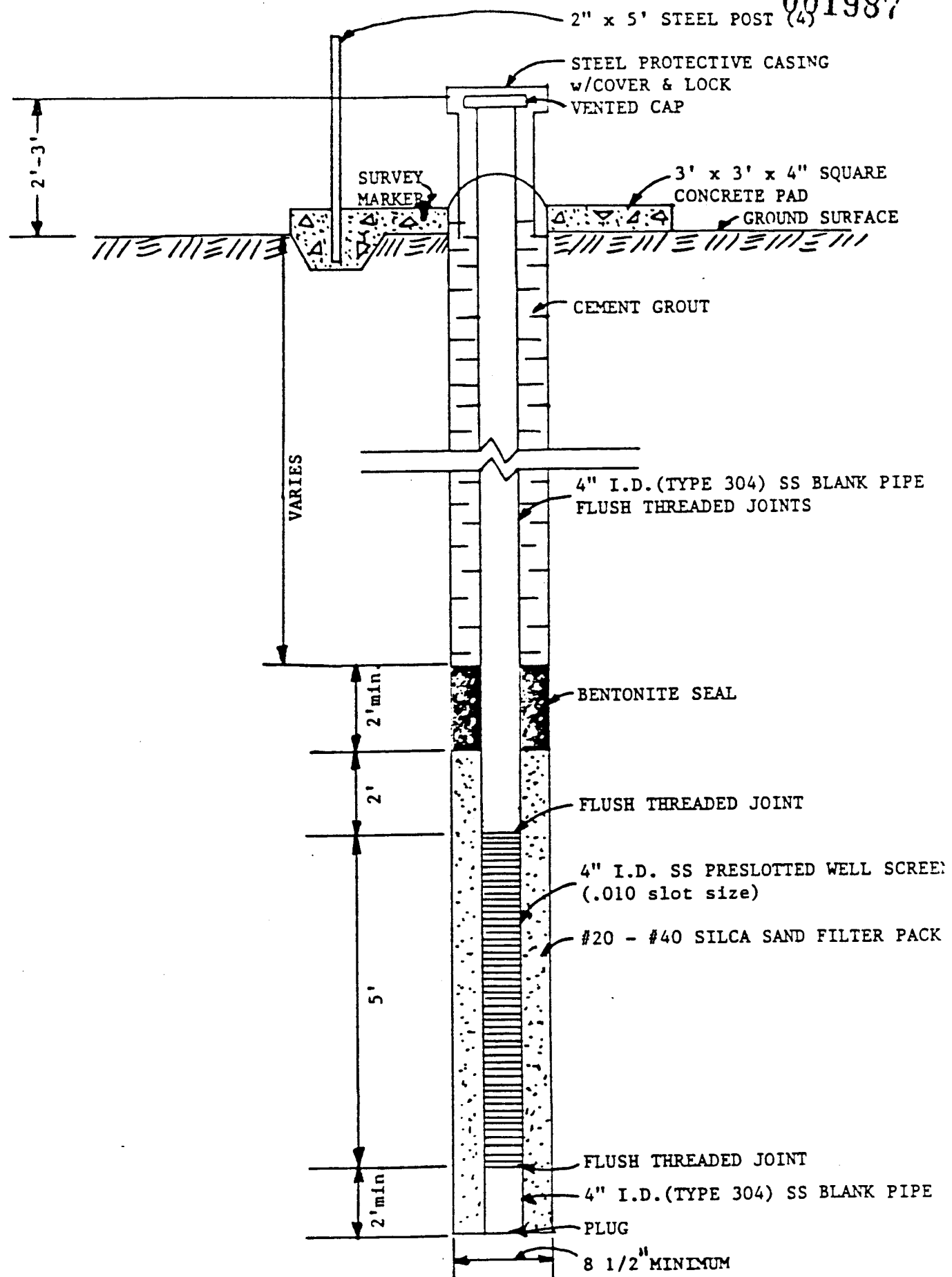


Figure 17. Typical Construction Detail for Shallow Monitoring Well.

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except that gas detector readings were made not only for every 10 feet of boring advancement, but also for surging and bailing performed during well development, which began 48 hours after grouting. Each well was developed using a surge block and bailer which were steam cleaned prior to introduction to the well. Development lasted a minimum of 4 hours, or until the water was clear and free of sediment. Water removed from the well was discharged far enough away to prevent it from running back down the borehole.

After development, each well was equipped with a dedicated 3-foot long 2-inch O.D. stainless steel bailer suspended from the vent hole of the well cap on a teflon-coated stainless steel cable. Each bailer was thoroughly washed with a mild detergent, then rinsed with distilled water prior to installation.

Each well was finished at the ground surface by grouting a lockable 5-foot long 6-inch diameter protective steel casing over the well head. A 3- by 3-foot square concrete pad 4 inches thick was placed around the well. The pad is sloped to direct drainage away from the well. It has a steel post in each corner and a survey marker embedded in the surface. Each survey marker was later stamped with the well number and surveyed marker elevation. Protective posts and well casings were painted, and each protective casing was marked with the well number.

5.4 Installation of Wells MW-1 through MW-6. Six ground-water monitoring wells, MW-1 through MW-6, were installed around the closed

UEP to implement a Compliance Monitoring Program at the Point of Compliance for the UEP, and to implement a Corrective Action Monitoring Program downgradient of the UEP, as proposed in the document "U.S. Army Proposal for Additional Groundwater Monitoring at the Closed Unlined Evaporation Pond (UEP), Longhorn Army Ammunition Plant, Marshall, Texas," prepared by the USACE, Huntsville Division, February 1987, and submitted by LHAAP to the TWC on 27 April 1987. The wells were installed at the proposed locations and were constructed in accordance with the proposed well construction detail, shown on Figure 17. Wells were to be screened at depths approximating the depths previously monitored by USAEHA wells that were removed during closure of the UEP, although construction details for these wells are not available. Boring logs showed all of the USAEHA wells drilled to a depth of 50 feet. The personal communication cited by CDM in the CDM report states that the USAEHA wells screened the top 10 feet of the water table, which is considerably higher than the final 50-foot depths of the well borings.

Examination of the USAEHA boring logs for well borings BH-1 through BH-11 consistently showed various types of clay encountered at approximate el. 150. Because both USATHAMA wells, screened at shallow depths, and USAEHA wells, screened at unknown depths but penetrating to 50 feet, had shown contamination above this clay stratum, it was decided to treat this clay as a possible aquiclude and screen the materials lying immediately above it. Available boring logs and well

installation details for the USAEHA and USATHAMA wells are contained in Appendix L.

The six wells were installed from 24 August to 30 September 1987. A copy of the drill request detailing decontamination, sampling, well installation, and safety procedures is provided as Appendix M. After the installation of the first two wells, MW-1 and MW-2, it became necessary to drill an exploratory soil boring, MW-1A, for the purpose of positively identifying the target clay and the soils immediately overlying it. Boring MW-1A was drilled at the location shown on Sheet 21 in a direction believed to be upgradient from the UEP. The boring was augered dry to a depth of 53.0 feet. Soil samples for soil classification analysis were taken every change of material, and the boring was immediately grouted upon completion. A very silty, sandy, low to medium plasticity clay was encountered from 40.2 to 44.0 feet, and a medium to high plasticity clay occurred from 44.0 feet to the bottom of the boring. The occurrence of these clays at these depths agreed well enough with the USAEHA logs and the materials encountered in MW-1 and MW-2 to continue using the clays they identified at approximate el. 150 as the bottom of the MW wells being installed. Geologic logs for soil boring MW-1A and well borings MW-1 through MW-6 are provided in Appendix N. Well installation details are provided in Appendix O and are summarized on Table 8. No unusual conditions were noted during development of any of the wells.

A total of 16 soil samples were taken to be analyzed for VOCs,

TABLE 8.

SUMMARY OF MONITORING WELL INSTALLATION DATA^a FOR MW-1 THROUGH MW-15

Well No.	Survey Marker Elevation ^b (ft msl)	Total Boring Depth (ft)	Depth to Top of Screen (ft)	Depth to Top of Sand (ft)	Depth to Top of Bentonite (ft)	Top of Well Pipe Elevation (ft msl)
MW-1	197.73	38.0	31.0	28.8	25.2	199.24
MW-2	195.18	40.4	33.4	31.0	27.0	197.00
MW-3	194.02	46.0	39.0	36.5	31.0	196.51
MW-4	195.77	43.0	36.0	33.2	29.1	197.31
MW-5	193.34	40.8	33.8	31.5	27.2	195.21
MW-6	190.26	45.8	38.8	36.4	32.2	192.18
MW-7	186.62	25.0	18.0	15.0	11.5	188.56
MW-8	185.47	32.0	24.0	11.0	8.0	186.85
MW-9	182.58	27.0	20.0	11.0	8.0	184.78
MW-10	176.23	34.5	26.5	21.5	18.0	177.99
MW-11	176.52	11.6	4.6	2.6	0.6	177.65
MW-12	176.77	28.8	20.8	18.8	16.0	178.37
MW-13	174.64	46.0	38.0	36.0	32.0	176.72
MW-14	180.93	51.0	43.0	40.0	36.0	182.99
MW-15	195.70	69.5	61.5	59.5	57.0	197.32

a For well installation details, see Appendix O.

b For survey data, see Appendix K.

total metals, and explosives concentrations. Samples were taken at the 2- and 10-foot depths in each boring, as well as at the depth where free water was encountered in borings MW-3 through MW-6. All samples were delivered by Fort Worth District personnel to SWDL in Dallas, Texas, where the total metals analyses were performed. Volatile organics and explosive analyses were performed by Southwest Laboratory of Oklahoma in Tulsa, Oklahoma, under contract to SWDL.

Analytical results from these 16 soil samples are summarized on Table 9. No volatile organics were detected in any of the well borings. Total barium concentrations were low, ranging from no detection (<20 mg/kg) to a maximum concentration of 73 mg/kg in boring MW-5. Very low concentrations of the explosive HMX were found at both the 2- and 10-foot sampling depths in MW-1 and MW-2, with a maximum concentration of 0.31 ug/g. The explosive RDX was the only other explosive detected, which was found at a concentration of 0.22 ug/g at 2 feet in MW-3. Complete analytical results are contained in Appendix P, and quality assurance is discussed in Volume 5.

5.5 Deep Stratigraphic Test Borings. Before siting additional monitoring well locations to monitor the contaminant plume underlying the western corner of the ABG, three deep stratigraphic test borings were drilled and geophysically logged to determine if there was enough stratigraphic correlation across this area to define a confining bed above which to screen the new wells. Only two wells, 120 and C-2, were located downgradient from the ACD, and neither boring had encountered any type of impermeable material before reaching their

TABLE 9. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES FROM WELL BORINGS MW-1 THROUGH MW-6

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
MW-1	2.0	27	ND	HMX 0.31
	10.0	27	ND	HMX 0.21
MW-2	2.0	27	ND	HMX 0.28
	10.0	58	ND	HMX 0.18
MW-3	2.0	21	ND	RDX 0.22
	10.0	ND	Acetone ^c 28	ND
	15.0	ND	Acetone ^c 20	ND
MW-4	2.0	ND	ND	ND
	10.0	31	Acetone ^c 38	ND
	15.0	26	Acetone ^c 33	ND
MW-5	2.0	73	ND	ND
	10.0	57	Acetone ^c 19	ND
	17.0	68	Acetone ^c 34	ND
MW-6	2.0	68	Acetone ^c 12	ND
	10.0	59	Acetone ^c 28	ND
	18.0	29	Acetone ^c 26	ND

ND = Not detected or detected below calibration limits.

^aAnalyses performed by USACE Southwestern Division Laboratory. Calibration limit for Ba was 20.0 mg/kg.

^bAnalyses performed by Southwest Laboratory of Oklahoma, under contract to USACE Southwestern Division Laboratory. Calibration limits for specific VOCs are contained in Appendix P. Explosive cpds analyzed and respective calibration limits were TNT (0.05 ug/g), 2,4 DNT (0.05 ug/g), 2,6 DNT (0.05 ug/g), RDX (0.05 ug/g), HMX (0.05 ug/g), and tetryl (0.05 ug/g).

^cAcetone is a common lab contaminant, with normal allowable level five times detection limit reported.

Complete analytical results are contained in Appendix P.

final depths of 24.0 (el. 156) and 32.0 feet (el. 142), respectively. It also appeared likely that a contact between the Wilcox Group and Recent alluvium runs northeast-southwest somewhere across the western corner of the ABG, with the ACD situated on Wilcox and most of the downgradient area situated in alluvium. The test borings would help define this contact and how the stratigraphy of the Wilcox and alluvium relate with respect to contaminant movement in the ground water.

Three deep stratigraphic test borings, designated 3F-922 through 3F-924, were drilled from 20-26 May 1988 at the locations shown on Sheet 21. Drilling and logging were performed by a Fort Worth District drill crew and geologist following a standard set of procedures. All borings were drilled with a Failing 1500 drill rig. All downhole equipment was steam cleaned prior to drilling each boring. Borings were drilled with a 4½-inch diameter fishtail drill bit. A pure bentonite drill mud mixed with nonchlorinated water from the ABG water supply was kept under good circulation to avoid cross-contaminating any lower saturated zones. No samples were taken, but stratigraphy was logged from the drill cuttings and drilling action. All stratigraphic test borings were drilled into clay shale. When drilling was complete, a resistivity and gamma log were run in each boring. Spontaneous potential logs were not run because of equipment problems. Then each boring was backfilled in accordance with TWC requirements for plugging abandoned water wells, as stated in 31 TAC 287.49. Each boring was backfilled to within 10 feet of the ground surface with

a thick bentonite mud pumped through the drill rods and placed from the bottom of the boring up, displacing all drill fluid upward and out of the borehole. The top 10 feet of the boring were then grouted with a neat bentonite cement grout. After backfilling, each boring was staked to be surveyed at a later time.

A copy of the drill request for borings 3F-922, 3F-923, and 3F-924 is provided as Appendix Q. Geologic logs are shown on Sheet 22. Resistivity and gamma logs for each of the test borings are shown on Sheets 23 through 27. The geophysical logs agreed fairly well with the stratigraphy described from the drill cuttings. At least two saturated permeable zones were identified in each of the borings, with a third deeper zone occurring in 3F-922. The uppermost saturated zone consisted of a variable thickness of interbedded sandy silts and silty sands. Of primary concern was to identify a confining clay beneath this zone. This clay was found from el. 157-142 in 3F-922, from el. 165-149 in 3F-923, and from el. 148-142 in 3F-924, overlying a 20- to 30-foot thick sand occurring in each boring. A second confining clay was found in boring 3F-922, overlying a third permeable zone approximately 18 feet thick (el. 109-91). A second confining layer was not encountered in borings 3F-923 and 3F-924. Instead, the second saturated zones were underlain by a very sandy clay. All borings bottomed into clay shale. Clay shale was encountered at el. 71 in 3F-922, at el. 34 in 3F-923, and el. 25 in 3F-924.

A fourth stratigraphic test boring, 3F-925, was drilled and

geophysically logged after analyses of ground-water samples from newly installed wells MW-1 through MW-6 showed extremely high concentrations of methylene chloride and TCE still present around the closed UEP. Because ground-water contamination had now been identified as still being present around the pond, it became necessary to expand the investigation to include the UEP area of the ABG to delineate the plume underlying this corner of the site. Existing wells showing contamination around the UEP are screened in the uppermost saturated zone. Therefore, it became necessary to begin screening in the next deeper permeable zone to assess the vertical extent of contamination. Test boring 3F-925 was drilled and geophysically logged to define this second zone and any additional confining beds, as well as provide deep stratigraphic information to determine any correlation across the entire ABG site.

Boring 3F-925 was drilled and logged from 23-24 August 1988 at the location shown on Sheet 21. The geologic log is shown on Sheet 22. The resistivity and gamma logs are shown with the stratigraphy on both Sheets 24 and 26. As with test borings 3F-922, 3F-923, and 3F-924, stratigraphy logged from the drill cuttings agreed fairly well with the information shown by the geophysical logs for 3F-925. The upper clay confining bed encountered in exploratory boring MW-1A and well borings MW-2 and MW-4 was identified in 3F-925 as occurring from el. 156-146. This was underlain by a second permeable zone about 22 feet thick, logged as silty sand and sandy silt, occurring from

el. 146-124. A thin high plasticity clay layer was described as occurring from el. 124-122, underlain by about 35 feet of sandy clay and sandy silt. Clay shale was encountered at el. 87.

5.6 Installation of Wells MW-7 Through MW-15. Eight new wells, MW-7 through MW-14, were installed downgradient of the ACD to monitor the contaminant plume originating from the remnant trenches beneath the structure. The downgradient direction was determined from the 20-22 April 1988 water level data which showed ground water flowing to the west and to the north of the ACD, as shown on Sheet 19. Wells MW-7 through MW-12 were sited at the proposed locations shown on Sheet 19 for the purpose of determining the lateral extent of the contamination already identified in the upper interbedded saturated zone screened by wells 120 and 129. Based on the geology map shown on Figure 8, the contact between the Wilcox and floodplain alluvium roughly follows the contour of the 100-year floodplain shown on sheet 19, which indicates that wells MW-7, MW-8, and MW-9 would be constructed in the primary materials of the Wilcox, the same materials in which the trench materials are buried, while wells MW-10, MW-11, and MW-12 would be located in the alluvium of the floodplain, screened in either Wilcox or alluvial materials.

Wells MW-7 through MW-12 were screened at the base of the uppermost saturated zone as it was identified in test borings 3F-922, 3F-923, and 3F-924. Well location MW-7 was selected to define the southernmost extent of the plume using the "No Detection" contour derived from

the soil gas survey, shown on Sheet 28. Well location MW-8 was selected for being directly downgradient from contaminated well 129, and well location MW-9 was selected for being directly downgradient from the contamination source. Well location MW-10 is directly downgradient from the contamination source in a more northerly direction than MW-9, and is situated halfway between the source and well C-2, which has not shown contamination since it was installed in July 1984. Well MW-11 was sited halfway between the source and well 123 with the intention of defining the northernmost extent of the plume, since 123 has not shown contamination since July 1984. And well MW-12 was sited as the closest well to the source located downgradient in the floodplain with the intention of determining if the uppermost saturated zone of the Wilcox and the alluvium are hydraulically connected.

Wells MW-13 and MW-14, installed at the locations shown on Sheet 21, were screened in the second deeper permeable zone identified in test borings 3F-922, 3F-923, and 3F-924. Well MW-13 was installed 10 feet away from well C-2 to determine if the contaminant plume has been moving beneath C-2, which would account for C-2 not showing any contamination when it is located downgradient from the contaminant source. Well MW-14 was installed 10 feet away from well 120 to determine the vertical extent of contamination at a known contaminated location, since well 120 has consistently shown the highest concentrations of methylene chloride in this area of the ABG.

A ninth well, MW-15, located in the UEP area of the ABG, was also

screened in the second deeper permeable zone as it was identified in test boring 3F-925. Well MW-15 was installed 10 feet away from well MW-2, the most contaminated well in this area of the ABG, to determine if contamination occurring in MW-2 extends downward into this new saturated zone.

The nine new monitoring wells were installed from 29 June to 16 September 1988. Copies of the drill requests detailing decontamination, sampling, well installation, and safety procedures are provided in Appendix R. Estimated well depths shown on the drill requests were determined using the geophysical data obtained from the deep stratigraphic test borings, the stratigraphic data from the well borings of existing wells at the ABG contained in Appendix L and the surveyed elevations of the proposed well locations shown in Appendix K. (Note that survey data shown in Appendix K for well locations MW-12, MW-13, and MW-14 are for originally proposed locations further north and west of well C-2, not shown on Sheet 19. These proposed shallow well locations were later changed to the cluster well locations discussed here and shown on Sheet 21 after the May 1988 water analyses for the LHAAP quarterly monitoring program had been received. The drill requests for these wells address the actual installation locations shown on Sheet 21). Geologic logs for well borings MW-7 through MW-15 are provided in Appendix N. Well installation details are provided in Appendix O. No unusual conditions were noted for any of the wells during development.

The target confining clay for well MW-7 was encountered approximately 11 feet shallower than was anticipated. This boring was originally drilled to a depth of 36 feet at the proposed surveyed location listed in Appendix K. The medium to high plasticity clay first encountered at 21 feet was never penetrated, indicating that this was most likely the target confining clay, so the boring was backfilled with a neat bentonite cement grout and redrilled to a depth of only 25 feet at the location shown on Sheet 21. The target confining clays for wells MW-8 and MW-9 were encountered close to the anticipated depths. A weak odor was noted in MW-9 directly downgradient of the contaminant source. No confining clay was encountered at the anticipated depths in borings MW-10, MW-11, and MW-12. However, these borings were not drilled much deeper than the estimated well depths shown on the drill request. A weak odor was noted in MW-12 when free water was encountered.

Deeper wells MW-13 and MW-14 were cased off in questionable confining bed materials. The upper saturated zone in MW-13 was cased off in a 2-foot thick medium to high plasticity clay encountered at el. 147-145 that appeared comparable to the 3-foot thick plastic clay logged at el. 148-145 in test boring 3F-924. The well was completed in an underlying fine-grained sand. Well MW-14 was originally drilled to a depth of 39 feet at a location on the other side of well 120 before it was backfilled with a thick bentonite drill mud and redrilled at the location shown on Sheet 21. The boring was backfilled and

offset after a thin low plasticity clay was penetrated at el. 155-153 and no other confining materials were encountered. Backfilling was performed in the same manner as followed for the stratigraphic test borings to prevent cross-contamination of the upper and lower zones. The upper saturated zone of the new well boring was cased off in the 1.7 feet thick low plasticity clay encountered at el. 155-153, and the well was completed in an underlying fine to medium grained sand. A weak odor was noted to a depth of 32.8 feet, about 5 feet below the questionable confining layer.

Well boring MW-15 encountered about 6.5 feet of medium to high plasticity clay at the anticipated el. 155. This clay was slightly thinner than that logged in test boring 3F-925, but correlated well with other well borings around the UEP. Some odor was noted while drilling from el. 170-149, but no measurable amounts were detected during monitoring. The well was completed in an underlying very silty fine-grained sand.

A total of 18 soil samples were taken for chemical analysis while drilling well borings MW-7 through MW-15. Samples were taken at 2- and 10-foot depths in each boring and were analyzed for total metals, VOCs, and explosives in accordance with the quality assurance/quality control plan contained in Appendix D. Samples were delivered by Fort Worth District personnel to the SWDL in Dallas, Texas, where total metals analyses were performed. Volatile organics and explosives analyses were performed by Southwest Laboratory of Oklahoma, in Tulsa Oklahoma, under contract to SWDL. Analytical results for chemical

soil analyses are summarized on Table 10. Complete results are contained in Appendix S.

Very little contamination was detected in any of the soil samples taken. The maximum concentration of total barium detected was 200 mg/kg in well boring MW-14. Well boring MW-12 also showed a similar concentration of 180 mg/kg of total barium at 2 feet. All other samples ranged from below detection to less than 100 mg/kg total barium. Volatile organics were detected in only three of the well borings- MW-10, MW-11, and MW-12. Borings MW-10 and MW-11 showed low concentrations of TCE at the 10-foot depth, with a trace of 1,2-dichloroethane also occurring in MW-11. Boring MW-12 showed 33 ug/kg of TCE at 2 feet, and 670 ug/kg of methylene chloride at 10 feet. No other VOCs were detected. Also, no explosives were detected in any of the borings. The quality assurance for these analyses is discussed in Volume 5.

5.7 Slug Testing and Water Sampling. Each of the 15 new wells, MW-1 through MW-15, were slug tested and sampled from 18-30 September 1988. An additional 10 existing wells were also sampled at this time. These wells were C-2, C-3, C-4, C-5, 109, 120, 123, 124, 125, and 129, which were selected because they are downgradient from both the closed UEP and the trenches beneath the ACD, and would therefore best define the contaminant plume(s) emanating from these sources.

Requests for slug testing and water sampling were originally prepared to perform each as a separate event. The order of wells

TABLE 10. SUMMARY OF ANALYTICAL RESULTS FOR CHEMICAL SOIL SAMPLES
FROM WELL BORINGS MW-7 THROUGH MW-15

Boring No.	Sample Depth (ft)	Total Barium ^a (mg/kg)	VOCs ^b (ug/kg)	Explosives ^b (ug/g)
MW-7	2.0	23	ND	ND
	10.0	96	ND	ND
MW-8	2.0	28	ND	ND
	10.0	20	ND	ND
MW-9	2.0	51	ND	ND
	10.0	29	ND	ND
MW-10	2.0	ND	ND	ND
	10.0	ND	Trichloroethene 44	ND
MW-11	2.0	43	ND	ND
	10.0	ND	1,2-Dichloroethane 14 Trichloroethene 140	ND
MW-12	2.0	180	Trichloroethene 33	ND
	10.0	34	Methylene Chloride 670	ND
MW-13	2.0	11	Acetone ^c 44	ND
	10.0	15	Acetone ^c 23	ND
MW-14	2.0	200	Acetone ^c 31	ND
	10.0	28	ND	ND
MW-15	2.0	70	Acetone ^c 13	ND
	10.0	92	ND	ND

ND = Not detected or detected below calibration limits.

^aAnalyses performed by USACE Southwestern Division Laboratory. Calibration limit for Ba was 20.0 Mg/kg.

^bAnalyses performed by Southwest Laboratory of Oklahoma, under contract to USACE Southwestern Division Laboratory. Calibration limits for specific VOCs are contained in Appendix S. Explosive cpds analyzed and respective calibration limits were HMX (1.6 ug/g), RDX (1.8 ug/g), tetryl (5.5 ug/g), TNT (0.8 ug/g), 2,4 DNT (0.8 ug/g), and 2,6 DNT (0.8 ug/g).

^cAcetone is a common lab contaminant, with normal allowable level five times detection limit reported.

