LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS

ADMINISTRATIVE RECORD

Volume 11 of 19

2010

Bate Stamp Numbers 00091097 – 00091772

Prepared for

Department of the Army Longhorn Army Ammunition Plant

1976 - 2010

LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS ADMINISTRATIVE RECORD – CHRONOLOGICAL INDEX

VOLUME 11 of 19

2010

A. Title: Report – (Continued) Final Feasibility Study, LHAAP-29, Former TNT

Production Area, Group 2, Longhorn Army Ammunition Plant, Karnack,

Texas, April 2010

Author(s): US Army Corps of Engineers

Recipient: USEPA

Date: April 30, 2010

Bate Stamp: 00091097 - 00091772

FINAL FEASIBILITY STUDY LHAAP-29, FORMER TNT PRODUCTION AREA, GROUP 2 LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS







APRIL 2010



Date: <u>April 30, 2010</u> Project No.:<u>117591</u>

Phone: (281) 531-3100/Fax: (281) 531-3136

TRANSMITTAL LETTER:

Mr.	Aaron William	ns				
s: US	Army Corps of	f Engineers - T	`ulsa	-		
CES	WT-PP-M			=		
1645	South 101st I	East Ave		_		
Tulsa	a, Oklahoma	74128		-		
			AAP-29			
Cont	ract No. W912	2QR-04-D-002	27/DS02	_		
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CC: Distribution List:

Mr. J. Lambert- USACE, Tulsa (sent to A. Williams for distribution)

Mr. M. Mechenes – USAEC

Ms. Rose Zeiler – BRAC-LHAAP

Mr. S. Tzhone – EPA Region 6 (2)

Ms. F. Duke-TCEQ, Austin (2)

Mr. D. Vodak-TCEQ, Tyler

Mr. P. Bruckwicki- U.S. Fish and Wildlife Service



DEPARTMENT OF THE ARMY LONGHORN ARMY AMMUNITION PLANT POST OFFICE BOX 220 RATCLIFF, AR 72951

April 30, 2010

DAIM-ODB-LO

Ms. Fay Duke (MC-136) SSDAT/Superfund Section Remediation Division Texas Commission on Environmental Quality 12100 Park 35 Circle, Bldg D Austin, TX 78753

Re: Final Feasibility Study, LHAAP-29, Former TNT Production Area, Group 2, Longhorn Army Ammunition Plant, Karnack, Texas, April 2010

SUP 126

Dear Ms. Duke,

The above-referenced document is being transmitted to you for your files. The document has been prepared by Shaw Environmental, Inc. (Shaw) on behalf of the Army as part of Shaw's performance based contract for the facility.

The point of contact for this action is the undersigned. I ask that Praveen Srivastav, Shaw's Project Manager be copied on any communications related to the project. I may be contacted at 479-635-0110, or by email at rose.zeiler@us.army.mil.

Sincerely,

Rose M. Zeiler, Ph.D. Longhorn AAP Site Manager

RoseM.Zjiler

Copies furnished:

S. Tzhone, USEPA Region 6, Dallas, TX

D. Vodak, TCEQ, Tyler, TX

P. Bruckwicki, Caddo Lake NWR, TX

J. Lambert, USACE, Tulsa District, OK

M. Mechenes, USAEC, MD

A. Williams, USACE, Tulsa District, OK

P. Srivastav, Shaw, Houston, TX (for project files)



DEPARTMENT OF THE ARMY LONGHORN ARMY AMMUNITION PLANT POST OFFICE BOX 220 RATCLIFF, AR 72951

April 30, 2010

DAIM-ODB-LO

Mr. Stephen Tzhone US Environmental Protection Agency Superfund Division (6SF-AT) 1445 Ross Avenue Dallas, TX 75202-2733

Re: Final Feasibility Study, LHAAP-29, Former TNT Production Area, Group 2, Longhorn Army Ammunition Plant, Karnack, Texas, April 2010

Dear Mr. Tzhone,

The above-referenced document is being transmitted to you for your files. The document has been prepared by Shaw Environmental, Inc. (Shaw) on behalf of the Army as part of Shaw's performance based contract for the facility.

The point of contact for this action is the undersigned. I ask that Praveen Srivastav, Shaw's Project Manager, be copied on any communications related to the project. I may be contacted at 479-635-0110, or by email at rose.zeiler@us.army.mil.

Sincerely.

Rose M. Zeiler, Ph.D. Longhorn AAP Site Manager

RoseM.Zjiler

Copies furnished:

F. Duke, TCEQ, Austin, TX

D. Vodak, TCEQ, Tyler, TX

P. Bruckwicki, Caddo Lake NWR, TX

J. Lambert, USACE, Tulsa District, OK

A. Williams, USACE, Tulsa District, OK

M. Mechenes, USAEC, MD

P. Srivastav, Shaw – Houston, TX (for project files)

From: Tzhone.Stephen@epamail.epa.gov [mailto:Tzhone.Stephen@epamail.epa.gov]

Sent: Friday, April 30, 2010 9:01 AM **To:** Zeiler, Rose Ms CIV USA OSA

Cc: Srivastav, Praveen; Jones, Greg N; Lambert, John R SWT; Everett, Kay; Watson, Susan; Fay Duke;

Burton.Terry@epamail.epa.gov; Forsythe.Barry@epamail.epa.gov; Williams, Aaron K SWT **Subject:** Longhorn: EPA Review of LHAAP-29 DF FS Track Changes and RTC Table for Review

Hi Rose:

The EPA has completed review of the Army *LHAAP-29 DF FS Track Changes and RTC Table for Review* (email 4/29/2010) and agrees with the submittal. Please proceed with finalization of the LHAAP-29 Feasibility Study.

Thanks,

Stephen L. Tzhone Superfund Remedial Project Manager USEPA Region 6 (6SF-RA) 214.665.8409 tzhone.stephen@epa.gov

From: Fay Duke [mailto:FDUKE@tceq.state.tx.us]

Sent: Thursday, April 29, 2010 3:04 PM **To:** Srivastav, Praveen; Tzhone, Stephen

Cc: Everett, Kay; Jones, Greg N; Lambert, John R SWT; Watson, Susan; Wililams, Aaron; Zeiler, Rose Ms

CIV USA OSA

Subject: Re: FW: LHAAP-29 DF FS Track Changes and RTC Table for Review

Rose/Praveen,

The TCEQ has completed its review of the Track Changes of the Draft Final Feasibility Study. We concur with the changes with one exception. However, it is our opinion that the issuance of the final FS need not be held up. The exception was due to TCEQ review oversight by not providing the comment regarding the shallow groundwater cleanup level for perchlorate at site LHAAP-29. As we have expressed in previous FS reports and proposed plans, because the groundwater at site LHAAP-29 has a potential to discharge to surface water, the residential MSC for groundwater must be the cleanup level for the shallow groundwater. We believe that this can be made clear in the proposed plan and finalize in the ROD and therefore, the final FS report need not be revised.

Please let me know if you should have any questions regarding this matter.

Thanks, fd

Fay Duke (MC-136) Remediation Division, TCEQ PO Box 13087 Austin, Texas 78711-3087 512-239-2443 512-239-2450 (Fax)

- Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 Commentor Agrees (A) with response, or Does not Agree (D) with response.

chromium from well proved over previous acceptable to EPA.	C No	U.S. Environmental Protection Agency loted. Section 2.3.2 – Groundwater, dditional Sampling 2008 and 2009, eplace the 4 th , 5 th and 7 th paragraphs with the following:	A D	Increasing concentrations should require additional monitoring, not less. If the	COCs that have been confirmed to have concentrations above MCL. MSC or risk-	С	Nickel, arsenic, and mercury will	
chromium from well proved over previous acceptable to EPA. ear to EPA how positive for nickel, mercury, and as can be discarded. For s given are not	C No	oted. Section 2.3.2 – Groundwater, dditional Sampling 2008 and 2009, eplace the 4 th , 5 th and 7 th paragraphs	A D			С	Nickel, arsenic, and mercury will	
proved over previous acceptable to EPA. ear to EPA how positive for nickel, mercury, and as can be discarded. For s given are not	C In Ac re wi	n Section 2.3.2 – Groundwater, dditional Sampling 2008 and 2009, eplace the 4 th , 5 th and 7 th paragraphs	A D			С	Nickel, arsenic, and mercury will	
for nickel, mercury, and see can be discarded. For s given are not	Ac re wi	dditional Sampling 2008 and 2009, eplace the 4 th , 5 th and 7 th paragraphs	D			С	Nickel, arsenic, and mercury will	l .
		"Of the 80 nickel samples collected since 1993, nickel was detected above the GW-Ind of 2,000 μg/L in only 3 samples. Prior to 2008, the nickel concentration in only one well had an associated HQ greater than 1 (8,400 μg/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 μg/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 μg/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 μg/L in May 1995 and 600 μg/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (i.e., above the MCL of 100 μg/L for chromium), indicating that corrosion of the stainless steel well material is a likely source of the high nickel concentrations. Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 10 μg/L in only 7 samples. Four of the elevated results (115, 29WW16, 29WW20, and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were		sample was performed incorrectly or is otherwise not representative of the subsurface, then the sample should be redone properly. Currently, it could be argued that the existing remedy is now allowing metals to be released to the environment, and thus is not protective. EPA recommends retaining nickel, arsenic, and mercury, given that their recent concentrations could also support a contention of increasing contamination. If the metals are not an issue, then future monitoring will verify that, and the sampling protocol can be revisited at a later time.	based standards must be retained for remedial action except in cases where samples taken recently have shown the concentrations are now below the cleanup levels. If the sample result that exceeds cleanup level is believed not to be a representative groundwater samples (i.e., turbidity), than a representative sample should be collected and re-analyzed. Additionally, With in-situ chemical oxidation as the potential remedy at this site, metals should be monitored to ensure metals are not mobilized as a result of the pH change.		be added to the COC Table 2-5 with footnotes that they are isolated COCs limited to certain wells defined in Tables 2-2 and 2-3 and in Section 2.3.2. The following will be revised in Section 2.3.2 response: Nickel – last sentence will be replaced with the following: "Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a site-wide COC and will be considered a COC limited to shallow groundwater zone wells 29WW07 and 29WW11." Arsenic – last sentence will be replaced with the following: "It is concluded that arsenic is not considered a site-wide COC since the arsenic detections have been sporadic, are not repeatable, and can be attributed to sampling methodology or natural occurrence in the deep zone. Thus, arsenic is an isolated COC limited to shallow groundwater zone wells 116, 29WW08, and 29WW25." Mercury- last sentence will be replaced with the following: "Thus, mercury is not considered a site-wide COC and will be an isolated COC limited to the shallow groundwater zone Well 118." In Section 2.4.2, the following will be added to the shallow water groundwater discussion, paragraph 5: "Three metals,	
			(8,400 μg/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 μg/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 μg/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 μg/L in May 1995 and 600 μg/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (i.e., above the MCL of 100 μg/L for chromium), indicating that corrosion of the stainless steel well material is a likely source of the high nickel concentrations. Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 10 μg/L in only 7 samples. Four of the elevated results (115, 29WW20, and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59	(8,400 μg/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 μg/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 μg/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 μg/L in May 1995 and 600 μg/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (i.e., above the MCL of 100 μg/L for chromium), indicating that corrosion of the stainless steel well material is a likely source of the high nickel concentrations. Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 10 μg/L in only 7 samples. Four of the elevated results (115, 29WW16, 29WW20, and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59	(8.400 μg/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 μg/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 μg/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 μg/L in May 1995 and 600 μg/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations in individual vells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (i.e., above the MCL of 100 μg/L for chromium), indicating that corrosion of the stainless steel well material is all likely source of the high nickel concentrations. Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 10 μg/L in only 7 samples. Four of the elevated crocuncentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59	(8.400 g/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 g/L. In 2008, the highest nickled concentration was found at 28WW07 with 3,190 g/L. and would have an HC greater than 1.0. Previous results for 29WW07 were less than 40 g/L in May 1995 and 600 g/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (e., above the MCL of 100 g/L for chromium), indiceting that corrosion of the stainless steel wells, nickel detections are isolated in each event, and appear to be related to cornosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 100 g/L in only 7 samples. Four of the elevated cresults (115, 29WW20, and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations concentrations could be a result of sampling. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59	(8,400 µg/L at 29WW/11 in April 1995). The 2006 result from this well had a concentration of 40 µg/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 µg/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 µg/L in May 1996 and 600 µg/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations (Le, above the MCL of 100 µg/L for chromium), indicating that corrosion of the stainless steel well material is a likely source of the high nickel concentrations. Since the nickel detections are isolated in each event, and appear to be related to corrosion of the stainless steel wells, nickel is not considered a COC." "Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 101 µg/L in only 7 samples. Four of the elevated results (115, 29WW16, 29WW02) and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59	is a concentration of 40 µg/L. In 2004 best in the picked in the concentration was found at 29WW07 with 3,190 µg/L and would have an Holpest nicket concentration was found at 29WW07 with 3,190 µg/L and would have an Holpest nicket concentration in was found at 29WW07 with 3,190 µg/L and would have an Holpest nicket concentration in individual wells have not been repeatable or consistently detected. The isolated high nicket concentrations at 29WW07 and 29WW11 coincided with elevated chromitum concentrations (individual wells have not been repeatable or consistently detected. The isolated high nicket concentrations at 29WW07 and 29WW11 coincided with elevated chromitum concentrations (individual wells have not been repeatable or consistently detected. The salaness seed well material is a likely concentrations. Since he nicket detections are isolated in each event, and appear to be related to sampling methodology or natural network and proposed properties of the stainless steed well material is a likely concentrations. Since he nicket detections are isolated in each event, and appear to be related to sampling methodology or natural network and proposed properties of the stainless steed well material is a likely or natural network and proposed to the proposed properties of the stainless steed well material is a likely or natural occurrence in the deep zone. Thus, arsenic is an isolated concentration concerned and properties of the proposed properties of the stainless steed well material is a likely or natural network to the properties of the stainless steed well material is a likely or natural network to the proposed properties of the stainless steed well material to sampling methodology or natural network to the properties of the properties of the properties of the stainless steed well material is a likely or natural network to the properties of the prope

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).

 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

			2. Commentor Agrees (A) with	respons	se, or Does not Agree (D) with response.					
Comment Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	EPA Comments to RTCs	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to EPA/TCEQ Comments on the RTCs	A or D ²
				44 μg/L at intermediate well 29WW16). The wells were redeveloped prior to sampling. In 2008, only 3 samples (116, 29WW08, and 29WW25) had arsenic concentrations above the MCL. The well with the highest concentration (29WW25) had high turbidity (237.1 NTUs) and was noted to be reddish brown. This sample result is questionable due to the high turbidity. The next highest sample (116) was qualified as an estimated value since the field duplicate relative percent difference criteria was exceeded. It should also be noted that the aluminum concentration was high at 430 μg/L. This sample result is also questionable due to QC issues. The third sample from deep well 29WW08 had arsenic concentrations of 40.1 μg/L with a high aluminum concentration of 713 μg/L. The high aluminum concentration in the same sample indicates that the arsenic may be naturally occurring. Additionally, this deep well is clustered with a shallow well, 29WW07, and intermediate well, 29WW14, neither of which has had an arsenic detection. Thus, the contamination is not from vertical migration. It is concluded that arsenic is not considered a COC since the arsenic detections have been sporadic, are not repeatable, and can be attributed to sampling methodology or natural occurrence in the deep zone." "Of the 80 mercury samples collected since 1993, mercury has been detected only twice, both in shallow zone Well 118. The latest round from 2008 detected mercury at 6.1 μg/L in Well 118 – higher than the previous result of 3 μg/L in 1993. The MCL for mercury is 2 μg/L. In 1995 and 1998, mercury was not detected (less than detection limit of 0.2 μg/L) in Well 118. Mercury is not detected in any other well, and the detections are intermittent and appear to be isolated. Well 118 is located along the southern edge of the site, away from active industrial areas that are possible sources. Mercury was detected at low concentrations in					up goals in certain wells and do not define a plume in the groundwater. These metals have been included as COCs." Additionally, the notes on Tables 2-2 and 2-3 will be revised to note that arsenic and nickel are isolated COCs in certain shallow groundwater zone wells and are not site wide. The list of analytes to be monitored during the remedy (including metals potentially mobilized by in situ oxidation) will be addressed in the remedial design. The alternatives will be revised to include groundwater monitoring for these analytes for the wells defined in Section 2.3.2.	

- Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 Commentor Agrees (A) with response, or Does not Agree (D) with response.

		1		r	2. Commentor Agrees (A) with	respons	e, or Does not Agree (D) with response.		·		
Comment #	Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	EPA Comments to RTCs	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to EPA/TCEQ Comments on the RTCs	A or D ²
"		raragraphi		COLX	three soil samples (29SB04, 29SB12 and 29SB55) and one sediment sample (29SD13), but all of these locations are more than 1,500 feet from Well 118. Sample results from wells located between the soil sample locations and Well 118 did not detect mercury. Soil and sediment samples near Well 118 (29SD08, 29SD09, 29SB71, and 29SB72) did not show any detectable mercury, so the mercury in groundwater is not related to the mercury in soil. Additionally, the Final Baseline Human Health and Screening Ecological Risk Assessment for Group 2 Sites (Jacobs, 2002) calculated a hazard index (HI) of 0.098 for mercury in groundwater using the maximum mercury value of 3 µg/L. Adjusting this HI for the new higher maximum of 6.1 µg/L gives an HI of 0.20, still less than 1.0. Thus, mercury is not considered a COC in groundwater."			April 14, 2010 E-mail from Faye Duke to Rose Zeiler: We cannot concur with the conclusion that the three metals: arsenic, mercury, and nickel are not considered site wide COC and will only be monitored in wells where these metal concentrations have exceeded the MCLs. We believe there are insufficient data to conclude that these metal contamination is limited in these wells currently and have not traveled since the last sampling event. We recommend that the monitoring locations and frequencies be assessed and determined during the remedial design after additional samples have been collected.		While we do not believe these metals are site-wide, we do agree that this can be further addressed during remedial design (RD). Therefore, the text will be modified to indicate that the extent of these inorganic COCs will be assessed at wells site-wide during the RD. Also, the RD will present a plan for subsequent monitoring locations and frequencies based on the latest assessment data in conjunction with historical groundwater monitoring results for inorganics at the site.	
3	2-9	Section 2.4.2 3 rd para	The phrase "concentrations less that the EPC" should replace "that" with "than".	С	Text will be revised.	A					
4			Is the kinetics curves information given in Appendix C solely used to extrapolate future kinetics and determine whether the remedy (post excavation/oxidation) is working appropriately?	С	The kinetic curves were used to extrapolate future kinetics. Future results will serve to determine whether or not the chosen remedy is working appropriately. The curves will be reevaluated after additional MNA data are obtained.	А					
Reviewer: 3	-	Tzhone, Superf	und Remedial Project Manager, USEPA Regior	1 6 (6SF-R	RA), U.S. Environmental Protection Agency						
5		General	Please modify statements such as: "MNA ensures that ground water contamination is localized" or "MNA prevents human exposures". Allowing the natural healing processes of nature to work and keeping track of that progress is not the same as "ensuring" or "preventing".	С	Page ES-3 is the only place this phrasing appears. Executive Summary, Alternative 2 bullet, MNA sentence, will be revised as follows: "Implementation of MNA in both the shallow and intermediate zones would ensure that groundwater contamination concentrations and plume stability/size are monitored as	А	Note: new language is acceptable.				

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
- 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Comment #	Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	EPA Comments to RTCs	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to EPA/TCEQ Comments on the RTCs	A or D ²
					the plume degrades over time."						
					Executive Summary, Alternative 3 bullet, MNA sentence, will be revised as follows:						
					"Implementation of MNA in both the shallow and intermediate zones would ensure that groundwater contamination concentrations and plume stability/size are monitored as the plume degrades over time."						
					Section 6.3.2.3.2, last sentence of 4 th paragraph will be revised as follows:						
					"In both zones, long-term success will be verified by monitoring the progress of natural attenuation."						
	•	•	fund Remedial Project Manager, USEPA Region Is presented April 28-29, 2009:	6 (6SF-F	RA), U.S. Environmental Protection Agency						
1			The screening data for anaerobic biodegradation and the geologic crosssections are helpful and appreciated.	С	Noted.	Α					
2	5-6	5.2.2.3	The criterion for ending the oxidation/extraction phase remains unclear. Are all MC expected to be remediated before the oxidation is completed, or is there a set figure which is expected to be attained?	С	Based on the treatability study (Appendix B), the MC concentrations will be reduced by approximately 75% through heat activated persulfate. MNA will be initiated after the formation has recovered from the oxidation treatment activities. Also, see 9B response.	Α	Note: EPA agrees with Army that 75% reduction in Methylene Chloride concentrations for this site is sufficient to allow continued remediation by MNA.				
3		6.5	Discussed eliminating recommendation section.	С	The recommendation section will be deleted.	Α					

Comment #	Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or D ²
	•	Remediation D	ivision, TCEQ ria email at 6:40 p.m., RE: TCEQ Comments on LF	HAAP-17 I	-s					
1		Table 3-3	Please note that comment No. 5 regarding action specific ARARs should also be considered a comment for LHAAP-29 FS. Comment 5 for LHAAP-17 FS - Section 3.2.4.1.2 (Waste and Disposal Activities) – It states that requirements for managing, storing and disposal will be conducted in accordance with ARAR listed in Table 3-3. However, we believe that the action specific ARARs discussion and requirements listed in Table 3-3		CERCLA section 121(d) requires on-site Superfund remedial actions to comply with Federal, and more stringent State, environmental requirements that are determined to be applicable or relevant and appropriate requirements (ARARs); thus, even though requirements for off-site actions are not ARARs, they must be complied with. The following will be added to the second paragraph of Section 3.2.4.1.2:	D	Despite recent clarifications from EPA, we believe that action specific ARARs table is still incomplete. 1. With in-situ chemical oxidation as one of the alternative, why is federal and state requirements for UIC not listed as a potential ARARs?	С	The UIC is not listed as a potential action specific ARAR since it is only an administrative requirement. The other requirements for drilling the wells are already included in the action specific ARARs. Since Longhorn is a CERCLA site, a permit for a Class V injection well would not be required. The Army and USEPA are currently discussing the	
			is incomplete. The discussion in this section is focus on the AOC concept, which applies mainly		"Other requirements for hazardous waste such as manifesting for off-site disposal (40 CFR 262.20) and planning/implementing off-site		Please explain the rational for deleting Table 3-2, which addresses the location- specific ARARs?		location-specific ARARs. For purposes of moving forward with the FS, the location-specific ARARs will	

- Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 Commentor Agrees (A) with response, or Does not Agree (D) with response.

Comment #	Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or
			to on-site disposal. Please note the waste management and disposal requirements under RCRA are usually "appropriate and relevant" requirements for on-site disposal but these requirements are typically "applicable" for off-site disposal. Additionally, certain requirements such as procedures for planning and implementing off-site response action (40 CFR 300.440) are applicable to CERCLA response action waste. Please revise.		response action (40 CFR 300.440) will be complied with even though they are not considered an ARAR." Additionally - the ARAR discussion will be revised to address only environmental laws, and the potential location-specific Table 3-2 will be deleted; and the USEPA MCLs/TCEQ MSCs will be used for groundwater cleanup and the Texas Safe Drinking Water Act will be removed from the chemical-specific ARAR discussion.		April 14, 2010 E-mail from Faye Duke to Rose Zeiler: We concur that CERCLA permit exemption means that administrative requirements are exempt. We disagreed with your statement that TAC chapter 331 contains only administrative requirements. We believe that at a minimum, TAC chapter 331 Subchapter H must be included as action specific ARARs. Please also keep in mind that to ensure that the design meets the substantive requirements, the review and evaluation is deferred to the staff from the TCEQ UIC program for the review of the design documents. Please let me know if you should have any questions or concerns regarding these comments. If the final LHAAP-29 FS incorporates these changes, please proceed with the issuance of the final FS.		be retained as "potential" ARARs. Based on the outcome of these discussions, the appropriate ARARs will be included in the ROD. Text in Section 3.2.4 and Table 3-3 will be modified to indicate that substantive requirements of TAC Chapter 331 Subchapter H that are relevant and appropriate to installation of the injection points will be included as potential action-specific ARARs.	
Comments f	from the A	April 2009 mee	<u> </u>			1				
			readings versus depth. Reading dropped notice readings are inconclusive given the method of driproof that the contamination was not in the Upper rather than wait. P. Srivastav said it would take was some discussion of the best location for approximately 50 feet downgradient (northeast).	eably after Illing (mud l er Deep zo at least 6 v the new of 29WW4 !. C. Sanc	WW40 was examined, specifically with regard to PID the intermediate zone, but the group agreed that the rotary). F. Duke said that the TCEQ needed conclusive one. Shaw and Army preferred to install this well now weeks to install the well and get sample results. There well. It was decided that the well will be installed to. Data from this well will be evaluated to determine if thez asked about the earlier TCEQ concern about the ce trends within the zone would be tracked.					
		The new well (29WW41) was installed, and a follow-up email was sent location, boring log, groundwater sampling form, and lab results. incorporated into the Feasibility Study as follows in Comments 1A thro			results. This information relating to 29WW40 will be					
1A		Table 1-1			The following bullet will be added under Additional Investigations: Installed new well, 29WW41, in the Upper Deep Zone and sampled the well for VOCs (Appendix D).					

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
- 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

				Commentor Agrees (A) with response, or Do	es not A	igree (D) with response.	ı		-
Comment #	Page Section/ Paragraph	Comment	C, D ¹ , E or X	Response	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or D ²
2A	1.3		v v ii t e s	New next-to-last paragraph will be added as follows: "In June 2009, one new monitoring well (29WW41) was installed and sampled for VOCs to determine whether groundwater in the upper deep zone immediately below the highest MC concentration in the intermediate zone (at 29WW16) showed any evidence of contamination. Well 29WW41 was screened at a depth of 102.5 to 117.5 feet bgs. A groundwater sample was collected for VOC analysis."		The text should include the rationale for sampling only VOCs.	С	The following sentence will be added: "This deeper well was installed to evaluate the potential downward migration of contaminants in the intermediate zone. Only VOCs have been identified as COCs in the intermediate zone, and thus the sample was analyzed for VOCs."	
ЗА	2.3.2			The following will be added as a new 11 th paragraph (before the paragraph beginning with " Tables 2-2 and 2-3)":					
				"A sample was collected from the newly installed well, 29WW41, in the upper deep zone and analyzed for VOCs, which were not detected in the sample. Therefore, groundwater in the upper deep zone is not affected by VOCs."					
			r	The second sentence of the 12 th paragraph will be revised as follows: " Appendix D contains the table of the results and analytical data reports from the October 2008, January 2009, and June 2009 sampling events."					
4A	2.4.3		5	A new last paragraph will be added as follows: "As demonstrated by previous sample results and sampling of new monitoring well 29WW41 in June 2009, the deep groundwater zone is not affected at LHAAP-29."					
5A	Figures 1-6, 1-7, 2-2, 2-3, and 2-4			29WW41 will be added as a deep well.					
6A	Appendix D		7	The title of Appendix D will be revised as follows:					
				"Summary Table, Field Sheets, Well Log (29WW41), and Analytical Data Reports (October 2008, January 2009, and June 2009)"					
The following	ng are in response to ac	ditional comments from the Army on May 27, 200	009						
1B		Your response for LHAAP-29 that concentrations above MSCs in the cooling and waste lines will be immobilized by plugging the lines does not address Army's concern for the eventual leaching of the contamination via vertical percolation after the pipes have degraded. Shaw's response is also inconsistent with the response provided to Carlos Sanchez at the on-board review meeting to address Carlos's similar concern in leaving the contamination in the lines. The high concentrations in the lines need to be properly addressed.		Even though the plugging of the waste lines was discussed during the April 27-28, 2009 meeting, the proposed remedial action has been modified depending upon the type of the line and its history, as discussed below. A further review of historical information revealed that the wooden line was clear flushed, and the RCRA Facility Assessment recommended no further action for the wooden line. Investigations noted that the line was in poor condition, but analytical results for soil samples collected near the line did not indicate any contamination from the wooden pipeline. Thus, no further action will be proposed for the deteriorated wooden line.		TCEQ has a few questions and concerns regarding the new approach. 1. Were confirmation samples taken after the "clear flush?" What method was utilized to visually inspect the inside of the line? 2. We are concern that the decision making for the wooden line is depending upon the RFA. I spoke to my colleague in the RCRA program regarding the RFA and RFI process. It is my understanding that the RFA process is solely based on visual inspection. It is very typical that additional sample collection or a full-blown RFI is required even if the RFA recommends no		1. Unknown. 2. Soil samples were collected and results indicated that explosive levels in the soil did not exceed either the SAI-ind or the GWP-Ind. See revised Table 2-5. 3. There is only one transite pipe at the site and it is buried underground for the most part, except near the former pump location. As part of the remedial design, the line will be surveyed for deed recordation purposes and all exposed areas will be buried with at least 2 feet of soil. 4. The site-specific MSC and SAM modelling will be	

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			Some points within the transite line have been reported to contain a thick viscous semi-solid residue in the bottom. Material from within the line was tested by Shaw and exceeds both the GWP-Ind and SAI-Ind. The transite lines will be flushed with water to remove the residue. The rinsate wate will be containerized, transported and treated at the on-site wastewater treatment plant or disposed of an off-site facility based on analytical results for explosives. In the manholes of the gravity feed portion of the cooling water lines, explosives were detected in the solid residue and water at concentrations above the GWP-Ind and the GW-Ind, respectively. SAM modeling was conducted to estimate the potential impact of the solid residue remaining in the manholes to the groundwater if the line degraded in the future. The SAM modeling indicated that there would not be an impact from the solid residue in the manholes. The manholes should be low spots in the lines where solid residue would collect and minimal solid residue is expected to be found in the actual lines between the manholes. To determine it there is contaminated solid residue in the lines, field staff will attempt to collect solid residue samples during the remedial action from within the lines between the manholes with GWP-Ind exceedances Where there is sufficient residue for such samples to be collected, they will be analyzed to determine it he residue is above the proposed cleanup levels (calculated site-specific medium-specific concentration [MSC] by SAM modeling). If there is no measurable amount of solid residue in the lines, no action will be taken. If there is a measurable amount of solid residue in the lines, to measurable amount of solid residue in the lines, to measurable amount of solid residue in the lines, but explosives are detected below the GWP-Ind or site-specific MSC, no action will be taken. If solid residue concentrations are found to be above the proposed cleanup levels in the lines (GWP-Ind or site-specific MSC), the affected segment of		further action. Please also note that the RFA recommendation is made based on the conditions of the line ("structurally sound and bedded securely") at the time of the inspection. 3. Please note that transite pipes are considered a category II non-friable asbestos-containing material under the TCEQ rules, as such, must be managed so asbestos materials are not release when the pipes deteriorate. Please clarify whether these pipes are currently embedded or exposed. 4. We are concerned and question the applicability of using a calculated site specific MSC to determine the management method for the waste residual left in the pipes. Please note that the risk reduction standard No. 3 are typically applicable only for to contaminated media (e.g., soil) and not waste. The residuals are"waste-like" and therefore the residual should be classified in accordance with TAC 335 Subchaper R and the TCEQ guideline for the classification of industrial and hazardous waste. Waste must be managed in accordance with the substantive requirements of 30 TAC Subchapter A, B, C, E, and/or F. We believe that it is appropriate to leave the residual in place only if the waste residual is classified as nonhazardous; the concentrations of constituents are below Standard No. 2 MSCs for soil and the leachate is below groundwater protection standards. However, the location of the abandon pipe must be deed recorded.		removed. Text and table has been revised as indicated in the track-changed text attached to these RTCs. Please note that the cooling water lines are made of vitrified clay pipes. There are two cooling water lines (north and south). Historically, there has been very little residue in the cooling water lines as observed in the manholes. An attempt will be made to sample and analyze the residue and water in the cooling water lines as part of the RD phase. If there is not enough residue volume to sample or the concentrations in the sample are less than the GW-Ind (water) or GWP-Ind (solid) and the residue is nonhazardous, the pipe will be plugged and abandoned. No solid residue or liquid will be left in the pipe if the explosive constituents exceed the GWP-Ind (residue), the GW-Ind (water) or the solid or liquid is determined to be hazardous (residue or water). If explosive concentrations are above the GWP-Ind (residue) or GW-Ind (water) or the material is found to be hazardous, the line will be flushed before pluging and abandoning. The rinsate will be characterized for waste handling. The FS cost estimates will be revised. The estimates will be based on the assumption that the north cooling water line and the transite wastewater line will be flushed before abandoning.	
2B	1.2.3.1		Section 1.2.3.1 – Operation Summary, 3rd paragraph the second sentence will be replaced with the following: "The underground lines consisted of TN wastewater (red liquor) lines and the cooling wate (blue water) lines (Figure 1-3). The red liquor TN	e T er	It is stated that the "transite pipe was in good condition when it was unearthed in 1993" What is the current condition of the pipe? Is the pipe exposed?		It is assumed to still be in good condition. Please see response to Comment 1B above.	

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Comment	Page Section/	Comment	C, D ¹ ,	Commentor Agrees (A) with response, or	A or	TCEQ Comments to RTCs	C, D ¹ ,	Posnonso to TCEO Comments on the PTCs	A or
#	Page Section/ Paragraph	Comment	E or X	Response stewater line, originally SWMU LHAAP-30 ar		ICEQ Comments to RICs	E or X	Response to TCEQ Comments on the RTCs	D ²
				er included as part of IRP/DSERTS LHAAP-2					
				s originally installed as a wooden pipeline. The					
				dendum to the Phase 2 Work Plan noted th					
				transite waste line was added 5 feet north					
				wooden line based on a modified drawin	_				
				ed March 30, 1943 (Bate Stamp 12651). Th					
				nsite material is a combination of cement ar					
				estos. The TNT red water line was clea					
				shed in 1946 (Bate Stamp 001446, RCR					
				cility Assessment, April 1988). The transi					
				eline was in good condition when it wa					
				earthed in 1993 at a location approximately 40					
			fee	t northwest of the pond and at the thre	ee				
			loca	ations sampled along the line as part of the	ne				
			Sha	aw additional investigation in 2006."					
			5th pa	ragraph will be replaced with following:					
				o blue cooling water lines exist at LHAAP-2					
			nor	th and south (Figure 1-3), and range from	8				
			inc	hes to 18 inches in diameter. These gravity fe	ed				
				es are thought to be constructed of vitrified cla					
				e with asbestos wicking. These lines collecte					
				ter from each TNT washing area. Manhole					
				st along both the north and south cooling wat					
				es. The northern line is connected to lines fro					
				ch plant (approximately 280 feet					
				inch-diameter pipe). The lines drain into a ditoing 16th street which eventually flows in					
				ng Totti street which eventually hows in ose Prairie Creek.	10				
3B	2.3.3								
38	2.3.3			n 2.3.3, Process Lines, text will be replaced	in				
			its ent	irety and is attached.					
4B	2.4.1		The la	ast paragraph of Section 2.4.1 will be delete	ed	See comments above.			
				new section 2.4.3, Process Lines, will be adde					
			as foll		,				
				ontaminated explosives residue remains with					
				transite TNT wastewater line at concentration					
				ove the SAI-Ind and GWP-Ind, but access to the					
				e is limited to the inlets and outlets unless th					
				e is penetrated. Additionally, the line is deep					
			tha	n the cleanup depth of 2 feet bgs for	or				
				nresidential use. The gravity flow portion of the					
				e is approximately 3,000 linear feet. The					
				ssurized portion of the line is approximate 00 linear feet. The line is in good condition.	чу				
				· ·					
				ooden TNT wastewater line was flushed ar					
				oned. The results from soil samples collected					
				he line indicate there has not been a release					
				rrounding soil. Further, the line is deeper that					
			the ne	ear-surface soil depth of 2 feet bgs considered	ea				
			tor	nonresidential use (TAC335.559(g))).				
			Furthe	ermore, it was noted in site documentation th	al				

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 Commentor Agrees (A) with response, or Does not Agree (D) with response.

		Commentor Agrees (A) with response, or Does not Agree (D) with response.									
Comment #	Page	Section/ Paragraph	Comment	C, D ¹ , E or X	Respons	se	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or
					o additional action is necessa astewater line (Bate Stamp (
				ac re TI cc ar re in	the north and south cool ccessible through manholes, esidue contents from the mathe liquid and solid residues frontaminated with explosives are above the GW-Ind (liquid) assidue). There are approximate the main lines, approximate pe from each production are 2 manholes."	and the liquid and solid inholes were sampled. from the manholes are at concentrations that and the GWP-Ind (solid ately 5,000 feet of pipe ely 1,680 linear feet of					
5B		3.1			ection 3.1, RAOs, 1 st bullet v e following:	vill be replaced with					
					"Protect the hypothetical worker by preventing contaminants in the soil, s wastewater line, cooling groundwater."	exposure to the ediment, transite TNT					
6B		3.3/ 3.3.3			ection 3.3, second sentence e following:	will be replaced with		omments regarding cleanup levels and waste ications.			
					"The cleanup levels for soil, residue in the cooling water determined with considerati health, the risk to ecologic ARARs identified for the sit	lines at LHAAP-29 are ion of the risk to human cal receptors, and the				Revised response to reflect Comment1B.	
				A	dd New Section 3.3.3 Coolin "The cleanup levels for solid	d residue in the cooling				Add New Section 3.3.3 Cooling Water Lines	
					water lines at LHAAP-29 MSCs calculated using the SE). Solid residue in the	SAM model (Appendix				"The cleanup levels for solid residue in the cooling water lines at LHAAP-29 are the GWP-Ind values Solid residue in the cooling water lines exceeded the	s.
					exceeded the site-specific manholes 8 and 10. If si	MSC for 2,4-DNT in milar thicknesses and				GWP-Ind for 2,4-DNT in manholes 8 and 10. similar thicknesses and concentrations of solid	If id
					concentrations of solid resid pipelines, then 2,4-DNT cou groundwater at unacceptab	ıld potentially leach into				residue exist in the adjacent pipelines, then 2,4-DN could potentially leach into groundwater a unacceptable concentrations if the pipe deteriorates	at
					pipe deteriorates. Table COCs and the proposed cresidue in the lines using the	leanup levels for solid				Table 3-6 summarizes the COCs and the proposed cleanup levels for solid residue in the lines using the GWP-Ind values."	d
				residue in the lines using the site-specific MSC Table 3-6 Proposed Cleanup Levels for Target COCs i Cooling Water Lines						Table 3-6 Proposed Cleanup Levels for Target COCs in Cooling Water Lines	
					Explosive	Site-Specific MSC (mg/kg)				Explosive GWP-Ind (mg/kg)	
					2,4,6-Trinitrotoluene	250				2,4,6-Trinitrotoluene 5.1	
					2,4-Dinitrotoluene	0.38				2,4-Dinitrotoluene 0.042	
					2,6-Dinitrotoluene	0.31				2,6-Dinitrotoluene 0.042	
					2-amino-4,6-Dinitrotoluene	160				2-amino-4,6-Dinitrotoluene 1.7	

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
- 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

		T	2. Commentor Agrees (A) with response, or		I	1	T	1
Comment #	Page Section/ Paragraph	Comment	C, D ¹ , E or X	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or D ²
			4-amino-2,6-Dinitrotoluene 100 Abbreviations: mg/kg milligrams per kilogram MSC medium-specific concentration				4-amino-2,6-Dinitrotoluene 1.7 Abbreviations: GWP-Ind Soil MSC for industrial use based on groundwater protection mg/kg milligrams per kilogram MSC medium-specific concentration	
7B	4.4.1.3.1		Section 4.4.1.3.1, under Plug and Abandon Lines, "migration of sediment and residue" will be revised to "migration of solid residue"	II.				
8B	5.1.2		Section 5.1.2, 1st sentence, will be revised as follows: "sediment in the outfall ditch, and solid residue in the cooling water lines and manholes."	ле				
9B	5.2.2.2 and 5.2.3.2		Sections 5.2.2.2 and 5.2.3.2, will be revised as follows: "The transite TNT wastewater line will be flush with water to remove visual residue. The rinsa water will be containerized, transported a treated at the on-site wastewater treatment plant disposed of off-site based on the explosi chemical concentrations. The inlets and outlets the transite TNT wastewater line will be plugg with a bentonite slurry mix or equivalent. The cooling water lines showed no significate contamination except for 2,4-DNT in the solid resid in manholes 8 and 10. The cooling water lines will inspected to determine if there is contaminated so residue in the lines adjacent to manholes 8 and 10. An attempt will be made to collect samples from the solid residue within the lines adjacent to manholes and 10, and samples will be analyzed to determine 2,4-DNT concentrations in solid residue in the pipes above the proposed cleanup level (site-specific MSC) If there is no measurable amount of residue in the lines, no action will be taken. If there is measurable amount of residue in the lines a sample will collected if concentrations are below the site specific MSC, action will be taken. If solid residue concentration are found to be above the proposed cleanup level the lines (site-specific MSC), the affected segment the line will be flushed, the rinsate water will containerized, transported and treated at the on-swastewater treatment plant. The manholes will the plugged with a bentonite slurry mix or equivaler.	ate and cor ve cof ed ant ue be did 10. he s 8 e if s is C). he ble ed. no ns in of be ite en	Please note that method of handling the rinsate water would depend on the classification of the waste residue. It state attempts will be made to collect samples. If no samples are taken, the pipe must be flushed clean and rinsate collected to determine its waste classification.	D	Rinsate will be handled based on the waste classification of the rinsate. Prior experience indicates that manholes are typically the accumulation points for solid residues. Previous field work by Shaw demonstrated that the cooling water lines are generally clean and very little residue exists in the manholes. Flushing is not considered necessary if there in no residue in the pipelines or if the residue amount is so little that it cannot be sampled. See response to Comment 1B, part 4. The following revisions will be made to the Sections 5.2.2.2 and 5.2.3.2 (see Response column) as follows: "Site-specific MSC" will be revised to "GWP-Ind". A new sentence will be added as follows: "Appropriate rinsate handling procedures will be followed based on the its waste classification."	
10B	5.2.2.3		Add to the end of Section 5.2.2.3: "Based on the Treatability Study (included Appendix B), the MC concentrations will reduced by approximately 75% through her activated persulfate application. MNA will initiated after the formation has recovered from the section of the secti	be at- be				

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
- 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Comment	Section/		2. Commentor Agrees (A) with response, o		Ī	C. D ¹ .		A or
#	Page Section/ Paragraph	Comment	C, D ¹ , Response	A or D ²	TCEQ Comments to RTCs	C, D ¹ , E or X	Response to TCEQ Comments on the RTCs	A or D ²
			oxidation treatment activities."					
11B	Figures, Tables, and Appendix Lists		Due to adding Tables 2-4 through 2-7, existing Table 2-4 and 2-5 become Tables 2-8 and 2-9. Table 3-added.				Original Appendix E in the Draft final will remain as Appendix E. The SAM modeling appendix attached to the RTCs will be removed.	
	Listo		Due to adding Figure 2-5, existing Figures 2-5 and 6 become Figures 2-6 and 2-7.	12-				
			Original Appendix E in the Draft Final will be chang to Appendix F.	ged				
12B	In general		Figure 2-5 is attached.		See comments above regarding the proposed cleanup levels.		See response to above comment concerning Appendix E.	
			Appendix E, Soil Attenuation Model, is attached.		Greatup levels.		Appendix E.	
			Table 1-1, Additional Investigations, 5 th bullet will revised as follows:	be				
			"Collected 8 solid residue samples fr manholes"	om				
			And 8 th bullet will be revised as follows:					
			"29SD49, 3 solid residue samples from transite"	the				
			For clarity of meaning, the words "cleanup goals" be changed to "cleanup levels" in the document. Toccurs five times – on pages 3-4, 5-3, 5-6, 6-11, a 6-19.	his				
			SAM Soil Attenuation Model will be added to acronyms.	the				
			Appendix A – references in text, tables and figures "sediment samples" collected in the lines will revised to "solid residue" samples.					
			Section 1.1, Appendix E description will be added	i.				
			"Deed recordation" language will be updated "recordation notification with the county" in following sections:					
			Section 3, Table 3-3, Land Use Controls wh Hazardous Substances are Left in Place	nen				
			• Section 3.2.4.1.3, 2 nd paragraph, 2 nd sentence	е				
			 Section 4.4.1.2.1, Covenants, 1st sentence, n to last sentence of Administrative Controls bull 	let.				
			Section 4.4.2.2.1, Covenants, 1 st sentence, I	ast				

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 Commentor Agrees (A) with response, or Does not Agree (D) with response.

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			sentence of effectiveness bullet, next to last sentence of Administrative Controls bullet.					
13B		General FS consistency changes	The language in the LHAAP-29 FS will be revised to be consistent with the recent finalized FSs (LHAAP-46, LHAAP 50, and LHAAP-35A(58)), which include the following: The remedial action objectives will be revised as follows: "The Army recognizes USEPA's policy to return all groundwater to potential beneficial uses, based on the non-binding programmatic expectation in the NCP. The RAOs for LHAAP-29, which address contamination associated with the media at the site and take into account the future uses of LHAAP streams, land, and groundwater are:					
			 Protect the hypothetical future maintenance worker by preventing exposure to the contaminants in the soil, sediment, transite TNT wastewater line, cooling water lines, and groundwater. Prevent migration of contaminants to groundwater and surface water from potential sources in the soil, sediment and process lines (TNT wastewater and cooling water) 					
			 Protect ecological receptors by preventing exposure to the contaminated soil and sediment Return groundwater to its potential beneficial uses, wherever practicable, within a reasonable time period given the particular site circumstances." 					
			 Other changes include the following: Throughout document, when discussing potential beneficial use of groundwater, "restore" will be revised to "return". 					
			 MNA sampling frequency will be revised to reflect the most recent schedule (i.e. two years of quarterly sampling, etc.). 					
			 Future maintenance worker will be changed to hypothetical future maintenance worker throughout the document. 					

00091114

Comments on Draft Final Feasibility Study (published March 2009) LHAAP-29, Former TNT Production Area, Group 2 Longhorn Army Ammunition Plant, Karnack, Texas

Reviewers: USEPA, TCEQ, US Army, plus additional changes since April 2009 Meeting Respondents: Prayeen Srivastay, Project Manager; Susan Watson, Shaw Environmental, Inc.

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 - 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Section 2.3.3, Process Lines

At LHAAP-29 there are red liquor TNT wastewater lines (transite and wooden) and blue cooling water lines with manholes (north and south). It should be noted that the explosives sample results from Phase I and Phase II (29WL01 through 29WL11) were deemed unusable for environmental decision making per USEPA (Jacobs, 2002). Additional investigations were conducted for both lines since the risk assessment (**Appendices A** and **B**).

2.3.3.1 TNT Wastewater Lines

During the Phase I Remedial Investigation, the transite TNT wastewater line was found at 29WL04 and 32WL02 but was not found near 29WL01, 29WL02, and 29WL03. This investigation also noted that the wood stave line was found to be soft and severely weathered. Soil samples (29SB81 through 29SB85) were collected in 2004 along the wastewater line near the wash house sumps to check for contamination possibly leaking from the wooden wastewater line into the surrounding soil (**Appendix A**). In 2006, the transite line was found approximately 5-feet north of the wooden line location and sampled near original locations 29WL01 (2006 sample ID 20WL14), 29WL02 (2006 sample ID 29WL13), and 32WL02 (2006 sample ID 32WL05) (**Appendix B**).

The risk assessment contained soil EPC values for 2,4,6-TNT (190 mg/kg), 2-amino-4,6-DNT (25 mg/kg), and 4-amino-2,6-DNT (16 mg/kg). The other explosives were not detected. In 2006, the sample results for 2,4,6-TNT at 29WL13 was above the EPC. The results of the other two explosives were below their EPCs. For evaluation of the additional data collected in 2004 and 2006, the results were compared to SAI-Ind and GWP-Ind values. There were several explosives detected in the transite wastewater line that were above the GWP-Ind. Table 2-4 summarizes the solid residue sample results from within the TNT transite wastewater line that are above the GWP-Ind. Only two explosives (2,4,6-TNT and 2,4-DNT) had concentrations above the SAI-Ind in the solid residue from within the pipe. The explosive sample results above the SAI-Ind in the solid residue from within the transite pipe are shaded in **Table 2-5**. The sample locations are shown on **Figure 2-5**.

Reviewers: USEPA, TCEQ, US Army, plus additional changes since April 2009 Meeting Respondents: Prayeen Srivastay, Project Manager; Susan Watson, Shaw Environmental, Inc.

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 - 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Table 2-5
Summary of Solid Residue Sample Results from Transite TNT Wastewater Line

Explosive	EPC from Risk Assessment (mg/kg)	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	Concentration* (mg/kg)	Sample location
2,4,6 TNT	190 (associated HI of 0.77)	510	5.1	<mark>526</mark> 58.4 17 JL	<mark>29WL13</mark> 29WL14 32WL05
2,4 DNT		4.2	0.042	<mark>5.15 JL</mark> 89 7.21	32WL05 29WL13 29WL14
2-amino-4,6-DNT	25 (associated HI of 0.33)	170	1.7	19 JH	29WL14
4-amino-2,6-DNT	16 (associated HI of 0.21)	170	1.7	13.3	29WL14
1,3-DNB		100	1	1.08	29WL13

Notes and Abbreviations:

* Concentrations included in table are above the GWP-Ind. Shaded concentrations are also above the SAI-Ind.

DNB dinitrobenzene DNT dinitrotoluene

EPC exposure point concentration

GWP-Ind soil MSC for industrial use based on groundwater protection

HI hazard index

JL concentration is estimated and biased low JH concentration is estimated and biased high

mg/kg milligrams per kilogram
MSC medium-specific concentration

SAI-Ind soil MSC for industrial use based on inhalation, ingestion and dermal contact

TNT trinitrotoluene

Samples of soil (29SB81 – 29SB85) were collected near the wooden TNT wastewater line in 2004 and were analyzed for explosives (**Appendix A**). **Table 2-6** lists the detected explosive concentrations in the samples from the soil near the TNT wooden wastewater line. The concentrations were all below their associated EPC. These concentrations were also compared to both the SAI-Ind and GWP-Ind, and no exceedances were found in the soil near the wooden TNT wastewater line. The sample locations are shown on **Figure 2-5**.