Complete analytical results are contained in Appendix S.

to be slug tested and the order of wells to be sampled were specified in each request in an increasing order of likely contamination to prevent cross-contaminating the wells. However, time constraints required that both slug testing and sampling be performed simultaneously, and muddy ground conditions necessitated doing those wells that could be accessed with the drill rig first.

5.7.1 Slug Testing. In most cases, slug testing was performed first, then the well was purged and sampled. Slug testing was performed by a Fort Worth District drill crew and geologist following a standard set of procedures for a slug withdrawal test developed from pp 299-304 of Geological Survey Water-Supply Paper 1536-I, "Methods of Determining Permeability, Transmissibility, and Drawdown." These procedures are shown on Figure 19. The data sheet for recording field measurements is shown on Figure 20.

Slug testing was performed using a steam cleaned 10-foot bailer operated by a Failing 1500 drill rig. Procedures specified removing one bailer volume of water from the well and recording the recharge rate until at least 85 percent recovery had occurred. This did not work well in practice, however, because recovery of this small volume of water was too quick to record at least 10 minutes of measurements. Therefore, slug test procedures were modified in the field to remove as much water as possible from the well prior to recording the recharge. This method allowed for recording more complete recovery data and also served as purging the well for water sampling. If a well was

SLUG TEST PROCEDURES

1. Decontaminate bailer and length of sandline equivalent to well depth by steam cleaning using a nonphosphate detergent and rinsing with distilled water.
2. Decontaminate water level indicator probe and length of cable equivalent to well depth by thoroughly rinsing with distilled water.
3. Measure depth to bottom of the well (BOW) to nearest 0.01 foot using marked top of well casing as reference.
4. Measure static water level (SWL) to nearest 0.01 foot. Record time.
5. Compute 100 percent recovery water level (100 RWL) for fast recharging wells and 85 percent recovery water level (85 RWL) for slow recharging wells.

$$100 \text{ RWL} = \text{SWL}$$

$$85 \text{ RWL} = \text{BOW} - (0.85 \times \text{RWL}), \text{ where RWL} = \text{BOW} - \text{SWL}$$
6. Put bailer in bottom of the well.
7. Record water level with bailer in well (BWL). Record time.
8. Begin slug test when BWL = SWL. Remove bailer. Note time (t_0) and immediate water level (WL) after water is removed.
9. Record water level measurements every minute for the first 10 minutes, every 5 minutes for the next 20 minutes, then every 10 minutes for the next 30 minutes. If the well has not reached 85 percent recovery after 1 hour from t_0 , continue to read water levels at 20-minute increments for the next 2 hours, then every hour until complete.
10. Stop recording water levels after 100 percent recovery (100 RWL) is achieved in fast recharging wells, or 85 percent recovery (85 RWL) is achieved in slow recharging wells.
11. Record amount of water bailed from the well. Either calculate using $V = \pi r^2 L$, or measure amount collected.
12. Under "Remarks," note any problems or unusual characteristics while testing.
13. Person performing slug test should initial the data sheet.

Figure 19. Slug Test Procedures.

SLUG TEST FIELD DATA SHEET						PROJECT:
1.	DATE					
2.	WELL NO.					
3.	Csg dia/Type					
4.	BCN					
5.	SWL					
6.	SWL Time					
7.	100 RWL					
8.	85 RWL					
9.	BWL					
10.	BWL Time					
11.	Amt Boiled					
12.	SLUG TEST					
	t_0 /WL					
	every minute					
	t_1 /WL					
	t_2 /WL					
	t_3 /WL					
	t_4 /WL					
	t_5 /WL					
	t_6 /WL					
	t_7 /WL					
	t_8 /WL					
	t_9 /WL					
	t_{10} /WL					
	every 5 minutes					
	t_{11} /WL					
	t_{12} /WL					
	t_{13} /WL					
	t_{14} /WL					
	every 10 minutes					
	t_{15} /WL					
	t_{16} /WL					
	t_{17} /WL					
	every 20 minutes					
	t_{18} /WL					
	t_{19} /WL					
	t_{20} /WL					
	t_{21} /WL					
	t_{22} /WL					
	t_{23} /WL					
13.	REMARKS					
14.	INITIALS					

Figure 20. Slug Test Field Data Sheet.

sampled prior to slug testing, the "DEPTH TO WATER" measurement recorded prior to purging was used as the static water level ("SWL") measurement for the slug test. All water removed from the wells was contained in 55-gallon drums, then was hauled to a sump specified by Morton Thiokol, Inc., personnel for their later collection and treatment. Breathing space around the well was monitored for methylene chloride and TCE during each slug test using Dräger tubes. Slug testing procedures provided to the field personnel are detailed on the request for slug testing contained in Appendix T.

Slug test recovery data were recorded using a Slope Indicator Company Model 51453 water level indicator. Complete field data are provided in Appendix U. Water level recovery time was relatively slow in all wells except MW-14 and MW-15, ranging from 80 minutes up to 6 hours. Wells MW-14 and MW-15 recharged quickly, in 40 minutes and 10 minutes, respectively, which was anticipated because these wells were screened in the next lower sandier unit. Quick recharge was also anticipated in MW-13, which was screened in a deeper sandier zone, but recovery time was slow, taking 2 hours and 20 minutes to reach 100 percent recovery. An odor was noted in only two of the wells tested, MW-1 and MW-2, and was noted as being very strong; however the odors were not strong enough to be measured by the monitoring equipment.

5.7.2 Water Sampling. A total of 25 wells were sampled by Fort Worth District personnel following a set of procedures developed in accordance

with the guidelines specified in the USEPA publication "RCRA Ground-Water Monitoring Technical Enforcement Guidance Document." All procedures are detailed on the water sampling request contained in Appendix V. Because wells could not be sampled in the order specified on the water sampling request, special care was taken for decontaminating all downhole and laboratory equipment following the procedures listed on Figure 21 prior to sampling each well.

A **Water Sampling Field Data Sheet**, shown on Figure 22, was developed to record all field measurements made during sampling. Instructions for sampling and filling out the **Field Data Sheet** are provided on Figure 23. Water well depths and depths to screened intervals were provided to the field personnel to spot any anomalous readings.

Prior to obtaining water samples, it was necessary to purge each well a minimum of 3 casing volumes of standing water. The well depth and the depth to water was measured in each well to calculate the volume of water to be purged. The volume of standing water in the well was calculated using a rough conversion of 1 foot = 1 gallon for 4-inch diameter wells, and 1 foot = $\frac{1}{2}$ gallon for 2-inch diameter wells. The total volume to be purged was calculated by multiplying this number of gallons by 3. Each well was purged at least three times or until dry. Breathing space was monitored during purging and water sampling using both methylene chloride and TCE Dräger tubes. Purging of 4-inch diameter wells was accomplished using a 10-foot long bailer operated by a Failing 1500 drill rig. Two-inch diameter

DECONTAMINATION PROCEDURES

1. Water level measuring equipment shall be decontaminated prior to each use by thoroughly rinsing with distilled water.
2. Purging equipment shall be decontaminated prior to each use by steam cleaning with a nonphosphate detergent, then thoroughly rinsing with distilled water.
3. Water sampling equipment and laboratory equipment shall be decontaminated prior to each use using the following procedures:
 - a. Thoroughly wash with a nonphosphate detergent.
 - b. Rinse with tap water.
 - c. Rinse with dilute hydrochloric acid (10 parts distilled water to 1 part HCl).
 - d. Rinse with distilled water.
 - e. Rinse with pesticide grade hexane.
 - f. Rinse with pesticide grade methanol.

Figure 21. Decontamination Procedures for Ground-Water Sampling.

WATER SAMPLING FIELD DATA SHEET					PROJECT:	
A. PURGING —						
1.	DATE					
2.	WELL NO.					
3.	CSQ DIA/TYPE					
4.	TOTAL DEPTH					
5.	DEPTH TO WATER					
6.	WATER IN FT.					
7.	GALS. TO PURGE					
8.	START TIME					
9.	STOP TIME					
10.	AMT. BAILED					
B. SAMPLING —						
1.	DATE					
2.	DEPTH TO WATER					
3.	BAILER TYPE					
4.	START TIME					
5.	MEASUREMENTS					
	pH					
	TEMP °C					
	COND. μ S					
6.	STOP TIME					
7.	MEASUREMENTS					
	pH					
	TEMP °C					
	COND. μ S					
8.	RECHARGE					
9.	SAMPLE TYPES					
10.	DUPPLICATES					
11.	TRAVEL BLANKS					
12.	EQUIP BLANKS					
13.	COOLER NO.					
14.	STRAP NO.					
15.	BUS BILL NO.					
REMARKS						
INITIALS						

Figure 22. Water Sampling Field Data Sheet.

GROUND-WATER SAMPLING PROCEDURES

1. Calibrate field instruments.
2. Begin taking water samples after water level has recovered in well.
3. Record depth to water prior to sampling.
4. Record time begin sampling.
5. Record type of sampler (e.g., dedicated stainless steel, dedicated PVC, portable teflon, etc).
6. Collect samples in the following order:
 - a. pH/conductivity/temperature - collect in clean beaker. Measure immediately at time of collection. Recorded value of pH and conductivity should be an average of four readings. Discard sample.
 - b. Volatile organics (VOCs) - Overfill three 40 ml glass vials. No air or bubbles in sample. No agitation.
 - c. Total organic halides (TOX) - Overfill two glass liter bottles. Preservative to be added in laboratory.
 - d. Metals - Overfill one plastic liter bottle. Preservative to be added in laboratory.
 - e. Nitrite/Nitrate - Overfill one plastic liter bottle. Preservative to be added in laboratory.
 - f. Chloride - Overfill one plastic liter bottle.
 - g. Explosives - Overfill two glass liter bottles.
 - h. pH/Conductive/Temperature - Collect in clean beaker and measure as in Step a. Also fill one glass liter bottle for laboratory measurements.
7. Record time at end of sampling.
8. Describe recharge rate (e.g., immediate, fast, slow, etc).
9. Record number of each type of sample container taken. For example: three vials, four liter glass, and three liter plastic would be 3/4/3. Don't count the glass liter bottle taken for pH/conductivity/temperature because this sample will be discarded prior to shipment. However, do include duplicates and blanks.
10. Record the parameter for duplicates, travel blanks, or equipment blanks when taken.
11. Shipping information should be filled out after samples are preserved.
12. Under "Remarks," note any problems with the well structure or unusual characteristics while sampling.
13. Person collecting the samples should initial the data sheet.

Figure 23. Procedures for Ground-Water Sampling

wells were purged using their dedicated bailers. Four-inch diameter PVC wells C-2, C-3, C-4, and C-5 were purged using a portable 3-foot long 2-inch diameter teflon bailer suspended on a teflon coated stainless steel cable. Purged water from all 25 wells was collected in 55-gallon drums, then hauled to a sump specified by Morton Thiokol, Inc., personnel for their later collection and treatment. Purging procedures are listed on Figure 24.

If a well was sampled after slug testing, it was considered sufficiently purged for sampling if it bailed dry during the slug test and recharged too slowly to allow for three purgings in a single day. The well was then sampled after it recovered. Only 8 of the 25 wells sampled required purging a minimum of 3 times. These wells were 125, 129, C-2, C-3, C-4, C-5, MW-14, and MW-15. Wells 125 and 129 both purged dry, but recovered in a sufficient amount of time to continue purging the required minimum 3 casing volumes prior to sampling. The other six wells did not purge dry and recharged quickly.

Water samples were taken after the water level had recovered in the well. If a well purged dry and recovered slowly, sampling did not begin until the next day. All wells except C-2, C-3, C-4, and C-5 were sampled with dedicated bailers following the procedures listed on Figure 23. In all cases, efforts were made to sample each well opposite the well screen and not in the sump.

Field measurements for pH, temperature, and conductivity were made at both the beginning and end of sampling for each well. Each

PURGING PROCEDURES

1. Decontaminate bailer and length of sandline equivalent to well depth by steam cleaning using a nonphosphate detergent and rinsing with distilled water.
2. Decontaminate water level indicator by thoroughly rinsing with distilled water.
3. Measure depth to bottom of the well to the nearest 0.01 foot using marked top of well casing as reference.
4. Measure depth to water to nearest 0.01 foot.
5. Calculate standing column of water in feet by subtracting depth to water from total depth of well.
6. Calculate number of gallons to be bailed by multiplying standing column of water by 3.
7. Begin bailing. Record start time.
8. Stop bailing when three casing volumes of water have been removed or the well goes dry, whichever occurs first. Record stop time.
9. Record approximate amount of water bailed.

Figure 24. Purging Procedures for Ground-Water Sampling.

of these parameters was measured four times and the average value was recorded. Samples were then taken in the following order of parameters: VOCs, total organic halogens (TOX), metals, nitrites/nitrates, chloride, and explosives. Numbers and types of containers for each parameter are shown on Table 11. Appropriate duplicate, travel, and equipment blanks were also taken in accordance with quality assurance procedures described in the Quality Assurance/Quality Control Plan in Appendix D. To ensure that the proper number and types of blanks were taken or prepared, a schedule for quality assurance samples was drawn up prior to sampling. This schedule is shown on Table 12. Quality assurance procedures for field samples are listed on Figure 25.

Complete water sampling field data are provided in Appendix W. New monitoring wells MW-1 through MW-15 showed no silt during purging and sampling, although MW-6 was slightly milky in color. On the other hand, several of the existing wells sampled did show silt during purging and sampling. These wells were 109, 123, 124, 125, 129, and C-5, with wells 124 and 129 exhibiting the worst silt and sand conditions during purging. A milky white, yellow, or gray color was noted about the water from several of the wells. Odors were noted in only three of the wells sampled. Wells MW-1 and MW-2 exhibited very strong solvent odors during purging and sampling, but not strong enough to measure, and well C-2 had a salty odor.

All samples were preserved in accordance with the procedures

TABLE 11. SAMPLE CONTAINER AND PRESERVATION PLAN

VIALS			
3	40 ml	VOCs	4°C, Full
GLASS			
2	Liter	Tox	Full, pH < 2 w/ H ₂ SO ₄ , 1 ml Sodium Sulfite
2	Liter	Explosives	4°C
1	Liter	pH/Cond/Temp	Dispose
PLASTIC			
1	Liter	Metals (As, Ba, Cd, Cr, Pb, Hg, Ni, Se, Ag, Zn)	pH < 2 w/ HNO ₃
1	Liter	Nitrite/Nitrate	pH < 2 w/ H ₂ SO ₄
1	Liter	Chloride	4°C

TABLE 12. SAMPLING PLAN FOR DUPLICATES, TRAVEL BLANKS,
AND EQUIPMENT BLANKS

WELL NO.	PARAMETER					
	VOCs	TOX	Metals	N/N	CI	EXPI.
MW-1	D					
MW-2		D				
MW-3				D		
MW-4			D			
MW-5					D	
MW-6						D
MW-7	T					
MW-8			E			
MW-9			E			
MW-10	D					
MW-11		D				
MW-12			D			
MW-13				D		
MW-14					D	
MW-15						D
C-2			T			
C-3	E					
C-4	D					
C-5		D				
109			D			
120				D		
123					D	
124						D
125	T					
129						

D = duplicate
 T = travel blank
 E = equipment blank

DUPLICATE, TRAVEL, AND EQUIPMENT BLANK PROCEDURES

1. The sampling pattern for duplicates, travel blanks, and equipment blanks is shown on the attached table.
2. A duplicate sample consists of the same number and type of containers as taken for the original sample for a specific parameter. Duplicates are taken, preserved, and labeled in the same manner as the original sample, but have the word "duplicate" included on the label.
3. Travel blanks for a specific parameter consist of distilled water placed in the required number and types of containers for that parameter. These are placed in the ice chest prior to sampling a well. Travel blanks are then preserved and labeled in the same manner as the original sample, but have the words "travel blank" included on the label.
4. Equipment blanks for a specific parameter are taken from either the bailer used to purge a well or the portable bailer used to sample a well. An equipment blank is made after the equipment has been decontaminated but before the equipment is used at the well. The bailer is rinsed with distilled water. The rinsate is collected directly off the bailer in the number and types of containers specified for the parameter. Travel blanks are then preserved and labeled in the same manner as the original sample, but have the words "EQUIPMENT BLANK" included on the label. Specify either "PURGER" or "SAMPLER" on the label, also.
5. All blanks should be appropriately noted on the Field Data Sheet for the well where they are taken.
6. A separate Field Data Form and Chain of Custody record should be filled out for blanks taken at each well.

Figure 25. Quality Assurance Procedures for Field Samples.

described in the Quality Assurance/Quality Control Plan. Sample preservations were done in a temporary laboratory set up by Fort Worth District personnel on LHAAP. Preservation procedures are listed on Figure 26. All samples were kept on ice from the time they were taken until they were delivered by Fort Worth District personnel to the SWDL in Dallas, Texas.

Prior to sending samples to the laboratory, all documentation was completed for each sampled well following the recordkeeping procedures listed on Figure 27. This documentation consisted of completing the data listed on the **Water Sampling Field Data Sheet**, summarizing this data on a **Ground-Water Monitoring Well Data Form**, and completing and signing the **Chain of Custody Form**. The **Ground-Water Monitoring Well Data Form** was designed as a permanent record of the pertinent data recorded for each well sampling event. A copy of this form is shown on Figure 28. Completed forms for the round of water sampling are provided in Appendix X. The **Chain of Custody Form** was developed to show the numbers and types of containers in each shipment, as well as the parameters to be analyzed. A copy of this form is shown on Figure 29. Completed forms are provided in Appendix Y.

A copy of each the **Monitoring Well Data Form** and the **Chain of Custody Form** was enclosed with the appropriate water samples in an ice chest prior to shipping samples to the laboratory. Shipping procedures, detailed on Figure 30, were designed to deliver water samples to the laboratory within 24 hours of being taken. All samples

SAMPLE PRESERVATION PROCEDURES

1. Keep all samples packed in ice until delivered to SWD Laboratory.
2. Preserve samples at a laboratory set up on-site.
3. Preserve water samples in the following manner for the parameters specified.
 - a. Volatile Organic Compounds (VOCs) - No bubbles or air space in vials. Keep on ice at 4°C.
 - b. Total Organic Halides (TOX) - No bubbles or air space in bottles. Add enough sulfuric acid (H_2SO_4) to bring pH to <2. Add 1 ml sodium sulfite solution.
 - c. Metals (As, Ba, Cd, Cr, Pb, Hg, Ni, Se, Ag, Zn) - Add enough nitric acid (HNO_3) to bring pH to <2.
 - d. Nitrite/Nitrate - Add enough sulfuric acid (H_2SO_4) to bring pH to <2.
 - e. Chloride - Keep on ice at 4°C.
 - f. Explosives - Keep on ice at 4°C.
 - g. pH/Conductivity/Temperature - Make readings same as for the field. Record on Field Data Form. Discard sample after all other samples for well have been properly preserved.
4. Complete labels showing sample has been preserved and sign.

Figure 26. Preservation Procedures for Ground-Water Samples.

RECORDKEEPING PROCEDURES

1. Three forms will be filled out for each well sampled. These are Field Data Sheet, Field Data Form, and Chain of Custody Form.
2. Copies of each form will be distributed in the following manner:
 - a. Field Data Sheet - One field copy
- One copy to CESWF-ED-GG
 - b. Field Data Form - One field copy
- One copy to CESWF-ED-GG
- One copy to CESWD-ED-GL
 - c. Chain of Custody Form - One field copy
- One copy to CESWF-ED-GG
- One copy to CESWD-ED-GL
3. All bus tickets will be kept in the field.

Figure 27. Recordkeeping Procedures for Ground-Water Sampling.

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GROUND WATER MONITORING WELL
FIELD DATA FORM

Location _____ Date _____

Site _____ Type of sample _____

Well number _____ Csg diameter _____ Csg type _____

Rate of recharge _____

Riser elevation _____

Depth to water
from top of casing _____ Time of measurement _____

Depth to water
at time of sampling _____ Time of sampling _____

Water table _____ Measuring device _____

pH _____ Time of measurement _____

_____ Meter type and model _____

Conductivity, unhos/cm _____ Time of measurement _____

Meter type and model _____ Temperature _____

Chest # _____ Strap # _____ Bus bill _____

Notes concerning condition of well, odor , color, and any problems:

Sample collector _____

Figure 28. Ground-Water Monitoring Well Data Form.

GROUND WATER MONITORING WELL
CHAIN OF CUSTODY FORM

FORT WORTH DISTRICT, CORPS OF ENGINEERS

Location _____ Date _____

Site _____ Well number _____

Number of containers in shipment:

	glass	plastic
liter	_____	_____
vial	_____	_____

volatile organics

regular detection limits _____

0.5 ppb detection limits _____

Parameters sampled:

pH	_____
conductivity	_____
TOC	_____
Hardness as CaCO ₃	_____
metals, total *	_____
COD	_____
hexavalent chromium	_____
alkalinity	_____
chloride	_____
sulfate	_____
TOX	_____
nitrate	_____
volatile organics	_____
semi-organics	_____
total hydrocarbons	_____
BTX	_____
EXPLOSIVES	_____

* As, Ba, Be, Cd, Cr, Pb, Hg, Ni, Se, Ag, Zn, Fe, Mn, Mg, K,

Na, Ca, Cu

* _____ (all of the above)

CUSTODY RECORD
signature and title

Relinquished by	Received by	Date	Time
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____
_____	_____	_____	_____

Figure 29. Chain of Custody Form for Water Samples.

SHIPPING PROCEDURES

1. Pack all containers securely in ice chest, one well per chest. Include blanks for that well number.
2. Fill chest completely with ice.
3. Record chest number, strap number, and bus bill number on Field Data Sheet and Field Data Form. Fill out and sign Chain of Custody Form.
4. Make two copies of Field Data form and Chain of Custody Form.
5. Enclose a sealed plastic bag containing one copy each of Field Data Form and Chain of Custody Form in ice chest.
6. Close chest and secure with shipping strap.
7. Apply appropriate labels for shipping. Ship ice chests by bus each night to SWD Lab. Call SWD the following morning to tell them how many ice chests were sent.

Figure 30. Shipping Procedures for Ground-Water Samples.

were delivered by Fort Worth District personnel within 48 hours of being taken.

5.8 Water Sampling Results. A total of 25 well samples were analyzed for total metals, chlorides, total organic halogens (TOX), nitrates, VOCs, and explosives in accordance with the EPA test methods cited in the Quality Assurance/Quality Control Plan contained in Appendix D. Three duplicates were taken and analyzed for each of these six parameters. Three equipment blanks and three travel blanks were also taken and were analyzed for VOCs and total metals. The distribution of QA/QC samples is presented on Table 12.

Total metals, chloride, and nitrate analyses were performed by SWDL. Volatile organics, TOX, and explosives analyses were performed by Southwest Laboratory of Oklahoma, under contract to SWDL. Quality assurance samples were analyzed by Southwest Laboratory of Oklahoma and Controls for Environmental Pollution, Inc., in Santa Fe, NM, also under contract to the SWDL. Laboratory results for all analyses are contained in Appendix Z, and quality assurance is discussed in Volume 5.

Complete water quality results are summarized on Table 13. This table includes the three readings for pH, conductivity and temperature made during sampling, with the first reading made at the beginning of sampling, the second reading made at the end of sampling, and the third reading made in the laboratory while preserving the samples. Equipment problems with the pH meter required using pH paper several times to make a reading. These readings are noted. Each pH,

TABLE 13. SUMMARY OF ANALYTICAL RESULTS FOR WATER SAMPLES^a

Well No. (Sample No.)	MW-1 (8-1391)		MW-2 (8-1392)		MW-3 (8-1415)		MW-4 (8-1416)		MW-5 (8-1417)		MW-6 (8-1393)	
	1	2	1	2	1	2	1	2	1	2	1	2
pH	6.7	6.8	6.2	6.3	6.0	6.1	6.5	6.6	5.4	5.5	6.4	6.4
	6.8	6.8	6.6	6.6	6.2	6.2	6.8	6.8	5.7	5.7	6.4	6.4
Conductivity (umhos/cm)	2480	2440	2380	2480	1867	1850	3180	3180	1501	1510	2380	2380
	2700	2700	2550	2550	1864	1864	3280	3280	1517	2040	2210	2210
Temperature (°C)	22	22	22	22.5	23	24	22	25	21	21	23	23
	18	18	14	14	24	24	21	23	23	23	15	15
Chloride (mg/l)	930	930	890	890	540	540	750	750	420:490.0	420:490.0	980	980
TOX (mg/l)	4030	4030	3644.0:1300	3644.0:1300	259.0	259.0	502.0	502.0	178.9	178.9	2747.0	2747.0
Nitrates (mg/l)	2.7	2.7	3.1	3.1	3.2: <2.0	3.2: <2.0	<0.2	<0.2	4.2	4.2	<0.2	<0.2
Total Metals (ug/l)												
Ag	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0: <50	<5.0	<5.0	<5.0	<5.0	<5.0
As	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0: <2	<1.0	<1.0	<1.0	3.0	3.0
Ba	2200	2200	3600	3600	1900	1900	270: <1000	270: <1000	2000	2000	1800	1800
Cd	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0: 40	<5.0	<5.0	<5.0	<5.0	<5.0
Cr	5.8	5.8	8.0	8.0	27	27	9.8: 100	9.8: 100	18	18	7.5	7.5
Hg	0.42	0.42	0.42	0.42	0.42	0.42	<0.1: <2	<0.1: <2	0.42	0.42	<0.1	<0.1
Pb	14	14	16	16	16	16	12: <100	12: <100	10	10	17	17
Ni	33	33	38	38	24	24	75: 110	75: 110	44	44	42	42
Se	0.6	0.6	<0.4	<0.4	<0.4	<0.4	<0.4: <2	<0.4: <2	<0.4	<0.4	<0.4	<0.4
Zn	63	63	100	100	45	45	65: 60	65: 60	70	70	48	48
Explosives (ug/l) ^d	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
VOCs (ug/l)												
Methylene Chloride	4,200,000E: 4,820,000	4,200,000E: 4,820,000	17,000,000E	17,000,000E	19BJ	19BJ	58B	58B	14B	14B	88B	88B
Acetone	< 100,000: NA	< 100,000: NA	<100,000	<100,000	<39	<39	<83	<83	<10	<10	<10	<10
1,2-Dichloroethene (total)	< 50,000: NA	< 50,000: NA	<50,000	<50,000	32	32	120	120	31	31	15	15
1,2-Dichloroethane	< 50,000: <28,000	< 50,000: <28,000	<50,000	<50,000	<19	<19	<42	<42	43	43	<5	<5
Trichloroethene	< 200,000: 165,000	< 200,000: 165,000	1,400,000	1,400,000	550	550	1100	1100	150	150	91	91
Tetrachloroethene	< 50,000: <41,000	< 50,000: <41,000	17,000J	17,000J	<19	<19	<42	<42	<5	<5	<5	<5
Remarks	Very strong odor milky white color	Very strong odor milky white color	Very strong odor milky white color	Very strong odor milky white color	Milky yellow color	Milky yellow color	Slightly milky white color	Slightly milky white color	Slightly milky white color	Slightly milky white color	Slight odor milky white color	Slight odor milky white color

For footnotes, see last page of Table 13.

TABLE 13. SUMMARY OF ANALYTICAL RESULTS FOR WATER SAMPLES^a (cont'd)

Well No. (Sample No.)	MM-7 (8-1418)	Travel Blank (8-1419)	MM-8 (8-1480)	Equip Blank (8-1481)	MM-9 (8-1426)	Equip Blank (8-1427)	MM-10 (8-1428)	MM-11 (8-1465)
pH	1 2 3	- - 6.5 - 7b	5.2 5.2 6 - 6.5b		6b 5.5 - 6b 6b		6b 6 - 6.5b 6.5b	4.3 4.3 4.3
Conductivity (umhos/cm)	1 2 3	1472 1487 1492	857 849 890		212 204 210		995 992 962	309 288 316
Temperature (°C)	1 2 3	22 21.5 18	20.5 21 24		20 22 22.5		20 21 20.5	26 25 24.5
Chloride (mg/l)		280	200		43		310	40
TOX (mg/l)		169.5	1,608.0		9.2		2.0	3.2±0.8
Nitrates (mg/l)		0.25	6.1		0.85		<0.2	<0.2
Total Metals (ug/l)								
Ag	<5.0		<5.0	<5.0	<5.0	<5.0	<5.0	<5.0
As	<1.0		<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
Ba	110		470	<5.0	130	14	640	67
Cd	<5.0		<5.0	<5.0	<5.0	<5.0	24	<5.0
Cr	15		12	<5.0	7.5	<5.0	7.0	8.2
Hg	0.42		<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Pb	<1.0		16	8.8	14	<1.0	20	13
Ni	23		20	11	12.8	<5.0	28	18
Se	<0.4		<0.4	<0.4	0.5	<0.4	<0.4	<0.4
Zn	29		200	10	64	32	130	30
Explosives (ug/l) ^d	ND		ND		ND		ND	ND
OCs (ug/l)								
ethylene Chloride	<250	18B	<480		5,900		120B: <2,800	<13
acetone	810	<10	<960		<1,000		<10: NA	<25
2-Dichloroethene (total)	<250	<5	<480		<500		<5: NA	16
2-Dichloroethane	<250	<5	<480		<500		<5: <2,800	52
trichloroethene	7,600	10B	13,000		11,000		61: ND	770B
tetrachloroethene	<250	<5	<480		<1,000		<5: <4,100	<13
Remarks	Milky white color				Slightly cloudy.			

^a footnotes, see last page of Table 13.

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TABLE 13. SUMMARY OF ANALYTICAL RESULTS FOR WATER SAMPLES^a (cont'd)

Well No. (Sample No.)	MW-12 (8-1483)	MW-13 (8-1466)	MW-14 (8-1482)	MW-15 (8-1394)	C-2 (8-1459)	Travel Blank (8-1460)	C-3 (8-1461)	Equip Blank (8-1462)
pH	1 5.7 2 _b 3 6	7.3 7.3 6.7	6.1 6.1 6.5 - 7.0 ^b	6.3 6.3 6.4	6.1 6.1 6.3		6.1 6.2 6.2	
Conductivity (umhos/cm)	1 1172 2 1173 3 1163	860 859 860	-C -C 1796	644 629 694	758 755 734		1068 1055 1052	
Temperature (°C)	1 22.5 2 23.5 3 22	23.5 22.5 19	23.5 24 19	25 22 20	19 19 18		20 20 22	
Chloride (mg/l)	260	240	660:1020.0	120	170		310	
TOX (mg/l)	1.7	0.12	3.6	185.0	0.03		0.24	
Nitrates (mg/l)	2.0	2.4:2.0	<0.2	<0.2	<0.2		2.3	
Total Metals (ug/l)								
Ag	<5.0:50	<5.0	<5.0	<5.0	<5.0	<5.0	<5.0	
As	<1.0:2	<1.0	<1.0	4.3	3.0	<1.0	8.8	
Ba	560:1200	280	1300	280	540	<5.0	730	
Cd	24:10	9.0	20	15	29	<5.0	24	
Cr	9.2:60	6.5	7.5	8.0	7.8	5.0	8.0	
Hg	<0.1:2	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	
Pb	20:220	13	23	28	70	<1.0	28	
Ni	18:90	6.5	16	20	5.8	<5.0	7.8	
Se	<0.4:2	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	
Zn	120:100	18	110	220	260	9.0	94	
Explosives (ug/l) ^d	ND	ND	ND	ND:ND	ND		ND	
OCs (ug/l)								
ethylene Chloride	<40	<5	<10	58	33		<5	10
acetone	<81	<10	<21	<25	<10		<10	<10
2-Dichloroethene (total)	57	<5	<10	<13	<5		<5	<5
1,2-Dichloroethane	<40	<5	<10	<13	<5		<5	<5
trichloroethene	1100	13	250	23	17		<5	<5
tetrachloroethene	<40	<5	<10	<13	<5		<5	<5
Remarks			Slight odor. Reddish brown color.	Very faint odor. Slightly cloudy yellowish color.	Salty odor. Very dirty.		Dingy gray color.	002028

^a Footnotes, see last page of Table 13.

TABLE 13. SUMMARY OF ANALYTICAL RESULTS FOR WATER SAMPLES^a (cont'd)

Well No. (Sample No.)	C-4 (8-1463)	C-5 (8-1464)	109 (8-1420)	120 (8-1479)	123 (8-1421)	124 (8-1422)	125 (8-1423)	Travel Blank (8-1424)	129 (8-1425)
pH	1 5.9 2 5.9 3 6.0	6.5 6.5 6.7	6.6 6.7 6.7	-b -b 6b	7.1 7.4 6-7b	5.7 5.7 5-5.5b	5.9 5.9 6.1		5.8 5.8 6.0
Conductivity (umhos/cm)	1 212 2 209 3 202	386 383 374	3280 2850 2850	5890 6000 6300	3350 3470 3500	62 64 66	132 110 115		986 1006 1051
Temperature (°C)	1 18.5 2 18.5 3 19	19 18.5 19	23 22.5 22.5	26 24.5 27	24 24 22	21.5 23.0 20	21 22 17		21.5 21 21
Chloride (mg/l)	41	64	760	720	3.9:13.8	5.9	19		21
TOX (mg/l)	0.05	0.03:0.005	12.7	20:1.0	0.02	0.04	2.0		290
Nitrates (mg/l)	<0.2	<0.2	0.26	590:735.0	6.3	<0.2	0.28		15.3
Total Metals (ug/l)									14
Ag	<5.0	<5.0	<5.0:50	<5.0	<5.0	<5.0	<5.0		<5.0
As	2.5	1.6	<1.0:2	4.7	<1.0	1.1	<1.0		<1.0
Ba	280	340	1500:2700	580	250	590	420	ND	680
Cd	<5.0	<5.0	<5.0:10	5.5	<5.0	<5.0	<5.0		<5.0
Cr	6.8	5.8	6.2:120	11	6.2	5.5	8.2		7.5
Hg	<0.1	<0.1	<0.1:2	<0.1	<0.1	<0.1	<0.1		<0.1
Pb	20	21	18:100	34	12	47	20		31
Ni	8.5	5.8	5.2:50	100	5.9	10	<5.0		21
Se	<0.4	<0.4	<0.4:2	0.5	2.6	0.4	<0.4		<0.4
Zn	92	29	22:40	150	10	46	21		46
Explosives (ug/l)	ND	ND	ND	ND	ND	ND	ND		ND
Diethyl Chloride	<5:2,800	110	9B	310,000	<5	<5	<50	2BJ	<33
etone	<10: NA	<10	<13	<25,000	<10	<10	<100	<13	<67
2-Dichloroethene (total)	<5: NA	<5	11	<13,000	<5	<5	<50	<7	4J
2-Dichloroethane	<5:2,800	<5	<6	<13,000	<5	<5	<50	<7	35
1-chloroethene	9:1,900	77	190	32,000	<5	80	<50	<7	930
trachloroethene	50:4,100	<5	<6	<13,000	<5	<5	<50	<7	4J
marks	Milky white color		Milky yellow color silty	Strong odor like oil or gas	Cloudy	Very silty	Very cloudy silty Yellow/red color		Slight odor Very silty

^aCompiled from field data in Appendices W and X, and from laboratory data in Appendix Z.

meter broken. Paper used if available.

ductivity meter broken.

Explosive cpds analyzed and respective calibration limits were HMX (26.0 ug/l),
DX (22.0 ug/l), tetryl (26.0 ug/l), TNT (14.0 ug/l), and 2, 4 DNT (10.0 ug/l).

ND = Not detected or detected below calibration limits

< = Not detected below calibration limits

E = Concentration exceeded calibration limits

B = Possible laboratory blank contamination

J = Estimated concentration below calibration limits

NA = No analysis

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conductivity, and temperature reading recorded are the average of four measurements that were made. Also included are the field notes made pertaining to color, odor, and siltation. Duplicate results follow the colon.

5.8.1 Field Parameters. The field parameters pH, conductivity, and temperature did not vary much from the beginning to the end of sampling, indicating that representative formation water was being sampled. The pH of most of the water samples was on the acidic side of 7.0, averaging around 6.1 and ranging from 4.3 in MW-11 to 7.3 in MW-13. Conductivity values were typically around 2,000 umhos/cm, but ranged from 64 umhos/cm (possible equipment problem) in well 124 up to 6,000 umhos/cm in well MW-9. Temperatures were typically around 20°C, but ranged from 18.5°C in well C-4 up to 26°C in wells 120 and MW-11. These parameters remained essentially unchanged when measured a third time during sample preservations in the laboratory on-site, indicating the chemistry of the water samples was fairly stable. The decrease in temperature for the third set of readings was due to the samples being on ice prior to preservation.

5.8.2 Chlorides. Chlorides exceeded the maximum allowable concentration limit of 300 mg/l specified in the Texas Department Health (TDH) Drinking Water Standards in 11 of the wells sampled. Six of these wells, MW-1 through MW-6, are located around the closed UEP, with two more wells, 109 and C-3 located downgradient of the UEP. The other three wells, 120, MW-10, and MW-14, are located

downgradient of the ACD. Wells 120 and MW-14 are a cluster well that showed chlorides increasing from 720 mg/l in the shallow well to 1,020 mg/l in the deeper. Chloride concentrations associated with the UEP ranged from 310 mg/l in C-3 downgradient of the pond up to 980 mg/l in MW-6 at the Point of Compliance. Chloride concentrations in other wells sampled were as low as 5.9 mg/l in well 124. Laboratory detection limits for chloride were 5.0 mg/l.

5.8.3 Total Organic Halogens (TOX). For the most part, TOX concentrations were high in wells where high VOC concentrations were detected. The three wells having exceedingly high VOC concentrations were MW-1, MW-2, and well 120. These wells also showed high TOX concentrations of 4,030 mg/l, 3,644 mg/l, and 2,011 mg/l, respectively. The only anomalous TOX concentration noted was in well MW-6, which showed TOX at 2,747 mg/l, but VOC concentrations of only 91 ug/l TCE and 15 ug/l of 1,2-dichloroethene (total).

5.8.4 Nitrates. Nitrates exceeded the maximum allowable concentration of 10 mg/l specified by TDH Drinking Water Standards in only two wells. Well 120, at the ACD, showed an exceptionally high concentration of nitrates at 735 mg/l. The other well high in nitrates was well 129, which had 14 mg/l. All other wells ranged from below the detection limits shown on Table 13 up to 6.0 mg/l for nitrate concentrations.

5.8.5 Total Metals. The 10 metals analyzed in the water samples were silver (Ag), arsenic (As), barium (Ba), cadmium (Cd), chromium (Cr), mercury (Hg), lead (Pb), nickel (Ni), selenium (Se), and zinc

(Zn). Five metals were detected at concentrations equal to or exceeding the maximum allowable limits specified for drinking water by the TDH. These were Ba, Cd, Cr, Hg, and Pb.

5.8.5.1 Barium. Barium was found at concentrations exceeding the TDH limit of 1,000 ug/l in wells MW-1, MW-2, MW-3, MW-5, MW-6, MW-12, MW-14, and 109. The maximum concentration of Ba detected was 3,600 ug/l in MW-2. All wells except MW-12 and MW-14 are located around the UEP or downgradient of the pond. Well MW-14 is the deeper cluster well at the ACD. Well MW-12 is located north of the ACD. Duplicate analyses for Ba in MW-12 were 560 ug/l and 1200 ug/l. Detection limits for Ba were 5.0 and 1000 ug/l, respectively.

5.8.5.2 Cadmium. Cadmium exceeded TDH drinking water standards in seven of the wells sampled. The TDH specifies a maximum allowable concentration of 10 ug/l, which was exceeded in wells C-2, C-3, MW-4, MW-10, MW-12, MW-14, and MW-15. The highest concentration of Cd detected was 40 ug/l in a duplicate analysis for MW-4. The other duplicate was below the detection limit of 5.0 ug/l.

5.8.5.3 Chromium. Chromium exceeded the TDH limit of 50 ug/l in duplicate analyses for three of the wells sampled. Well MW-4 detected both 9.8 ug/l and 100 ug/l, MW-12 detected 9.2 ug/l and 60 ug/l, and 109 detected 6.2 ug/l and 120 ug/l.

5.8.5.4 Mercury. Mercury was detected at the maximum allowable limit for drinking water, 2.0 ug/l, in a duplicate analysis for MW-12. The other analysis was below the detection limit of 0.10 ug/l.

5.8.5.5 Lead. The drinking water standard for Pb was exceeded in only two of the wells sampled. Duplicate analyses for well MW-12 showed Pb concentrations of 20 ug/l and 220 ug/l. Well C-2 detected Pb at 70 ug/l. The maximum allowable concentration for Pb in drinking water is 50 ug/l. Detection limits for Pb were 10 ug/l.

5.8.6 Explosives. Specific explosives analyzed for were HMX, RDX, tetryl, TNT, and 2,4 DNT. No explosives were detected above detection limits in any of the water samples analyzed. Detection limits for each explosive are shown on Table 13.

5.8.7 Volatile Organic Compounds. As shown on Table 13, the only VOCs detected were trichloroethene (TCE), methylene chloride, 1,2-dichloroethene (total), 1,2-dichloroethane, acetone, and tetrachloroethane.

5.8.7.1 TCE. By far, the most prevalent VOC detected was TCE, which was found in 20 of the 25 wells sampled. The five wells showing no TCE were MW-13, MW-15, C-3, 123, and 125. Concentrations detected for TCE in the other 20 wells ranged from 9 ug/l in C-4 up to 1,400,000 ug/l in MW-2. Well MW-14 was the only deep cluster well showing TCE contamination, which was at a concentration of 250 ug/l. Well 120, the shallow well clustered with MW-14, showed a concentration of 32,000 ug/l of TCE. Detection limits for TCE are shown on Table 13.

5.8.7.2 Methylene Chloride. Although not as prevalent as TCE, methylene chloride showed the highest VOC concentrations. These concentrations exceeded 17,000,000 ug/l in MW-2 and exceeded 4,200,000

ug/l in MW-1. Well 120 had the third highest concentration of 310,000 ug/l, which is consistent with LHAAP's past quarterly monitoring results. Other wells detecting methylene chloride were MW-9, MW-15, and C-5, at concentrations of 5,900 ug/l, 58 ug/l, and 110 ug/l, respectively. Well MW-15 is the deep cluster well next to MW-2. Detection limits for methylene chloride are shown on Table 13.

5.8.7.3 Other VOCs. The compound 1-2 dichloroethene (total) was detected at low concentrations ranging from 11 ug/l up to 120 ug/l in seven wells, five of which are located around and downgradient of the closed UEP (MW-3, MW-4, MW-5, MW-6, and 109) and two are located downgradient and north of the ACD (MW-12 and MW-11). The compound 1,2-dichloroethane was also detected at very low concentrations of 35 ug/l and 52 ug/l in the two wells 129 and MW-11, respectively. Acetone was detected at 810 ug/l in well MW-7, and tetrachloroethane was found at 50 ug/l in well C-4. Detection limits for each of these compounds are shown on Table 13.

6.0 HYDROGEOLOGICAL CONDITIONS.

6.1 Ground-Water Flow Direction. Ground water in the ABG area occurs under unconfined conditions. Depth to ground water varies approximately 2 feet over a 6-month period, from a high elevation of 176.0 recorded in April 1988 (Sheet 19), to a high elevation of 174.30 recorded in August 1988 (Sheet 20). Because recharge of the Wilcox is primarily by infiltration from the surface, these variations in ground-water elevation are most likely due to seasonal fluctuations in rainfall.

Although ground-water elevations vary seasonally, the configuration of the ground-water surface varies little. The ground water is mounded under the southern quadrant of the ABG in an elongated configuration extending from well 102 northward towards the middle of the site. Mounding most likely reflects the ABG as a topographic high (Figure 8), as well as being a potential recharge area due to the lack of vegetation. Ground-water flow is in all directions off this mounded high, as shown on Sheets 19 and 20, with flow directions in the vicinities of the ACD, the old burn trench areas east of the ACD, and the UEP being distorted due to construction activities that have disturbed the natural regime. An inexplicable low occurs in the area of MW-2 that possibly reflects a past activity not yet accounted for.

Regional ground-water flow across the ABG area is towards Harrison Bayou, to the west and north, and towards Caddo Lake, to the northeast. Extrapolation of the scant water level data available in wells far from the ABG can close the lower ground-water elevation contours around

the ABG to show these regional trends.

The direction of flow across the source areas in the ABG differ, reflecting their location with respect to the ground-water mound underlying the site. Flow across the buried trenches in the western corner of the site is roughly perpendicular to the 100-year floodplain contour, flowing northwest towards Harrison Bayou. Based on this direction of flow, wells 120, MW-14, MW-12, MW-10, C-2, and MW-13 are located directly downgradient from this source, as shown on Sheet 20. Seasonal variation of ground-water elevations would also place wells MW-9 and MW-11 in the downgradient direction (Sheet 19). Direction of ground-water flow below the line of old burn pits in the center of the old burn trench areas cannot be determined from the April 1988 water level data, but appears to be west towards MW-11 based on the August 1988 data (Sheet 20). Flow direction beneath the UEP, however, is not as straightforward. Ground water flows generally to the north and northeast, but distorted ground-water contours in the vicinity of MW-2 show ground water flowing towards this location within a 400-foot diameter area, encompassing the suspected trench area south of the closed pond (Sheet 20). This low on the April 1988 data is shown centered around well BH-11 (Sheet 19).

6.2 Ground-Water Gradient. The horizontal hydraulic gradient for ground-water beneath the ABG is extremely low. A representative gradient of .0048 was determined for ground-water flow perpendicular

to the least disturbed ground-water contours around the ABG as they are depicted on Sheet 20. Regional gradient, most likely represented by the ground-water contours shown northeast of the site on Sheet 20, is even less, computing to roughly .0025. The less complete April 1988 water level data shown on Sheet 19 yield similar gradients of .0050 and .0018 for the ABG and the regional flow, respectively.

The vertical hydraulic gradient for the site cannot be determined from the data developed from these Phase I investigations. Water level data recorded for the three sets of cluster wells - MW-2 and MW-15, 120 and MW-14, and C-2 and MW-13 - are inconclusive. The water levels recorded for wells MW-2 and MW-15 on 31 August 1988 show a difference in head of 0.42 foot, with MW-15 having the higher head. However, this was 1 day after the installation of MW-15, and it is likely that the well had not yet stabilized from development. Water levels recorded on 18 September 1988 during the slug testing and sampling of MW-2 and MW-15 probably better reflect the stable conditions of the wells, with MW-15 having 2.91 feet of head less than C-2. The same conditions could apply to wells 120 and MW-14. Well MW-14 was installed on 10 August 1988. Water levels recorded on 31 August 1988 showed 1.24 feet of head difference between the two wells, with the greater head in well 120. When measured during sampling almost 1 month later, the two wells differed by 0.15 foot in head, with MW-14 being greater. Well MW-13 was not yet installed when water levels were measured on 31 August 1988, and was therefore newly installed

at the time of sampling on 25 September 1988 when the head difference between it and well C-2 was only 0.3 foot.

Concentrations of contaminants detected in water samples from the deeper wells MW-13, MW-14, and MW-15 showed some VOCs present in MW-14 and MW-15, but at very small concentrations relative to those detected in each of their adjacent shallower wells, 120 and MW-2, as shown on Table 13. This indicates that the confining clay separating the two saturated zones in these wells is either a low permeability clay under high vertical hydraulic gradient conditions, or it is a higher permeability clay under low vertical hydraulic gradient conditions. Laboratory classifications made on the confining bed materials sampled from the three deeper well borings classified them as lean sandy silty clay and clayey sand, which would lend support to a low vertical hydraulic gradient. Lower confining bed materials sampled in the shallow well borings around the UEP were classified as either lean clay or clay shale. Lower confining bed materials sampled in well borings MW-7 through MW-9, situated on the outcrop of the Wilcox, all tested as clay shale, with wells MW-7 and MW-9 screened in this material. Lower confining bed materials were not encountered in well borings MW-10, MW-11, and MW-12, situated in the floodplain. Samples analyzed from the bottom of each of these well borings showed a silty sand. Complete laboratory analyses for Atterberg limits, moisture content, and grain size analyses performed on selected samples from well borings MW-1 through MW-15 are contained in Appendix AA.

6.3 Hydraulic Conductivity. Horizontal hydraulic conductivity (K)

values for screened materials in wells MW-1 through MW-15 were calculated from the September 1988 slug test data using Hvorslev's time lag method for calculating soil permeability, described in USACE Waterways Experiment Station Bulletin No. 36, "Time Lag and Soil Permeability in Ground-Water Observations." The two equations used to arrive at a K value for each well were the shape factor (F) equation for a well screen extended in uniform soil conditions, and the basic time lag (T) equation. Both equations are shown on Figure 31. To determine the T value for computing K, the slug test data were plotted on a semi-logarithmic time versus drawdown plot, with time plotted along the arithmetic axis and drawdown plotted as the ratio of head to initial head (H/H_0) along the logarithmic axis. The T value was then picked where the $\ln H/H_0 = 0.37$ when the slope of the data points passed through $\ln H/H_0 = 1$. Data plots and K computations for each well are contained in Appendix BB.

The K values calculated for each well are shown on Table 14. Hydraulic conductivities for the 12 shallow wells tested ranged from 1.58×10^{-5} cm/sec in MW-9 up to 3.00×10^{-4} cm/sec in MW-4. The median K value for these wells was 5.45×10^{-5} cm/sec, calculated for MW-6. Because there appears to be no correlation between the K values listed for these 12 wells and the location or types of screened materials, the median K value of 5.45×10^{-5} cm/sec is selected to best characterize the hydraulic conductivity of the shallower screened

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19 Oct 84

COMPUTATION SHEET

(SWFED SOP)

BY	DATE	PROJECT LHAP-6WQA Phase I	SHEET ____ OF ____
CHKD BY	DATE	FEATURE	
DETAILS			

EQUATIONS AND DATA USED TO DETERMINE K AND \bar{V} VALUES FROM SLUG TEST DATA:

Shape Factor Equation¹:

$$F = \frac{2\pi L}{\ln \left[\frac{L}{D} + \sqrt{1 + \left(\frac{L}{D} \right)^2} \right]}$$

where F = shape factor, cm
 L = length of intake (screen), cm
 D = diameter of intake (screen), cm

If $L/D > 4$, use simplified formula:

$$F = \frac{2\pi L}{\ln \left(\frac{2L}{D} \right)}$$

$L = 5\text{ft} \times 30.48\text{cm/ft} = 152.40\text{cm}$
 $D = 4\text{in} \times 2.54\text{cm/in} = 10.16\text{cm}$

Basic Time Lag Equation²:

$$T = \frac{A}{FK} \Rightarrow K = \frac{A}{FT}$$

where K = hydraulic conductivity, cm/sec
 A = cross-sectional area of standpipe, cm^2
 F = shape factor, cm
 T = time lag, sec, where $\ln H/H_0 = 0.37$

$$A = \pi R^2 = (3.14)(5.08\text{cm})^2 = 81.03\text{cm}^2$$

Average Velocity Equation³:

$$\bar{V} = \frac{K dh/dl}{\Theta}$$

where \bar{V} = average velocity, cm/sec
 K = hydraulic conductivity, cm/sec
 dh/dl = hydraulic gradient
 Θ = effective porosity

$$dh/dl = 0.0048$$

$$\Theta = 0.20^4$$

¹ Hvorslev, M. Juul, "Time Lag and Soil Permeability in Ground-water Observations," Corps of Engineers, U.S. Army, Waterways Experiment Station, Vicksburg, Mississippi, Bulletin No. 36, April 1951, p. 31, case (B).

² ibid, p. 10, equation (3).

³ Lohman, S.W., "Ground-water Hydraulics," U.S. Geological Survey, Geological Survey Professional Paper 708, 1979, p. 10, equation (28).

⁴ Hantush, D., and Sunada, D.K., "Ground-water Hydrology and Hydraulics," 1977, p. 31.