Reviewers: USEPA, TCEQ, US Army, plus additional changes since April 2009 Meeting Respondents: Prayeen Srivastay, Project Manager; Susan Watson, Shaw Environmental, Inc.

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 - 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Table 2-6
Explosive Compounds Detected in Soil Samples near Wooden TNT Wastewater Line

Explosive	EPC from Risk Assessment (mg/kg)	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	Concentration (mg/kg)	Sample Location	Associated Depth
2,4,6-TNT	190 (associated HI of 0.77)	510	5.1	0.43	29SB83	4-5 ft bgs
2-amino-4,6-DNT	25 (associated HI of 0.33)	170	1.7	0.23 J 0.9	29SB85 29SB85	4-5 ft bgs 8-9 ft bgs
4-amino-2,6-DNT	16 (associated HI of 0.21)	170	1.7	0.30 J	29SB85	8-9 ft bgs

Abbreviations:

DNT dinitrotoluene

EPC exposure point concentration ft bgs feet below ground surface

GWP-Ind soil MSC for industrial use based on groundwater protection

HI hazard index

J concentration is estimated mg/kg milligrams per kilogram MSC medium-specific concentration

SAI-Ind soil MSC for industrial use based on inhalation, ingestion and dermal contact

TNT trinitrotoluene

2.3.3.2 Cooling Water Lines

LHAAP-29 was constructed with two vitrified clay cooling lines as shown on **Figure 2-5**, referred to as the north and south cooling water lines. These lines are accessible through manholes. Liquid and solid residue from these manholes were sampled in 2004 (**Appendix A**). 1,3,5-TNB; 2,4,6-TNT; 2,4-DNT; 2,6-DNT; 2-amino-4,6-DNT; and 4-amino-2,6-DNT were detected. None of the detected explosives were above the EPCs in the risk assessment. The detected results were also compared to the GWP-Ind. Several explosives were detected above the GWP-Ind in both the north and south cooling lines. The detected concentration of 1,3,5-TNB (0.440 mg/kg) at MH02 was less than the GWP-Ind of 310 mg/kg and is not shown on **Table 2-7**.

Reviewers: **USEPA, TCEQ, US Army, plus additional changes since April 2009 Meeting Respondents:** Prayeen Srivastay, Project Manager; Susan Watson, Shaw Environmental, Inc.

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 - 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Table 2-7
Summary of Solid Residue Sample Results from Cooling Water Lines

Explosive	EPC from Risk Assessment (mg/kg)	GWP- Ind (mg/kg)	Concentration* (mg/kg)	Sample location	Associated line
2,4,6-TNT	190	5.1	11	MH02	S Cooling
	(associated HI of 0.77)		7	MH10	N Cooling
			5.5	MH08	N Cooling
2,4-DNT		0.042	0.71	MH08	N Cooling
			1.1	MH10	N Cooling
2,6-DNT		0.042	0.24 J	MH10	N Cooling
			0.30 J	MH08	N Cooling
2-amino-4,6-	25	1.7	3.8 J	MH02	S Cooling
DNT	(associated HI of 0.33)		2.4 J	MH09	N Cooling
	·		9	MH10	N Cooling
4-amino-2,6-	16	1.7	2.6 J	MH02	S Cooling
DNT	(associated HI of 0.21)		2.5 J	MH09	N Cooling
			7.8	MH10	N Cooling

Notes and Abbreviations:

DNT dinitrotoluene

EPC exposure point concentration

GWP-Ind soil MSC for industrial use based on groundwater protection

HI hazard index

J concentration is estimated mg/kg milligrams per kilogram MSC medium-specific concentration

TNT trinitrotoluene

Liquid samples were also collected from the cooling water line manholes. The detected explosives in the water in the manholes of both the north and south lines included 1,3,5-TNB, 2,4,6-TNT, 2,4-DNT, 2,6-DNT, 2-amino-4,6-DNT, and 4-amino-2,6-DNT. **Table 2-8** lists the detected liquid samples that were above the GW-Ind. For MH09, there were two sets of samples collected (2004 and 2005). Though some of the results from the 2005 sampling round are lower than the GW-Ind, they have been included in **Table 2-8**. Both the north and south cooling lines have sample results that indicate the liquid within the cooling water lines are above the GW-Ind."

^{*} Concentrations included in table are above the GWP-Ind.

Reviewers: USEPA, TCEQ, US Army, plus additional changes since April 2009 Meeting Respondents: Prayeen Srivastay, Project Manager; Susan Watson, Shaw Environmental, Inc.

- 1. Respondent Concurs (C), Does Not Concur (D), Takes Exception (E), or Delete (X).
 - 2. Commentor Agrees (A) with response, or Does not Agree (D) with response.

Table 2-8
Explosive Compounds Detected in Liquid Samples from Cooling Water Lines

Explosive	EPC from Risk Assessment (µg/I)	GW-Ind (μg/l)	Concentration (μg/l)	Sample location	Associated line
2,4,6-TNT		51	250 84.3 JL 430 5200 20	MH01 MH05 MH06 MH09 (12/04) MH09 (2/05)	South South South North North
2,4-DNT	530 (HI=2.6)	0.42	15 0.8 J 1.13 1.05 0.922 J 0.934 J	MH01 MH09 (12/04) MH09 (2/05) MH10 MH11 MH12	South North North North North North
2,6-DNT	530 (HI=5.2)	0.42	4.1 27 1.27 1.35 1.15 1.31	MH01 MH09 (12/04) MH09 (2/05) MH10 MH11 MH12	South North North North North North
2-amino-4,6- DNT	5.9 (HI=0.35)	17	220 1.68	MH09 (12/04) MH09 (2/05)	North North
4-amino-2,6- DNT	5.9 (HI=0.35)	17	33 290 2.42	MH01 MH09 (12/04) MH09 (2/05)	South North North

Abbreviations:

DNT dinitrotoluene

EPC exposure point concentration GW-Ind groundwater MSC for industrial use

HI hazard index

J concentration is estimated

JL concentration is estimated and biased low

MSC medium-specific concentration

TNB trinitrobenzene TNT trinitrotoluene

FINAL FEASIBILITY STUDY LHAAP-29, FORMER TNT PRODUCTION AREA, GROUP 2 LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS



Prepared for

U.S. Army Corps of Engineers Tulsa District 1645 South 101st Avenue Tulsa, Oklahoma

Prepared by

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Contract Number W912QR-04-D-0027 Task Order No. DS02

April 2010

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Appendix B Additional Investigation Data Summary Report (2006 and 2008)

Appendix C LHAAP-29 Natural Attenuation Evaluation

Appendix D Summary Table, Field Sheets, Well Log (29WW41), and Analytical Data Reports

(October 2008, January 2009, and June 2009)

Appendix E Basis of Estimate for LHAAP-29 Remediation

Acronyms and Abbreviations

°C degrees Celsius
°F degrees Fahrenheit
μg/L micrograms per liter
AOC area of contamination
AR Administrative Record

ARARs applicable or relevant and appropriate requirements

AST aboveground storage tank

BERA baseline ecological risk assessment

bgs below ground surface

CERCLA Comprehensive Environmental Response, Compensation, and Liability Act

of 1980

CFR Code of Federal Regulations

CLI Caddo Lake Institute
COCs contaminants of concern

COPECs contaminants of potential ecological concern

CWA Clean Water Act of 1972

cy cubic yards
DCA dichloroethane

DNAPL dense non-aqueous phase liquid

DNT dinitrotoluene

EcoPRG ecological preliminary remediation goal

EEQ ecological effects quotient
ELCR excess lifetime cancer risk
EPC exposure point concentration
ESA environmental site assessment
FFA Federal Facility Agreement

FR Federal Register
FS Feasibility Study
g/L grams per liter

GAC granulated activated carbon GRAs general response actions

GW-Ind groundwater MSC for industrial use

GWP-Ind soil MSC for industrial use based on groundwater protection

HI hazard index

HMX octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine

HQ hazard quotient

Acronyms and Abbreviations (continued) ____

IRP/DSERTS Installation Restoration Program/Defense Site Environmental Restoration

Tracking System

LHAAP Longhorn Army Ammunition Plant LOAEL lowest-observed adverse effect level

LUCs land use controls

MARC Multiple Award Remediation Contract

MC methylene chloride

MCLs maximum contaminant levels

mg/kg milligrams per kilogram

MNA monitored natural attenuation
MSC Medium-Specific Concentration

NCP National Oil and Hazardous Substances Pollution Contingency Plan

NOAEL no-observed adverse effect level

NPL National Priorities List
O&M operation and maintenance

OSHA Occupational Safety and Health Administration

pH hydrogen ion concentration

PP Proposed Plan

PPE personal protective equipment

PVC polyvinyl chloride

RAOs remedial action objectives

RCRA Resource Conservation and Recovery Act RDX hexahydro-1,3,5-trinitro-1,3,5-triazine

RI Remedial Investigation

RI/FS Remedial Investigation/Feasibility Study

ROD Record of Decision

SAI-Ind soil MSC for industrial use based on inhalation, ingestion and dermal contact

Shaw Shaw Environmental, Inc.

STEP Solutions to Environmental Problems, LLC

SVOC semivolatile organic compound SWMU solid waste management unit TAC Texas Administrative Code

TBC to-be-considered

TCDD tetrachlorodibenzo-p-dioxin

TCE trichloroethene

TCEQ Texas Commission on Environmental Quality

TNB trinitrobenzene

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Acronyms and Abbreviations (continued) _____

TNT trinitrotoluene

TRV toxicity reference value

TSD treatment, storage, and disposal USACE U.S. Army Corps of Engineers U.S. Army U.S. Department of the Army

USC United States Code

USEPA U.S. Environmental Protection Agency

USFWS U.S. Fish and Wildlife Services VOC volatile organic compound

ZVM zero-valence metals

Executive Summary

This Feasibility Study (FS) was prepared by Shaw Environmental, Inc. (Shaw), for the U.S. Army Corps of Engineers (USACE), Tulsa District, under the Louisville District's Multiple Award Remediation Contract (MARC) No. W912QR-04-D-0027, for remediation activities on the former Longhorn Army Ammunition Plant (LHAAP) in Karnack, Texas. This FS presents the analysis of remediation alternatives for the Former Trinitrotoluene (TNT) Production Area, designated as LHAAP-29, in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act of 1980 (CERCLA), and provides for the remedy selection consistent with the intended use of LHAAP as a national wildlife refuge.

LHAAP is an inactive, government-owned, formerly contractor-operated and maintained Department of Defense facility located in central-east Texas. LHAAP-29 is a heavily wooded, 85-acre site in the western-central portion of the LHAAP installation. The site is currently inactive, but once contained five active and one standby TNT production lines. The area still contains the foundations for the former production facilities and the underground pipe lines that were originally built for cooling water drainage and TNT wastewater conveyance.

The entire installation was under the control of the U.S. Department of the Army (U.S. Army) until May 5, 2004, when approximately two thirds of the property was transferred to the U.S. Department of Interior's Fish and Wildlife Service (USFWS). The U.S. Army Environmental Command provides funding for the environmental remedial activities. The Base Realignment and Closure Division is responsible for all aspects of LHAAP including the environmental programs, operations, and land transfer.

Surface runoff from the northern part of the site (about 40 percent of the site area) enters Goose Prairie Creek located approximately 1,500 feet to the north and east of the site. In the southern portion of the site (about 60 percent of the site), surface runoff flows into a tributary of Central Creek located near the southeast portion of the site. Via these two creeks, the runoff from LHAAP-29 eventually enters Caddo Lake.

There are three groundwater zones at LHAAP-29: shallow, intermediate and deep. The bottom of each of the zones is defined by a continuous or semi-continuous clay layer of varying thickness. The predominant flow of both the shallow and intermediate groundwater zones is to the east/northeast.

Sampling specific to LHAAP-29 media was conducted during several investigations prior to and after the human health risk assessment (Jacobs, 2002). The baseline human health risk

assessment (Jacobs, 2002) indicates a hazard for the hypothetical future maintenance worker with a hazard index of 1 from soil and 3,000 from groundwater. There is no unacceptable cancer risk to the hypothetical future maintenance worker from soil at LHAAP-29, but the cancer risk from groundwater is 1.3×10^{-4} , which is outside the United States Environmental Protection Agency (USEPA) target risk range of 1×10^{-6} to 1×10^{-4} for the excess lifetime cancer risk.

Additional investigations were conducted after the risk assessment was completed. The additional data do not change the overall outcome of the risk assessment, but did change some of the contaminants of concern (COCs). Although COCs have been detected in the shallow and intermediate groundwater zones beneath LHAAP-29, the horizontal extent of contamination is not widespread and appears to be isolated to a few specific areas at the site. The COCs identified for soil are 2,4,6-TNT, 2,4-dinitrotoluene (DNT), and perchlorate. The COCs identified for the shallow groundwater zone are 1,2-dichloroethane (DCA), trichloroethene (TCE), 2,4-DNT, 2,6-DNT, 2-nitrotoluene, 3-nitrotoluene, 4-nitrotoluene, and perchlorate. The COCs in the intermediate zone are methylene chloride (MC), 1,2-DCA, and TCE.

An ecological conceptual exposure model was developed for various "sub-areas" throughout the LHAAP as part of the *Final Facility-Wide Baseline Ecological Risk Assessment* (BERA) (Shaw, 2007b). Ecological hazards were found to be acceptable for the Industrial Sub-Area that includes LHAAP-29; however, elevated concentrations of nitrotoluenes (TNT, 2,4-DNT and 2,6-DNT) were identified at one location at the site. Further data determined that analysis identified the nitrotoluenes at this one location and the adjacent area possibly represent a small area of highly elevated concentrations (i.e., a hot spot) that could pose a threat to small-range ecological receptors (Shaw, 2007b). Therefore, nitrotoluenes are considered as contaminants of potential ecological concern (COPECs) for the soil at LHAAP-29.

Explosive compound releases resulting from the manufacturing process of TNT, releases from process tanks and process pipelines, are the suspected contamination sources at LHAAP-29. From 1959 to the mid 1970's, "soak-out" of out-of-specification motors was conducted at the site using MC, and these operations along with the MC storage tank could have all had releases. Potential sources of contamination at the site are co-located wood and transite TNT wastewater pipelines, cooling water lines and manholes, explosives compounds in stained soils around the foundation of Buildings 806-A and –D, isolated perchlorate-containing soils in the northeastern portion of LHAAP-29, and TNT-contaminated sediment in the cooling water outfall ditch.

The U.S. Army recognizes USEPA's policy to return all groundwater to potential beneficial uses, based on the non-binding programmatic expectation in the National Contingency Plan. The remedial action objectives (RAOs) for LHAAP-29, which address contamination associated with the media at the site and take into account the future uses of LHAAP streams, land, and groundwater are:

- Protect the hypothetical future maintenance worker by preventing exposure to the contaminants in the soil, sediment, transite TNT wastewater line, cooling water lines, and groundwater.
- Prevent migration of contaminants to groundwater and surface water from potential sources in the soil, sediment and process lines (TNT wastewater and cooling water).
- Protect ecological receptors by preventing exposure to the contaminated soil and sediment.
- Return groundwater to its potential beneficial uses, wherever practicable, within a reasonable time period given the particular site circumstances.

The FS identifies and screens remedial technologies and associated process options that may be appropriate for satisfying the RAOs for LHAAP-29 with respect to effectiveness, implementability and cost. Select remedial technologies and process options were carried forward after the initial screening and were combined to develop the following remedial alternatives for LHAAP-29:

- Alternative 1 No action. Leaves the contaminated soil, groundwater, waste water lines in place with no remedial action or additional measures to prevent exposure to the COCs or their migration, and serves as a baseline for comparison with the other alternatives. The 'No action' alternative is an evaluation requirement under CERCLA.
- Alternative 2 Excavation and off-site disposal for soil; plug waste lines; in situ chemical oxidation, Monitored Natural Attenuation (MNA) and Land Use Controls (LUCs) for intermediate zone groundwater, and MNA and LUCs for shallow zone groundwater. Alternative 2 excavates the contaminated soil from LHAAP-29 and addresses the former TNT wastewater and cooling water lines by plugging and abandoning the lines and manholes. This alternative reduces contamination in the intermediate groundwater zone by in situ chemical oxidation with simultaneous extraction. Implementation of MNA in both the shallow and intermediate zones would ensure that groundwater contamination concentrations and plume stability/size are monitored as the plume degrades over time. Groundwater monitoring would continue until cleanup levels are met. LUCs will restrict use of groundwater until it is returned to beneficial use.
- Alternative 3 Excavation and off-site disposal for soil; plug lines; intermediate zone groundwater extraction, MNA and LUCs for groundwater. As with Alternative 2, contaminated soil is removed, the lines and manholes are plugged and abandoned. Groundwater contamination is reduced in the intermediate zone via groundwater extraction, treatment at the existing LHAAP groundwater treatment plant, and discharge into surface water in accordance with plant permit. Implementation of MNA in both the shallow and intermediate zones would ensure that groundwater contamination concentrations and plume stability/size are monitored as the plume degrades over time. Similar to Alternative 2, LUCs will be maintained until groundwater is returned to beneficial use.

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Each of the alternatives was evaluated against CERCLA criteria to provide a basis for selecting a preferred alternative to be published in Proposed Plan and Record of Decision documents.

Table ES-1 summarizes the comparative analysis of the alternatives presented in this study.

Table ES-1 Comparative Analysis of Alternatives

Comparative Analysis of Alternatives										
Criteria Overall protection of human health and the environment	Alternative 1 No Action No protection. Does not achieve RAOs.	Alternative 2 Excavation and off-site disposal for soil; plug lines; in situ chemical oxidation, MNA and LUCs for intermediate zone groundwater; and MNA and LUCs for shallow zone groundwater Achieves RAOs. Protection of human health and environment provided by soil removal and remediation of groundwater COCs to cleanup levels	Alternative 3 Excavation and off-site disposal for soil; plug lines; groundwater extraction, MNA and LUCs for groundwater Achieves RAOs. Protection of human health and environment provided by soil removal and remediation of groundwater COCs to cleanup levels.							
Compliance with ARARs	No compliance with chemical-specific ARARs.	Complies with all ARARs.	Complies with all ARARs.							
Long-term effectiveness and permanence	Is not effective at protection of human health and the environment and does not provide permanence.	In situ chem-ox for intermediate zone should be effective and permanent; however, uncertainty exists concerning the effectiveness of in situ treatment for reducing groundwater contaminant concentrations to cleanup levels. Treatability and pilot studies would be required to further assess the effectiveness of this treatment method and a pre-design would be required to determine the optimum extraction technique configuration. Evaluation of natural attenuation suggests that contaminants are degrading naturally. MNA sampling will be conducted to confirm its effectiveness. Land use controls would be effective and reliable so long as they are maintained. Excavation of soil is effective long-term and permanent as contamination would be removed from the site and placed in a permitted landfill.	Should be effective and permanent for intermediate zone via extraction and treatment, based on the efficiency exhibited by the current groundwater treatment system. A pre-design study would be required to determine the optimum extraction technique/configuration. Evaluation of natural attenuation suggests that contaminants are degrading naturally. MNA sampling will be conducted to confirm its effectiveness. Land use controls would be effective and reliable so long as they are maintained. Excavation of soil is effective long-term and permanent as contamination would be removed from the site and placed in a permitted landfill.							
Reduction of toxicity, mobility, or volume through treatment	No reduction.	Provides permanent and irreversible reduction of intermediate zone. Provides active reduction of toxicity and volume of groundwater contaminants through biological degradation component of MNA.	Extraction and treatment of contaminated groundwater intermediate zone reduces toxicity, mobility, and volume of groundwater contaminants in this area outside of natural processes. Provides active reduction of toxicity and volume of groundwater contaminants through biological degradation component of MNA.							

Table ES-1 (continued) Comparative Analysis of Alternatives

Criteria Short-term effectiveness	Alternative 1 No Action No short-term impacts.	Alternative 2 Excavation and off-site disposal for soil; plug lines; in situ chemical oxidation, MNA and LUCs for intermediate zone groundwater; and MNA and LUCs for shallow zone groundwater Greater potential for impacts to the	Alternative 3 Excavation and off-site disposal for soil; plug lines; groundwater extraction, MNA and LUCs for groundwater Greater potential for impacts to the					
Short-term ellectiveness	No short-term impacts.	community or hypothetical future maintenance worker through off-site transportation of contaminated soil. Release to environment can be controlled during construction.	community or hypothetical future maintenance worker through offsite transportation of contaminated soil. Release to environment can be controlled during construction.					
Implementability	Inherently implementable.	Implementable, but uncertainty exists whether in situ chemical oxidation would lower contaminant concentrations to cleanup levels. Specialized knowledge required for implementation. Use of on-site storage tanks may limit storage capacity. A groundwater treatment system is already operating at LHAAP.	Implementable. Use of on-site storage tanks may limit storage capacity. A groundwater treatment system is already operating at LHAAP. Potential exists for limited groundwater recovery which may affect ability of system to remove contaminants to cleanup levels. A pre-design study would be required.					
Cost* (present worth)								
Capital	\$0	\$2,109,000	\$1,360,000					
O&M	\$0 \$0	\$919,000	\$1,558,000					
Total	\$0	\$3,028,000	\$2,918,000					
State Acceptance								
Community Acceptance	This criterion will be evalua	iteu in the Proposed Pian after commun	ity comments are provided.					

Notes and Abbreviations:

ARAR applicable or relevant and appropriate requirement

COC contaminant of concern

LHAAP Longhorn Army Ammunition Plant

LUC land use controls

MNA monitored natural attenuation
O&M operation and maintenance
RAO remedial action objective

^{*} Costs have been rounded to nearest \$1,000.

Shaw Environmental, Inc.

1.0 Introduction

This Feasibility Study (FS) was prepared by Shaw Environmental, Inc. (Shaw), for the U.S. Army Corps of Engineers (USACE), Tulsa District, under the Louisville District's Multiple Award Remediation Contract (MARC) No. W912QR-04-D-0027, for remediation activities at the former Longhorn Army Ammunition Plant (LHAAP) in Karnack, Texas. This FS presents an analysis of remediation alternatives for the Former Trinitrotoluene (TNT) Production Area, designated as LHAAP-29, in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act of 1980 (CERCLA).

The U.S. Army Environmental Command provides funding for the environmental remedial activities at LHAAP. The Base Realignment and Closure Division is responsible for all aspects of LHAAP including the environmental program, operations, and land transfer.

1.1 Purpose and Organization of Report

Under CERCLA, environmental cleanup decision-making follows a prescribed sequence: Remedial Investigation (RI), FS, Proposed Plan (PP), and Record of Decision (ROD). The RI serves as the mechanism for collecting data to characterize site conditions, determining the nature and extent of the contamination, and assessing risks to human health and the environment from this contamination. The investigatory element of decision making for LHAAP-29 has been completed and documented in an RI report (Jacobs, 2001) and a baseline risk assessment report (Jacobs, 2002).

The FS takes the next step of identifying and evaluating remedial solutions to the environmental problems identified for LHAAP-29. This step begins with the formulation of viable alternatives, which involves defining remedial action objectives (RAOs), general response actions (GRAs), volumes or area of media to be addressed, and potentially applicable technologies and process options. After a reasonable number of appropriate alternatives have been formulated, the alternatives undergo a detailed analysis using nine established evaluation criteria. The detailed analysis evaluates individual alternatives against the criteria and compares them with each other to gauge their relative performance. Each alternative that makes it to this stage of the analysis, with the exception of the required "No Action" alternative, is expected to be protective of human health and compliant with applicable or relevant and appropriate requirements (ARARs) (unless a waiver is justified), both threshold requirements under CERCLA. The alternatives developed in this FS address the media and contaminants of concern (COCs) at LHAAP-29 through combinations of source control and groundwater actions.

The main text of this FS is composed of the following sections:

- Section 2, "Risk and Site Assessment," summarizes the risk assessment approach and conclusions. It also provides the conceptual site model for LHAAP-29 and discusses the LHAAP-29 media contamination assessment.
- **Section 3**, "Remedial Action Objectives and Cleanup Levels," presents the RAOs and a discussion of cleanup levels. The chemical-, location- and action-specific ARARs are presented in this section.
- **Section 4**, "Identification and Screening of Technologies and Process Options," summarizes the rationale for selecting technologies and process options for remediation of contamination to meet the RAOs.
- **Section 5**, "Development and Description of Alternatives," presents the rationale for developing a range of alternatives as well as a description of each alternative.
- **Section 6**, "Detailed Analysis of Alternatives," evaluates, compares, and contrasts the benefits and costs of the alternatives.
- Section 7, "References," presents the references cited in this document.

Appendix A presents the *Investigation Results* – 2004 and 2005 which summarizes the activities and results of previous investigations performed at LHAAP-29 by Shaw and USACE during 2004 and 2005 and not previously included in the Administrative Record (AR).

Appendix B presents the *Additional Investigation Data Summary Report* for various sampling activities performed at LHAAP-29 between August 2006 and February 2008 to further delineate the extent of contamination and includes the activated persulfate oxidation study report.

Appendix C presents the *Natural Attenuation Evaluation Report* which provides an evaluation of natural attenuation of groundwater contaminants at LHAAP-29.

Appendix D presents tables and field documentation for sampling events in October 2008, January 2009, and June 2009.