Figure 31. Equations Used to Determine Hydraulic Conductivity and Average Velocity Values from Slug Test Data.

TABLE 14. HYDRAULIC CONDUCTIVITY (K) VALUES
COMPUTED FROM SLUG TEST DATA

<u>Well No.</u>	<u>K (cm/sec)</u>
MW-1	2.18×10^{-4}
MW-2	5.21×10^{-5}
MW-3	1.91×10^{-4}
MW-4	3.00×10^{-4}
MW-5	1.69×10^{-4}
MW-6	5.45×10^{-5}
MW-7	2.39×10^{-5}
MW-8	2.99×10^{-5}
MW-9	1.58×10^{-5}
MW-10	5.71×10^{-5}
MW-11	1.51×10^{-4}
MW-12	2.58×10^{-5}
MW-13	3.31×10^{-4}
MW-14	4.80×10^{-4}
MW-15	2.40×10^{-3}

NOTE: Slug test calculations are contained
in Appendix Z.

materials at the ABG.

The K values for the three deeper wells, which were screened in sandier materials, were higher, ranging from 3.31×10^{-4} cm/sec in MW-13 up to 2.40×10^{-3} cm/sec in MW-15, with the median, and therefore representative, K values for these deeper screened materials being 4.80×10^{-4} cm/sec, calculated for MW-14. The K values for each well that was slug tested are shown on the subsurface profiles on Sheets 23 through 27.

6.4 Average Velocity. The average horizontal velocity for the ground water monitored by wells MW-1 through MW-12 at the ABG is 1.31×10^{-6} cm/sec. This velocity was calculated using Lohman's average velocity (V) equation, shown on Figure 31, taken from the Geological Survey Professional Paper 708, "Ground-Water Hydraulics." The median K value of 5.45×10^{-5} cm/sec, as it was determined from the slug test data recorded for these wells, and the hydraulic gradient of .0048, as it was determined from the August 1988 water level data, were used in the equation. An effective porosity of 0.20 was selected from McWhorter and Sunada in "Ground-Water Hydrology and Hydraulics" as best reflecting the silty nature of the screened materials in the 12 shallow wells. It is important to note that this average velocity is, at best, only a rough estimate for characterizing the shallow saturated zone because of the heterogeneity of the materials screened for which the slug tests were performed.

Average horizontal velocities for the deeper screened intervals

in wells MW-13, MW-14, and MW-15 were not calculated because there is not yet enough data to determine a hydraulic gradient for this deeper saturated zone.

6.5 Contaminant Plume. Sheet 29 shows the extent of TCE contamination in the ground water as it was detected in the 22 shallow wells sampled in September 1988. The concentrations of TCE are contoured to define the contaminant plume underlying the ABG area. Trichloroethene was selected as the parameter to best present plume definition because it was detected in the most number of wells sampled.

Although there are at least two sources contributing to ground-water contamination at the ABG, the contoured concentrations of TCE define a single plume with two separate "highs," each associated with a contaminant source. The highest concentrations of TCE are centered around well MW-2 just southeast of the UEP. The other high TCE concentration contour defines a "ridge" beginning at well 120 and running south past wells MW-9 and MW-8, paralleling the 100-year floodplain contour of Harrison Bayou west of the ABG. There are no highs centered over the old line of burn pits, a potential third source identified from the contaminant source investigations.

The configuration of the contaminant plume shows that contaminants that have entered the ground water from past operation of the UEP and the buried trenches over the past 30 years have not moved far downgradient of these sources toward Harrison Bayou and Caddo Lake. The plume appears to be confined to within the ABG boundaries in the

northern corner of the site, but may extend further than 200 feet north of the western corner of the site, with high concentrations exceeding 10,000 ug/l of TCE occurring in well MW-8, approximately 250 feet west of the ABG boundary. This well and MW-7, which detected a similar high concentration of TCE, are not located downgradient of the trenches in the western corner of the ABG. Ground-water contours on Sheets 19 and 20 show them both to be situated downgradient of the southern corner of the ABG, which poses the question of whether a contaminant source is in this area. The only solid waste management activity documented for this area of the ABG is the washout pad and sump area, which have been in use for the entire life of the ABG. The southern extent of the contaminant plume has not yet been determined because wells in this area were not sampled during this phase of the RFI.

Although well C-5, located approximately 1,500 feet northeast of the UEP, showed concentrations of methylene chloride at 110 ug/l and TCE at 77 ug/l, there is little reason to suspect contamination from the ABG to extend this far away from the site. There is a possibility that an error in the decontamination procedures used for the portable bailer prior to sampling the well may have caused the contamination in the water sample, or that another source other than the ABG may be contaminating the well. It is also possible that well C-4 is not screened in the shallow contaminated zone, but instead is screened in the next deeper intermediate zone. However, based

on the data developed during this phase of the RFI, there is little reason to believe that this well is within the ABG contaminant plume.

The vertical extent of the contaminant plume cannot yet be determined. Samples from wells MW-14 and MW-15 showed that contamination extends vertically down to at least el. 130 at the two known contaminant source locations. The sample obtained from MW-13 showed no contamination, indicating this well to be outside any deeper contaminant plume.

6.6 Uppermost Aquifer. The base of the uppermost aquifer underlying the ABG is the base of the regional Cypress aquifer, which is represented as the contact between the overlying Wilcox and the underlying Midway Groups. As shown for the ABG area on Figure 7, this contact occurs at roughly el. 50 and dips to the northwest at about 20 feet per mile. Evidence obtained from the drill cuttings and downhole geophysical logs for the deep stratigraphic test borings drilled at the site suggest this contact occurs anywhere from approximate el. 87 at boring location 3F-925 on the eastern side of the site down to approximate el. 25 at the boring location 3F-924 on the western side of the site, as depicted on Sheets 23 through 27.

Attempts were made during Phase I investigations to define a confining bed in this area that was continuous across the site. It appears that one does not exist. Although well borings did encounter lower permeability materials at the depths anticipated, these materials cannot be conclusively correlated across the entire ABG area to define

a shallower uppermost aquifer.

The best correlation of a single confining bed is shown on profile E-E' (Sheet 24), drawn across the entire site along the strike of the Wilcox strata. This upper confining bed identified in test borings 3F-922 and 3F-925, and identified in most of the well borings around the UEP, appears to be continuous for the length of the profile, except at the eastern end where it appears to be pinching out in the direction of well location C-3. This bed is most likely confining the contaminant plume to the screened shallow strata around the UEP. However, as shown by the water sample analyzed from the deeper well MW-15, the bed is not impermeable, and contamination has reached the underlying zone.

The remainder of the vertical section portrayed by profile E-E' illustrates the lenticular and discontinuous nature of the interbedded sandy, silty, clayey strata of the Wilcox Group. The second confining bed identified in test borings 3F-922 and 3F-925 appears to pinch out east of 3F-925, which indicates that the second and third deeper permeable zones identified in 3F-922 are actually a single unit separated by a clay lens at that boring location.

If the confining bed shown on Profile E-E' is indeed continuous for the Wilcox, which comprises most of the ABG site, it loses its continuity at the edge of the Harrison Bayou floodplain as depicted on profiles D-D', F-F', G-G', and H-H' (Sheets 23, 25, 26, and 27). A clear contact between alluvium and Wilcox materials cannot be drawn

because the depositional nature of the two are so similar. There is definitely more sand in the shallow alluvial materials sampled, but where these sandy alluvial materials end and the sandy Wilcox materials begin is impossible to tell on the sections. Actually, whether this contact can be determined or not is not so important as the fact that the strata of the entire ABG area, whether alluvial or Wilcox in nature, appear to be hydraulically connected horizontally into the floodplain of the Harrison Bayou and vertically down to the base of the Cypress aquifer, with perhaps locally confining conditions occurring around the UEP only.

6.7 Potential Contaminant Migration Pathways. The potential contaminant migration pathways for each of the contaminant sources identified by this phase of the RFI are discussed below.

6.7.1 UEP. Ground-water contamination at the UEP has not moved significantly in the past 30 years. The source contributing to the contamination was removed in 1986. However, the plume is still present. The reason it has not moved significantly appears to be the very low hydraulic gradient across the site and the relatively low hydraulic conductivity of the uppermost saturated materials. Although confined locally beneath the ABG by a relatively low permeability clay stratum of the Wilcox, contamination has reached the next lower permeable stratum which may, depending on its hydraulic characteristics, be more conducive to carrying the contaminants away from the site into Harrison Bayou and/or Caddo Lake. The relationship between the

structure of the closed UEP and wells MW-2, MW-6, and MW-15 is shown on Sheet 30.

6.7.2 Buried Trenches. The source materials contributing to the contaminant plume emanating from the western corner of the ABG still remain in some places around the foundation of the ACD, as shown on Figure 16. These source materials lie in the water table, as shown on Sheet 18, and are actively contributing to the ground-water contamination. The primary route of contaminant migration appears to be along the direction of ground-water flow in this area, as evidenced by the ground-water contours, shown on Sheets 19 and 20, and the configuration of the contaminant "ridge," shown on Sheet 29. Movement of contaminants does not seem to be affected by the change from Wilcox to alluvial materials primarily because the materials are very much alike both physically and hydraulically, as shown by the laboratory and slug test data. What poses some concern is that wells MW-7, MW-8, and MW-9, which are screened in lower K materials, are showing high contaminant concentrations. As in the UEP area, the deeper well MW-14, located adjacent to the source, indicated that contamination has migrated downward into a lower permeability stratum which may hydraulically be more conducive to carrying contaminants more quickly towards Harrison Bayou.

6.7.3 18 Burn Pits. It cannot be determined at this time whether the contamination resulting from past operation of these burn pits is contributing to the ground-water contamination at the ABG. It

appears that the elevation of the bottom of the pits, as indicated by the bottom of fill material encountered while drilling in this area, occurs approximately 15 feet above the water table. Therefore, contaminants must leach downward before ground-water contamination would occur. Well 124, on the fringe of any plume that may be emanating from the pits, showed a small amount (80 ug/l) of TCE, but this contamination could also be resulting from the UEP. Well 123, more directly downgradient from the pits, showed no contamination. However, wells MW-11 and MW-12, located further downgradient from this potential source, did show contamination, but because they are also located downgradient from the buried trenches, the source of the contaminants detected is inconclusive.

7.0 RECOMMENDATIONS FOR PHASE II TASKING.

7.1 Finish defining the horizontal extent of the contaminant plume by installing eight shallow monitoring wells, MW-16 through MW-23, at the locations shown on Sheet 31. Sample confining and screened materials for soil classification purposes.

7.2 Complete location C-4 as a three-well cluster at the suspected edge of the contaminant plume. Space wells 10 feet apart.

7.2.1 Install well C-4A as a deep well at the base of the uppermost aquifer at the Wilcox/Midway Contact, taking undisturbed samples every 5 feet for visual and laboratory classification. Geophysically log the boring prior to installing the well.

7.2.2 Install well C-4B as either a shallow or intermediate well, depending on the strata identified and correlation obtained from boring C-4A. At this time it is questionable whether C-4 is screened in the shallow contaminated zone or in the deeper intermediate zone, as shown on Sheet 25. Sample confining and screened materials for soil classification purposes.

7.3 Slug test all 10 new wells. Sample all 10 new wells and 8 existing wells C-1, C-5, C-6, C-7, C-8, 102, 126, and 130 to further define the contaminant plume and to site additional wells.

7.4 Measure water levels at least quarterly for a full year to determine seasonal variations in ground-water flow.

7.5 Designate or install at least one upgradient well for the purpose of monitoring elevated concentrations of metals in the ground water

at the ABG. At this time, C-7 looks to be a good upgradient location.

7.6 Sample Harrison Bayou for VOCs and metals downgradient of the ABG at the locations designated HB-1 through HB-5 on Sheet 31 to verify if contamination has reached surface waters.

7.7 Drill 12 shallow soil borings, 8A-974 through 8A-975, for the purpose of identifying any additional sources that are contributing to ground-water contamination at the ABG. Boring locations are shown on Figure 32. Boring 8A-974 is located at the suspected trench location shown on the 1963 aerial photos (Figures 10 and 11). Boring 8A-975 is located in an old suspected burn pit shown on the 1970 aerial photos (Figures 12 and 13) that is still visible in the field due to a change in vegetation. These two borings will be used to verify whether any contaminant sources have contributed to the ground-water contamination around the UEP. Location 8A-976 is located adjacent to the sump at the washout pad, and 8A-977 is located along the surface drainage leading away from the sump. These two locations will verify whether sump leakage or overflow may have contributed to the ground-water contamination in this area of the site. Location 8A-978 through 8A-982 are located at old trench and pit locations identified by USAEHA on Figure 14. Locations 8A-983 through 8A-985 are located at locations sampled during the Phase I RFI that showed high VOC concentrations down to depths of 10 feet. Borings should be sampled for chemical analysis down to the water table to verify whether soil contamination, if found, is contributing to ground-water contamination.

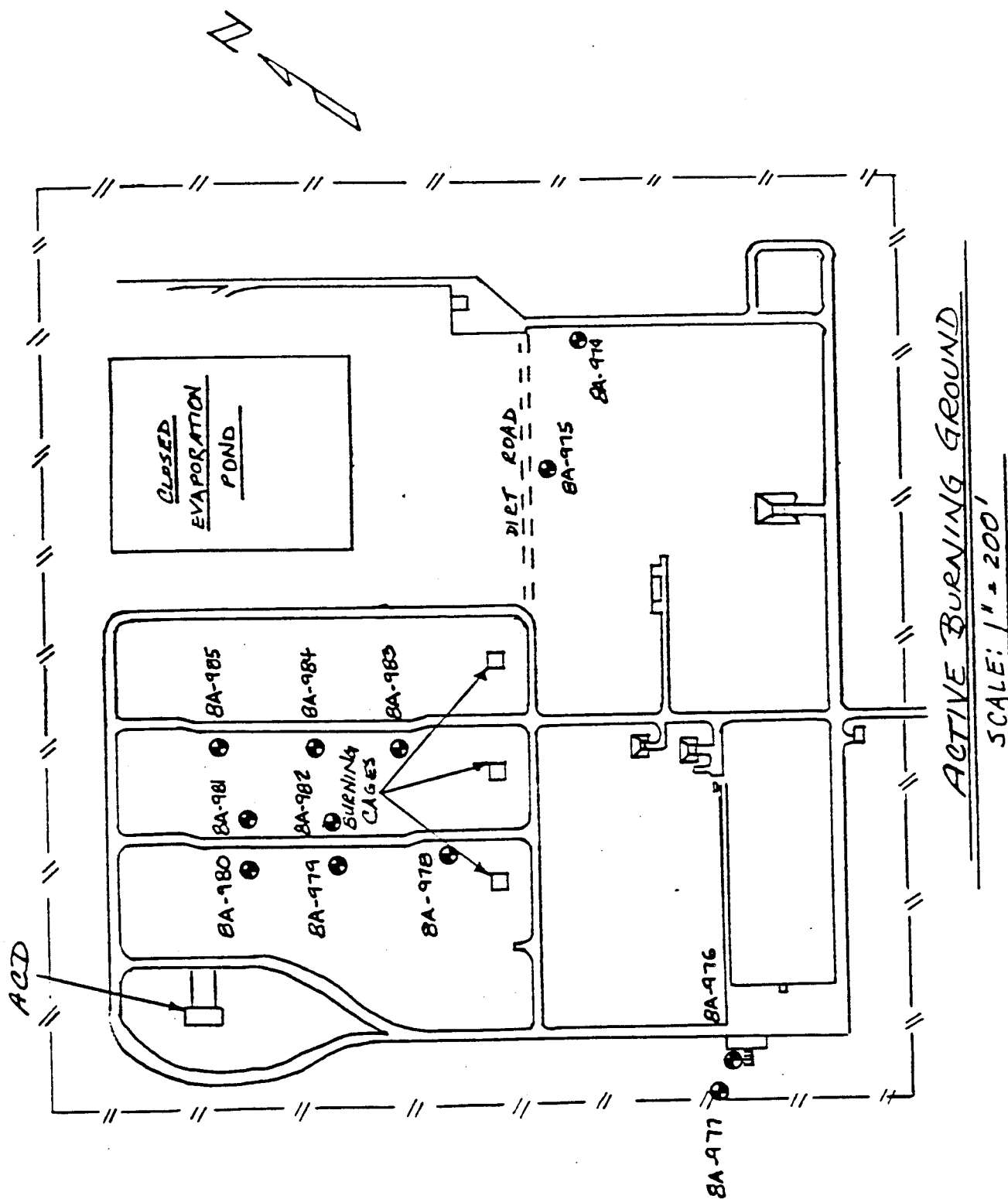


Figure 32. RFI Phase II Proposed Soil Boring Locations.

7.8 Consider plugging these wells for the following reasons:

- 101 - Water levels are heavily influenced by surface recharge down the well boring. Well is poorly constructed.
- 125 - Too shallow to monitor UEP contamination. Also poorly constructed with high silting during sampling.
- BH-3 - Replaced in 1987 by MW-4.
- BH-4 - Replaced in 1987 by MW-3.
- BH-11 - Replaced in 1987 by MW-2. Lack of construction details makes water quality data questionable.
- BH-22 - Lack of construction details makes water quality data questionable.

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RCRA FACILITY INVESTIGATION
-FOR-
ACTIVE BURNING GROUND
-AND-
UNLINED EVAPORATION POND
PHASE I

LONGHORN ARMY AMMUNITION PLANT
KARNACK, TEXAS

VOLUME 2
(SHEETS)

-PREPARED BY-
U.S. ARMY ENGINEER DISTRICT, FORT WORTH
CORPS OF ENGINEERS
FORT WORTH, TEXAS

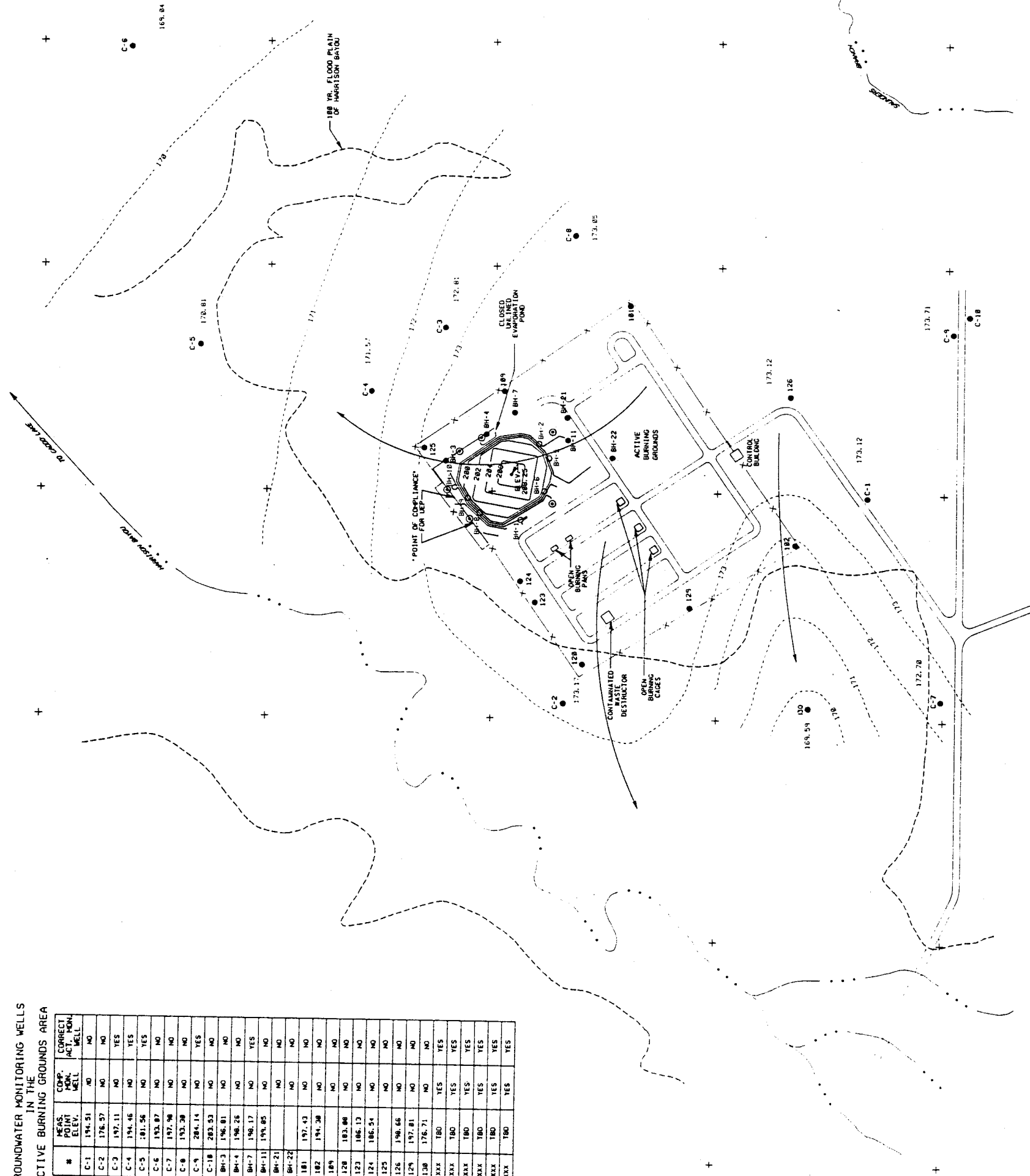
-PREPARED BY-
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FORT WORTH, TEXAS

JULY 1989

002058

GROUNDWATER MONITORING WELLS
ACTIVE BURNING GROUNDS AREA

#	MEAS. POINT ELEV.	COMP. MON. WELLS	CORRECT MON. WELLS
C-1	194.51	NO	NO
C-2	176.57	NO	NO
C-3	197.11	NO	YES
C-4	194.46	NO	YES
C-5	181.56	NO	YES
C-6	193.87	NO	NO
C-7	197.96	NO	NO
C-8	193.38	NO	NO
C-9	284.14	NO	YES
C-18	283.93	NO	NO
BH-3	196.81	NO	NO
BH-4	198.28	NO	NO
BH-7	190.17	NO	YES
BH-11	199.85	NO	NO
BH-21		NO	NO
BH-22		NO	NO
181	197.43	NO	NO
182	191.38	NO	NO
189		NO	NO
128	183.88	NO	NO
123	186.13	NO	NO
124	186.54	NO	NO
125		NO	NO
126	198.66	NO	NO
129	197.81	NO	NO
138	176.71	NO	NO
XXX T80		YES	YES
XXX T80		YES	YES
XXX T80		YES	YES
XXX T80		YES	YES
XXX T80		YES	YES
XXX T80		YES	YES



LEGEND

- EXISTING GROUNDWATER MONITORING WELL
- ABANDONED GROUNDWATER MONITORING WELL
- ⊙ PROPOSED LOCATION FOR ADDITIONAL COMPLIANCE MONITORING WELLS
- 173- GROUNDWATER SURFACE ELEVATIONS (2/8/84)
- GROUNDWATER FLOW DIRECTIONS
- BH-2 USAEHA WELL DESIGNATION
- IOB USTHAMA WELL DESIGNATION
- C-3 CIM WELL DESIGNATION
- MW-2 USAE WELL DESIGNATION

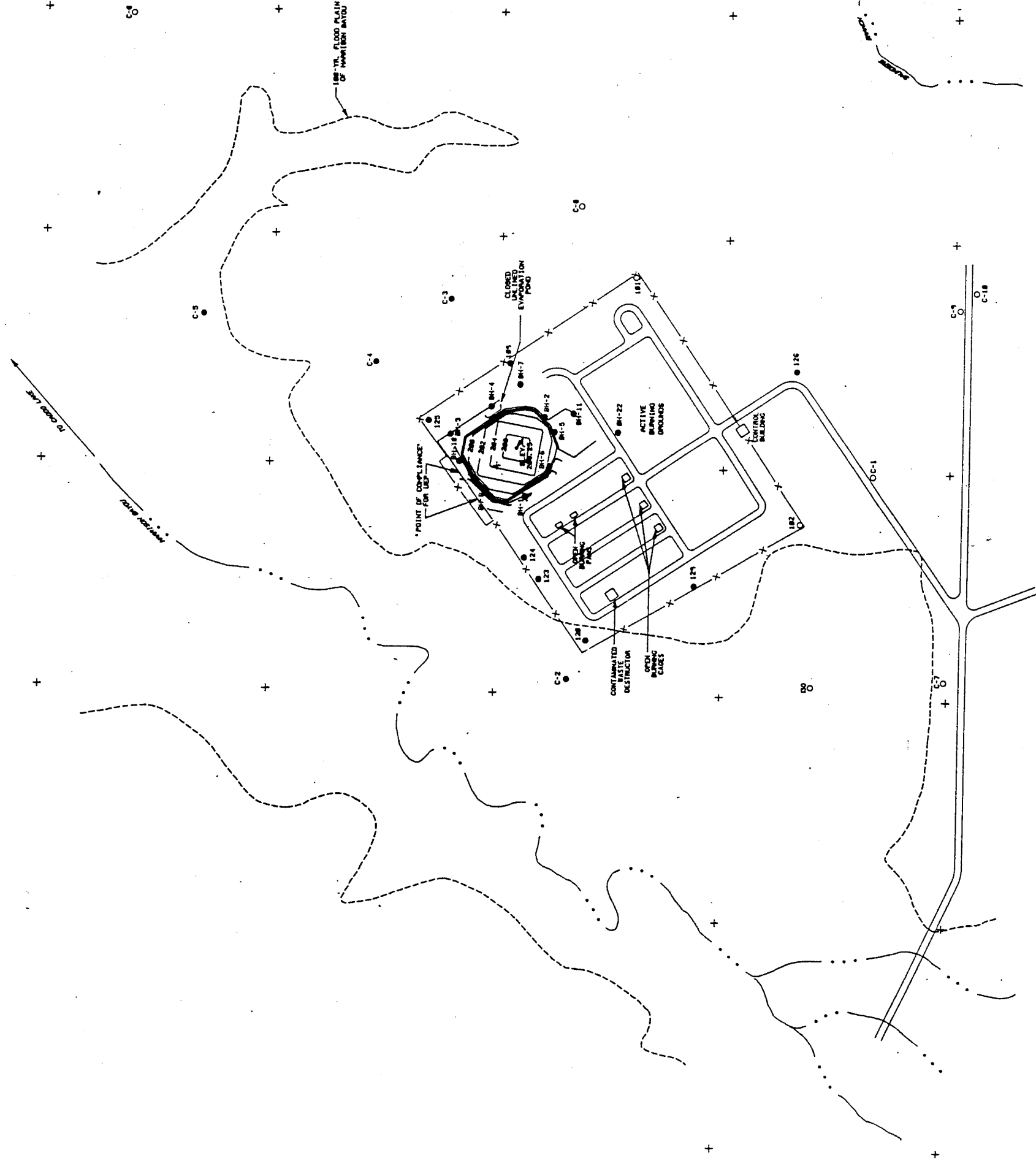
200 0 200 400
SCALE IN FEET

NOTE

1. MAP IS PLATE 2 FROM "US ARMY PROPOSAL FOR ADDITIONAL GROUNDWATER MONITORING AT UNLINED EVAPORATION POND(UWP), LONGHORN ARMY AMMUNITION PLANT, MARSHALL, TEXAS", PREPARED BY USAE HUNTSVILLE DIVISION, FEB 1987.