Appendix E presents the cost estimates for the remedial action alternatives.

The preferred alternative for LHAAP-29 will be presented in the PP. The PP will briefly summarize the alternatives studied in this FS, highlighting the key factors that led to identifying the preferred alternative. The U.S. Department of the Army (U.S. Army) will submit the PP to the regulatory agencies, Texas Commission on Environmental Quality (TCEQ) and the U.S. Environmental Protection Agency (USEPA), and then the public for review. After this review, the U.S. Army will release a ROD that documents the selected remedy, certifies that the remedy selection process was carried out in accordance with CERCLA, and addresses public comments

on the PP. Relevant documentation, including the RI, FS, and subsequent documents, are or will be available to the public in the AR for this project. The AR is housed at LHAAP and at the Marshall Public Library in Marshall, Texas.

1.2 Longhorn Army Ammunition Plant Background

1.2.1 Location

The LHAAP is an inactive, government-owned, formerly contractor-operated and -maintained industrial facility located in central-east Texas in the northeastern corner of Harrison County. The installation occupies nearly 8,416 acres between State Highway 43 at Karnack, Texas, and the western shore of Caddo Lake as shown in **Figure 1-1**.

The nearest cities are Marshall, Texas, approximately 14 miles to the southwest, and Shreveport, Louisiana, approximately 40 miles to the east. Caddo Lake, a large freshwater lake situated on the Texas-Louisiana border, bounds LHAAP to the north and east. The industries in the surrounding area consist of agriculture, timber, oil and natural gas production, and recreation.

1.2.2 History

LHAAP was established in December 1941, near the beginning of World War II, when the U.S. Army issued a contract to build a six-line production facility for manufacturing TNT. Various media have been contaminated by past industrial operations and waste management practices at Industrial operations involved the use of secondary explosives, rocket motor LHAAP. propellants, and various pyrotechnics, such as illuminating and signal flares and ammunition. Explosives included TNT and black powder. Typical composite propellants were composed of a rubber binder, an oxidizer such as ammonium perchlorate, and a powdered metal fuel such as aluminum. Pyrotechnics were generally composed of an inorganic oxidizer, such as sodium nitrate, a metal powder such as magnesium, and a binder. Other materials used in the industrial operations included acids, lubricants, and solvents, particularly trichloroethene (TCE) and methylene chloride (MC). Waste management included sanitary wastewater treatment, industrial wastewater treatment, holding/evaporation ponds, storm water drainage, sanitary and contaminated waste landfills, and demolition/burning grounds. Discharges and releases to surface water, groundwater, and other secondary media have occurred from the historical operations and practices.

LHAAP was placed on the National Priorities List (NPL) August 9, 1990. A Federal Facility Agreement (FFA) among the USEPA, the U.S. Army, and the Texas Natural Resources Conservation Commission, now the TCEQ, became effective December 30, 1991. LHAAP became inactive in July 1997, and a year later the U.S. Army issued a contract to remove salvageable property. On May 5, 2004, the U.S. Army transferred approximately 5,032 acres to the U.S. Fish and Wildlife Service (USFWS) for management as the Caddo Lake National

Wildlife Refuge. Approximately 800 acres have been transferred to the USFWS since the initial transfer and the process will continue as response is completed at individual sites. The remaining land is under the U.S. Army's control and includes the Group 2 and 4 sites currently undergoing remedial investigation/feasibility study (RI/FS) studies. The U.S. Army intends to transfer this land to the USFWS after the environmental response is completed.

1.2.3 LHAAP-29 Site Summary

1.2.3.1 Operational History

LHAAP-29 was originally listed as an NPL site in the FFA due to threatened releases of hazardous substances, pollutants or contaminants. LHAAP-29 is a heavily wooded, 85-acre site in the western-central portion of the LHAAP installation (**Figure 1-2**). The site is bounded by Avenue E on the southwest, Zeugner Drive (also known as 1st Street) on the northwest, and 18th Street on the southeast (**Figure 1-3**). Avenue D serves as a portion of the northeastern boundary of LHAAP-29 includes the Former Bulk Toluene Storage Area, which is a wooded area that extends for approximately 500 feet northeast of Avenue D. The site is currently inactive, but once contained one standby and five regular TNT production lines. The area still contains the foundations of the former production facilities and the underground pipe lines that were originally built for cooling water drainage and TNT wastewater conveyance.

The production facilities at LHAAP-29 manufactured TNT from October 1942 to August 1945. The facility produced approximately 400 million pounds of flake TNT during its operation. Each production line was essentially the same and consisted of four main elements; an unloading area where acids and toluene were unloaded and held in aboveground storage tanks (ASTs) until use, a nitrating area where flake TNT was produced by nitrating toluene with nitric acid, a wash area where the flake TNT was washed to remove impurities and then dried, and an unloading area where cardboard-boxed flake TNT was loaded onto trucks (Jacobs, 2002).

The former production facilities at LHAAP-29 were served by a network of underground pipelines. The underground lines consisted of TNT wastewater (red liquor) lines and the cooling water (blue water) lines (**Figure 1-3**). The red liquor TNT wastewater line, originally solid waste management unit (SWMU) LHAAP-30 and later included as part of Installation Restoration Program/Defense Site Environmental Restoration Tracking System (IRP/DSERTS) LHAAP-29, was originally installed as a wooden pipeline. The Addendum to the Phase 2 Work Plan noted that the transite waste line was added 5 feet north of the wooden line based on a modified drawing dated March 30, 1943 (Bate Stamp 12651). The transite material is a combination of cement and asbestos. The TNT red water line was clear-flushed in 1946 (Bate Stamp 001446, Resource Conservation and Recovery Act (RCRA) Facility Assessment, April 1988). The transite pipeline was in good condition when it was unearthed in 1993 at a location approximately 400 feet northwest of the pond and at the three locations sampled along the line as

part of the Shaw additional investigation in 2006. The gravity portion of the TNT wastewater line terminates in the pump house area near the intersection of 16th Street with Avenue D.

During TNT production, the wastewater was collected here and pumped through the pressure portion of the TNT wastewater line into storage tanks across Avenue D. The storage tanks and treatment facility are now known as LHAAP-32. As part of the closure, the TNT wastewater pipeline was clear flushed and abandoned in place (Plexus, 2005), and the pump house at LHAAP-29 was removed, and the soil beneath it was excavated. The excavated area subsequently filled with water, and a pond now exists at the former pump house location. The cooling wastewater was conveyed to the Neutralization House (Building 612-A) for neutralization and discharged to surface water.

Two blue cooling water lines exist at LHAAP-29, north and south (**Figure 1-3**), and range from 8 inches to 18 inches in diameter. These gravity fed lines are thought to be constructed of vitrified clay pipe with asbestos wicking. These lines collected water from each TNT washing area. Manholes exist along both the north and south cooling water lines. The northern line is connected to lines from each plant (approximately 280 feet of 10-inch-diameter pipe). The lines drain into a ditch along 16th street which eventually flows into Goose Prairie Creek.

The TNT production facility was inactive from August 1945 to 1959. In 1959, most of the buildings and ASTs were removed. The debris was burned or flashed at Burning Ground No. 2/Flashing Area (LHAAP-17). Concrete foundations, open-top concrete-lined pits, and most of the underground utilities still remain at the site.

Since the end of World War II, the only activity that has been documented to have occurred at LHAAP-29 is the "soak out" of out-of-specification rocket motors. This took place from 1959 to the mid-1970s and involved the use of Turco[®], a MC-based industrial solvent, at tank 801-F. Waste from this operation was sent to LHAAP-18/24 (Jacobs, 2001).

1.2.3.2 Surface Water Hydrology

The terrain of the site generally slopes toward the east and south from a topographic high at the intersection of Zeugner Drive (1st Street) and Avenue E, near the location of former Production Line A. Most of the surface runoff is collected by ditches constructed in 1942 when the production facility was built. Separate drainage ways were constructed for each production line, and these drain to the southeast toward 18th Street. Surface runoff from the northern part of the site (about 40 percent of the site area) enters Goose Prairie Creek located approximately 1,500 feet to the north and east of the site. In the southern portion of the site (about 60 percent of the site), surface runoff flows into a tributary of Central Creek located near the southeast portion of the site (**Figure 1-2**). Via these two creeks, the runoff from LHAAP-29 eventually enters Caddo

Lake. Goose Prairie and Central Creeks, like all drainage systems at LHAAP, are intermittent (Jacobs, 2001).

1.2.3.3 Hydrogeology

Based on investigations, there are three groundwater zones at LHAAP-29: shallow, intermediate, and deep. Clay or silty clay layers separate the three groundwater zones. The shallow groundwater zone has wells that are screened at two depths (shallow and lower shallow); however, the wells have similar water level elevations and are all considered to be shallow zone wells. The depth of the shallow groundwater zone generally ranges from 17 to 45 feet below ground surface (bgs) because of variable ground surface elevations across the site. The intermediate zone is less defined, but its depth has been measured to approximately 88 feet bgs. The deep groundwater zone extends to a depth of approximately 155 feet bgs. The predominant flow of both the shallow and intermediate groundwater zones is to the east/northeast based on November 2007 water levels.

Groundwater in the deep zone under and near LHAAP is currently used as a drinking water source. There are currently five active water supply wells near LHAAP. Known depths of these wells range from 313 to 430 feet bgs and are at least 4,000 feet away from LHAAP. Water removal from these wells is not expected to affect groundwater flow at the site because of the remote locations of these wells from LHAAP and their depth of completion. In addition, there are several livestock and domestic wells located in the vicinity of LHAAP with depths averaging 250 feet. There are three water supply wells located on LHAAP, and they supply water to the buildings currently in use on the installation. None of these wells is used for drinking water. Two additional wells previously supplied water to the installation, but these have been plugged and abandoned. None of the potable water supply wells are associated with or are in imminent danger from the localized contaminated groundwater at any of the Group 2 sites, including LHAAP-29.

1.3 Sampling Investigations at LHAAP-29

The environmental media (soil, groundwater, surface water, sediment, and residue in process water lines) at LHAAP-29 have been the subject of numerous investigations to identify potential contamination and are summarized in **Table 1-1**. These include the Pre-RI investigations by Environmental Protection Systems in 1982 and 1987; the Phase I, Phase II, and Phase III RIs conducted by Jacobs in 1993, 1995, and 1998, respectively; the site-wide perchlorate investigation conducted by Solutions To Environmental Problems, Inc. (STEP) in 2002 and the Environmental Site Assessment (ESA) activities performed by Plexus in 2003. Additional samples were not collected in the ESA, but soil staining was noted around Buildings 806-A and 806-D (Plexus, 2005). Reports mentioned above are included in the AR for the LHAAP.

Between 2004 and 2005, several follow-up investigations at LHAAP-29 were performed by Shaw and USACE to further delineate the extent of contamination identified during the previous sample events. These sample events include the data gaps investigation by Shaw in the spring and summer of 2004 (Shaw, 2007a); additional explosives and perchlorate sampling by Shaw in December 2004 and February 2005 (**Appendix A**), and explosives sampling by USACE at a building foundation in February 2005 (**Appendix A**). A summary of activities and analytical results for the 2004 through 2005, Shaw and USACE sample events, is presented in the *Investigation Results – December 2004 and February 2005* (**Appendix A**).

Between August 2006 and February 2008, Shaw conducted additional investigation activities for various environmental media at LHAAP-29. The objective of this sampling event was to collect samples of the transite wastewater line residual contents, sediment samples along the former cooling water ditch, and groundwater from existing and newly installed monitoring wells to further delineate the extent of contamination at the site. A summary of activities and data results for these sample events are included in the *Additional Investigation Data Summary Report* (**Appendix B**).

In October 2008 and January 2009, additional groundwater samples were collected and analyzed for metals and volatile organic compounds (VOCs) in the shallow and intermediate zones.

In June 2009, one new monitoring well (29WW41) was installed and sampled for VOCs to determine whether groundwater in the upper deep zone immediately below the highest MC concentration in the intermediate zone (at 29WW16) showed any evidence of contamination. Well 29WW41 was screened at a depth of 102.5 to 117.5 feet bgs. A groundwater sample was collected for VOC analysis. This deeper well was installed to evaluate the potential downward migration of contaminants in the intermediate zone. Only VOCs have been identified as COCs in the intermediate zone, and thus the sample was analyzed for VOCs.

The sample locations from all phases of investigations performed at LHAAP-29 are presented on **Figures 1-4** through **1-7** for soil, sediment and surface water, and groundwater, respectively.

1.4 Additional Evaluations at LHAAP-29

The baseline ecological risk assessment (BERA) was completed in February 2007 (Shaw, 2007b). The BERA concluded there is an ecological impact in an isolated area at LHAAP-29, as discussed in **Section 2.2**.

Appendix B includes the Activated Persulfate Oxidation Treatability Study Report completed by Shaw in 2006 to evaluate the effectiveness of chemical oxidation using activated sodium persulfate to treat the MC groundwater plume in the intermediate zone. The treatability study

concluded that heat- and alkaline-activated persulfate oxidation was the best treatment evaluated for the reduction of MC.

In February 2007, monitored natural attenuation (MNA) was evaluated by Shaw as a potential site remedy at LHAAP-29. The results and conclusions of the assessment are included in the *Natural Attenuation Evaluation* for LHAAP-29 presented in **Appendix C**.

In February 2007, Shaw issued a modeling report that concluded the VOC contaminants in the shallow zone will not reach Central Creek. The model indicates that even though perchlorate reaches the creek, the concentration in surface water will be below the surface water action level (Shaw, 2007c). Thus, there is no impact of surface water from the shallow groundwater at LHAAP-29.

Table 1-1 Summary of Investigations at LHAAP-29

Pre-Phase I (Jacobs, 2001)

LHAAP Plant Contamination Survey Environmental Protection System, June 1984

- Six monitoring wells were installed and sampled (114 to 119)
- Four surface water and four sediment samples were collected (stations 005-008)
- Eight soil samples were collected within the former TNT production area

Final Remedial Investigation Report for LHAAP, Karnack, Texas, Environmental Protection System, May 1988

- Six groundwater samples were collected from existing monitoring wells
- Thirty-five soil boreholes were sampled at the 0-0.5', 1-1.5', 2-2.5' and 3-3.5' intervals
- Four surface water and four sediment samples were collected

Phase I - Phase III (Jacobs, 2001)

Jacobs, Phase I, 1993

- Eighteen surface water and 18 sediment samples were collected (29SW01-29SW18 and 29SD01-29SD18)
- Seventy-five soil samples were collected from borings 29SB01-29SB15
- Four waste line samples were collected
- Groundwater samples were collected from the existing wells 114-119

Jacobs, Phase II, 1995

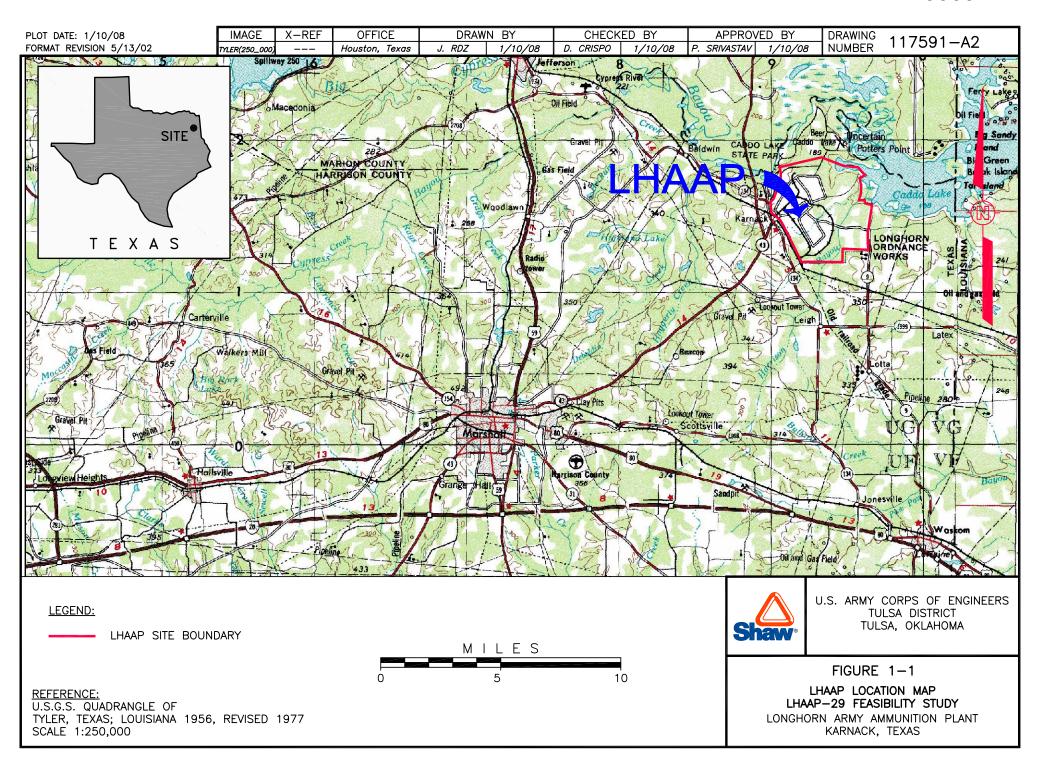
- Three surface water and three sediment samples were collected (29SW19-29SW21 and 29SD29-29SD21)
- Forty-four soil samples were collected from borings 29SB53-29SB76
- Four waste line samples and six waste line associated soil samples were collected
- Eleven monitoring wells were installed (29WW01 29WW11) and groundwater was collected from each new well and from six existing wells (114-119)

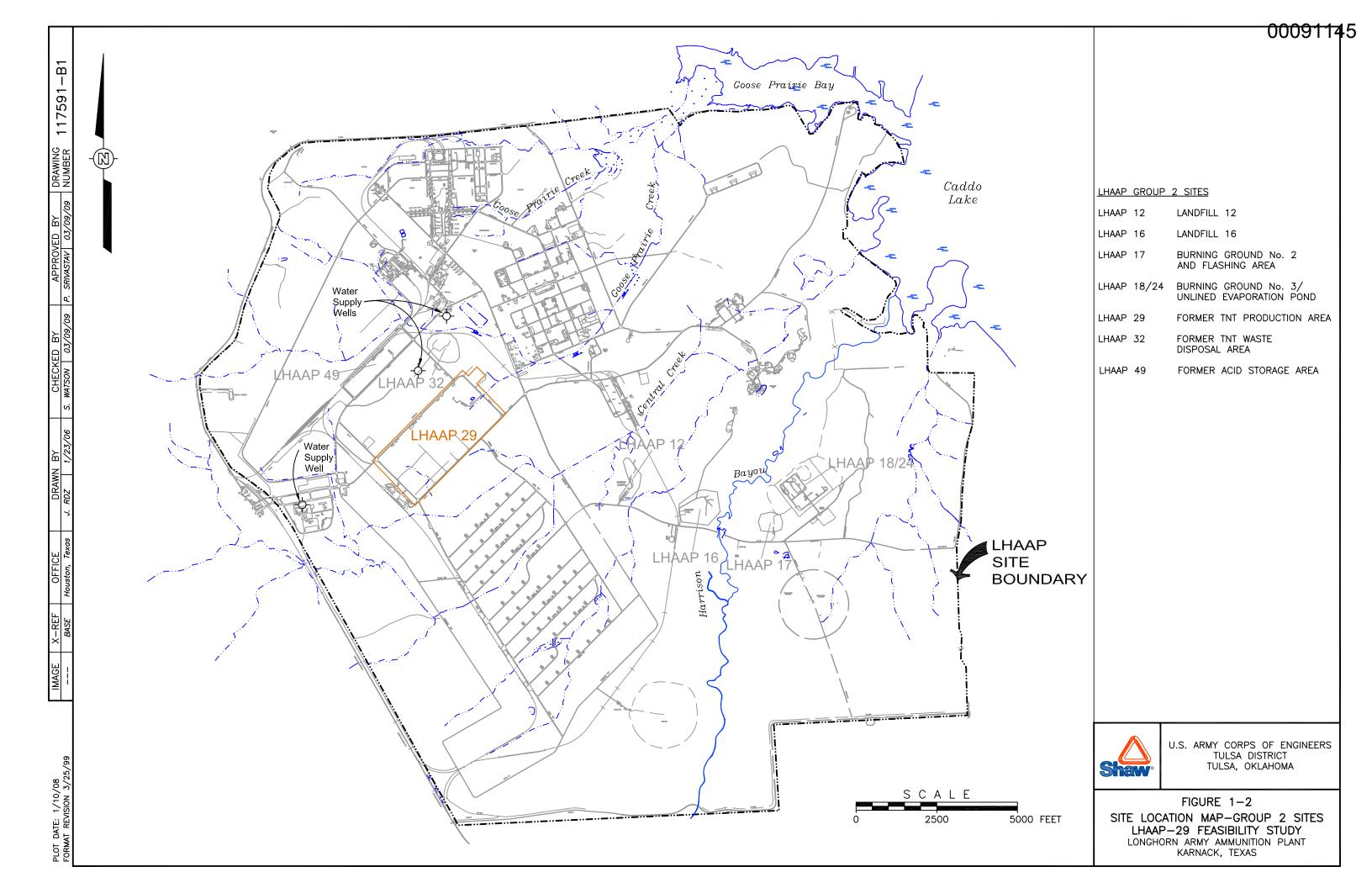
Jacobs, Phase III, 1998

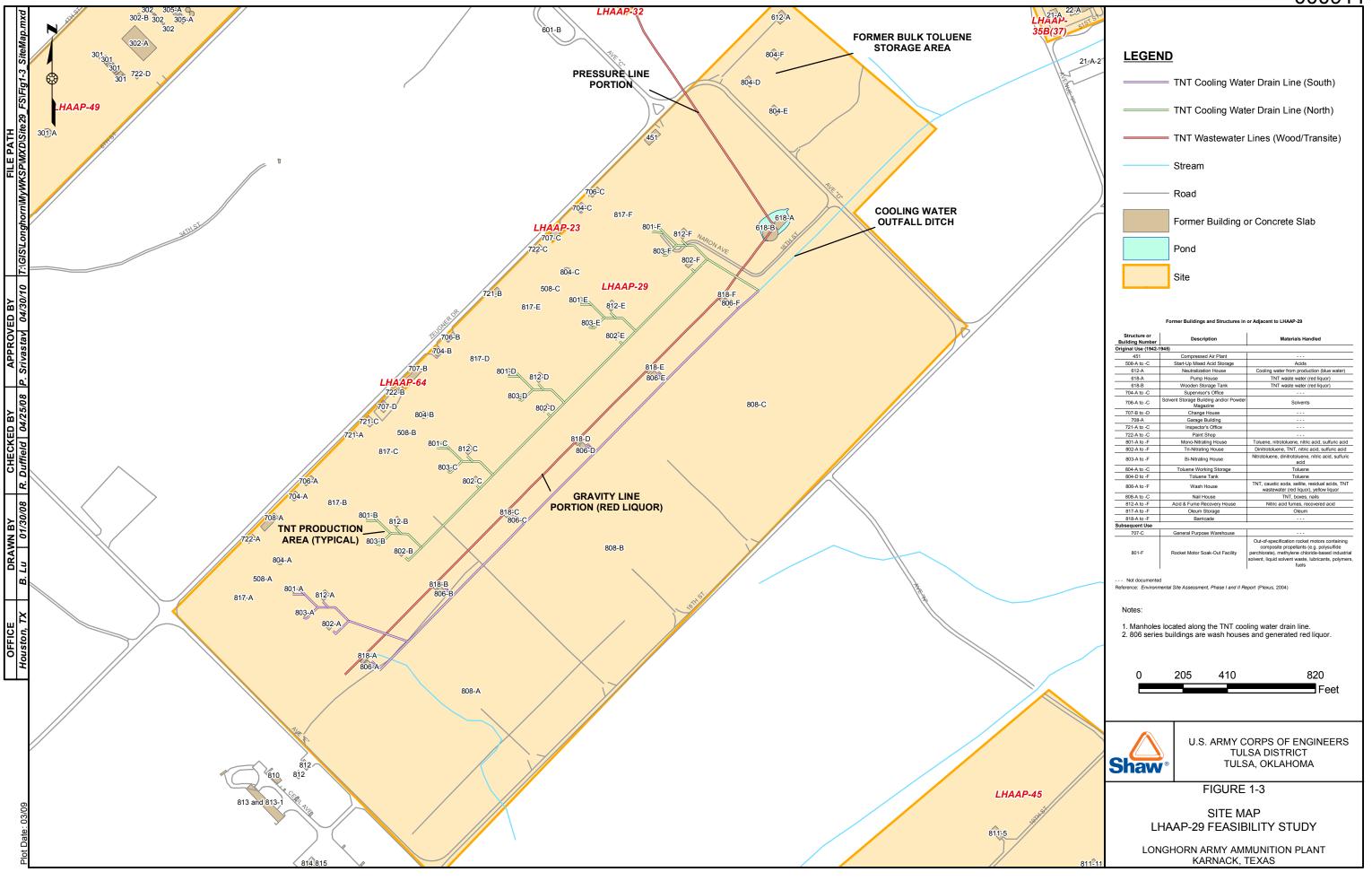
- Ten surface water and ten sediment samples were collected (29SW22-29SW31 and 29SD22-29SD31)
- Fourteen soil samples were collected from borings 29SS01 29SS08
- Twenty-two monitoring wells were installed (29WW12-29WW33) and groundwater was collected from each new well and from 17 existing wells (114-119 and 29WW01-29WW11)