U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS	
RCRA FACILITY INVESTIGATION ASG AND UEP SITES PHASE I	
PIEZOMETRIC SURFACE MAP 18 FEBRUARY 1986	
DESIGNED BY: D. FITZGERALD	REVIEWED BY: R. BEHM
DRAWN BY: C. KIRBY	DATE: FEB 1986
CONTR. NO. 100-100-100	PLANNING NUMBER 100-100-100
SUBMITTED BY: ROBERT C. BEHM	
ENGINEER:	

000000

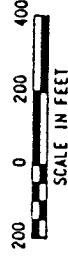


LEGEND

- O MONITORING WELL
 ● CONTAMINATED MONITORING WELL
 BH-4 USAEHA WELL DESIGNATION
 109 USATHAMA WELL DESIGNATION
 C-2 USACE (CDM) WELL DESIGNATION

NOTES

1. WELLS DESIGNATED AS CONTAMINATED ARE ALSO CONTAMINATED WITH METHYLENE CHLORIDE AND/OR TCE. SEE TABLES 1 AND 2.
2. BASE MAP FROM "U.S. ARMY PROPOSAL FOR ADDITIONAL GROUNDWATER MONITORING AT THE UNLINED EVAPORATION POND/UGRA LONGHORN ARMY AMMUNITION PLANT, MARSHALL TEXAS", PREPARED BY USACE, HUNTSVILLE DIVISION, FEB 1987.

[illegible]

DATE	TIME	BY	FIGURE NUMBER	U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS
LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I LOGS OF BORINGS FOUNDATION DESIGN ANALYSIS			NO. 10. CONTR. NO. DRAWING NUMBER	
DESIGNED BY: R. F. WILSON DRAWN BY: C. BEHM CHECKED BY: S. F. WILSON			SPECIFIED BY: ROBERT C. BEHM PROJECT:	
			SHEET NO. 3 OF 31	

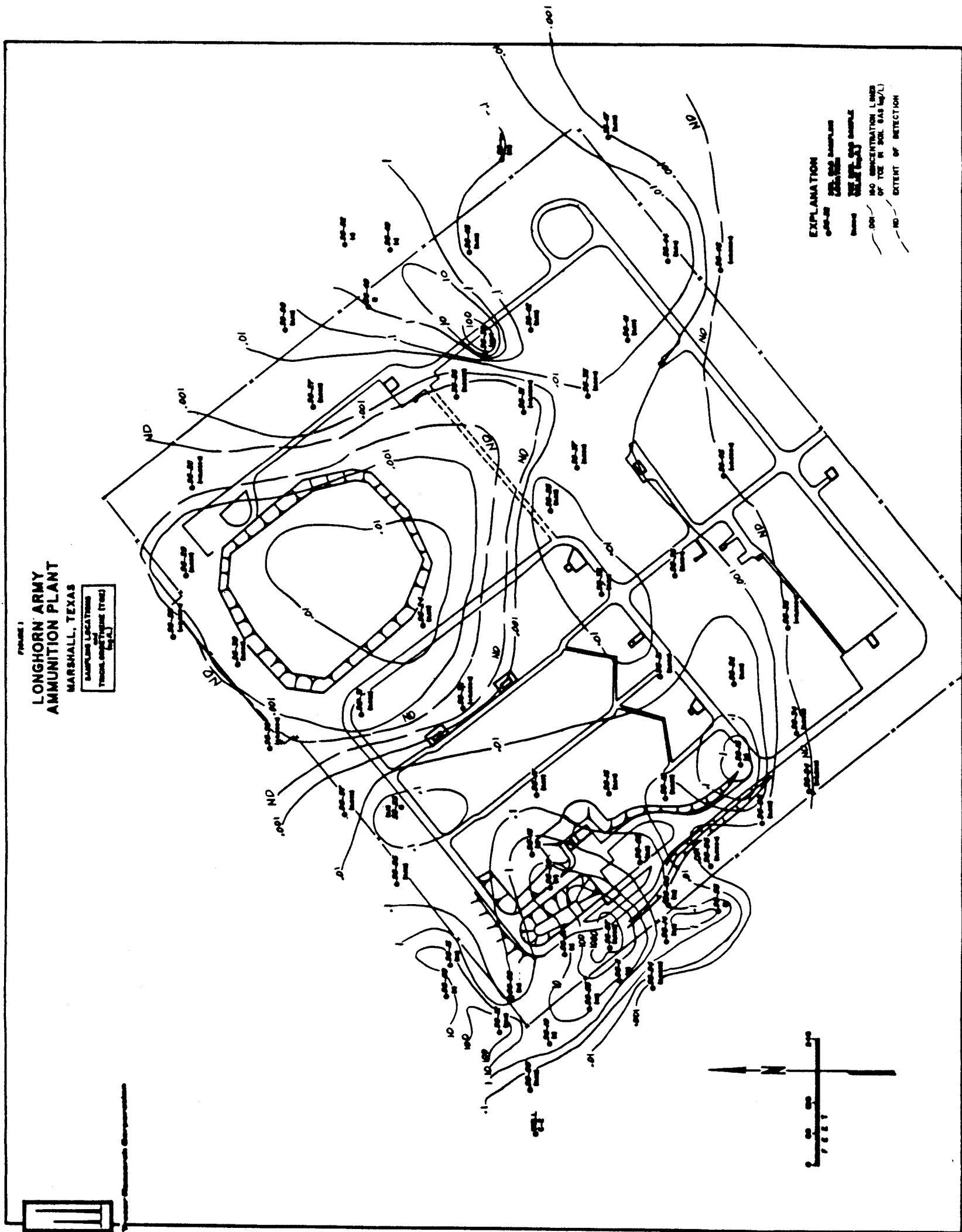
Year	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	1910	1911	1912	1913	1914	1915	1916	1917	1918	1919	1920	1921	1922	1923	1924	1925	1926	1927	1928	1929	1930	1931	1932	1933	1934	1935	1936	1937	1938	1939	1940	1941	1942	1943	1944	1945	1946	1947	1948	1949	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099
Year	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	1910	1911	1912	1913	1914	1915	1916	1917	1918	1919	1920	1921	1922	1923	1924	1925	1926	1927	1928	1929	1930	1931	1932	1933	1934	1935	1936	1937	1938	1939	1940	1941	1942	1943	1944	1945	1946	1947	1948	1949	1950	1951	1952	1953	1954	1955	1956	1957	1958	1959	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099

1. **Statement of Work:**
 2. **Project Objectives:**
 3. **Deliverables:**
 4. **Timeline:**
 5. **Budget:**
 6. **Risks:**
 7. **Stakeholders:**
 8. **Conclusion:**

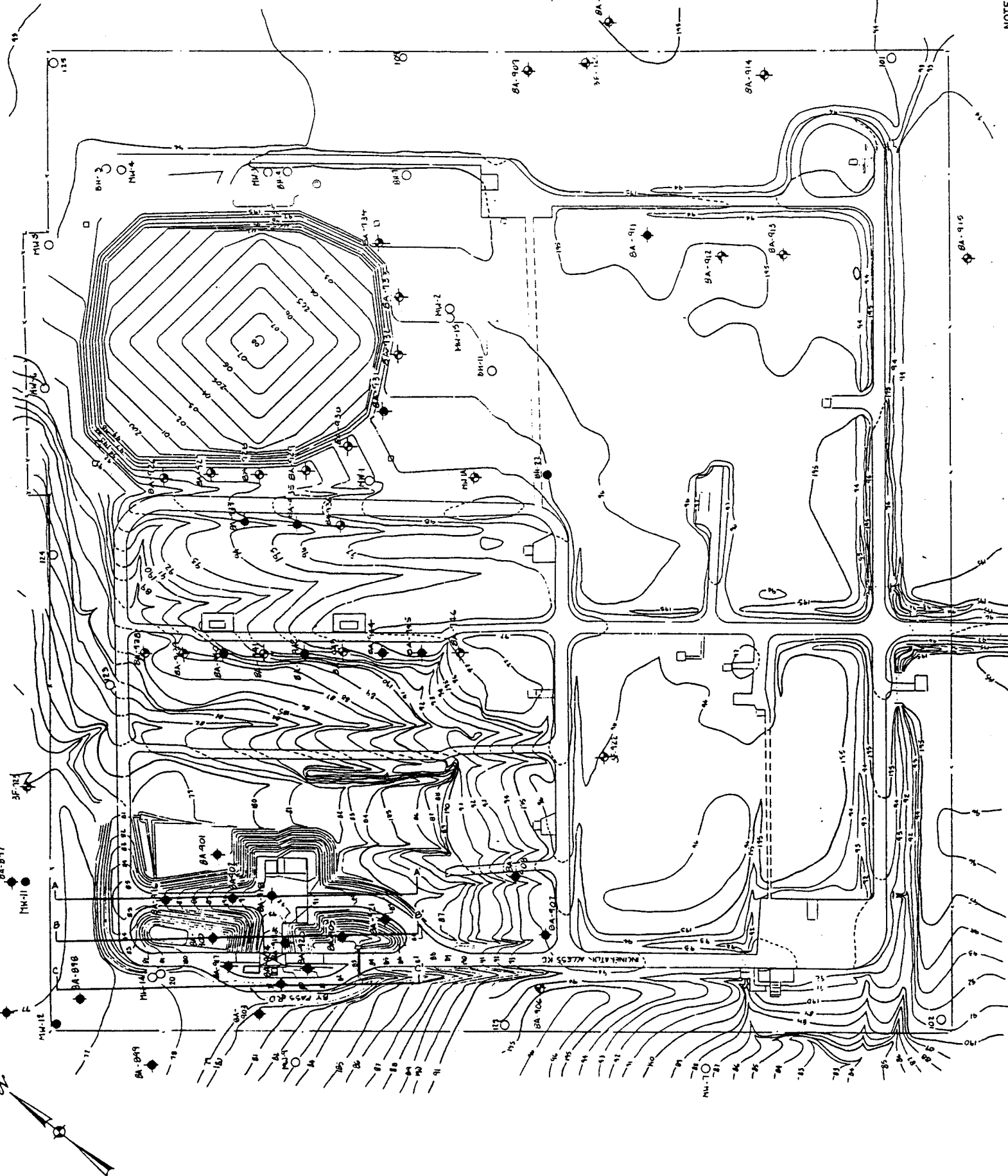
Reviewed by S. Sturte
Checked by H. Ruddy
Forwarded by L. Shepherd

NOTE

1. SOL GAS SURVEY PERFORMED BY TRACER RESEARCH CORPORATION, SEPT 1987. BASE MAP AND SAMPLING DATA FROM FINAL REPORT DATED OCT 1987, CONTAINED IN APPENDIX B.

[illegible]

002062



- LEGEND**
- MONITORING WELLS
 - SOIL BORING LOCATIONS
 - SOIL CONTAMINATED WITH > 20 mg/L VOCs
 - 15' CONTOUR INTERVAL IN FT-Ms.
 - - - FENCE
 - ⊙ MANHOLE
 - - - INFERRED CONTOUR
 - UEP MONUMENTS

- NOTES**
1. FOR SUBSURFACE PROFILES, SEE SHEET 18.
 2. FOR ANALYTICAL RESULTS FOR CONTAMINATED SOIL AND WELL BORINGS, SEE TABLES 5, 6, 7, 10, AND 11.
 3. BASE MAP COMPILED FROM FORT WORTH DISTRICT SURVEY DATA AND AS-BUILT'S, CONTRACT NO. DAC63-78-B-0010, AND AS-BUILT'S CONTRACT NO. DAC687-84-C-0039.



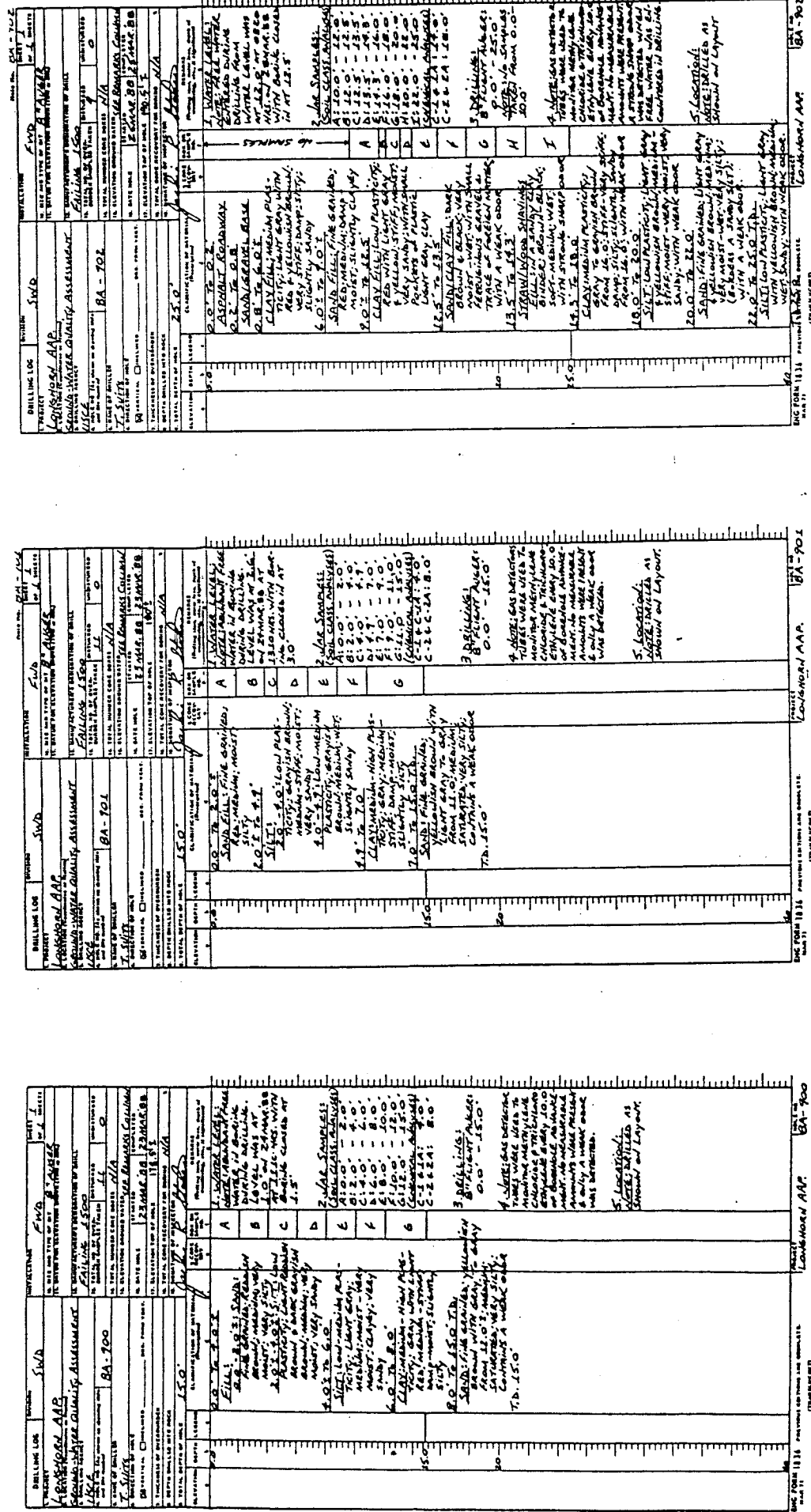
TITLE: SOIL CONTAMINATION AND BORING LOCATION MAP	
U.S. ARMY ENGINEER DISTRICT, FORT WORTH, TEXAS	
CORPS OF ENGINEERS	
PROJECT NO. 002062	
DRAWN BY: C. KIRBY	
CHECKED BY: R. BEHM	
APPROVED BY: ROBERT C. BEHM	
DATE: 5/31/84	
SHEET NO. 5	

[illegible]

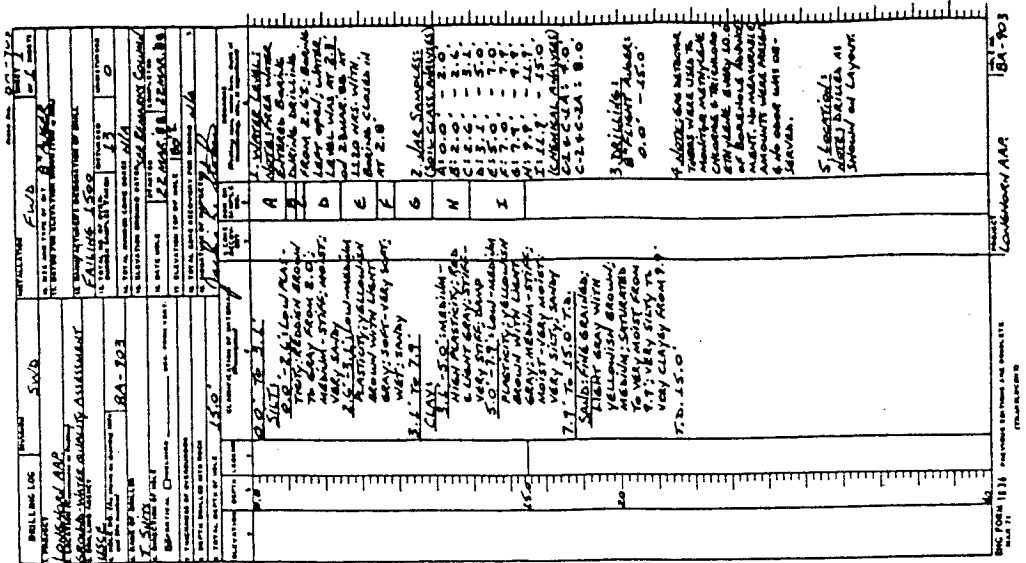
FOR BORING LOCATIONS, SEE SHEET 5.

[illegible]

002064



NOTE
FOR BORING LOCATIONS, SEE SHEET 5.



U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS POST OFFICE, TEXAS	
LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS	
RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I	
LOGS OF BORINGS	
ENGINEERED BY: R. C. BEHM	DATE: 7/23/81
DESIGNED BY: R. C. BEHM	DATE: 7/23/81
DRAWN BY: R. C. BEHM	DATE: 7/23/81
CHECKED BY: R. C. BEHM	DATE: 7/23/81
APPROVED BY: R. C. BEHM	DATE: 7/23/81

PROJECT	GRIDING LINE	SWD	INFECTION	SWD	DATE	BY
1. NAME OF PROJECT						
2. NAME OF CLIENT						
3. NAME OF DESIGNER						
4. NAME OF CONTRACTOR						
5. NAME OF SUBCONTRACTOR						
6. NAME OF MATERIAL SUPPLIER						
7. NAME OF LABORER						
8. NAME OF INSPECTOR						
9. NAME OF APPROVER						
10. NAME OF REVIEWER						
11. NAME OF DESIGNER						
12. NAME OF CONTRACTOR						
13. NAME OF SUBCONTRACTOR						
14. NAME OF MATERIAL SUPPLIER						
15. NAME OF LABORER						
16. NAME OF INSPECTOR						
17. NAME OF APPROVER						
18. NAME OF REVIEWER						
19. NAME OF DESIGNER						
20. NAME OF CONTRACTOR						
21. NAME OF SUBCONTRACTOR						
22. NAME OF MATERIAL SUPPLIER						
23. NAME OF LABORER						
24. NAME OF INSPECTOR						
25. NAME OF APPROVER						
26. NAME OF REVIEWER						
27. NAME OF DESIGNER						
28. NAME OF CONTRACTOR						
29. NAME OF SUBCONTRACTOR						
30. NAME OF MATERIAL SUPPLIER						
31. NAME OF LABORER						
32. NAME OF INSPECTOR						
33. NAME OF APPROVER						
34. NAME OF REVIEWER						
35. NAME OF DESIGNER						
36. NAME OF CONTRACTOR						
37. NAME OF SUBCONTRACTOR						
38. NAME OF MATERIAL SUPPLIER						
39. NAME OF LABORER						
40. NAME OF INSPECTOR						
41. NAME OF APPROVER						
42. NAME OF REVIEWER						
43. NAME OF DESIGNER						
44. NAME OF CONTRACTOR						
45. NAME OF SUBCONTRACTOR						
46. NAME OF MATERIAL SUPPLIER						
47. NAME OF LABORER						
48. NAME OF INSPECTOR						
49. NAME OF APPROVER						
50. NAME OF REVIEWER						
51. NAME OF DESIGNER						
52. NAME OF CONTRACTOR						
53. NAME OF SUBCONTRACTOR						
54. NAME OF MATERIAL SUPPLIER						
55. NAME OF LABORER						
56. NAME OF INSPECTOR						
57. NAME OF APPROVER						
58. NAME OF REVIEWER						
59. NAME OF DESIGNER						
60. NAME OF CONTRACTOR						
61. NAME OF SUBCONTRACTOR						
62. NAME OF MATERIAL SUPPLIER						
63. NAME OF LABORER						
64. NAME OF INSPECTOR						
65. NAME OF APPROVER						
66. NAME OF REVIEWER						
67. NAME OF DESIGNER						
68. NAME OF CONTRACTOR						
69. NAME OF SUBCONTRACTOR						
70. NAME OF MATERIAL SUPPLIER						
71. NAME OF LABORER						
72. NAME OF INSPECTOR						
73. NAME OF APPROVER						
74. NAME OF REVIEWER						
75. NAME OF DESIGNER						
76. NAME OF CONTRACTOR						
77. NAME OF SUBCONTRACTOR						
78. NAME OF MATERIAL SUPPLIER						
79. NAME OF LABORER						
80. NAME OF INSPECTOR						

DATE	TIME	LOCATION	U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS
REPORTED BY: BETHANWALP	LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS		
ISSUED BY: C. B. BENT	RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I		
REVISED BY: B. BENT	LOGS OF BORINGS		
SUBMITTED BY: ROBERT C. BENT	SUB. NO. CONTR. NO.	DATE:	REMARKS SHEET NO. 8 OF 31
DRAWN BY: BETHANWALP			PLANTING NUMBER

BRALL LOC	DATE	SWD	INSTRUMENT	TIME	DATE	TIME	DATE	TIME
1. PROJECT								
2. LOCATION								
3. NAME								
4. DATE								
5. TIME								
6. NAME								
7. DATE								
8. TIME								
9. NAME								
10. DATE								
11. TIME								
12. NAME								
13. DATE								
14. TIME								
15. NAME								
16. DATE								
17. TIME								
18. NAME								
19. DATE								
20. TIME								
21. NAME								
22. DATE								
23. TIME								
24. NAME								
25. DATE								
26. TIME								
27. NAME								
28. DATE								
29. TIME								
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31. DATE								
32. TIME								
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36. NAME								
37. DATE								
38. TIME								
39. NAME								
40. DATE								
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57. NAME								
58. DATE								
59. TIME								
60. NAME								
61. DATE								
62. TIME								
63. NAME								
64. DATE								
65. TIME								
66. NAME								
67. DATE								
68. TIME								
69. NAME								
70. DATE								
71. TIME								

DATE	TIME	ROOM	BY	INITIALS OF WORKER
U.S. ARMY ENGINEER DETNCT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS				
LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS				
RORA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I				
LOGS OF BORINGS				
DOL. NO.				DATE
CONTR. NO.				SHEET NO.
				9 of 31
BORING NUMBER				9
REQUISITED BY: ROBERT C. BEHM ENGINEER				
DRAWN BY: S. J. JOHNSON				
CHECKED BY: S. J. JOHNSON				
REVISED BY:				
E. B. BIRD				

ROLLING LOG	FORM	SWD	DESCRIPTION	ANALYSIS	REMARKS
1. PROJECT	100	100	100	100	100
2. DATE	100	100	100	100	100
3. TIME	100	100	100	100	100
4. LOCATION	100	100	100	100	100
5. OPERATOR	100	100	100	100	100
6. INSTRUMENT	100	100	100	100	100
7. METHOD	100	100	100	100	100
8. SAMPLE NO.	100	100	100	100	100
9. ANALYST	100	100	100	100	100
10. REVIEWER	100	100	100	100	100
11. APPROVAL	100	100	100	100	100
12. COMMENTS	100	100	100	100	100
13. DATE	100	100	100	100	100
14. TIME	100	100	100	100	100
15. LOCATION	100	100	100	100	100
16. OPERATOR	100	100	100	100	100
17. INSTRUMENT	100	100	100	100	100
18. METHOD	100	100	100	100	100
19. SAMPLE NO.	100	100	100	100	100
20. ANALYST	100	100	100	100	100
21. REVIEWER	100	100	100	100	100
22. APPROVAL	100	100	100	100	100
23. COMMENTS	100	100	100	100	100
24. DATE	100	100	100	100	100
25. TIME	100	100	100	100	100
26. LOCATION	100	100	100	100	100
27. OPERATOR	100	100	100	100	100
28. INSTRUMENT	100	100	100	100	100
29. METHOD	100	100	100	100	100
30. SAMPLE NO.	100	100	100	100	100
31. ANALYST	100	100	100	100	100
32. REVIEWER	100	100	100	100	100
33. APPROVAL	100	100	100	100	100
34. COMMENTS	100	100	100	100	100
35. DATE	100	100	100	100	100
36. TIME	100	100	100	100	100
37. LOCATION	100	100	100	100	100
38. OPERATOR	100	100	100	100	100
39. INSTRUMENT	100	100	100	100	100
40. METHOD	100	100	100	100	100
41. SAMPLE NO.	100	100	100	100	100
42. ANALYST	100	100	100	100	100
43. REVIEWER	100	100	100	100	100
44. APPROVAL	100	100	100	100	100
45. COMMENTS	100	100	100	100	100
46. DATE	100	100	100	100	100
47. TIME	100	100	100	100	100
48. LOCATION	100	100	100	100	100
49. OPERATOR	100	100	100	100	100
50. INSTRUMENT	100	100	100	100	100
51. METHOD	100	100	100	100	100
52. SAMPLE NO.	100	100	100	100	100
53. ANALYST	100	100	100	100	100
54. REVIEWER	100	100	100	100	100
55. APPROVAL	100	100	100	100	100
56. COMMENTS	100	100	100	100	100
57. DATE	100	100	100	100	100
58. TIME	100	100	100	100	100
59. LOCATION	100	100	100	100	100
60. OPERATOR	100	100	100	100	100
61. INSTRUMENT	100	100	100	100	100
62. METHOD	100	100	100	100	100
63. SAMPLE NO.	100	100	100	100	100
64. ANALYST	100	100	100	100	100
65. REVIEWER	100	100			

[illegible]

STATION NO.	AREA	DATE	LOGGING METHOD	U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS
DESIGNED BY: D. F. TITENBERG	SKETCH BY: C. JOHNSON	REVIEWED BY: S. BARNES	NON-REGISTERED BY:	LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS
RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I LOGS OF BORINGS				RCR NO. CONTR. NO. QUANTITIES NUMBER
ROBERT C. BEHM SERVICES:				DATE: 12 97 31 PROJECT NO. 12

002070

BELLING LOG		BELLING LOG		BELLING LOG		BELLING LOG	
PROJECT	BA-728	PROJECT	BA-728	PROJECT	BA-728	PROJECT	BA-728
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DATE	10/1/54	DATE	10/1/54	DATE	10/1/54	DATE	10/1/54
TIME	10:00	TIME	10:00	TIME	10:00	TIME	10:00
DRILLER	BA-728	DRILLER	BA-728	DRILLER	BA-728	DRILLER	BA-728
LOGGERS	BA-728	LOGGERS	BA-728	LOGGERS	BA-728	LOGGERS	BA-728
TEST NO.	100	TEST NO.	100	TEST NO.	100	TEST NO.	100
TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100
TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100
TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100
TEST DATA	100	TEST DATA	100	TEST DATA	100	TEST DATA	100
TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100
TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100
TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100

BELLING LOG		BELLING LOG		BELLING LOG		BELLING LOG	
PROJECT	BA-729	PROJECT	BA-729	PROJECT	BA-729	PROJECT	BA-729
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DATE	10/1/54	DATE	10/1/54	DATE	10/1/54	DATE	10/1/54
TIME	10:00	TIME	10:00	TIME	10:00	TIME	10:00
DRILLER	BA-729	DRILLER	BA-729	DRILLER	BA-729	DRILLER	BA-729
LOGGERS	BA-729	LOGGERS	BA-729	LOGGERS	BA-729	LOGGERS	BA-729
TEST NO.	100	TEST NO.	100	TEST NO.	100	TEST NO.	100
TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100
TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100
TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100
TEST DATA	100	TEST DATA	100	TEST DATA	100	TEST DATA	100
TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100
TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100
TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100

BELLING LOG		BELLING LOG		BELLING LOG		BELLING LOG	
PROJECT	BA-730	PROJECT	BA-730	PROJECT	BA-730	PROJECT	BA-730
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DATE	10/1/54	DATE	10/1/54	DATE	10/1/54	DATE	10/1/54
TIME	10:00	TIME	10:00	TIME	10:00	TIME	10:00
DRILLER	BA-730	DRILLER	BA-730	DRILLER	BA-730	DRILLER	BA-730
LOGGERS	BA-730	LOGGERS	BA-730	LOGGERS	BA-730	LOGGERS	BA-730
TEST NO.	100	TEST NO.	100	TEST NO.	100	TEST NO.	100
TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100
TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100
TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100
TEST DATA	100	TEST DATA	100	TEST DATA	100	TEST DATA	100
TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100
TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100
TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100

BELLING LOG		BELLING LOG		BELLING LOG		BELLING LOG	
PROJECT	BA-731	PROJECT	BA-731	PROJECT	BA-731	PROJECT	BA-731
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DATE	10/1/54	DATE	10/1/54	DATE	10/1/54	DATE	10/1/54
TIME	10:00	TIME	10:00	TIME	10:00	TIME	10:00
DRILLER	BA-731	DRILLER	BA-731	DRILLER	BA-731	DRILLER	BA-731
LOGGERS	BA-731	LOGGERS	BA-731	LOGGERS	BA-731	LOGGERS	BA-731
TEST NO.	100	TEST NO.	100	TEST NO.	100	TEST NO.	100
TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100	TEST DEPTH	100
TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100	TEST RESULTS	100
TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100	TEST COMMENTS	100
TEST DATA	100	TEST DATA	100	TEST DATA	100	TEST DATA	100
TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100	TEST ANALYSIS	100
TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100	TEST CONCLUSIONS	100
TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100	TEST RECOMMENDATIONS	100

NOTE
FOR BORING LOCATIONS, SEE SHEET 5.

U.S. ARMY ENGINEER DISTRICT, FORT WORTH	
CORPS OF ENGINEERS	
PORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT	
KARNACK, TEXAS	
RCRA FACILITY INVESTIGATION	
ABG AND UEP SITES	
PHASE I	
LOGS OF BORINGS	
PROJECT NO.	BA-731
DATE	10/1/54
DRILLER	BA-731
LOGGERS	BA-731
TEST NO.	100
TEST DEPTH	100
TEST RESULTS	100
TEST COMMENTS	100
TEST DATA	100
TEST ANALYSIS	100
TEST CONCLUSIONS	100
TEST RECOMMENDATIONS	100

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[illegible][illegible]

DRILLING LOG	SECTION	DEPTH	REMARKS	DATE	BY
1. PROJECT	510			8-2-78	W. L.
2. LOCATION	LAKEHURST RAP				
3. SECTION	SEVEN-THREE-ONE				
4. DATE	8-2-78				
5. TIME	10:00				
6. SURFACE	LAKEHURST RAP				
7. ELEVATION	100'				
8. DIRECTION	LAKEHURST RAP				
9. DISTANCE	100'				
10. TOTAL DEPTH OF HOLE	100'				
11. DEPTH OF WATER	100'				
12. DEPTH OF SEDIMENT	100'				
13. DEPTH OF BEDROCK	100'				
14. DEPTH OF SOIL	100'				
15. DEPTH OF SAND	100'				
16. DEPTH OF GRAVEL	100'				
17. DEPTH OF COBBLES	100'				
18. DEPTH OF Boulders	100'				
19. DEPTH OF CLAY	100'				
20. DEPTH OF SILT	100'				
21. DEPTH OF MUD	100'				
22. DEPTH OF SLUDGE	100'				
23. DEPTH OF OTHER	100'				
24. DEPTH OF TOTAL	100'				
25. DEPTH OF REMAINING	100'				
26. DEPTH OF REMAINING	100'				
27. DEPTH OF REMAINING	100'				
28. DEPTH OF REMAINING	100'				
29. DEPTH OF REMAINING	100'				
30. DEPTH OF REMAINING	100'				
31. DEPTH OF REMAINING	100'				
32. DEPTH OF REMAINING	100'				
33. DEPTH OF REMAINING	100'				
34. DEPTH OF REMAINING	100'				
35. DEPTH OF REMAINING	100'				
36. DEPTH OF REMAINING	100'				
37. DEPTH OF REMAINING	100'				
38. DEPTH OF REMAINING	100'				
39. DEPTH OF REMAINING	100'				
40. DEPTH OF REMAINING	100'				
41. DEPTH OF REMAINING	100'				
42. DEPTH OF REMAINING	100'				
43. DEPTH OF REMAINING	100'				
44. DEPTH OF REMAINING	100'				
45. DEPTH OF REMAINING	100'				
46. DEPTH OF REMAINING	100'				
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49. DEPTH OF REMAINING	100'				
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51. DEPTH OF REMAINING	100'				
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68. DEPTH OF REMAINING	100'				
69. DEPTH OF REMAINING	100'				
70. DEPTH OF REMAINING	100'				
71. DEPTH OF REMAINING	100'				
72. DEPTH OF REMAINING	100'				
73. DEPTH OF REMAINING	100'				
74. DEPTH OF REMAINING	100'				
75. DEPTH OF REMAINING	100'				
76. DEPTH OF REMAINING	100'				
77. DEPTH OF REMAINING	100'				
78. DEPTH OF REMAINING	100'				
79. DEPTH OF REMAINING	100'				

[illegible][illegible]

NOTE
FOR BORING LOCATIONS, SEE SHEET 5.

[illegible]

002074

Boring Log		Boring Log		Boring Log	
DATE	BA-944	DATE	BA-944	DATE	BA-944
PROJECT	Longhorn AFB	PROJECT	Longhorn AFB	PROJECT	Longhorn AFB
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DEPTH	10.0	DEPTH	10.0	DEPTH	10.0
TIME	10.0	TIME	10.0	TIME	10.0
DRILLING LOG	10.0	DRILLING LOG	10.0	DRILLING LOG	10.0
INTEREST	10.0	INTEREST	10.0	INTEREST	10.0
DESCRIPTION	10.0	DESCRIPTION	10.0	DESCRIPTION	10.0
1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0
2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0
3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0
4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0
5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0
6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0
7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0
8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0
9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0
10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0

Boring Log		Boring Log		Boring Log	
DATE	BA-945	DATE	BA-945	DATE	BA-945
PROJECT	Longhorn AFB	PROJECT	Longhorn AFB	PROJECT	Longhorn AFB
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DEPTH	10.0	DEPTH	10.0	DEPTH	10.0
TIME	10.0	TIME	10.0	TIME	10.0
DRILLING LOG	10.0	DRILLING LOG	10.0	DRILLING LOG	10.0
INTEREST	10.0	INTEREST	10.0	INTEREST	10.0
DESCRIPTION	10.0	DESCRIPTION	10.0	DESCRIPTION	10.0
1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0
2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0
3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0
4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0
5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0
6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0
7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0
8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0
9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0
10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0

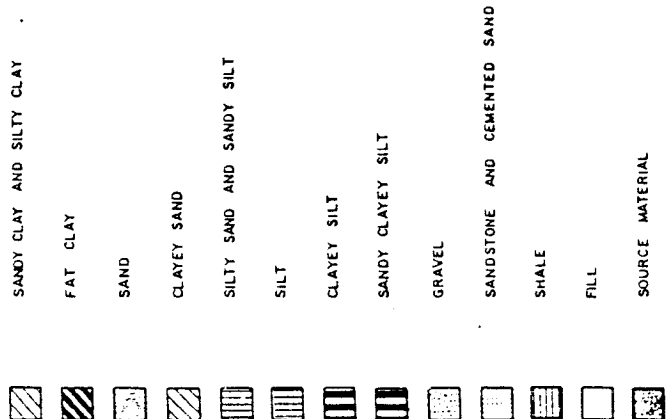
Boring Log		Boring Log		Boring Log	
DATE	BA-946	DATE	BA-946	DATE	BA-946
PROJECT	Longhorn AFB	PROJECT	Longhorn AFB	PROJECT	Longhorn AFB
LOCATION	Longhorn AFB	LOCATION	Longhorn AFB	LOCATION	Longhorn AFB
DEPTH	10.0	DEPTH	10.0	DEPTH	10.0
TIME	10.0	TIME	10.0	TIME	10.0
DRILLING LOG	10.0	DRILLING LOG	10.0	DRILLING LOG	10.0
INTEREST	10.0	INTEREST	10.0	INTEREST	10.0
DESCRIPTION	10.0	DESCRIPTION	10.0	DESCRIPTION	10.0
1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0	1. 0.0 - 1.0	10.0
2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0	2. 1.0 - 2.0	10.0
3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0	3. 2.0 - 3.0	10.0
4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0	4. 3.0 - 4.0	10.0
5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0	5. 4.0 - 5.0	10.0
6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0	6. 5.0 - 6.0	10.0
7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0	7. 6.0 - 7.0	10.0
8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0	8. 7.0 - 8.0	10.0
9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0	9. 8.0 - 9.0	10.0
10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0	10. 9.0 - 10.0	10.0

NOTE
FOR BORING LOCATIONS, SEE SHEET 5.

LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS		CORPS OF ENGINEERS FORT WORTH, TEXAS	
RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I		LOGS OF BORINGS	
REPORTED BY: R. C. BEHN	DATE: 17 9 31	DRILLING NO. BA-944	DATE: 17 9 31
PROJECT NO. BA-944		SHEET NO. 17	

002075

STRATIGRAPHIC SYMBOLS



LEGEND

FW FREE WATER ENCOUNTERED DURING DRILLING
O OOR ENCOUNTERED DURING DRILLING
T LIMITS OF OOR AND/OR FREE WATER IF NOT TO T.D.
I WATER LEVEL MEASURED 3 AUGUST 1988
V WELL GRAVEL PACK INTERVAL
I WELL SCREEN INTERVAL

GENERAL NOTES

1. STRATIGRAPHIC SYMBOLS ARE IN ACCORDANCE WITH DESCRIPTION OF MATERIALS ON THE FIELD LOGS.
2. THE BORING NUMBER AND ELEVATION ARE SHOWN AT THE TOP OF THE LOG. THE ELEVATION IS THE SURVEYED TOP OF CONCRETE PAD OR SURVEY MARKER.
3. TOTAL DEPTH OF BORING AND DATE COMPLETED ARE SHOWN AT THE BOTTOM OF THE LOG.
4. ASSUME THAT ONCE O AND/OR FW ARE ENCOUNTERED, THE BORING EXHIBITED AN OOR AND/OR THE BORING MADE WATER UNTIL T.D. WAS REACHED UNLESS OTHERWISE NOTED.
5. FOR 3F BORINGS, RESISTIVITY LOGS ARE SHOWN TO THE RIGHT OF THE BORING. THE RESISTIVITY CALIBRATION IS SHOWN IN OHM(C) AT THE BOTTOM OF THE LOG. THE GAMMA LOG IS SHOWN TO THE LEFT OF THE BORING. THE COUNT RATE AND TIME CONSTANT ARE SHOWN AT THE BOTTOM OF THE LOG.
6. FOR LOGS OF 8A BORINGS, SEE SHEETS 6 THROUGH 17.
7. FOR LOGS OF 3F BORINGS, SEE SHEET 22.
8. FOR LOGS OF USAHA, USTHAMA, AND USAQ(CDM) WELL BORINGS, SEE APPENDIX N.
9. FOR LOGS OF MW WELL BORINGS, SEE APPENDIX M.
10. FOR WELL INSTALLATION DETAILS FOR USTHAMA AND USAQ(CDM) WELLS, SEE APPENDIX L. THERE ARE NO WELL INSTALLATION DETAILS FOR USAHA WELLS.
11. FOR WELL INSTALLATION DETAILS FOR MW WELLS, SEE APPENDIX O.
12. HYDRAULIC CONDUCTIVITY VALUES DETERMINED FOR WELLS MW-1 THRU MW-15 ARE SHOWN OPPOSITE THE WELL SCREEN IN CM/SEC.

NOTES

1. APPROXIMATE LIMITS OF EXCAVATION ARE SHOWN FOR BORINGS 8A-902, 8A-903, 8A-904, 8A-905, 8A-906, 8A-907, 8A-908, 8A-909, 8A-910, 8A-911, 8A-912, 8A-913, 8A-914, 8A-915, 8A-916, 8A-917, 8A-918, 8A-919, 8A-920, 8A-921, 8A-922, 8A-923, 8A-924, 8A-925, 8A-926, 8A-927, 8A-928, 8A-929, 8A-930, 8A-931, 8A-932, 8A-933, 8A-934, 8A-935, 8A-936, 8A-937, 8A-938, 8A-939, 8A-940, 8A-941, 8A-942, 8A-943, 8A-944, 8A-945, 8A-946, 8A-947, 8A-948, 8A-949, 8A-950, 8A-951, 8A-952, 8A-953, 8A-954, 8A-955, 8A-956, 8A-957, 8A-958, 8A-959, 8A-960, 8A-961, 8A-962, 8A-963, 8A-964, 8A-965, 8A-966, 8A-967, 8A-968, 8A-969, 8A-970, 8A-971, 8A-972, 8A-973, 8A-974, 8A-975, 8A-976, 8A-977, 8A-978, 8A-979, 8A-980, 8A-981, 8A-982, 8A-983, 8A-984, 8A-985, 8A-986, 8A-987, 8A-988, 8A-989, 8A-990, 8A-991, 8A-992, 8A-993, 8A-994, 8A-995, 8A-996, 8A-997, 8A-998, 8A-999, 8A-1000, 8A-1001, 8A-1002, 8A-1003, 8A-1004, 8A-1005, 8A-1006, 8A-1007, 8A-1008, 8A-1009, 8A-1010, 8A-1011, 8A-1012, 8A-1013, 8A-1014, 8A-1015, 8A-1016, 8A-1017, 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002076

GROUNDWATER MONITORING WELLS
IN THE
ACTIVE BURNING GROUNDS AREA

WELL NO.	MEAS. PT. ELEVATION FT. MSL	COMP. MON. WELL	CORRECT ACT. MON. WELL
C-1	193.80	NO	NO
C-2	178.03	NO	YES
C-3	186.41	NO	YES
C-4	184.74	NO	YES
C-5	180.77	NO	YES
C-6	182.34	NO	NO
C-7	186.72	NO	NO
C-8	182.56	NO	NO
C-9	202.86	NO	YES
C-10	202.04	NO	NO
BH-3	186.30	NO	NO
BH-4	187.44	NO	NO
BH-7	187.24	NO	YES
BH-11	189.03	NO	NO
BH-21	REMOVED	NO	NO
BH-22	189.25	NO	NO
101	187.51	NO	NO
102	184.55	NO	NO
108	187.21	NO	NO
120	183.21	NO	NO
133	184.31	NO	NO
134	184.31	NO	NO
135	184.31	NO	NO
136	184.31	NO	NO
137	184.31	NO	NO
138	184.31	NO	NO
139	184.31	NO	NO
140	184.31	NO	NO
141	184.31	NO	NO
142	184.31	NO	NO
143	184.31	NO	NO
144	184.31	NO	NO
145	184.31	NO	NO
146	184.31	NO	NO
147	184.31	NO	NO
148	184.31	NO	NO
149	184.31	NO	NO
150	184.31	NO	NO
151	184.31	NO	NO
152	184.31	NO	NO
153	184.31	NO	NO
154	184.31	NO	NO
155	184.31	NO	NO
156	184.31	NO	NO
157	184.31	NO	NO
158	184.31	NO	NO
159	184.31	NO	NO
160	184.31	NO	NO
161	184.31	NO	NO
162	184.31	NO	NO
163	184.31	NO	NO
164	184.31	NO	NO
165	184.31	NO	NO
166	184.31	NO	NO
167	184.31	NO	NO
168	184.31	NO	NO
169	184.31	NO	NO
170	184.31	NO	NO
171	184.31	NO	NO
172	184.31	NO	NO
173	184.31	NO	NO
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181	184.31	NO	NO
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185	184.31	NO	NO
186	184.31	NO	NO
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194	184.31	NO	NO
195	184.31	NO	NO
196	184.31	NO	NO
197	184.31	NO	NO
198	184.31	NO	NO
199	184.31	NO	NO
200	184.31	NO	NO



LEGEND

- 174 - GROUND-WATER SURFACE ELEVATION
- 101 - EXISTING MONITORING WELL
- MU-8 - PROPOSED MONITORING WELL
- - - GROUND-WATER FLOW DIRECTION

NOTES

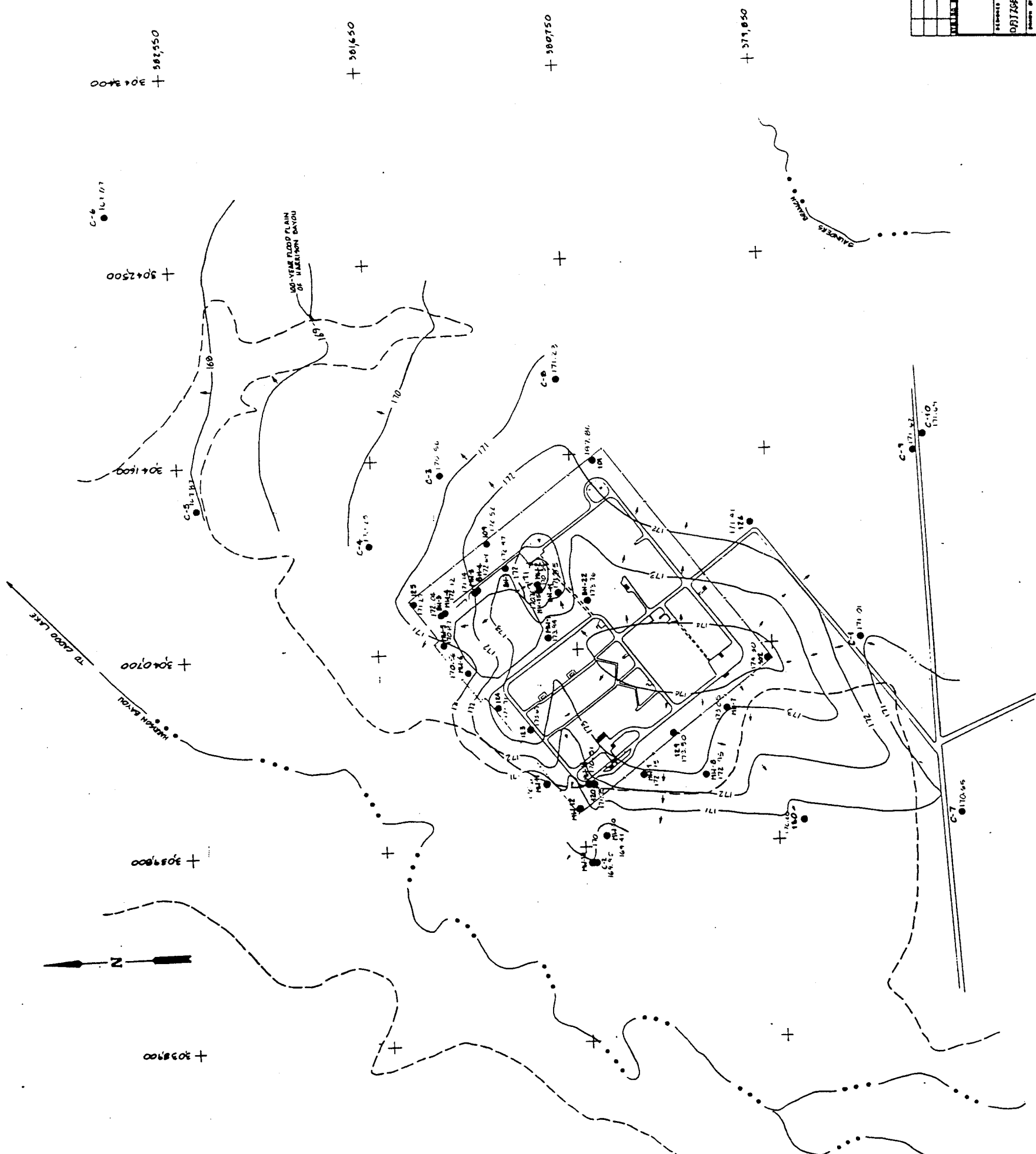
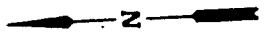
1. WATER LEVELS TAKEN 20-22 APRIL 1988.
2. CONTOURS ARE SHALLOW WELL DATA ONLY, EXCLUDING WELL 101.