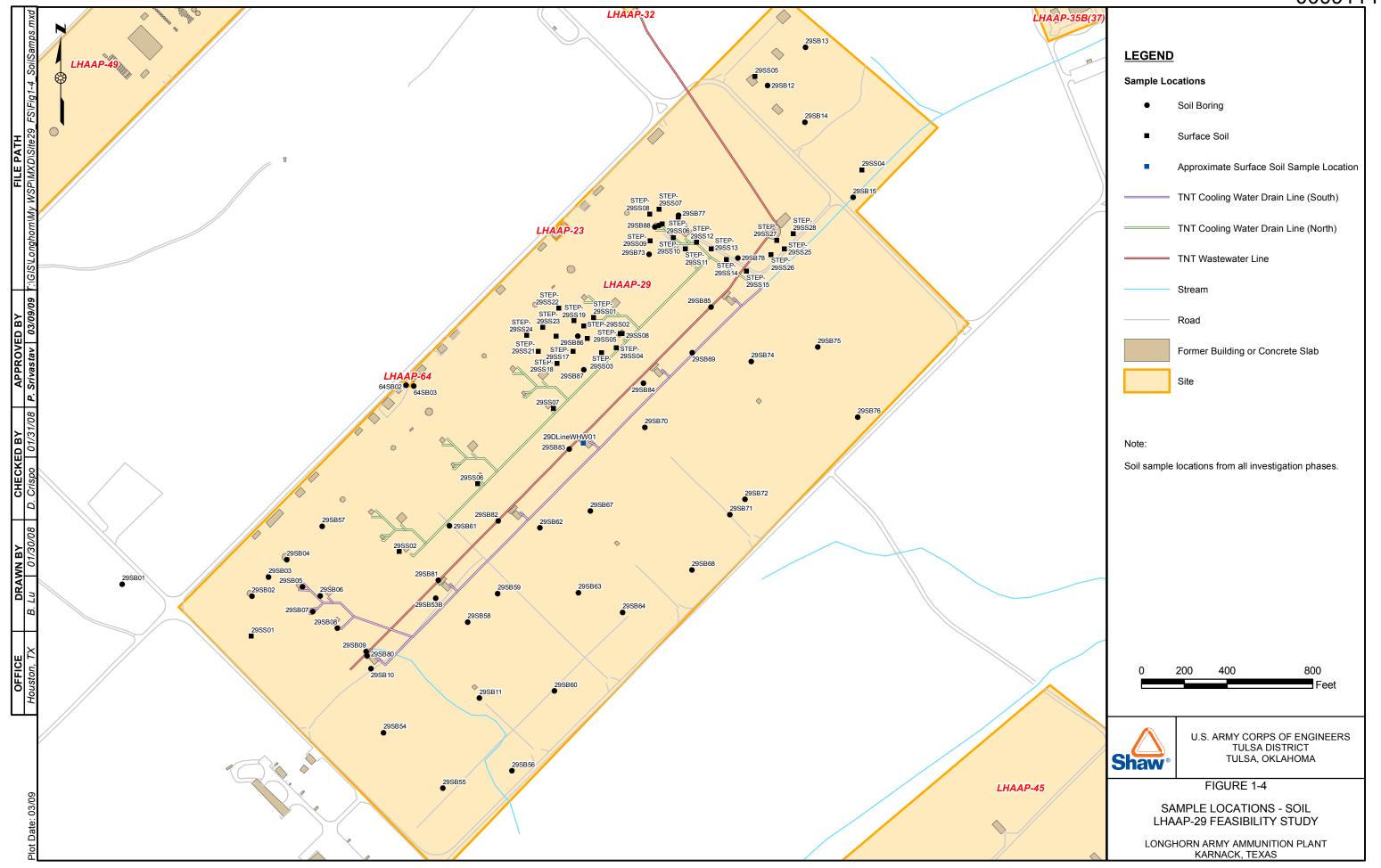
Additional Investigations

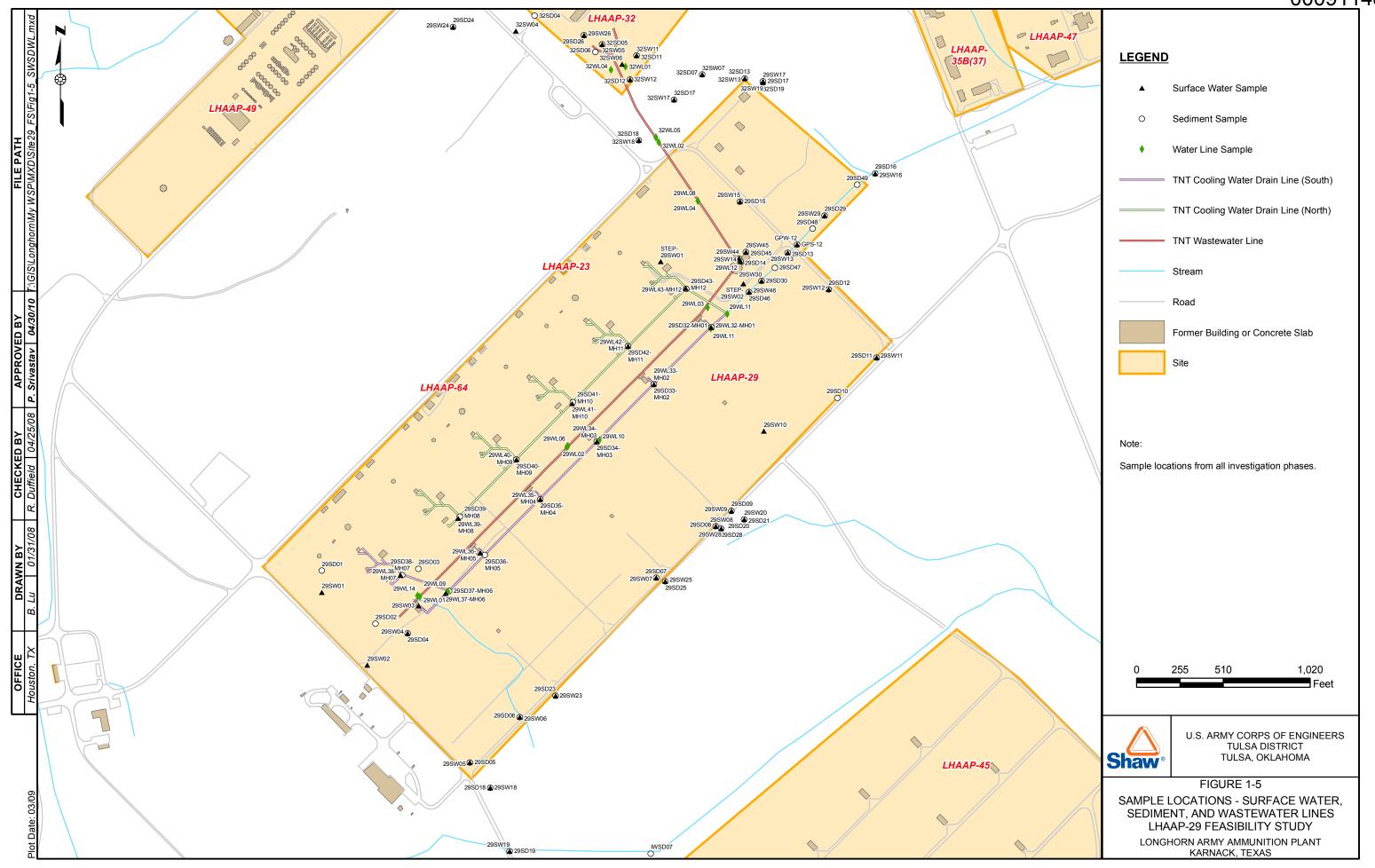
- Collected 56 soil samples and 72 groundwater samples for perchlorate analysis in 2000 through 2002 (STEP, 2005)
- Soil staining verified TNT through field tests at 2 locations (Plexus, 2005)
- USACE sampling of stained soil (Appendix A, Table A-5)
- Collected 10 soil samples from borings (29SB81-29SB85) for explosives, and 12 soil samples from borings (29SB86-29SB89) for perchlorate in 2004. (Appendix A)
- Collected 8 solid residue samples from manholes and 3 sediment samples from ditches (up through 29SD46) for explosives analysis in 2004. (Shaw, 2007a)
- Collected groundwater samples from 20 wells for explosives, VOCs and perchlorate in 2004. (Shaw, 2007a)
- Collected groundwater samples from 41 wells for explosives, VOCs and perchlorate in 2005. (Shaw, 2007a)
- Collected 3 sediment samples from ditches (29SD47-29SD49), 3 solid residue samples from the transite waste line for explosives analysis, and 1 deep soil sample (29WW40) for VOCs analysis in 2006. (Appendix B)
- Six monitoring wells were installed (29WW35-29WW40) and 15 groundwater samples were collected for volatiles, 11 for general chemistry, and 2 for perchlorate in 2006. (Appendix B)
- Collected 2 groundwater samples from 29WW37 and 29WW39 for VOCs analysis in February 2008. (Appendix B)
 Collected groundwater samples from 5 wells for natural attenuation evaluation (biological, VOCs, explosives, gases,
 general chemistry) in 2007. (Appendix C)
- Collected 20 additional groundwater samples for metals and VOCs in 2008 (Appendix D)
- Installed new well, 29WW41, in the upper deep zone and sampled the well for VOCs (Appendix D)

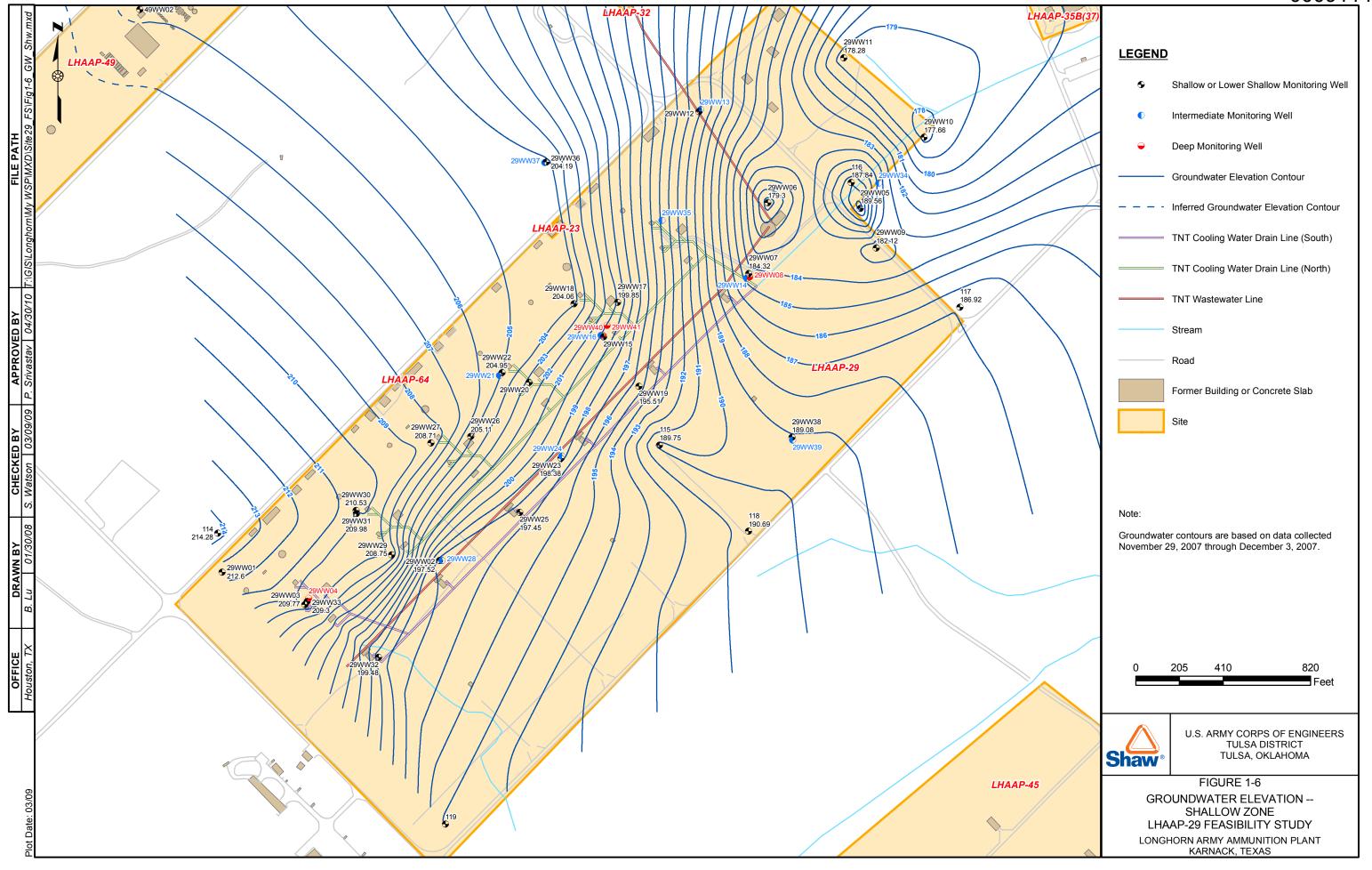


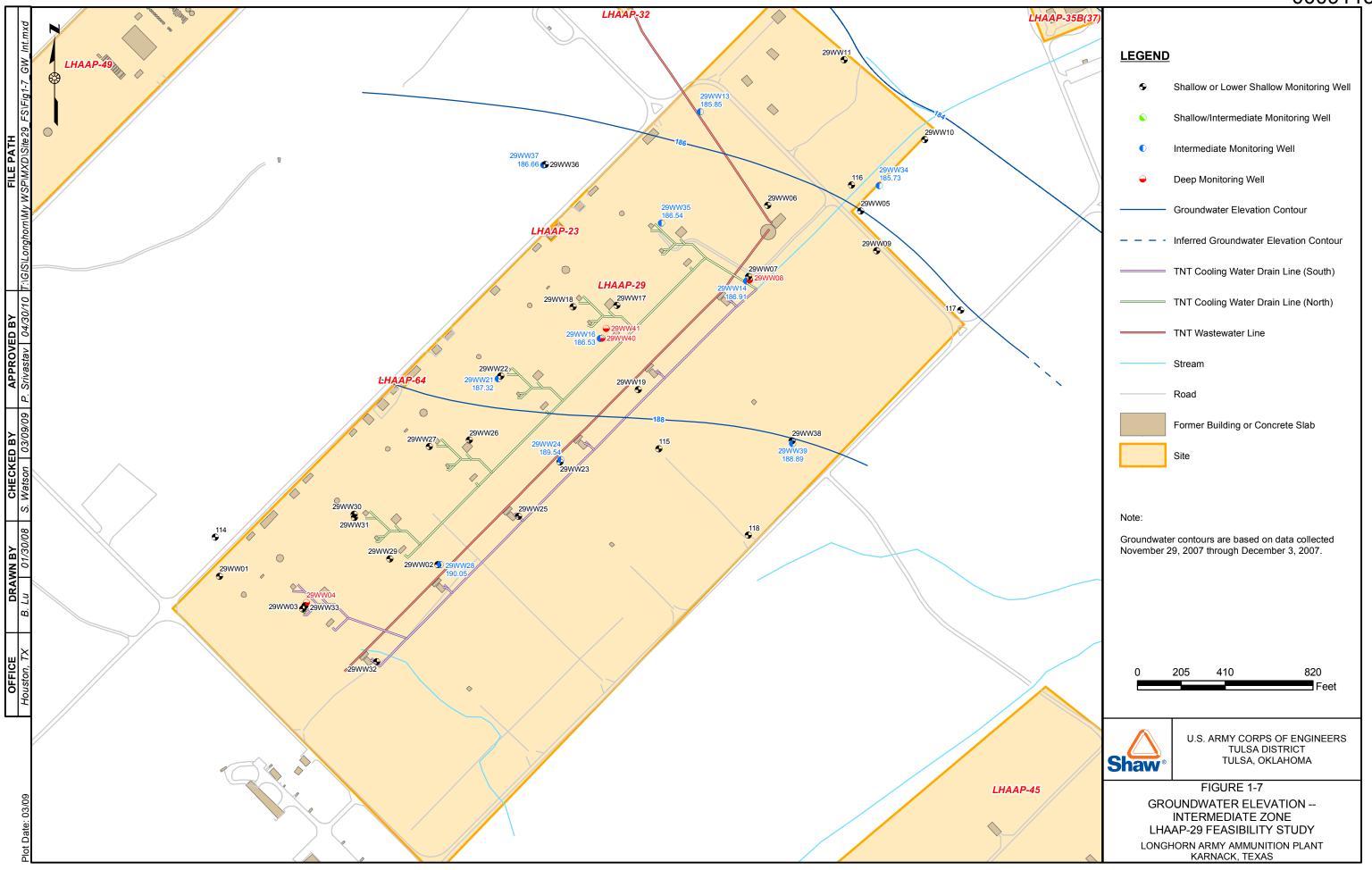












2.0 Risk and Site Assessment

This section summarizes the risk assessment approach, risk conclusions, media contamination evaluation, and the conceptual site model for LHAAP-29. Information in this section is based on data obtained from the following references:

- Group 2 Sites RI (Jacobs, 2001)
- Group 2 Sites Baseline Human Health Risk Assessment Report (Jacobs, 2002)
- Groups 2 and 4 Groundwater Data Gaps Investigation (Shaw, 2007a)
- Installation-Wide Baseline Ecological Risk Assessment (Shaw, 2007b)
- Environmental Site Assessment (Plexus, 2005)

2.1 Human Health Risk Assessment

This summary is based on the conclusions presented in the *Final Baseline Human Health and Screening Ecological Risk Assessment for the Group 2 Sites* (Jacobs, 2002). The Jacobs risk assessment presented the human health risks and hazards to a hypothetical future maintenance worker under an industrial scenario for soil and groundwater and a screening level ecological risk assessment. For the risk assessment, soil and groundwater data were used to calculate the aggregate risk values, which were then compared to the USEPA target risk range of 1×10^{-4} to 1×10^{-6} for the excess lifetime cancer risk (ELCR) and a hazard index (HI) of 1.

2.1.1 Soil

For the hypothetical future maintenance worker exposure to soil at LHAAP-29, the carcinogenic risk of 7.3×10^{-6} is within the USEPA target risk range of 1×10^{-4} to 1×10^{-6} ELCR, but the non-carcinogenic hazard has an HI of 1. Chemicals in soil with a hazard quotient (HQ) greater than 0.1 are listed in **Table 2-1**.

2.1.2 Groundwater

For the hypothetical future maintenance worker's exposure to the groundwater at LHAAP-29, the carcinogenic risk and non-carcinogenic hazard exceed the acceptable limits. Groundwater chemicals with unacceptable risk were also compared to their associated Safe Drinking Water maximum contaminant levels (MCLs), if applicable. The total carcinogenic risk from groundwater for a hypothetical future maintenance worker is 3.9×10^{-1} . The total HI is 3,000. Chemicals with a risk greater than 1×10^{-6} , and a HQ greater than 0.1 are listed in **Table 2-2** and **Table 2-3**, respectively. The data were evaluated to determine if the chemical should be retained as a COC as shown in **Table 2-2** and **Table 2-3**.

2.2 Ecological Risk Assessment

The Final Installation-Wide Baseline Ecological Risk Assessment (Shaw, 2007b) evaluated potential hazards to ecological resources at LHAAP by conducting a screening evaluation to identify initial contaminants of potential ecological concern (COPEC) in the individual sub-areas and watersheds. The potential of these COPECs to adversely affect communities was evaluated for (1) organisms that have direct contact with the COPECs (e.g., plants and earthworms growing and living in contaminated soil); and (2) organisms that may be exposed to the chemicals via food chain pathways (e.g., ingestion of an earthworm living in the contaminated soil by a shrew). Potential impacts to invertebrate and plant communities were evaluated by comparing COPEC concentrations to benchmark values available from multiple literature sources. For the food chain exposure assessment, a number of measurement receptors were selected as representative species for the various trophic levels in the food web that could be at risk from contaminants in site media. The measurement receptors that were selected and used in the food chain evaluation included the following:

- Deer Mouse
- Raccoon
- Modified Raccoon (as a surrogate for the Louisiana Black Bear)
- Short-Tailed Shrew
- Red Fox
- Muskrat
- River Otter
- Townsend's Big-Eared Bat
- Common Snapping Turtle
- Bank Swallow
- American Woodcock
- Belted Kingfisher
- Red-Tailed Hawk

A food chain model was developed and used to estimate the total dose for each measurement receptor based on species-specific considerations such as diet, body weight, ingestion rates, etc., using conservative exposure estimates. Ecological hazard estimates were developed based on exposure to all media including soil in a particular sub-area and surface water and sediment from any watersheds present in the sub-areas. Two different soil depths were used for modeling exposure to ecological receptors: surface soil (0 to 0.5 foot) and total soil (0 to 3 feet). Each receptor was assumed to be exposed to one of the two depths based on its life history characteristics (e.g., burrowing animals were assumed to be exposed to total soil). Bioaccumulation of chemicals up the food chain was initially estimated using uptake factors

obtained from available literature, and then refined using site-specific data obtained during the BERA.

Ecological effects quotients (EEQ) were developed for each of the measurement receptors. EEQs are similar to HQs for human health, and are calculated by dividing the total dose that the receptor is exposed to by the toxicity reference value (TRV), which is based on a no-observed adverse effect level (NOAEL) or the lowest-observed adverse effect level (LOAEL) concentration. If the EEQ exceeds 1 for a receptor (based on the NOAEL TRV), then that chemical is considered to have a realistic potential to cause adverse ecological impacts, and is identified as a final COPEC that should be addressed either through remediation or further investigation. As discussed in the BERA, there are several important uncertainties associated with the assumptions used in the EEQ process, and it should be noted that EEQs greater than 1 do not necessarily mean that ecological impacts have occurred, or are occurring.

For the Industrial Sub-Area (which includes LHAAP-29) four chemicals were selected as final COPECs: cadmium, chromium, zinc, and perchlorate. After that selection, additional sampling data became available, and further analysis was performed, leading to the calculation of ecological preliminary cleanup levels (EcoPRGs) for several chemicals in soil. The final COPECs that were initially selected were found to not be of concern and EcoPRGs were calculated for six other chemicals: barium, lead, 2,4-dinitrotoluene (DNT), 2,6-DNT, TNT, and 2,3,7,8-tetrachlorodibenzo-p-dioxin (TCDD).

Ecological hazards were found to be acceptable for the Industrial Sub-Area that includes LHAAP-29; however, elevated concentrations of nitrotoluenes (TNT, 2,4-DNT and 2,6-DNT) were identified at one location at the site (Shaw, 2007a). Although nitrotoluenes were not selected in the Industrial Sub-Area as final COPECs due to low frequency of detection and other considerations, the BERA evaluated measurement receptors and included a spatial analysis at this sample location at LHAAP-29. The results of this analysis identified that the nitrotoluenes at this location and the adjacent areas may represent a small area of highly elevated concentrations (i.e., a hot spot) that could pose a threat to small-range ecological receptors either through acute toxicity, or as a source area for downgradient surface water transport of contamination (Shaw, 2007b). Therefore, the nitrotoluenes are considered as COPECs at LHAAP-29 are compared to EcoPRGs in **Table 2-4**.

With the exception of the nitrotoluene hot spot near sample location 29SD46 along the former cooling water outfall ditch, ecological hazard was determined to be within acceptable limits in the Industrial Sub-Area, and therefore within LHAAP-29. The soil in the former cooling water outfall ditch is thought to be contaminated as a result of deposition, spills, and/or runoff of contamination on the surface. This residual contamination poses a potential risk to ecological

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receptors due to the direct contact with soil and indirect (i.e., dietary) exposure routes. The principal ecological risk drivers for the soil in the ditch are TNT and its breakdown products.

2.3 Evaluation of Data Collected Since the Risk Assessment

The risk assessment was completed using data from the samples through February 2001 for groundwater and through 1998 for soil samples. Since that time, additional groundwater and soil samples have been collected and analyzed.

2.3.1 Soil

Additional soil samples were collected during the perchlorate investigation in 2002 (STEP, 2005), during the data gaps investigation in 2004 (Shaw, 2007a), and in the USACE 2005 sampling of stained soil at Wash Building 806-D (Appendix A). The following text discusses chemicals that were detected in the 2004 and 2008 investigations (after the risk assessment) with concentrations higher than their associated exposure point concentration (EPC) used in the risk assessment.

From the data gaps investigation, the maximum perchlorate concentration detected in soil was 8.6 milligrams per kilogram (mg/kg) in sample 29SB86-002 (Shaw, 2007a). This is greater than the EPC for perchlorate of 0.0703 mg/kg used in the risk assessment, with an associated HO of 8.1×10^{-5} (Jacobs, 2002). Using ratios of the HQ to the perchlorate concentrations, the HQ for the maximum concentration of perchlorate detected since the risk assessment would yield a HQ of 0.0099. Thus, perchlorate in soil does not pose a hazard to human health. However, perchlorate is a contaminant in the groundwater. The most recent soil sample with a perchlorate concentration of 8.6 mg/kg exceeds the soil medium-specific concentration (MSC) for industrial use based on groundwater protection (GWP-Ind) (TCEQ, 2006) of 7.2 mg/kg for perchlorate. Thus, perchlorate in soil will be carried as a COC with the potential to migrate to groundwater.