TITLE: GROUND-WATER SURFACE ELEVATION		PROJECT: LONGHORN ARMY AMMUNITION PLANT	
DRAWN BY: C. KIRBY		CHECKED BY: R. BEHN	
DATE: 19 APR 1988		SCALE: AS SHOWN	
PROJECT NO: 19		SHEET NO: 3	
DRAWING NO: 19		DATE: 19	
U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS PORT WORTH, TEXAS			
GROUND-WATER QUALITY ASSESSMENT PIEZOMETRIC SURFACE MAP, 20-22 APRIL 1988 AND PROPOSED WELL LOCATIONS			
SUBMITTED BY: ROBERT C. BEHN			
DATE: 19 APR 1988			

002077

GROUNDWATER MONITORING WELLS
IN THE
ACTIVE BURNING GROUNDS AREA

WELL NO.	MEAS. PT. ELEVATION	COMP. MON. WELLS	CORRECT ACT. MON. WELLS
C-1	193.80	NO	NO
C-2	178.03	NO	NO
C-3	198.41	NO	YES
C-4	198.74	NO	YES
C-5	190.77	NO	YES
C-6	192.35	NO	NO
C-7	188.72	NO	NO
C-8	192.38	NO	NO
C-9	202.85	NO	YES
C-10	202.04	NO	NO
BM-3	196.30	NO	NO
BM-4	197.44	NO	NO
BM-7	197.24	NO	YES
BM-11	199.03	NO	NO
BM-21	REMOVED	NO	NO
BM-22	199.25	NO	NO
101	197.51	NO	NO
102	194.55	NO	NO
108	197.11	NO	NO
120	193.28	NO	NO
123	188.33	NO	NO
124	188.39	NO	NO
125	198.35	NO	NO
128	199.81	NO	NO
129	197.13	NO	NO
130	177.80	NO	NO
AM-1	189.24	YES	YES
AM-2	187.00	YES	YES
AM-3	194.51	YES	YES
AM-4	197.31	YES	YES
AM-5	195.21	YES	YES
AM-6	192.19	YES	YES
AM-7	181.51	NO	NO
AM-8	186.85	NO	NO
AM-9	185.78	NO	NO
AM-10	177.39	NO	NO
AM-11	177.85	NO	NO
AM-12	178.37	NO	NO
AM-13	178.72	NO	NO
AM-14	182.38	NO	NO
AM-15	197.32	NO	NO



LEGEND
GROUND-WATER SURFACE ELEVATION
MONITORING WELL
GROUND-WATER FLOW DIRECTION

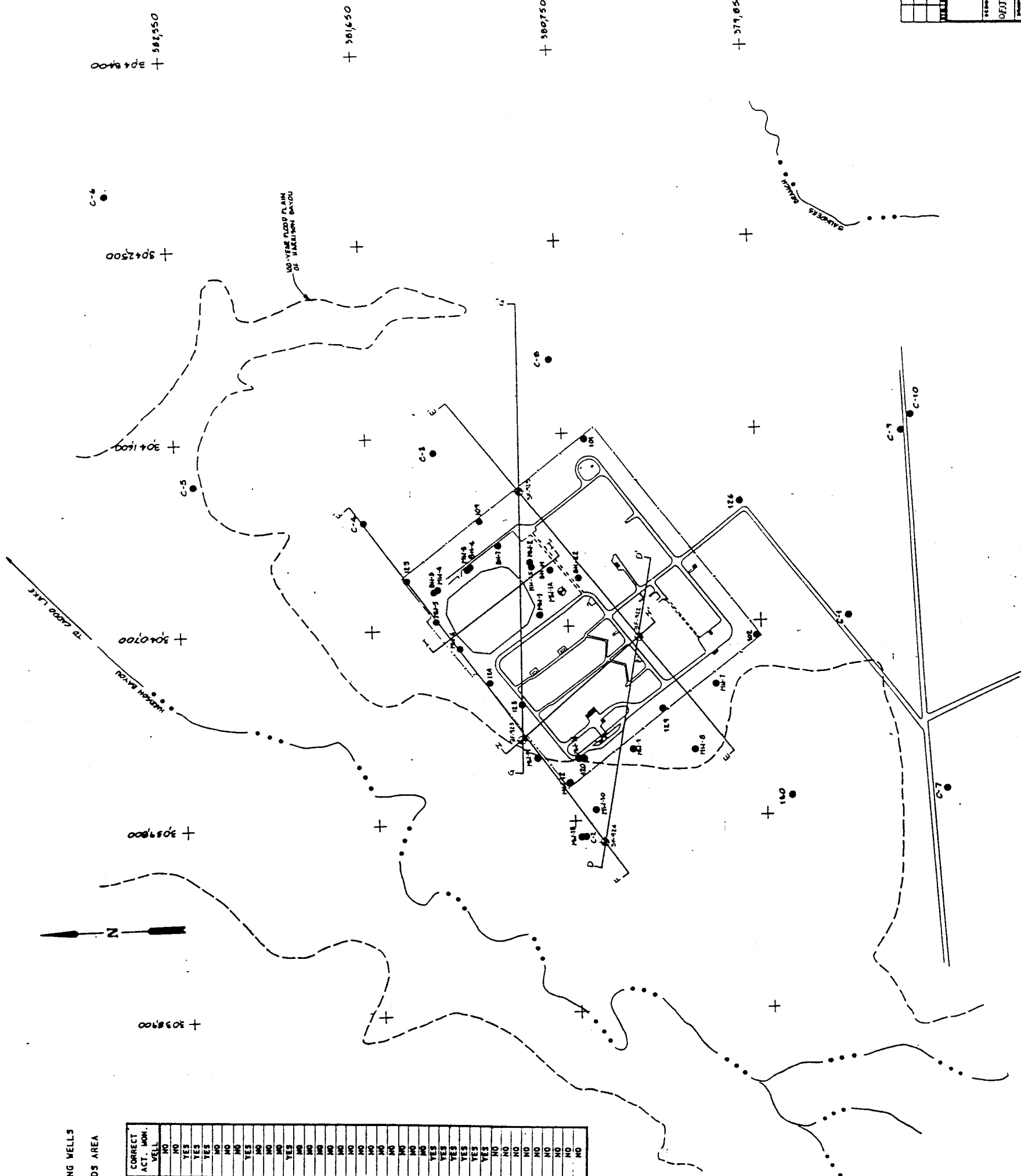
NOTES:
1. WATER LEVELS TAKEN 31 AUGUST 1988
2. CONTOURS ARE SHALLOW WELL DATA ONLY, EXCLUDING WELL 101.

U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
PROJECT NO.	002077
PROJECT NAME	LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS
PROJECT DESCRIPTION	RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I
PROJECT LOCATION	PEZOMETRIC SURFACE MAP 31 AUGUST 1988
PROJECTED BY	ROBERT C. BEHM
PROJECTED DATE	20 31 20

002078

GROUNDWATER MONITORING WELLS
IN THE
ACTIVE BURNING GROUNDS AREA

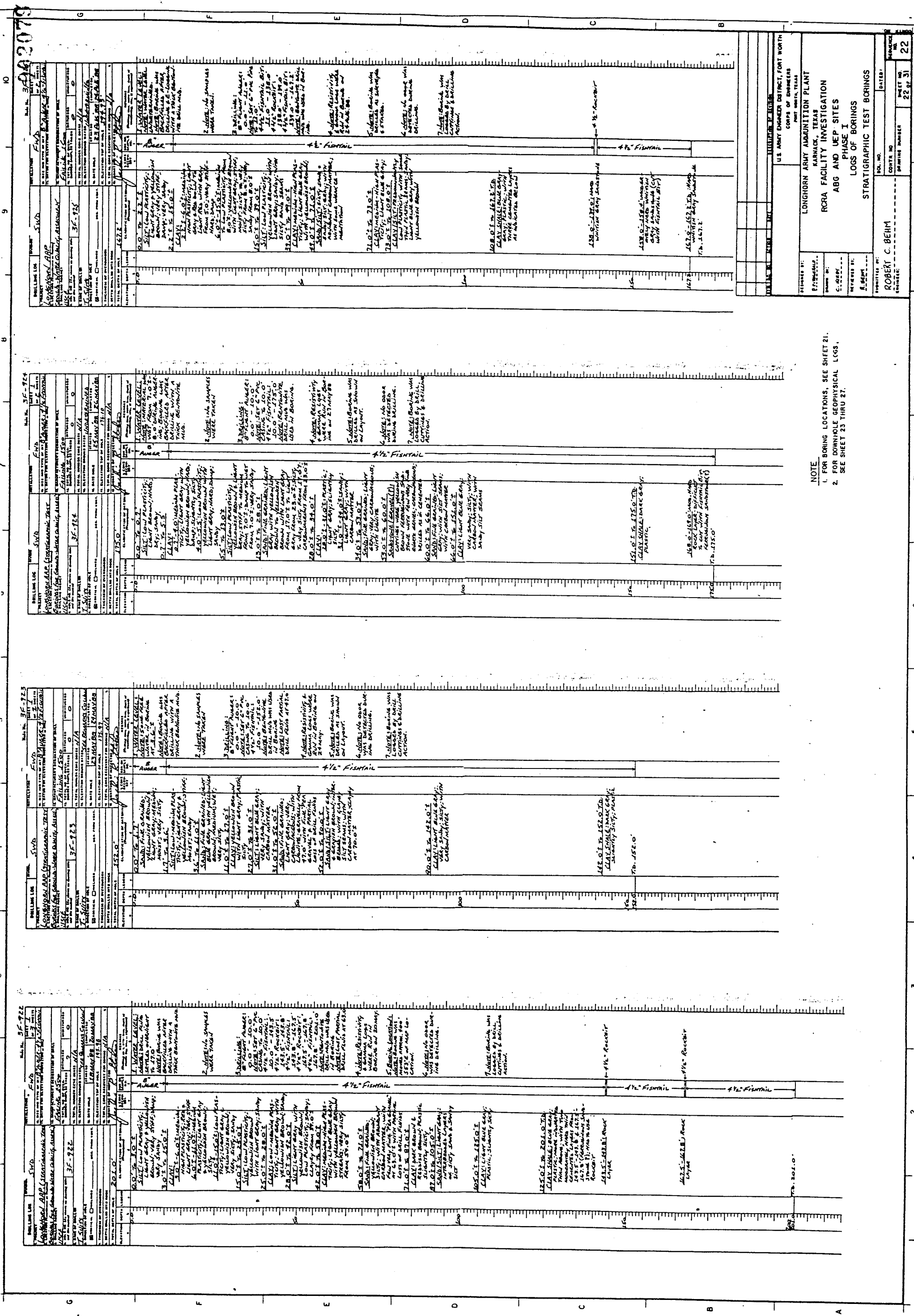
WELL NO.	MEAS. ELEVATION FT. MSL	PT. MON.	COMP. VELL	CORRECT MON. ACT. MON.
C-1	183.80	NO	NO	NO
C-2	178.03	NO	NO	YES
C-3	186.41	NO	NO	YES
C-4	184.74	NO	NO	YES
C-5	180.77	NO	NO	YES
C-6	182.34	NO	NO	NO
C-7	186.72	NO	NO	NO
C-8	182.58	NO	NO	YES
C-9	202.88	NO	NO	YES
C-10	202.04	NO	NO	NO
C-11	184.30	NO	NO	NO
C-12	187.44	NO	NO	YES
C-13	182.93	NO	NO	YES
C-14	182.93	NO	NO	YES
C-15	182.93	NO	NO	YES
C-16	182.93	NO	NO	YES
C-17	182.93	NO	NO	YES
C-18	182.93	NO	NO	YES
C-19	182.93	NO	NO	YES
C-20	182.93	NO	NO	YES
C-21	182.93	NO	NO	YES
C-22	182.93	NO	NO	YES
C-23	182.93	NO	NO	YES
C-24	182.93	NO	NO	YES
C-25	182.93	NO	NO	YES
C-26	182.93	NO	NO	YES
C-27	182.93	NO	NO	YES
C-28	182.93	NO	NO	YES
C-29	182.93	NO	NO	YES
C-30	182.93	NO	NO	YES
C-31	182.93	NO	NO	YES
C-32	182.93	NO	NO	YES
C-33	182.93	NO	NO	YES
C-34	182.93	NO	NO	YES
C-35	182.93	NO	NO	YES
C-36	182.93	NO	NO	YES
C-37	182.93	NO	NO	YES
C-38	182.93	NO	NO	YES
C-39	182.93	NO	NO	YES
C-40	182.93	NO	NO	YES
C-41	182.93	NO	NO	YES
C-42	182.93	NO	NO	YES
C-43	182.93	NO	NO	YES
C-44	182.93	NO	NO	YES
C-45	182.93	NO	NO	YES
C-46	182.93	NO	NO	YES
C-47	182.93	NO	NO	YES
C-48	182.93	NO	NO	YES
C-49	182.93	NO	NO	YES
C-50	182.93	NO	NO	YES
C-51	182.93	NO	NO	YES
C-52	182.93	NO	NO	YES
C-53	182.93	NO	NO	YES
C-54	182.93	NO	NO	YES
C-55	182.93	NO	NO	YES
C-56	182.93	NO	NO	YES
C-57	182.93	NO	NO	YES
C-58	182.93	NO	NO	YES
C-59	182.93	NO	NO	YES
C-60	182.93	NO	NO	YES
C-61	182.93	NO	NO	YES
C-62	182.93	NO	NO	YES
C-63	182.93	NO	NO	YES
C-64	182.93	NO	NO	YES
C-65	182.93	NO	NO	YES
C-66	182.93	NO	NO	YES
C-67	182.93	NO	NO	YES
C-68	182.93	NO	NO	YES
C-69	182.93	NO	NO	YES
C-70	182.93	NO	NO	YES
C-71	182.93	NO	NO	YES
C-72	182.93	NO	NO	YES
C-73	182.93	NO	NO	YES
C-74	182.93	NO	NO	YES
C-75	182.93	NO	NO	YES
C-76	182.93	NO	NO	YES
C-77	182.93	NO	NO	YES
C-78	182.93	NO	NO	YES
C-79	182.93	NO	NO	YES
C-80	182.93	NO	NO	YES
C-81	182.93	NO	NO	YES
C-82	182.93	NO	NO	YES
C-83	182.93	NO	NO	YES
C-84	182.93	NO	NO	YES
C-85	182.93	NO	NO	YES
C-86	182.93	NO	NO	YES
C-87	182.93	NO	NO	YES
C-88	182.93	NO	NO	YES
C-89	182.93	NO	NO	YES
C-90	182.93	NO	NO	YES
C-91	182.93	NO	NO	YES
C-92	182.93	NO	NO	YES
C-93	182.93	NO	NO	YES
C-94	182.93	NO	NO	YES
C-95	182.93	NO	NO	YES
C-96	182.93	NO	NO	YES
C-97	182.93	NO	NO	YES
C-98	182.93	NO	NO	YES
C-99	182.93	NO	NO	YES
C-100	182.93	NO	NO	YES



LEGEND
DS ● MONITORING WELL
3F-922 ○ STRATIGRAPHIC TEST BORING
MW-1A ○ SOIL BORING

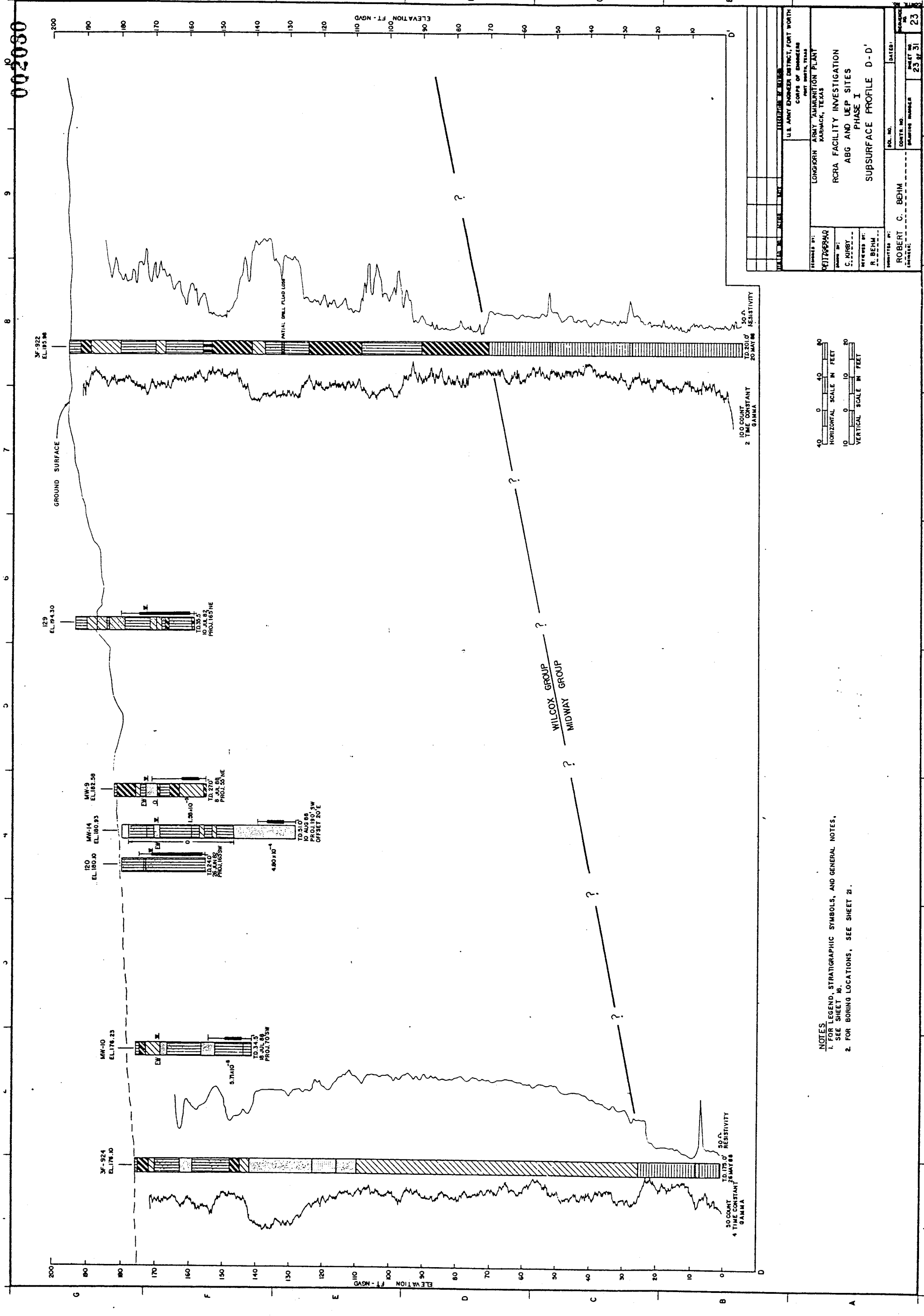
NOTE
1. FOR SUBSURFACE PROFILES, SEE SHEETS 23 THRU 27 AND SHEET 30.

TITLE: 002078		DATE: 21 31	
U.S. ARMY ENGINEER DISTRICT, FORT WORTH		CORPS OF ENGINEERS	
LONGHORN ARMY AMMUNITION PLANT		KARNACK, TEXAS	
RCRA FACILITY INVESTIGATION		ABG AND UEP SITES	
SUBSURFACE PROFILES AND		WELL LOCATION MAP	
APPROVED BY: C. NUNBY		REVIEWED BY: R. BENN	
SUBMITTED BY: ROBERT C. BENN		DATE: 21 31	

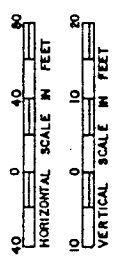


NOTE
1. FOR BORING LOCATIONS, SEE SHEET 21.
2. FOR DOWNHOLE GEOPHYSICAL LOGS, SEE SHEET 23 THRU 27.

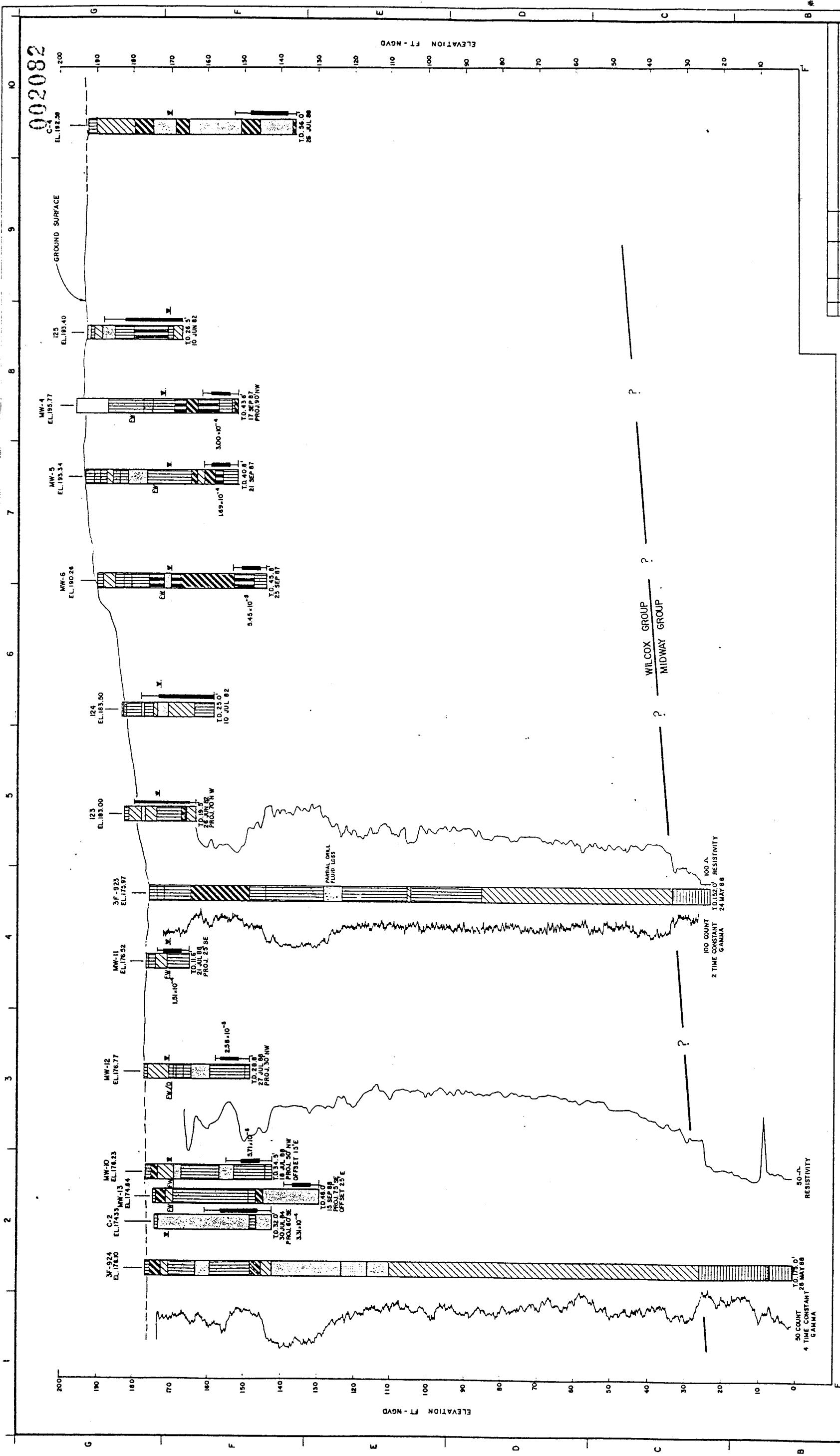
U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT KARNICK, TEXAS	
RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I LOGS OF BORINGS	
DESIGNED BY: E. J. HARRIS	REVIEWED BY: R. C. BERRY
DATE: 12/1/83	DATE: 12/1/83
PROJECT NO. 3F-922	
SHEET NO. 22	



NOTES
1. FOR LEGEND, STRATIGRAPHIC SYMBOLS, AND GENERAL NOTES, SEE SHEET 18.
2. FOR BORING LOCATIONS, SEE SHEET 21.



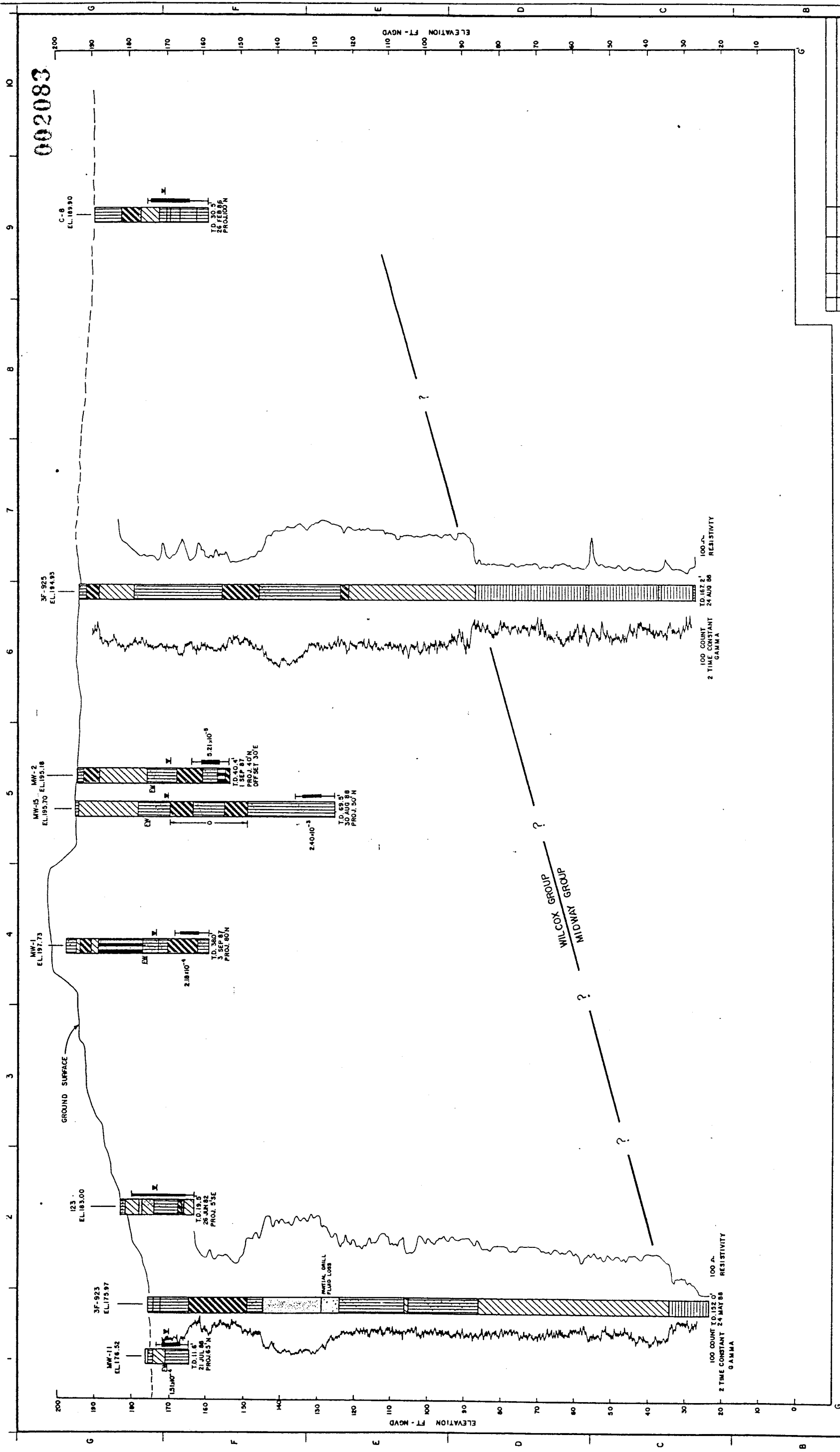
U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I SUBSURFACE PROFILE D-D'	
PROJECT NO. 0077099A02	DATE 23 OCT 88
DESIGNED BY C. MURPHY	CHECKED BY R. BEHM
APPROVED BY ROBERT C. BEHM	DATE 23 OCT 88



NOTES:
1. FOR LEGEND, STRATIGRAPHIC SYMBOLS, AND GENERAL NOTES, SEE SHEET 18.
2. FOR BORING LOCATIONS, SEE SHEET 21.

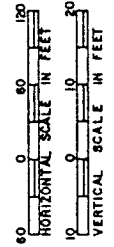
60 0 60 120
HORIZONTAL SCALE IN FEET
10 0 10 20
VERTICAL SCALE IN FEET

U.S. ARMY ENGINEER DISTRICT, FORT WORTH	
CORPS OF ENGINEERS	
LONGHORN ARMY AMMUNITION PLANT	
KARNAK, TEXAS	
RCRA FACILITY INVESTIGATION	
ABG AND UEP SITES	
PHASE I	
SUBSURFACE PROFILE F-F'	
DESIGNED BY: DEUTSCHER	DATE: 25 JUL 88
REVIEWED BY: C. KIRBY	CONTR. NO. 25 JUL 88
REVIEWED BY: R. BEHM	DATE: 25 JUL 88
REVIEWED BY: ROBERT C. BEHM	DATE: 25 JUL 88



002083

NOTES
1. FOR LEGEND, STRATIGRAPHIC SYMBOLS, AND GENERAL NOTES, SEE SHEET 1B.
2. FOR BORING LOCATIONS, SEE SHEET 21.



U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT RCRA FACILITY INVESTIGATION ABG AND UEP SITES PHASE I SUBSURFACE PROFILE G-G'	
DESIGNED BY: DEUTZGERALD	DATE: 1/28/88
DRAWN BY: C. KIRBY	DATE: 1/28/88
REVIEWED BY: R. BEHM	DATE: 1/28/88
APPROVED BY: ROBERT C. BEHM	DATE: 1/28/88
CONTRACT NO. 26	SHEET NO. 31

A vertical scale bar with numerical markings from 0 to 9. The markings are placed at regular intervals along a vertical line.

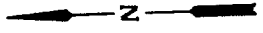


A vertical scale bar with numerical markings from 0 to 9. The markings are placed at regular intervals along a vertical line.



A vertical scale bar with numerical markings from 0 to 9. The markings are placed at regular intervals along a vertical line.

002085



+ 3038900

+ 3039800

+ 3040700

+ 3041600

+ 3042500

+ 3043400

+ 304550

+ 301650

+ 300750

+ 319850

C-6

C-5

C-4

C-3

C-2

C-1

C-10

C-11

C-7

100-YEAR FLOOD PLAIN
BY JACKSON BAYOU

TO CAUD LANE

JACKSON BAYOU

SANITARY DITCH

LEGEND

- 125 MONITORING WELL
- ISO CONCENTRATION LINES OF TRICHLOROETHENE IN SOIL GAS (ug/L)
- EXTENT OF TRICHLOROETHENE DETECTION IN SOIL GAS

NOTES

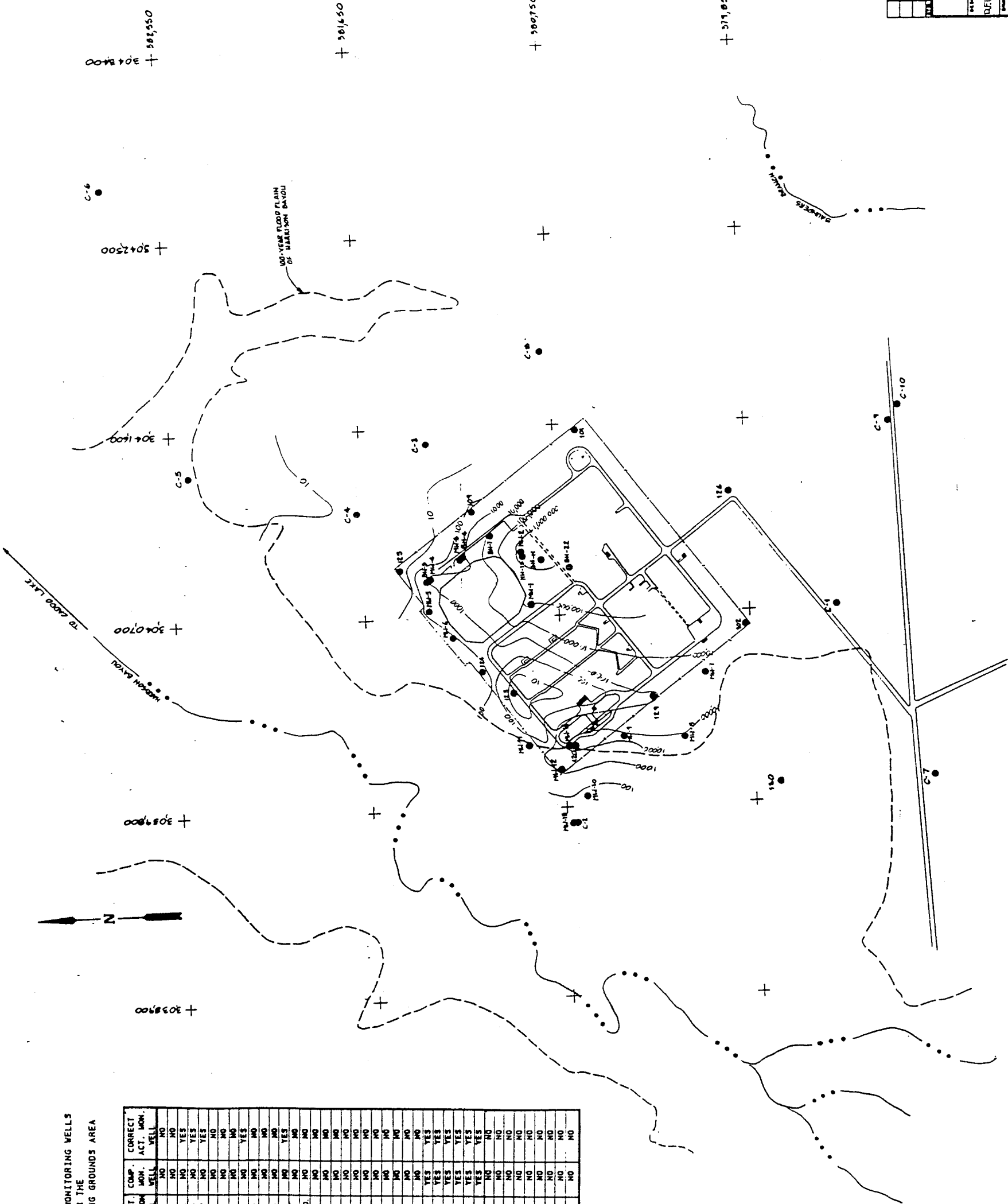
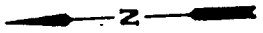
1. SOIL GAS SURVEY PERFORMED SEPT 1987
2. REFER TO SHEET 4 FOR SAMPLING LOCATIONS AND CONCENTRATIONS.

SCALE IN FEET
0 100 200 400

U.S. ARMY ENGINEER DISTRICT, FORT WORTH CORPS OF ENGINEERS FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT KARMAK, TEXAS	
RCRA FACILITY INVESTIGATION ABG AND LEP SITES PHASE I SOIL GAS CONTOURS AND WELL LOCATIONS	
Drawn by: D. L. ZEPHERO	Checked by: C. KIRBY
Reviewed by: R. BEHM	Submitted by: ROBERT C. BEHM
Scale: 1" = 100'	Date: 28 SEP 87
Sheet No: 28 of 31	Project No: 28

GROUNDWATER MONITORING WELLS
IN THE
ACTIVE BURNING GROUNDS AREA

WELL NO.	MEAS. PT. ELEVATION	COMP. MON. ACT. MON.	CORRECT MON. ACT. MON.
C-1	137.60	NO	NO
C-2	176.03	NO	NO
C-3	136.41	NO	YES
C-4	131.74	NO	YES
C-5	130.77	NO	YES
C-6	132.34	NO	NO
C-7	136.72	NO	NO
C-8	132.58	NO	YES
C-9	202.64	NO	YES
C-10	202.04	NO	NO
BM-3	136.30	NO	NO
BM-4	137.44	NO	NO
BM-7	137.24	NO	YES
BM-21	139.03	NO	NO
BM-22	139.25	NO	NO
101	137.51	NO	NO
102	131.55	NO	NO
108	137.11	NO	NO
120	133.28	NO	NO
123	138.33	NO	NO
124	138.33	NO	NO
125	136.33	NO	NO
126	133.41	NO	NO
129	137.13	NO	NO
130	177.60	NO	NO
MM-1	139.24	YES	YES
MM-2	137.00	YES	YES
MM-3	136.51	YES	YES
MM-4	137.31	YES	YES
MM-5	135.21	YES	YES
MM-6	132.18	YES	YES
MM-7	138.56	NO	NO
MM-8	136.85	NO	NO
MM-9	134.78	NO	NO
MM-10	177.89	NO	NO
MM-11	177.65	NO	NO
MM-12	178.37	NO	NO
MM-13	176.72	NO	NO
MM-14	132.89	NO	NO
MM-15	137.32	NO	NO



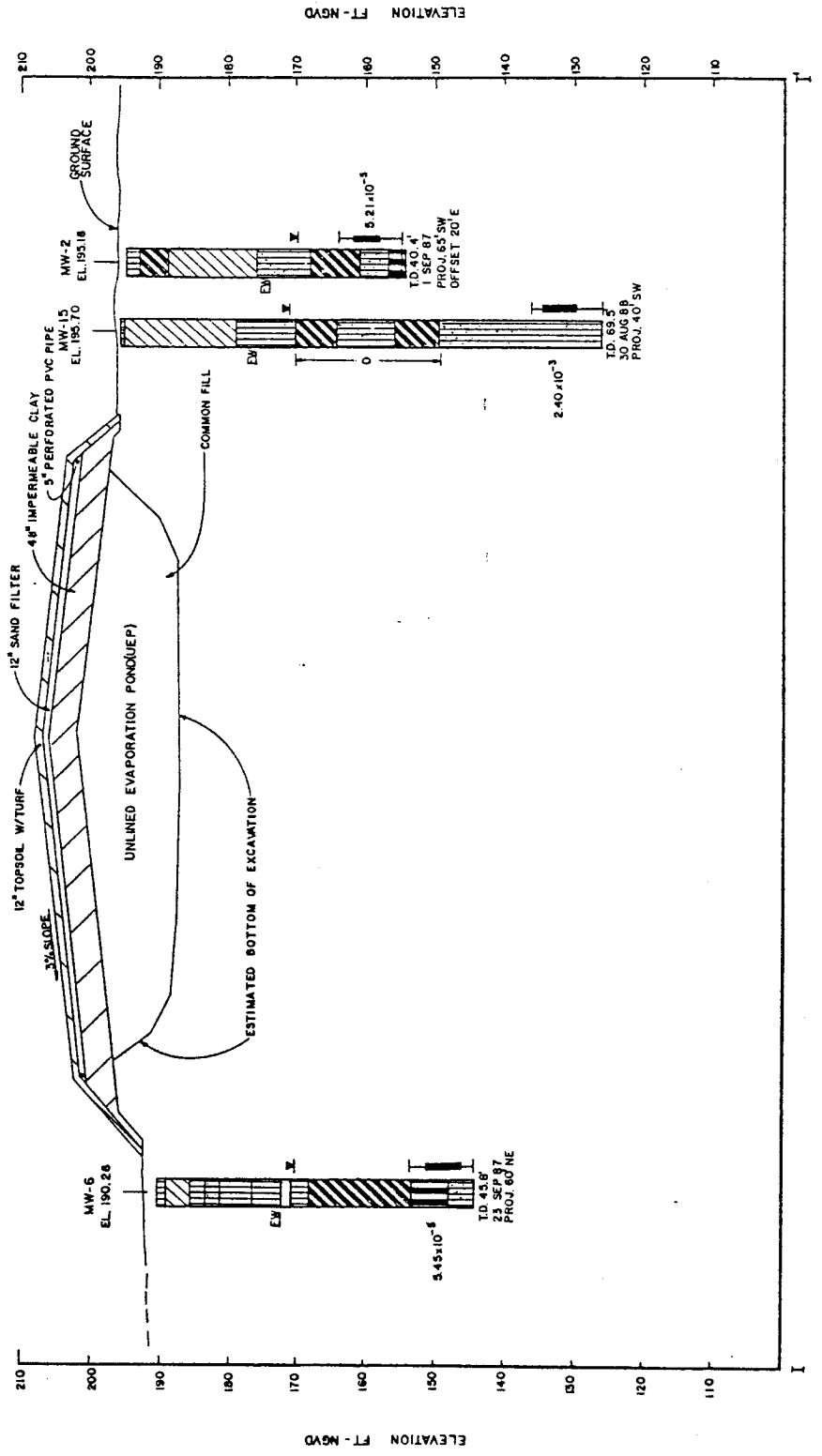
100 AND 1000000 CONCENTRATION LIMITS FOR MONITORING WELLS SAMPLED 10-27 SEPTEMBER 1988	
WELL NUMBER	CONCENTRATION LIMIT (ug/L)
MM-1	100,000
MM-2	1,000,000
MM-3	1,000,000
MM-4	1,000,000
MM-5	1,000,000
MM-6	1,000,000
MM-7	1,000,000
MM-8	1,000,000
MM-9	1,000,000
MM-10	1,000,000
MM-11	1,000,000
MM-12	1,000,000
MM-13	1,000,000
MM-14	1,000,000
MM-15	1,000,000
C-1	1,000,000
C-2	1,000,000
C-3	1,000,000
C-4	1,000,000
C-5	1,000,000
C-6	1,000,000
C-7	1,000,000
C-8	1,000,000
C-9	1,000,000
C-10	1,000,000
C-11	1,000,000
C-12	1,000,000
C-13	1,000,000
C-14	1,000,000
C-15	1,000,000

LEGEND
100 CONCENTRATION LINES OF TRICHLOROETHENE IN GROUND WATER (ug/L)
1000 MONITORING WELL

NOTES
1. SAMPLING PERFORMED 10-27 SEPTEMBER 1988.
2. REFER TO APPENDIX 2 FOR COMPLETE ANALYTICAL DATA.

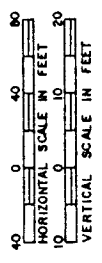
U.S. ARMY ENGINEER DISTRICT, FORT WORTH	
Corps of Engineers	
Longhorn Army Ammunition Plant	
Karnack, Texas	
RCRA Facility Investigation	
ABG and UEP Sites	
Phase I	
Extent of Trichloroethene in Shallow Ground Water	
Submitted by:	Robert C. Behm
Checked by:	Robert C. Behm
Drawn by:	Robert C. Behm
Scale:	1 inch = 400 feet
Sheet No.	29 of 31

002087



NOTES

1. FOR LEGEND, STATIGRAPHIC SYMBOLS, AND GENERAL NOTES, SEE SHEET 18.
2. UEP DETAILS ARE AS SHOWN ALONG THE BASELINE SECTION ON THE CONSTRUCTION AS-BUILT, USACE, FORT WORTH DISTRICT, CONTRACT NO. D4083-83-C-082.
3. FOR BORING LOCATIONS, SEE SHEET 21.



U.S. ARMY ENGINEER DISTRICT, FORT WORTH	
CORPS OF ENGINEERS	
FORT WORTH, TEXAS	
LONGHORN ARMY AMMUNITION PLANT	
KARNACK, TEXAS	
RCRA FACILITY INVESTIGATION	
ABG AND UEP SITES	
PHASE I	
SUBSURFACE PROFILE I-I'	
DESIGNED BY:	D. ELZGERAD
NAME:	J. MURPHY
REVIEWED BY:	R. BEHM
DATE:	30 SEP 87
PROJECT NO.	30 SEP 87
PROJECT NAME	30 SEP 87

002088

13 AND METHYLENE CHLORIDE CONCENTRATIONS IN
MONITORING WELLS DURING 1971 SEPTEMBER 1983

WELL NUMBER

TRICHLOROETHYLENE

METHYLENE CHLORIDE

WELL DEPTH

WELL TYPE

WELL STATUS

WELL LOCATION

WELL OWNER

WELL NOTES

WELL COMMENTS

WELL DATA

WELL ANALYSIS

WELL RESULTS

WELL SUMMARY

WELL CONCLUSION

WELL RECOMMENDATION

WELL ACTION

WELL FOLLOW-UP

WELL REVIEW

WELL REPORT

WELL SIGNATURE

WELL DATE

WELL TIME

WELL LOCATION

WELL OWNER

WELL NOTES

WELL COMMENTS

WELL DATA

WELL ANALYSIS

WELL RESULTS

WELL SUMMARY

WELL CONCLUSION

WELL RECOMMENDATION

WELL ACTION

WELL FOLLOW-UP

WELL REVIEW

WELL REPORT

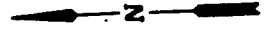
WELL SIGNATURE

WELL DATE

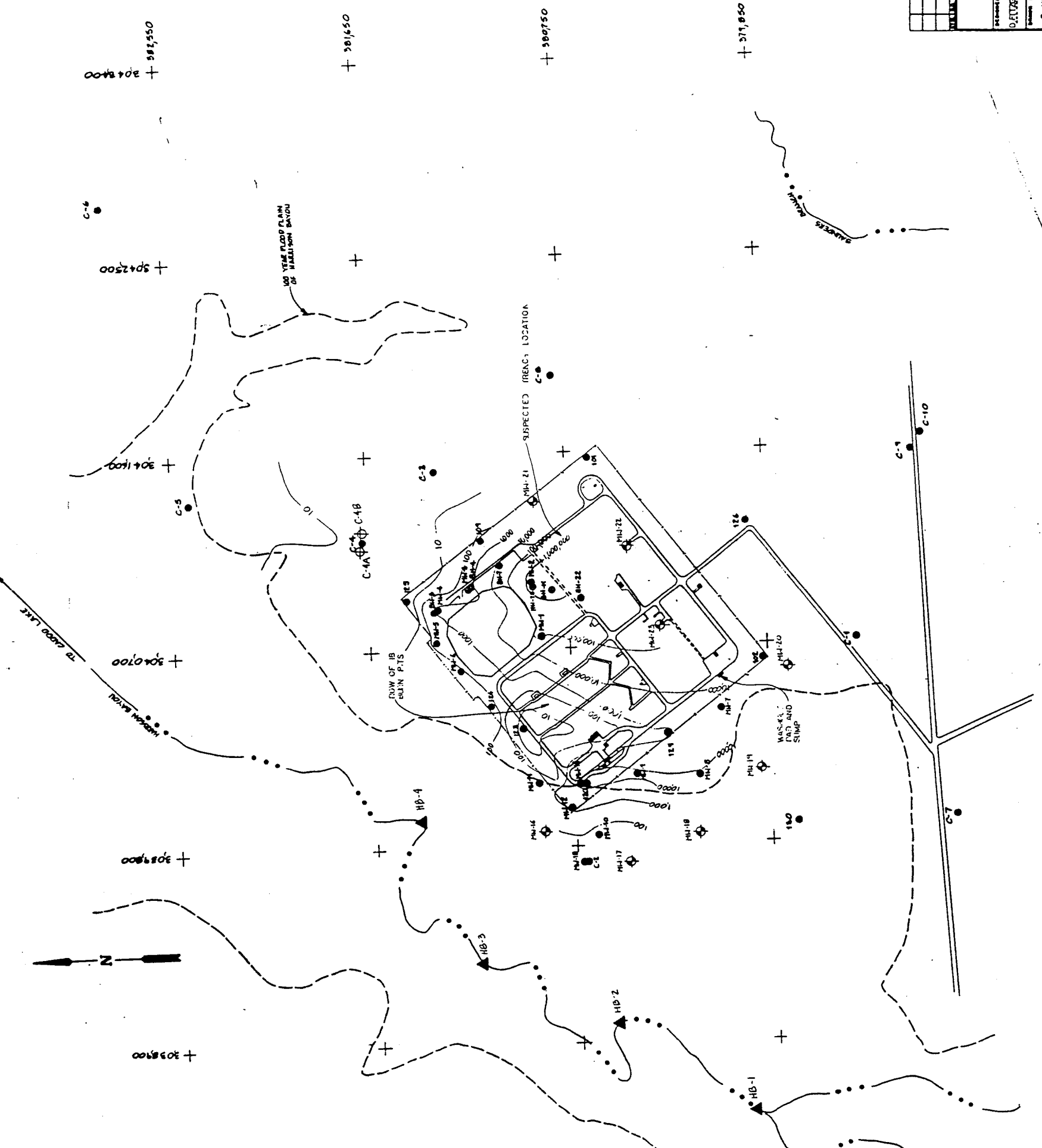
WELL TIME

GROUNDWATER MONITORING WELLS
IN THE
ACTIVE BURNING GROUNDS AREA

WELL NO.	MEAS. PT. ELEVATION	COMP. MON. WELLS	CORRECT ACT. MON. WELLS
C-1	173.80	NO	NO
C-2	178.03	NO	NO
C-3	186.41	NO	YES
C-4	184.74	NO	YES
C-5	180.77	NO	YES
C-6	182.34	NO	NO
C-7	184.78	NO	NO
C-8	184.38	NO	NO
C-9	202.04	NO	YES
C-10	202.04	NO	NO
C-11	186.30	NO	NO
C-12	187.44	NO	NO
C-13	187.24	NO	YES
C-14	188.03	NO	NO
C-15	188.25	NO	NO
C-16	187.41	NO	NO
C-17	187.41	NO	NO
C-18	187.41	NO	NO
C-19	187.41	NO	NO
C-20	187.41	NO	NO
C-21	187.41	NO	NO
C-22	187.41	NO	NO
C-23	187.41	NO	NO
C-24	187.41	NO	NO
C-25	187.41	NO	NO
C-26	187.41	NO	NO
C-27	187.41	NO	NO
C-28	187.41	NO	NO
C-29	187.41	NO	NO
C-30	187.41	NO	NO
C-31	187.41	NO	NO
C-32	187.41	NO	NO
C-33	187.41	NO	NO
C-34	187.41	NO	NO
C-35	187.41	NO	NO
C-36	187.41	NO	NO
C-37	187.41	NO	NO
C-38	187.41	NO	NO
C-39	187.41	NO	NO
C-40	187.41	NO	NO
C-41	187.41	NO	NO
C-42	187.41	NO	NO
C-43	187.41	NO	NO
C-44	187.41	NO	NO
C-45	187.41	NO	NO
C-46	187.41	NO	NO
C-47	187.41	NO	NO
C-48	187.41	NO	NO
C-49	187.41	NO	NO
C-50	187.41	NO	NO
C-51	187.41	NO	NO
C-52	187.41	NO	NO
C-53	187.41	NO	NO
C-54	187.41	NO	NO
C-55	187.41	NO	NO
C-56	187.41	NO	NO
C-57	187.41	NO	NO
C-58	187.41	NO	NO
C-59	187.41	NO	NO
C-60	187.41	NO	NO
C-61	187.41	NO	NO
C-62	187.41	NO	NO
C-63	187.41	NO	NO
C-64	187.41	NO	NO
C-65	187.41	NO	NO
C-66	187.41	NO	NO
C-67	187.41	NO	NO
C-68	187.41	NO	NO
C-69	187.41	NO	NO
C-70	187.41	NO	NO
C-71	187.41	NO	NO
C-72	187.41	NO	NO
C-73	187.41	NO	NO
C-74	187.41	NO	NO
C-75	187.41	NO	NO
C-76	187.41	NO	NO
C-77	187.41	NO	NO
C-78	187.41	NO	NO
C-79	187.41	NO	NO
C-80	187.41	NO	NO
C-81	187.41	NO	NO
C-82	187.41	NO	NO
C-83	187.41	NO	NO
C-84	187.41	NO	NO
C-85	187.41	NO	NO
C-86	187.41	NO	NO
C-87	187.41	NO	NO
C-88	187.41	NO	NO
C-89	187.41	NO	NO
C-90	187.41	NO	NO
C-91	187.41	NO	NO
C-92	187.41	NO	NO
C-93	187.41	NO	NO
C-94	187.41	NO	NO
C-95	187.41	NO	NO
C-96	187.41	NO	NO
C-97	187.41	NO	NO
C-98	187.41	NO	NO
C-99	187.41	NO	NO
C-100	187.41	NO	NO



HB-5
SEE NOTE 4.



LEGEND

- 100 ISO CONCENTRATION LINES OF TRICHLOROETHYLENE IN GROUND WATER
- MONITORING WELL
- PROPOSED MONITORING WELL LOCATION
- PROPOSED SURFACE WATER SAMPLING LOCATION

NOTES

1. SAMPLING PERFORMED 8-27 SEPTEMBER 1983.
2. REFER TO APPENDIX 2 FOR COMPLETE ANALYTICAL DATA.
3. FOR PNEUMETRIC SURFACE MAP, SEE SHEET 20.
4. HB-5 IS LOCATED APPROXIMATELY 3000 FEET DOWNSTREAM OF HB-4.

U.S. ARMY ENGINEER DISTRICT, FORT WORTH	
CORPS OF ENGINEERS	
LONGHORN ARMY AMMUNITION PLANT	
KANSAS, TEXAS	
RCRA FACILITY INVESTIGATION	
ABG AND UEP SITES	
PHASE I	
PROPOSED PHASE II	
SAMPLING & MONITORING WELL LOCATIONS	
PROJECT NO.	100
CONTRACT NO.	100
DESIGN NUMBER	31 OF 31
DATE	31
ROBERT C. BEHM	