The maximum 2-amino-4,6-DNT concentration detected in soil from the data gaps investigation was 48 mg/kg in sample 29SD46 (Shaw, 2007a). This is greater than the EPC for 2-amino-4,6-DNT of 25 mg/kg used in the risk assessment with an associated HQ of 0.33 (Jacobs, 2002). Using ratios of the HQ to the 2-amino-4,6-DNT concentrations, the HQ for the maximum concentration of 2-amino-4,6-DNT detected since the risk assessment would yield a HQ of 0.63, still less than 1.0 and not carried as a COC.

The maximum 2,4-DNT concentration detected in soil was 8,000 mg/kg in sample 29SD46 collected during the data gaps investigation (Shaw, 2007a). The risk assessment EPC for 2,4-DNT was 6.2 mg/kg, with an associated HQ of 0.0053 (Jacobs, 2002). Using ratios of the HQ to the 2,4-DNT concentrations, the HQ for the maximum concentration of 2,4-DNT detected since the risk assessment would yield a HQ of 6.8, which is unacceptable. Thus, 2,4-DNT will be carried as a COC for human health. The higher recent maximum also caused 2,4-DNT to be selected as a COPEC.

The additional detected soil sample results were less than the EPCs and do not change the conclusion of the risk assessment that soil poses an unacceptable total HI. The recent results indicate that 2,4-DNT and perchlorate should be added as COCs. **Figure 2-1** shows areas of soil contamination.

2.3.2 Groundwater

Additional groundwater samples have been collected since the risk assessment and analyzed for explosives, perchlorate, VOCs, semivolatile organic compounds (SVOCs), and attenuation parameters (**Appendices B** and **C**). No new chemicals were detected that would change the listed chemicals in **Table 2-2** or **Table 2-3**. Eight chemicals, (MC, 1,2-dichloroethane [DCA], 2,4-DNT, 2,6-DNT, arsenic, TCE, 2,3,7,8-TCDD, and chloroform) had a carcinogenic risk greater than 1×10^{-6} . Seventeen additional chemicals, (perchlorate, 4-nitrotoluene, 2-nitrotoluene, nickel, 3-nitrotoluene, aluminum, antimony, barium, selenium, manganese, vanadium, thallium, 2-amino-4,6-DNT, 4-amino-2,6-DNT, strontium, silver and cadmium) had an HQ greater than 0.1. **Figures 2-2** through **2-4** show areas of groundwater contamination.

The EPCs for 2,3,7,8-TCDD and chloroform were less than the MCLs and these chemicals were not retained as COCs.

Additional Sampling 2008 and 2009

In October 2008, groundwater samples were collected and analyzed for (1) VOCs in the intermediate wells within the VOC plume and (2) for metals in all three zones since the last sampling round for metals was conducted in 1998.

Four intermediate wells were sampled for VOCs. Prior to sampling, VOCs were found in two wells, but after the latest round only one well, 29WW16, had high VOC detections. Of the VOCs, MC has the highest concentration at 10,300,000 micrograms per liter (μ g/L), which is approximately 50% of saturation. Thus, based on this data, the plume boundary in the intermediate zone is shrinking. **Figure 2-4** shows the plume in the intermediate zone.

Seventeen wells from all three groundwater zones were sampled for metals in October 2008. It was suspected that sampling methodology may have influenced the historic results showing elevated levels of metals. The 2008 results were generally lower than previous results and many of the chemicals were excluded as COCs, as noted on **Tables 2-2** and **2-3**. However, nickel, arsenic and selenium still indicated a risk or hazard, and mercury and chromium were detected at concentrations above their MCLs.

Of the 80 nickel samples collected since 1993, nickel was detected above the groundwater MSC for industrial use (GW-Ind) of 2,000 μ g/L in only 3 samples. Prior to 2008, the nickel concentration in only one well had an associated HQ greater than 1 (8,400 μ g/L at 29WW11 in April 1995). The 2008 result from this well had a concentration of 40 μ g/L. In 2008, the highest nickel concentration was found at 29WW07 with 3,190 μ g/L and would have an HQ greater than 1.0. Previous results for 29WW07 were less than 40 μ g/L in May 1995 and 600 μ g/L in July 1998. Thus, high nickel concentrations in individual wells have not been repeatable or consistently detected. The isolated high nickel concentrations at 29WW07 and 29WW11 coincided with elevated chromium concentrations (i.e., above the MCL of 100 μ g/L for chromium), indicating that corrosion of the stainless steel well material is a likely source of the high nickel concentrations. The extent of nickel in groundwater will be assessed site-wide during remedial design.

Of the 80 arsenic samples collected since 1993, arsenic was detected above the MCL of 10 µg/L in only 7 samples. Four of the elevated results (115, 29WW16, 29WW20, and 29WW25) were obtained in 1998 or before. It was suspected that the elevated concentrations could be a result of sampling methodology and/or turbid samples. In 2008, nineteen additional samples were collected including the two wells with the highest historic concentrations (59 µg/L at shallow well 29WW25 and 44 μg/L at intermediate well 29WW16). The wells were redeveloped prior to sampling. In 2008, only 3 samples (116, 29WW08, and 29WW25) had arsenic concentrations above the MCL. The well with the highest concentration (29WW25) had high turbidity (237.1 nephelometric turbidity units) and was noted to be reddish brown. This sample result is questionable due to the high turbidity. The next highest sample (116) was qualified as an estimated value since the field duplicate relative percent difference criteria was exceeded. It should also be noted that the aluminum concentration was high at 430 µg/L. This sample result is also questionable due to quality control issues. The third sample from deep well 29WW08 had arsenic concentrations of 40.1 μg/L with a high aluminum concentration of 713 μg/L. The high aluminum concentrations in the same sample indicates that the arsenic may be naturally Additionally, this deep well is clustered with a shallow well, 29WW07, and intermediate well, 29WW14, neither of which has had an arsenic detection. contamination is not from vertical migration. The extent of arsenic in groundwater will be assessed site-wide during remedial design.

Of the 80 selenium samples collected since 1993, selenium was only detected above the MCL of $50 \,\mu\text{g/L}$ in one shallow zone well, 118. The selenium concentrations have fluctuated over the years. The most recent concentration has an associated adjusted HQ of 0.15. Therefore, selenium is not considered a COC.

Of the 80 mercury samples collected since 1993, mercury has been detected only twice, both in shallow zone Well 118. The latest round from 2008 detected mercury at $6.1 \mu g/L$ in Well 118 -

higher than the previous result of 3 μ g/L in 1993. The MCL for mercury is 2 μ g/L. In 1995 and 1998, mercury was not detected (less than detection limit of 0.2 μ g/L) in Well 118. Mercury is not detected in any other well, and the detections are intermittent and appear to be isolated. Well 118 is located along the southern edge of the site, away from active industrial areas that are possible sources. Mercury was detected at low concentrations in three soil samples (29SB04, 29SB12 and 29SB55) and one sediment sample (29SD13), but all of these locations are more than 1,500 feet from Well 118. Sample results from wells located between the soil sample locations and Well 118 did not detect mercury. Soil and sediment samples near Well 118 (29SD08, 29SD09, 29SB71, and 29SB72) did not show any detectable mercury, so the mercury in groundwater is not related to the mercury in soil. Additionally, the Final Baseline Human Health and Screening Ecological Risk Assessment for Group 2 Sites (Jacobs, 2002) calculated a HI of 0.098 for mercury in groundwater using the maximum mercury value of 3 μ g/L. Adjusting this HI for the new higher maximum of 6.1 μ g/L gives an HI of 0.20, still less than 1.0. The extent of mercury in groundwater will be assessed site-wide during remedial design.

Of the 84 chromium samples collected through January 2009, chromium has been detected several times. However, the higher concentrations that exceed the MCL are less frequent and are typically not reproducible in a well. Some of the wells sampled in 2008 with concentrations greater than the MCL were cloudy, murky or reddish/brown and four of these wells were resampled in January 2009. Of the four wells sampled, only one had a chromium concentration above the MCL. The wells at LHAAP-29 are stainless steel with stainless well screens. At three other LHAAP sites (LHAAP-12, LHAAP-49, and LHAAP-53) where chromium concentrations had isolated occurrences above the MCL, a collocated polyvinyl chloride (PVC) well was installed. In most cases, chromium concentrations in the PVC well were much lower and below MCLs. The isolated chromium concentrations above the MCL are not indicative of wide-spread contamination in the groundwater and could be attributable to well materials and sampling methodology. Additionally, no risk was identified from chromium. Thus, chromium is not considered a COC at LHAAP-29.

A sample was collected from the newly installed well, 29WW41, in the upper deep zone and analyzed for VOCs, which were not detected in the sample. Therefore, groundwater in the upper deep zone is not affected by VOCs.

Tables 2-2 and **2-3** have been revised to reflect the new data and adjusted HQs for individual chemicals. **Appendix D** contains the table of the results and analytical data reports from the October 2008, January 2009, and June 2009 sampling events.

The results obtained from the post risk assessment groundwater samples do not alter the risk assessment conclusion that groundwater poses risk. The results do remove some of the potential

COCs listed in the risk assessment and confirm the MC plume is stable. The post risk assessment data was used to determine the COCs as indicated on **Tables 2-2** and **2-3**.

2.3.3 Process Lines

At LHAAP-29 there are red liquor TNT wastewater lines (transite and wooden) and blue cooling water lines with manholes (north and south). It should be noted that the explosives sample results from Phase I and Phase II (29WL01 through 29WL11) were deemed unusable for environmental decision making per USEPA (Jacobs, 2002). Additional investigations were conducted for both lines since the risk assessment (**Appendices A** and **B**).

2.3.3.1 TNT Wastewater Lines

During the Phase I Remedial Investigation, the transite TNT wastewater line was found at 29WL04 and 32WL02 but was not found near 29WL01, 29WL02, and 29WL03. This investigation also noted that the wood stave line was found to be soft and severely weathered. Soil samples (29SB81 through 29SB85) were collected in 2004 along the wastewater line near the wash house sumps to check for contamination possibly leaking from the wooden wastewater line into the surrounding soil (**Appendix A**). In 2006, the transite line was found approximately 5-feet north of the wooden line location and sampled near original locations 29WL01 (2006 sample ID 20WL14), 29WL02 (2006 sample ID 29WL13), and 32WL02 (2006 sample ID 32WL05) (**Appendix B**).

The risk assessment contained soil EPC values for 2,4,6-TNT (190 mg/kg), 2-amino-4,6-DNT (25 mg/kg), and 4-amino-2,6-DNT (16 mg/kg). The other explosives were not detected. In 2006, the sample results for 2,4,6-TNT at 29WL13 was above the EPC. The results of the other two explosives were below their EPCs. For evaluation of the additional data collected in 2004 and 2006, the results were compared to soil MSC for industrial use (SAI-Ind) and GWP-Ind values. There were several explosives detected in the transite wastewater line that were above the GWP-Ind. Table 2-5 summarizes the solid residue sample results from within the TNT transite wastewater line that are above the GWP-Ind. Only two explosives (2,4,6-TNT and 2,4-DNT) had concentrations above the SAI-Ind in the solid residue from within the pipe. The explosive sample results above the SAI-Ind in the solid residue from within the transite pipe are shaded in Table 2-5. The sample locations are shown on Figure 2-5.

Samples of soil (29SB81 – 29SB85) were collected near the wooden TNT wastewater line in 2004 and were analyzed for explosives (**Appendix A**). **Table 2-6** lists the detected explosive concentrations in the samples from the soil near the TNT wooden wastewater line. The concentrations were all below their associated EPC. These concentrations were also compared to both the SAI-Ind and GWP-Ind, and no exceedances were found in the soil near the wooden TNT wastewater line. The sample locations are shown on **Figure 2-5**.

2.3.3.2 Cooling Water Lines

LHAAP-29 was constructed with two vitrified clay cooling lines as shown on **Figure 2-5**, referred to as the north and south cooling water lines. These lines are accessible through manholes. Liquid and solid residue from these manholes were sampled in 2004 (**Appendix A**). 1,3,5-trinitrobenzene (TNB); 2,4,6-TNT; 2,4-DNT; 2,6-DNT; 2-amino-4,6-DNT; and 4-amino-2,6-DNT were detected. None of the detected explosives were above the EPCs in the risk assessment. The detected results were also compared to the GWP-Ind Several explosives were detected above the GWP-Ind in both the north and south cooling lines. The detected concentration of 1,3,5-TNB (0.440 mg/kg) at MH02 was less than the GWP-Ind of 310 mg/kg and is not shown on **Table 2-7**.

Liquid samples were also collected from the cooling water line manholes. The detected explosives in the water in the manholes of both the north and south lines included 1,3,5-TNB, 2,4,6-TNT, 2,4-DNT, 2,6-DNT, 2-amino-4,6-DNT, and 4-amino-2,6-DNT. **Table 2-8** lists the detected liquid samples that were above the GW-Ind. For MH09, there were two sets of samples collected (2004 and 2005). Though some of the results from the 2005 sampling round are lower than the GW-Ind, they have been included in **Table 2-8**. Both the north and south cooling lines have sample results that indicate the liquid within the cooling water lines was above the GW-Ind.

2.4 Media Contamination Assessment

Chemicals in the soil and groundwater at LHAAP-29 pose an unacceptable risk to human health. Chemicals in soil may also have the potential to leach into groundwater, or have an unacceptable risk to ecological receptors. Evaluation of data generated after the risk assessment did not identify any additional COCs with risks exceeding the USEPA target risk level of 1×10^{-4} or an HQ greater than 0.1 as shown on **Table 2-1**, **Table 2-2**, and **Table 2-3**.

2.4.1 Soil

Based on the human health risk assessment, soil at LHAAP-29 poses an unacceptable non-carcinogenic hazard to a hypothetical future maintenance worker at LHAAP under an industrial scenario.

Soil contaminants identified as having an HQ greater than 0.1 in the risk assessment are listed in **Table 2-1**. From the additional investigation, 2,4-DNT was detected at higher concentrations than the EPC and resulted in an HQ greater than 1. Soil contaminants identified as posing ecological risks are listed in **Table 2-4**. The emerging contaminant, perchlorate, was detected at concentrations higher than the GWP-Ind. Thus, the COCs and COPECs for the LHAAP-29 soil are three explosives (2,4,6-TNT, 2,4-DNT and 2,6-DNT) and perchlorate.

Soil contamination from explosives that pose human health risks (2,4,6-TNT and 2,4-DNT) at LHAAP-29 is shown on **Figure 2-1**. The area around 29SD46 is the only area to pose human

health risks and has rough rectangular dimensions of 120 feet by 20 feet to a depth of 1 foot for a total volume of 90 cubic yards (cy).

The one perchlorate exceedance of the GWP-Ind is also plotted on **Figure 2-1** so that the correlation between perchlorate in soil and groundwater can be seen. The perchlorate area has rough dimensions of a 100 foot diameter circle around location 29SB86 to a depth of 10 feet for a total volume of 2,900 cy.

Soil contamination from three explosives that pose ecological risks (2,4,6-TNT, 2,4-DNT and 2,6-DNT) are shown on **Figure 2-1**. In addition to the area around location 29SD46, the following areas exceed the EcoPRGs:

- 60-foot diameter circular area around 29SB08 (Building 802-A)
- Stained soil area around Building 806-D (sample location 29DLineWHW01) and Building 806-A
- 150 foot by 20 foot area around locations 29SD13, 29SB15, and GPS-12 (cooling water ditch north of Avenue D)

The rough volume for these areas is 200 cy around 29SB08, 30 cy around 29DLineWHW01, and 440 cy around 29SD13, 29SB15, and GPS-12 for a total of 670 cy.

2.4.2 Groundwater

Based on the human health risk assessment, groundwater at LHAAP-29 poses an unacceptable carcinogenic risk and non-carcinogenic hazard to a hypothetical future maintenance worker at LHAAP under an industrial scenario.

Groundwater contaminants identified to have a risk greater than 1×10^{-6} are listed in **Table 2-2**. The COCs listed in **Table 2-2** for the LHAAP-29 groundwater are MC, 1,2-DCA, 2,4-DNT, 2,6-DNT, and TCE, due to their contribution to risk or exceedance of their respective MCLs. Other contaminants listed on **Table 2-2** are not considered COCs since the EPC or more recent data indicates lower concentrations that are below their MCL.

Groundwater contaminants with a HQ greater than 0.1 are listed in **Table 2-3**. Many detected chemicals have an MCL, but did not show unacceptable risk or hazard. For the chemicals without MCLs, the GW-Ind was used for evaluation. The COCs identified in **Table 2-3** for the LHAAP-29 groundwater are MC, perchlorate, 1,2-DCA, 4-nitrotoluene, 2-nitrotoluene, 2,6-DNT, TCE, 3-nitrotoluene, and 2,4-DNT due to the contribution to HI and exceedance of their respective MCLs. Other contaminants listed on **Table 2-3** are not considered COCs for various reasons including more recent data indicating concentrations less than the EPC or the MCL or newer data indicating a reduction in the HQ.

Thus, the COCs for groundwater at LHAAP-29 are three VOCs (MC, 1,2-DCA, and TCE), five explosives (2,4-DNT, 2,6-DNT, 4-nitrotoluene, 2-nitrotoluene, and 3-nitrotoluene), and perchlorate. **Table 2-9** lists these COCs and indicates their most recent maximum concentration in the shallow and intermediate zones. Based on the comparison of the maximum concentration to their associated MCL or GW-Ind, these COCs have been identified to be of concern in the shallow and/or intermediate groundwater zone.

In the shallow zone, VOCs (1,2-DCA and TCE) and perchlorate are COCs with their maximum concentration located at 29WW15. The associated plumes are shown on **Figure 2-2**. The estimated volume of the perchlorate plume is approximately 4 million gallons. The nitrotoluenes are also COCs in the shallow zone and are located near 29WW06 and 116 as shown on **Figure 2-3**. The volume of the nitrotoluene plume is estimated to be approximately 9 million gallons. Three metals, nickel, arsenic and mercury, had sporadic detections above cleanup levels in certain wells and do not define a plume in the groundwater. These metals have been included as COCs.

In the intermediate groundwater zone, the COCs are limited to VOCs (MC, 1,2-DCA, and TCE). The VOC groundwater plume in the intermediate zone has the maximum concentrations at 29WW16 as indicated on **Figure 2-4**. The estimated volume of the VOC plume is approximately 21 million gallons. Groundwater volumes were estimated using a porosity of 25 percent with a thickness ranging from 5 to 10 feet.

As demonstrated by previous sample results and sampling of new monitoring well 29WW41 in June 2009, the deep groundwater zone is not affected at LHAAP-29.

2.4.3 Process Lines

Contaminated explosives residue remains within the transite TNT wastewater line at concentrations above the SAI-Ind and GWP-Ind, but access to the pipe is limited to the inlets and outlets unless the pipe is penetrated. Additionally, the line is deeper than the cleanup depth of 2 feet bgs for nonresidential use. The gravity flow portion of the line is approximately 3,000 linear feet. The pressurized portion of the line is approximately 1,000 linear feet. The line is in good condition.

The wooden TNT wastewater line was flushed and abandoned. The results from soil samples collected near the line indicate there has not been a release to the surrounding soil. Further, the line is deeper than the near-surface soil depth of 2 feet bgs considered for nonresidential use (TAC335.559(g)). Furthermore, it was noted in site documentation that no additional action is necessary for the wooden TNT wastewater line (Bate Stamp 001446).

The north and south vitrified clay cooling water lines are accessible through manholes, and the liquid and solid residue contents from the manholes were sampled. The liquid and solid residues from the manholes are contaminated with explosives at concentrations that are above the GW-Ind (liquid) and the GWP-Ind (solid residue). There are approximately 5,000 feet of pipe in the main lines, approximately 1,680 linear feet of pipe from each production area to the main line, and 12 manholes.

2.5 Conceptual Site Model

Figure 2-6 illustrates the overall conceptual site model for LHAAP-29. The model presents the human health pathways that are complete and being considered for remediation. Those pathways that are likely to be incomplete or have negligible impact are not being considered for remediation as discussed below. The ecological conceptual model for LHAAP-29 (**Figure 2-7**) is similar to the one presented for human health in terms of the origin and fate and transport mechanisms of the contaminants present at the site. However, only exposure pathways and routes associated with soil are relevant for ecological risk assessment.

Explosive compound releases resulting from the manufacturing process of TNT as well as releases from process tanks and process waste pipelines are the suspected contamination sources at LHAAP-29. The remaining potential sources of contamination at the site are the gravity line "red liquor" portions of the co-located wood and transite TNT wastewater pipelines that transported LHAAP-29 process wastes to the former pump house, explosives compounds in stained soils around the foundation of Buildings 806-A and 806-D, isolated perchlorate-containing soils in the northeastern portion of LHAAP-29 at a depth of eight (8) feet bgs, and TNT contaminated sediment in the cooling water outfall ditch at a depth of seven (7) feet bgs. Low-levels of explosives were identified in both the cooling water "blue water" drain line and the "red liquor" TNT wastewater line to be a hazard.

Contamination in the form of explosive compounds, VOCs, and perchlorate is present in groundwater at LHAAP-29 and poses potential risk to the hypothetical future maintenance worker. Explosive compounds in the shallow groundwater at LHAAP-29 are intermittent and dispersed across the site. Perchlorate and VOC concentrations have been detected consistently throughout the shallow groundwater zone. Concentrations of VOCs were detected in the intermediate groundwater zones. The most significant contaminant result is MC in the intermediate zone. The MC concentrations at 29WW16 are at approximately half the solubility, which indicates a potential for the presence of dense non-aqueous phase liquid (DNAPL). In the general vicinity of 29WW16, however, DNAPL has not been encountered. The horizontal extent of contamination in the shallow and intermediate groundwater zones appears to be isolated to a few specific locations as presented in **Figures 2-2, 2-3** and **2-4**.

The soil and groundwater at LHAAP-29 may pose a risk for the hypothetical future maintenance workers. However, no impact to surface water from groundwater was determined (Shaw, 2007c). Thus the only pathways considered for remediation are soil, soil to groundwater, and future industrial groundwater use.

Final Feasibility Study, LHAAP-29 Shaw Environmental, Inc.

Table 2-1
Chemicals with Hazard Quotient Greater than 0.1 in Soil

	Baseline Risk Assessment			Data Through 2008			Comparison Level		Retained
Chemical	Soil Hazard Quotient ^a	EPC (mg/kg)	Soil Sample Location	Adjusted Hazard Quotient ^b	Maximum (mg/kg)	Soil Sample Location	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	as COC ?
2,4,6-Trinitrotoluene	0.77	190	29SD13	105	26,000	29SD46	510	5.1	Yes, 2
2-Amino-4,6-dinitrotoluene	0.33	25	29SD13	0.63	48	29SD46	170	1.7	No, 1
4-Amino-2,6-dinitrotoluene	0.21	16	29SD13	0.21	16	29SD13	170	1.7	No, 1
2,4-Dinitrotoluene	0.0053	6.2	29SB15	6.8	8,000	29SD46	4.2	0.042	Yes, 3
Perchlorate ^c	8.1 × 10 ⁻⁵	0.0703	Max from Table 3-66	0.0099	8.6	29SB86	950	7.2	Yes, 4

Notes and Abbreviations:

- 1. Not identified as contaminant of concern (COC) because HQ is less than 1.0.
- 2.. Identified as COC because risk assessment HQ is almost 1 and most recent sample concentration is greater than the SAI-Ind GWP-Ind.
- 3. Identified as COC because EPC is above the SAI-Ind and GWP-Ind values and Hazard Quotient is greater than 1.0.
- 4. Identified as COC because contaminant is COC in groundwater and exceeds the GWP-Ind.
- ^a HQ from Baseline Risk Assessment Table C-68 (Jacobs, 2002)
- b calculated HQ based on the most recent maximum concentration.
- ^c Even though HI <0.1, listed because recent maximum concentration is greater than EPC

EPC Exposure Point Concentration from Baseline Risk Assessment (Jacobs, 2002)

GWP-Ind Soil medium-specific concentration for industrial use based on groundwater protection

HQ hazard quotient mg/kg milligrams per kilogram.

SAI-Ind Soil medium-specific concentration for industrial use based on inhalation, ingestion, and dermal contact

Final Feasibility Study, LHAAP-29 Shaw Environmental, Inc.

Table 2-2
Chemicals Contributing to Carcinogenic Risk in Groundwater

Chemical	Baseline Risk Assessment			Data S	ince Risk As:	sessment	Comparison Levels		
	Cancer Risk Groundwater ^a	EPC (µg/L)	Well	Maximu m (µg/L)	Well	Adjusted Risk	MCL (µg/L)	TCEQ GW-Ind (µg/L)	Retained as COC ?
Methylene chloride	3.6 × 10 ⁻¹	6,600,000	29WW16	10,300,00 0	29WW16	5.6 × 10 ⁻¹	5	5	Yes, 1
1,2-Dichloroethane	2.9 × 10 ⁻²	14,000	29WW15	<12,500	29WW16		5	5	Yes, 1
2,4-Dinitrotoluene	1.3 × 10 ⁻³	530	29WW20	50.9 32.4	29WW05 29WW20	1.2 × 10 ⁻⁴		0.42	Yes, 2
2,6-Dinitrotoluene	1.3 × 10 ⁻³	530	29WW20	239 112	116 29WW20	5.9 × 10 ⁻⁴		0.42	Yes, 2
Arsenic	3.1 × 10 ⁻⁴	59	29WW25	141	29WW25	7.4 × 10 ⁻⁴	10	10	Yes, 5
Trichloroethene	2.3 × 10 ⁻⁴	1,200	29WW15	<12,500	29WW16		5	5	Yes, 1
2,3,7,8-TCDD	6.1 × 10 ⁻⁵	1.25 × 10 ⁻⁵	29WW03	NR			3.0 × 10 ⁻⁵		No, 4
Chloroform	2.1 × 10 ⁻⁵	14	29WW21	9.75 ND	29WW15 29WW21	1.5 × 10 ⁻⁵	80 b	1,000	No, 4

Notes and Abbreviations:

- 1. Identified as COC because most recent maximum concentration is above the MCL.
- 2. Identified as COC because carcinogenic risk is >10-4.
- 3. Excluded because detections are isolated.
- 4. Excluded because EPC is below the MCL.
- 5. Identified as a COC subject to further verification.
- ^a From Baseline Risk Assessment Table C-71 (Jacobs, 2002)
- b MCL for total trihalomethanes was used for chloroform.

µg/Lmicrograms per literCOCcontaminant of concernEPCexposure point concentration

MCL Safe Drinking Water Act maximum contaminant level

MSC medium specific concentration from Updated Examples of Risk Reduction Standard No. 2, Appendix II

NR not resampled for this constituent since Baseline Risk Assessment

TCEQ GW-Ind Texas Commission of Environmental Quality Groundwater MSC for Industrial Use

Final Feasibility Study, LHAAP-29 Shaw Environmental, Inc.

Table 2-3
Chemicals with Hazard Quotient Greater than 0.1 in Groundwater

Chemical	Baseline	Baseline Risk Assessment			Data Since Risk Assessment			Comparison Levels	
	Hazard Quotient Groundwater ^a	EPC ^a (µg/L)	Well	Maximum (µg/L)	Well	Adjusted Hazard Quotient	MCL (μg/L)	TCEQ GW-Ind (µg/L)	Retained as COC ?
Methylene chloride	1500	6,600,000	29WW16	7,110,000	29WW16	1600	5		Yes, 1
Perchlorate	960	88,000	29WW15	16,800	29WW15	180		72	Yes, 2
1,2-Dichloroethane	490	14,000	29WW15	5,520	29WW15	190	5		Yes, 1
4-Nitrotoluene (p-)	35	2,100	29WW20	1,400 374	116 29WW20	23		1,000	Yes, 2
Chloroform	8.0	14	29WW21	9.75 ND	29WW15 29WW21	5.6	80 b		No, 3
2-Nitrotoluene (o-)	7.3	4,400	116	8,140	116	14		1,000	Yes, 2
2,6-Dinitrotoluene	5.2	530	29WW20	239 112	116 29WW20	2.3		0.42	Yes, 2
Trichloroethene	4.6	1,200	29WW15	344	29WW15	1.3	5		Yes, 1
Nickel	4.1	8,400	29WW11	3,190 40	29WW07 29WW11	1.6 <0.1		2,000	Yes, 9
3-Nitrotoluene (m-)	4.0	240	29WW05	451 123	116 29WW05	7.5		1,000	Yes, 2
2,4-Dinitrotoluene	2.6	530	29WW20	50.9 32.4	29WW05 29WW20	0.33		0.42	Yes, 5
Arsenic	1.9	59	29WW25	141	29WW25	4.5	10		Yes, 9
Aluminum	1.3	130,000	115	713	29WW08 c	<0.1		100,000	No, 6
Antimony	1.3	52	29WW09	1.45	29WW08	<0.1	6		No, 7
Barium	0.91	6,500	116	1,100 48.5 J	115 116	0.15 <0.1	2,000		No, 6
Selenium	0.68	350	118	75.3	118	0.15	50		No. 4
Manganese	0.50	2,410	115	1,310	114 ^c	0.27		14,000	No, 8
Vanadium	0.50	360	115	7.5 J	29WW04 ^c	<0.1		720	No, 8
Thallium	0.37	3.0	29WW03	0.339 J	29WW25 ^c	<0.1	2		No, 7
2-Amino-4,6-dinitrotoluene	0.35	5.9	29WW05	ND	29WW05	-		17	No, 8
4-Amino-2,6-dinitrotoluene	0.35	5.9	29WW05	16.3	29WW05	0.97		17	No, 8
Strontium	0.31	19,000	119	NR	-	-		61,000	No, 8
Silver	0.16	80	29WW09	ND	All wells resampled c	-		510	No, 8
Cadmium	0.12	6.23	119	1.2 1.12	115 116	<0.1 <0.1	5		No, 6

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Table 2-3 (continued) Chemicals with Hazard Quotient Greater than 0.1 in Groundwater

Notes and Abbreviations:

- 1. Identified as COC because EPC is above the MCL
- 2. Identified as COC because HQ is > 1.0
- 3. Excluded because EPC is below the MCL
- 4. Excluded as COC because elevated concentrations are isolated. See Section 2.3.2 for further explanation
- 5. Already identified as a COC due to carcinogenic risk (Table 2-2)
- 6. More recent sample results indicate lower concentrations of chemical, reducing HQ to <1.0
- 7. More recent sample results indicate lower concentrations of chemical below the MCL
- 8. Excluded because EPC and/or most recent maximum is below the TCEQ GW-Ind MSC and HQ is <1.0
- 9. Identified as a COC subject to further verification.
 - ^a From Baseline Risk Assessment Table C-68 (Jacobs, 2002)
 - b MCL for total trihalomethanes was used for chloroform
 - Well with maximum in Baseline Risk Assessment was dry in most recent sampling event and the identified well has the most recent maximum

COC contaminant of concern EPC exposure point concentration

HQ hazard quotient

MSC medium specific concentration from Updated Examples of Risk Reduction Standard No. 2, Appendix II

TCEQ GW-Ind Texas Commission of Environmental Quality Groundwater MSC for Industrial Use

MCL Safe Drinking Water Act maximum contaminant level
NR chemical not resampled in most recent sampling event

μg/L micrograms per liter

Shaw Environmental, Inc.

Table 2-4
Chemicals in Soil Compared to EcoPRGs

Chemical	SS EcoPRG ^a (mg/kg)	TS EcoPRG ^a (mg/kg)	Maximum ^b (mg/kg)	Retained as Contaminant of Potential Ecological Concern?
2,4,6-Trinitrotoluene	6.1	4.7	26,000	Yes
2,4-Dinitrotoluene	_	12	8,000	Yes
2,6-Dinitrotoluene	2.7	6.8	15	Yes

Notes and Abbreviations:

- ^a From Baseline Ecological Risk Assessment Table 16-1 (Shaw, 2007b).
- b Maximum soil concentrations from samples collected in the upper 3 feet of soil at 29SD46 collected (Shaw, 2007a)

EcoPRG Ecological Preliminary Cleanup level

mg/kg milligrams per kilogram.

SS surface soil from 0-0.5 feet (applicable to deer mouse)
TS total soil form 0-3 feet (applicable to short-tailed shrew)

Table 2-5
Summary of Solid Residue Sample Results from Transite TNT Wastewater Line

Explosive	EPC from Risk Assessment (mg/kg)	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	Concentration* (mg/kg)	Sample Location
2,4,6 TNT	190 (associated HI of 0.77)	510	5.1	526 58.4 17 JL	29WL13 29WL14 32WL05
2,4 DNT		4.2	0.042	5.15 JL 89 7.21	32WL05 29WL13 29WL14
2-amino-4,6-DNT	25 (associated HI of 0.33)	170	1.7	19 JH	29WL14
4-amino-2,6-DNT	16 (associated HI of 0.21)	170	1.7	13.3	29WL14
1,3-DNB		100	1	1.08	29WL13

Notes and Abbreviations:

* Concentrations included in table are above the GWP-Ind. Shaded concentrations are also above the SAI-Ind.

DNB dinitrobenzene DNT dinitrotoluene

EPC exposure point concentration

GWP-Ind soil MSC for industrial use based on groundwater protection

HI hazard index

JL concentration is estimated and biased low JH concentration is estimated and biased high

mg/kg milligrams per kilogram
MSC medium-specific concentration

SAI-Ind soil MSC for industrial use based on inhalation, ingestion and dermal contact

TNT trinitrotoluene

Table 2-6 **Explosive Compounds Detected in Soil Samples** near Wooden TNT Wastewater Line

Explosive	EPC from Risk Assessment (mg/kg)	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	Concentration (mg/kg)	Sample Location	Associated Depth
2,4,6-TNT	190 (associated HI of 0.77)	510	5.1	0.43	29SB83	4-5 ft bgs
2-amino-4,6-DNT	25 (associated HI of 0.33)	170	1.7	0.23 J 0.9	29SB85 29SB85	4-5 ft bgs 8-9 ft bgs
4-amino-2,6-DNT	16 (associated HI of 0.21)	170	1.7	0.30 J	29SB85	8-9 ft bgs

Abbreviations:

DNTdinitrotoluene

EPC exposure point concentration feet below ground surface ft bgs

GWP-Ind soil MSC for industrial use based on groundwater protection

Ш hazard index

concentration is estimated mg/kg MSC milligrams per kilogram medium-specific concentration

SAI-Ind soil MSC for industrial use based on inhalation, ingestion and dermal contact

TNT trinitrotoluene

Table 2-7 **Summary of Solid Residue Sample Results from Cooling Water Lines**

Explosive	EPC from Risk Assessment (mg/kg)	GWP- Ind (mg/kg)	Concentration* (mg/kg)	Sample location	Associated line
2,4,6-TNT	190	5.1	11	MH02	S Cooling
	(associated HI of 0.77)		7	MH10	N Cooling
			5.5	MH08	N Cooling
2,4-DNT		0.042	0.71	MH08	N Cooling
			1.1	MH10	N Cooling
2,6-DNT		0.042	0.24 J	MH10	N Cooling
			0.30 J	80HM	N Cooling
2-amino-4,6-	25	1.7	3.8 J	MH02	S Cooling
DNT	(associated HI of 0.33)		2.4 J	MH09	N Cooling
			9	MH10	N Cooling
4-amino-2,6-	16	1.7	2.6 J	MH02	S Cooling
DNT	(associated HI of 0.21)		2.5 J	MH09	N Cooling
			7.8	MH10	N Cooling

Notes and Abbreviations:

Concentrations included in table are above the GWP-Ind.

DNT dinitrotoluene

EPC

exposure point concentration soil MSC for industrial use based on groundwater protection GWP-Ind

ΗΙ hazard index

concentration is estimated milligrams per kilogram mg/kg MŠC medium-specific concentration

TNT trinitrotoluene

Table 2-8 **Explosive Compounds Detected in Liquid Samples from Cooling Water Lines**

Explosive	EPC from Risk Assessment (µg/l)	GW-Ind (μg/l)	Concentration (µg/I)	Sample location	Associated line
2,4,6-TNT		51	250	MH01	South
			84.3 JL 430	MH05	South
			5200	MH06	South
			20	MH09 (12/04)	North
				MH09 (2/05)	North
2,4-DNT	530	0.42	15	MH01	South
	(HI=2.6)		0.8 J	MH09 (12/04)	North
			1.13	MH09 (2/05)	North
			1.05	MH10	North
			0.922 J	MH11	North
			0.934 J	MH12	North
2,6-DNT	530	0.42	4.1	MH01	South
	(HI=5.2)		27	MH09 (12/04)	North
			1.27	MH09 (2/05)	North
			1.35	MH10	North
			1.15	MH11	North
			1.31	MH12	North
2-amino-4,6-DNT	5.9	17	220	MH09 (12/04)	North
	(HI=0.35)		1.68	MH09 (2/05)	North
4-amino-2,6-DNT	5.9	17	33	MH01	South
	(HI=0.35)		290	MH09 (12/04)	North
			2.42	MH09 (2/05)	North

Abbreviations:

DNT dinitrotoluene

exposure point concentration groundwater MSC for industrial use EPCGW-Ind

Ш hazard index

concentration is estimated concentration is estimated and biased low JL

medium-specific concentration trinitrobenzene MSC

TNB TNT trinitrotoluene

Table 2-9 COCs by Groundwater Zone

		Shallow Zone			Inter	mediate Zono	Э
COCs	MCL (µg/L)	Max (µg/L)	Well ID of Max	COC?	Max (µg/L)	Well ID of Max	COC?
Methylene Chloride	5	3	29WW15	No	7,110,000	29WW16	Yes
1,2-Dichloroethane	5	5,520	29WW15	Yes	14.3	29WW16	Yes
Trichloroethene	5	344	29WW15	Yes	4,340	29WW16	Yes
Arsenic	10	141	29WW25	Yes	44	29WW16	Yes
Mercury	2	6.1	118	Yes	not detected		No
	GW-Ind (µg/L)						
2,4-Dinitrotoluene	0.42	50.9	29WW05	Yes	not detected		No
2,6-Dinitrotoluene	0.42	239	116	Yes	not detected		No
2-Nitrotoluene	1,000	8,140	116	Yes	not detected		No
3-Nitrotoluene	1,000	451	116	Yes 1	not detected		No
4-Nitrotoluene	1,000	1,400	116	Yes	not detected		No
Perchlorate	72	16,800	29WW15	Yes	21.5	29WW35	No
Nickel	2,000	8,400	29WW11	Yes	120	29WW24	No

Notes and Abbreviations:

Max is the maximum concentration of that COC from the most recent sample round.

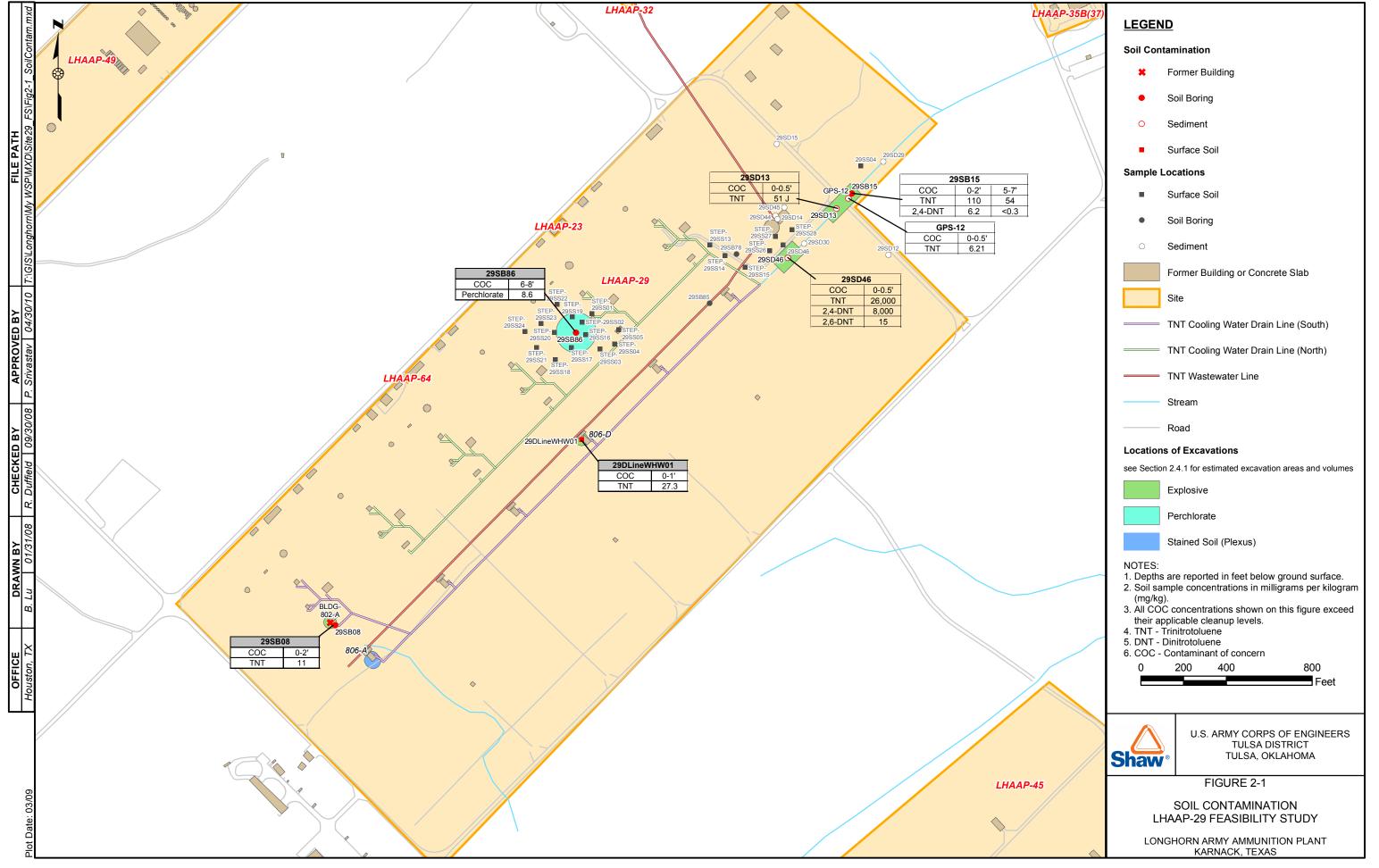
COC contaminant of concern

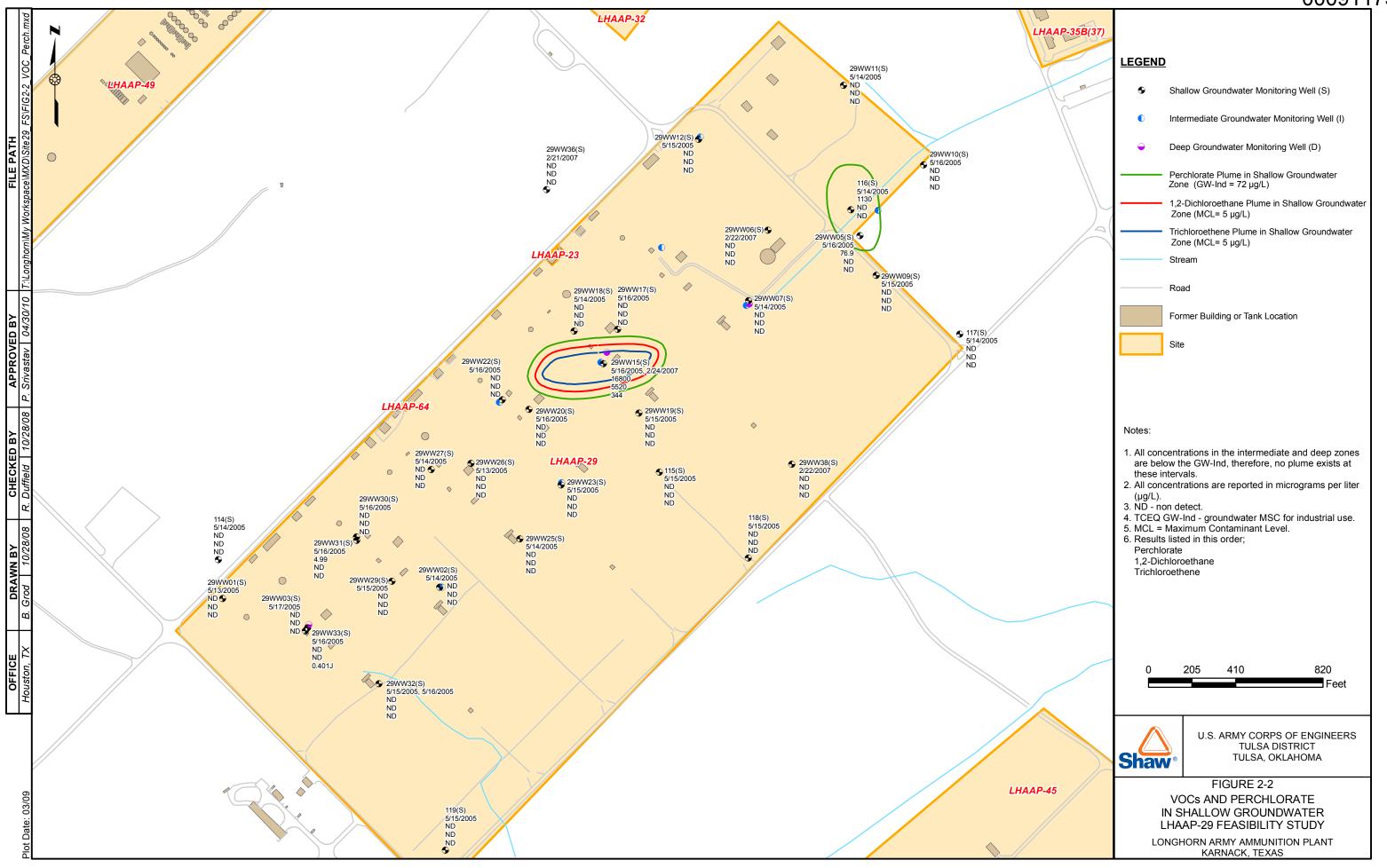
GW-Ind Texas Commission on Environmental Quality groundwater medium specific concentration for industrial use

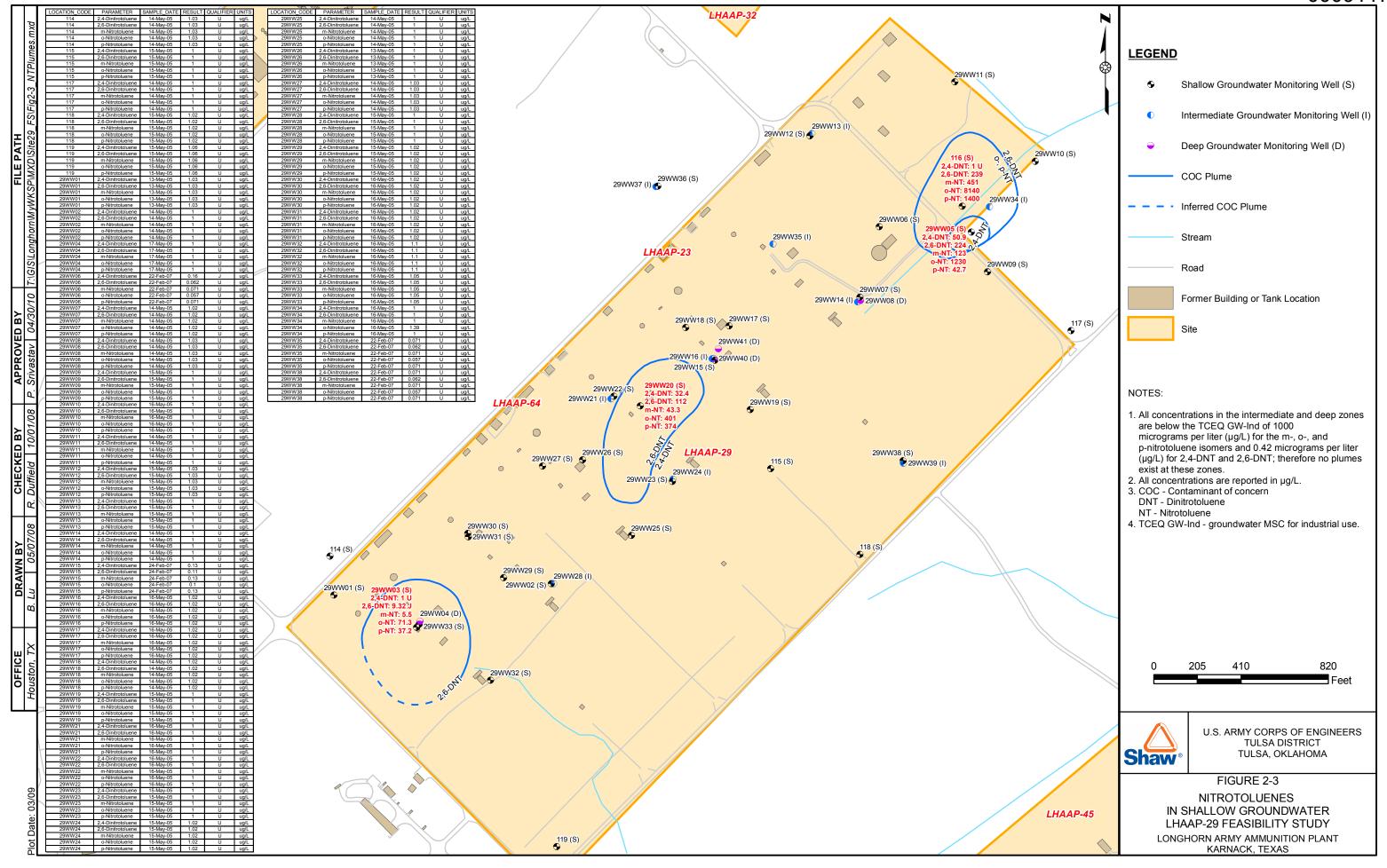
MCL Safe Drinking Water Act maximum contaminant level

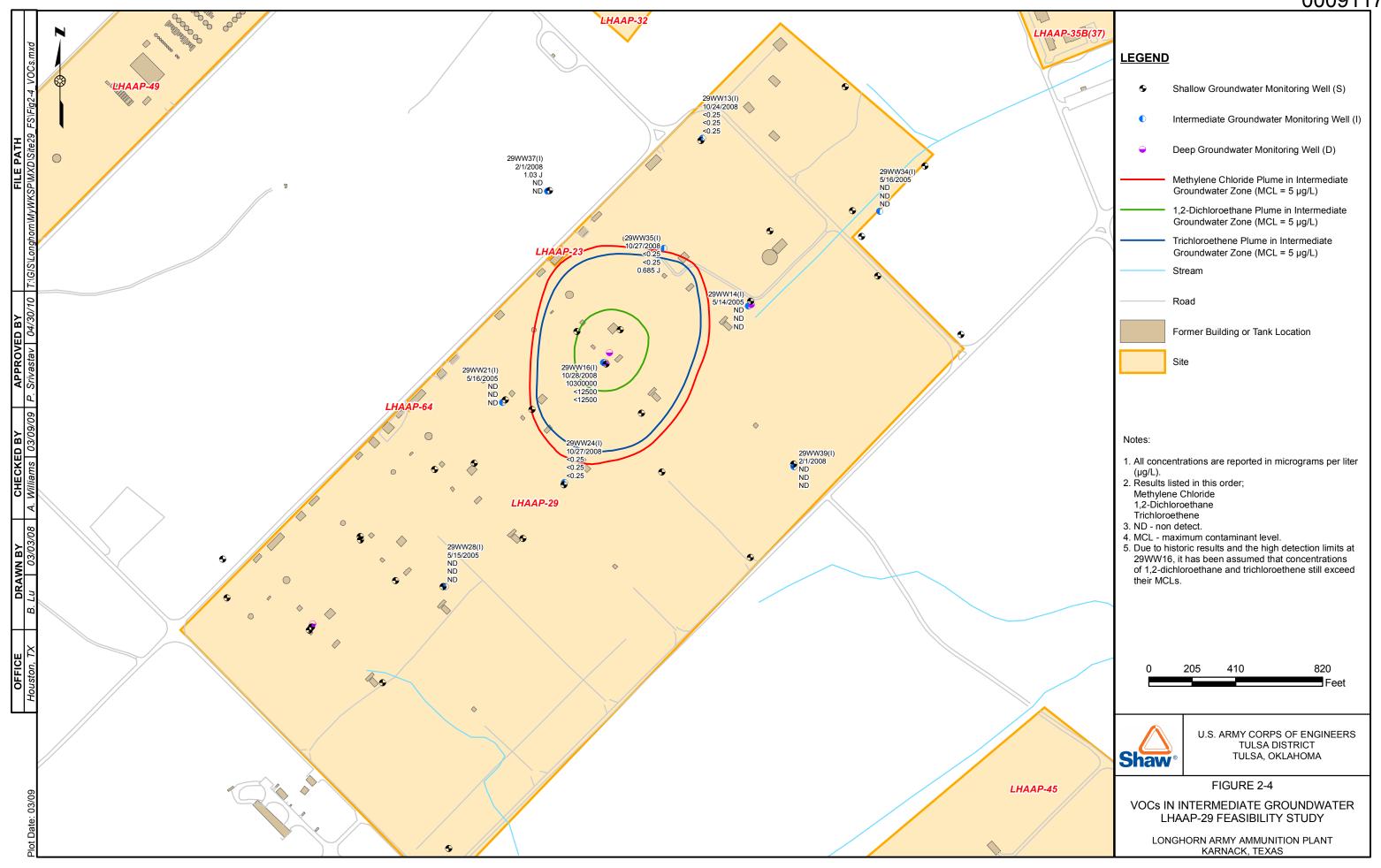
μg/L micrograms per liter

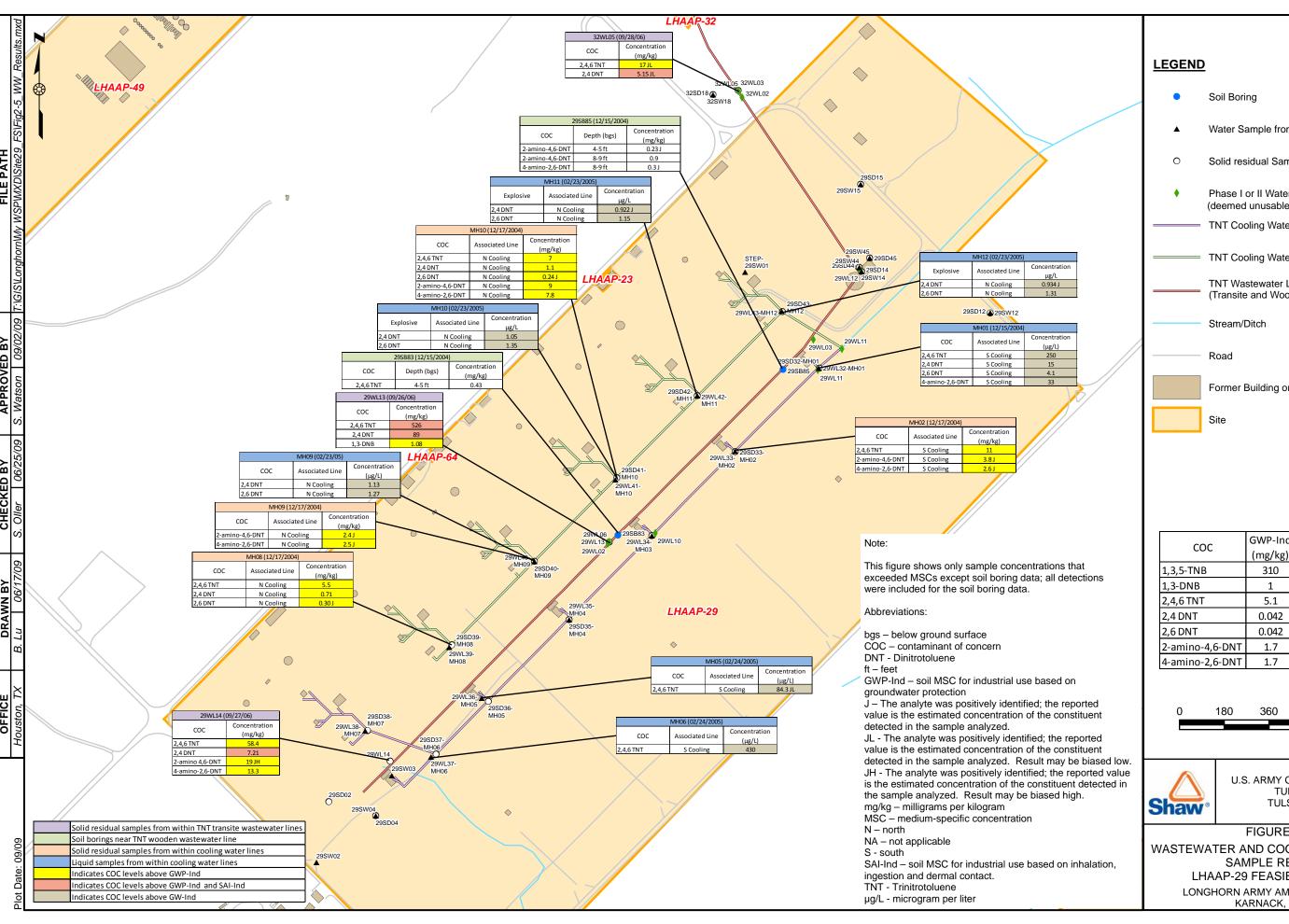
¹ Identified as a COC because hazard quotient value >1.











LEGEND

- Soil Boring
- Water Sample from Line or Man Hole
- Solid residual Sample from Line or Man Hole
- Phase I or II Water Line Sample (deemed unusable by USEPA)
- TNT Cooling Water Drain Line (South)
- TNT Cooling Water Drain Line (North)
- **TNT Wastewater Lines** (Transite and Wooden)
 - Stream/Ditch
 - Road

Site

Former Building or Concrete Slab



COC	GWP-Ind	SAI-Ind	GW-Ind
COC	(mg/kg)	(mg/kg)	(μg/L)
1,3,5-TNB	310	31,000	3100
1,3-DNB	1	100	10
2,4,6 TNT	5.1	510	51
2,4 DNT	0.042	4.2	0.42
2,6 DNT	0.042	4.2	0.42
2-amino-4,6-DNT	1.7	170	17





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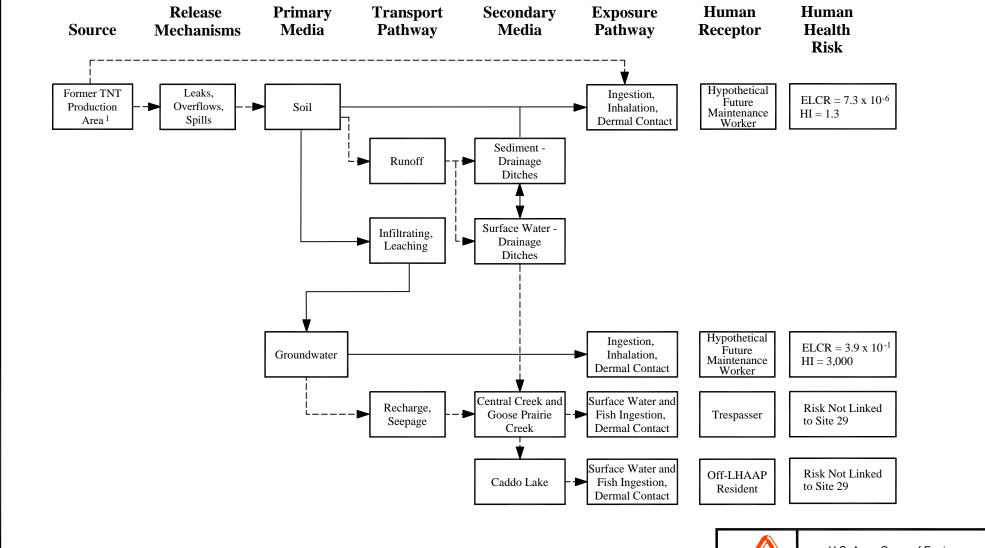
17

FIGURE 2-5

WASTEWATER AND COOLING WATER LINES SAMPLE RESULTS LHAAP-29 FEASIBILITY STUDY

> LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS

CHECKED BY APPROVED BY PLOT DATE: 10/22/08 **IMAGE** X-REF **OFFICE** DRAWN BY **DRAWING** 117591-A42 FORMAT REVISION 5/13/02 STOUGHTON, MA D. CRISPO 08/29/07 S. WATSON 03/09/09 P. SRIVASTAV 03/10/09 NUMBER



Pathway considered for remediation

Pathway not considered for remediation

Notes:

- 1. Most above ground structures have been removed
- 2. ELCR Estimated Life-time Cancer Risk
- 3. HI Hazard Index
- 4. ELCR and HI values are from risk assessment (Jacobs, 2002)



U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

Figure 2-6 Human Health Conceptual Site Model LHAAP-29 Feasibility Study

Longhorn Army Ammunition Plant
Karnack, Texas

00091178

MAGE X-REF **OFFICE** DRAWN BY CHECKED BY APPROVED BY **DRAWING** PLOT DATE: 1/30/06 117591-A43 NUMBER FORMAT REVISION 5/13/02 STOUGHTON, MA D. CRISPO 08/29/07 S. WATSON 03/09/09 P. SRIVASTAV 03/09/09 Release **Primary Transport Secondary Ecological Exposure** Mechanisms Media **Pathway** Media **Pathway** Receptor Source Source Areas: Industrial Sub-Area1 ABCDHI Ingestion Soil Terrestrial Plant Ingestion ACDE² Soil Invertebrate Ingestion ABCDH Biotic Uptake Edible Biota Small Mammal Ingestion CDI Bird Ingestion DI Runoff ABCDEFGHI Ingestion Surface Water Direct Contact Groundwater Leaching CFGH Ingestion Notes: Biotic Uptake Sediments Direct Contact 1. Industrial Sub-Area includes: landfills, burning grounds, and waste disposal areas. Aquatic Plant Ingestion 2. Although, the Bat is assumed to ingest moths, the moths are considered an indirect pathway for ingestion of chemicals in plants, which are the Aquatic Invertebrate Ingestion FG expected food items of the moths. Edible Biota Fish Ingestion CGIRECEPTORS A. Deer Mouse F. Bank Swallow Short-Tailed Shrew G. Belted Kingfisher American Woodcock U.S. Army Corps of Engineers Racoon (& Racoon [Louisiana Black Bear]) H. Tulsa District D. Red Fox I. Red-Tailed Hawk Tulsa, Oklahoma Townsend's Big-Eared Bat Aquatic Life (benthic invertebrates) --- = All receptors exposed to this pathway were determined not to be of concern. Figure 2-7 **Ecological Conceptual Exposure Model** Shaded cells indicate pathways that were not identified as significant, are background related, or were refined via site-specific investigations. LHAAP-29 Feasibility Study Longhorn Army Ammunition Plant Karnack, Texas

3.0 Remedial Action Objectives and Cleanup Levels

This section identifies the LHAAP-29 RAOs (Section 3.1), potential chemical-, location- and action-specific ARARs (Section 3.2), and cleanup levels (Section 3.3). The RAOs identify the general goals or end points that the remediation will accomplish, while the cleanup levels identify specific cleanup standards for each medium of concern based on risk or ARARs. The cleanup levels may be applied to individual contaminants.

3.1 Remedial Action Objectives

RAOs are established to protect human health and the environment while also meeting ARARs. The identification of RAOs must consider the environmental issues at the site and the receptors that are affected. As identified in the conceptual site models (**Section 2.5**), the primary environmental issues at LHAAP-29 are:

- Groundwater that poses an unacceptable risk or hazard to the hypothetical future maintenance worker from contamination by VOCs (MC, 1,2-DCA, and TCE), perchlorate, and explosives (2,4-DNT, 2,6-DNT, 2-nitrotoluene, 3-nitrotoluene, and 4-nitrotoluene) and has the potential to adversely impact human health.
- Soil near 29SB86 that has concentrations of perchlorate in excess of the TCEQ GWP-Ind concentration and has the potential to be a source of groundwater contamination.
- Surface soil that has concentrations of explosives that pose a risk to ecological receptors (near 29SB08 [Building 802-A], 29DLineWHW01, 29SD13, 29SB15, GPS-12, and the stained soil near Building 806-A) and a hazard to hypothetical future maintenance workers (near 29SD46).
- Buried TNT wastewater lines and cooling water lines/manholes that have residual explosive contaminants remaining in the line. If a hypothetical future maintenance worker came into contract with the residual contamination in the buried lines or in the manholes, it could pose risk. However, contact with the buried lines is unlikely since the lines are at least 3 feet bgs. If water is allowed to gain entrance into these pipes and flow through them to surface water outlets, the residual contamination could be transported out of the pipes. Thus, the primary concerns are direct contact with the residual contamination in the cooling water manholes and the potential transport of contaminants by water that enters the TNT wastewater and cooling water lines.

The future use of the entire LHAAP facility is as a national wildlife refuge. A hypothetical future maintenance worker has been proposed as a conservative human receptor scenario for this land use, and ecological risk is also a concern at LHAAP-29. The U.S. Army recognizes USEPA's policy to return all groundwater to potential beneficial uses, based on the non-binding programmatic expectation in the National Oil and Hazardous Substances Pollution Contingency

Plan (NCP). The RAOs for LHAAP-29, which address contamination associated with the media at the site and take into account the future uses of LHAAP streams, land, and groundwater are:

- Protect the hypothetical future maintenance worker by preventing exposure to the contaminants in the soil, sediment, transite TNT wastewater line, cooling water lines, and groundwater
- Prevent migration of contaminants to groundwater and surface water from potential sources in the soil, sediment and process lines (TNT wastewater and cooling water)
- Protect ecological receptors by preventing exposure to the contaminated soil and sediment
- Return groundwater to its potential beneficial uses, wherever practicable, within a reasonable time period given the particular site circumstances.

3.2 Applicable or Relevant and Appropriate Requirements

The NCP, 40 Code of Federal Regulations (CFR) 300.430(f)(1)(ii)(B) states that on-site remedial actions conducted under CERCLA must attain, or have waived, legally applicable ARARs under federal or more stringent state environmental or facility citing laws identified at the time of the ROD signature. This section provides a preliminary identification and evaluation of potential federal and State of Texas chemical-, location-, and action-specific ARARs for the remediation of LHAAP-29 under CERCLA.

3.2.1 Definitions and Methods

Applicable requirements are those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria, or limitations promulgated under federal or state law that specifically address a hazardous substance, pollutant, contaminant, remedial action, location, or other circumstance at a CERCLA site (40 CFR 300.5). A requirement is applicable if all the jurisdictional and site-specific prerequisites of the requirement are met; that is, a requirement is applicable if it directly and fully addresses the situation at the site.

Relevant and appropriate requirements are those substantive environmental protection requirements, criteria, or limitations promulgated under federal or state law that, while not applicable, address problems or situations sufficiently similar to those encountered at the CERCLA site so that their use is well suited to the particular site (40 CFR 300.5). The criteria for determining relevance and appropriateness are listed at 40 CFR 300.400(g)(2). A relevant and appropriate requirement must be complied with to the same extent as an applicable requirement.

To qualify as a state ARAR mandating cleanup standards under 40 CFR 300.400(g)(4) of the NCP, a state requirement must be (1) promulgated (of general applicability and legally

enforceable), (2) an environmental or facility citing law or regulation, (3) substantive (not procedural or administrative), (4) more stringent than a comparable federal requirement, (5) identified by the state in a timely manner, and (6) consistently applied throughout the state. Pursuant to USEPA guidance (USEPA, 1989a), where USEPA has delegated to a state the authority to implement a federal program, the state regulations replace the equivalent federal requirements as the potential ARARs.

ARARs are generally divided into chemical-, location-, and action-specific requirements. Chemical-specific ARARs are usually promulgated health- or risk-based numerical values or methods used to determine acceptable concentrations of chemicals that may be found in, or discharged to, the environment. Location-specific ARARs restrict actions or contaminant concentrations in certain environmentally sensitive areas. Action-specific ARARs are usually technology- or activity-based requirements or limitations on actions taken with respect to hazardous wastes.

An on-site action need not comply with administrative parts of requirements identified as ARARs. According to USEPA guidance (USEPA, 1988a), administrative requirements are mechanisms that facilitate the implementation of the related substantive requirements of a statute or regulation (e.g., approval of or consultation with administrative bodies, documentation, permit issuance, reporting, record keeping, and enforcement).

The NCP at 40 CFR 300.400(e)(1) exempts on-site actions from having to obtain federal, state, or local permits and defines "on-site" as meaning "the aerial extent of contamination and all suitable areas in very close proximity to the contamination necessary for the implementation of the response action." However, on-site actions must still be in compliance with any substantive permit requirements. Off-site actions must not only comply with requirements that are legally applicable, but they must comply with both the substantive and the administrative parts of those requirements. Permits, if required, must be obtained for all remedial activities conducted off site (40 CFR 300.400[e][2]). Statutory waivers of ARARs (40 CFR 300.430[f][1][ii][C]) may not be used for off-site actions.

The USEPA has noted in its CERCLA guidance that if attainment of a numerical value that is a potential chemical-specific ARAR is impossible because the background level of the chemical subject to CERCLA authority is higher than that of the potential ARAR, the numeric criterion would not be considered an ARAR (USEPA, 1991).

ARARs include only federal or more stringent state environmental laws and regulations and do not include occupational safety regulations. The USEPA requires compliance with the Occupational Safety and Health Administration (OSHA) standards and other worker protection requirements under Section 300.150 of the NCP, not through the ARARs process. Therefore,

none of the promulgated OSHA regulations (e.g., 29 CFR 1926, 29 CFR 1910) are addressed here as ARARs.

In addition to ARARs, 40 CFR 300.400(g)(3) states that federal or state nonpromulgated advisories or guidance may be identified as to-be-considered (TBC) guidance for contaminants, conditions, and/or actions at the site. TBCs include non-promulgated criteria, advisories, guidance, and proposed standards. TBCs are not ARARs because they are neither promulgated nor enforceable. TBCs may be used to interpret ARARs and to determine preliminary cleanup levels when ARARs do not exist for particular contaminants or are not sufficiently protective to develop cleanup levels. TBCs, such as guidance or policy documents, developed to implement regulations may be considered and used where necessary to ensure protectiveness. Potential TBCs evaluated as part of this investigation are listed in **Tables 3-1, 3-2,** and **3-3** and are discussed herein.

Chemical-specific requirements are discussed in **Section 3.2.2**; **Table 3-1** includes a narrative listing of chemical-specific ARARs/TBCs for LHAAP-29. Location-specific ARARs/TBCs for the sensitive resources potentially identified at LHAAP are discussed in **Section 3.2.3** and listed in **Table 3-2**. Action-specific ARARs/TBCs are discussed in **Section 3.2.4** and are listed and grouped by component action in **Table 3-3**.

3.2.2 Potential Chemical-Specific ARARs

This section identifies the potential chemical-specific ARARs that apply to surface/subsurface soils groundwater at LHAAP-29. These ARARs are summarized in **Table 3-1**.

3.2.2.1 Potential Chemical-Specific ARARs for Soil

There are no federal promulgated chemical-specific ARARs for soil. The TCEQ Texas Risk Reduction Rules are promulgated state standards for this site. It is anticipated that removal of perchlorate and explosives contaminated soils above the TCEQ GWP-Ind concentrations will prevent contamination of the groundwater at the site.

3.2.2.2 Potential Chemical-Specific ARARs for Air

Proposed remedial action alternatives (other than a "no action" alternative) developed during the FS stage may involve excavation activities that may release fugitive particulate matter into the ambient air. Contaminants emitted into the air during remediation must meet certain chemical-specific requirements for fugitive particulate matter and opacity; because these requirements; however, are triggered by a proposed action, they are addressed as action-specific ARARs in **Section 3.2.4**.

3.2.2.3 Potential Chemical-Specific ARARs for Surface Water

Section 121(d)(2) of CERCLA states that every remedial action shall require a level of control which at least attains surface water quality criteria established under Sections 304 or 303 of the Clean Water Act of 1972 (CWA). Therefore, surface water quality criteria are ARARs for surface water cleanup. The considered alternatives in this FS do not address surface water; however, measures will be implemented during construction to prevent off-site migration of contaminants to surface waters.

3.2.2.4 Potential Chemical-Specific ARARs for Groundwater

The human health risk assessment (Jacobs, 2002) indicated that the contaminated groundwater at LHAAP-29 presented an unacceptable hazard and risk to a hypothetical future maintenance worker. For the groundwater COCs at LHAAP-29, Safe Drinking Water Act MCLs are available and are considered relevant and appropriate because LHAAP-29 is an NPL site. Thus, MCLs are proposed as the preliminary cleanup levels in this FS for the groundwater at LHAAP-29. If MCLs are not available for certain COCs, MSCs provided under Texas RRR (Title 30 Texas Administrative Code [TAC] 335.551 through 335.569) will be used.

3.2.3 Potential Location-Specific ARARs

This section identifies the location-specific ARARs that may apply to LHAAP-29. These ARARs are summarized in **Table 3-2**.

3.2.3.1 Prehistoric and Historic Archaeological Sites and Paleontological Resources

In the event that significant archaeological or paleontological resources are discovered during remedial action activities at LHAAP-29, the federal National Historic Preservation Act (16 United States Code [USC] 470 et seq.) and Texas regulations for the protection of archaeological and cultural resources (13 TAC 15 and 13 TAC 25) would provide location-specific ARARs. These ARARs are included in **Table 3-2** to address this contingency. Texas regulations require that such discovered resources be surveyed, designated, and protected in accordance with relevant federal rules, regulations, standards, and guidelines.

Although highly unlikely, in the event that any historic cemeteries are discovered at LHAAP-29, certain provisions of Title 8, Texas Health and Safety Code, Chapters 711–715, may provide location-specific ARARs. For example, if an unknown or abandoned cemetery is discovered, Chapter 711.010 prohibits further construction or activity until the disturbed human remains are removed. Because the existence of cemeteries at LHAAP-29 is highly unlikely, cemetery protection laws are not included as location-specific ARARs in **Table 3-2**. If such resources are discovered during further investigation of these sites, the cemetery protection laws will be re-evaluated as ARARs in future decision documents.

3.2.3.2 Traditional Resources

A preliminary survey for significant Native American resources within the boundary of LHAAP has been conducted and indicates the presence of Native American resources on the property. Members of the Caddo Lake Indian Tribe have visited LHAAP, attended meetings, and expressed interest in and concern for the Native American resources on the site. In addition, discussions were held about establishing Native American educational displays covering the historical aspects of LHAAP property. The federal Native American Graves Protection and Repatriation Act (25 USC Section 3001) and it's implementing regulations (43 CFR 10.4[c]) are location-specific ARARs for the protection of such resources. These regulations require that activities in any area where such resources are discovered be stopped and reasonable effort be taken to secure and protect the objects discovered.

3.2.3.3 Threatened and Endangered Species

No federally endangered species are known to occur on the installation. There are 22 animal species that could potentially be present on or near LHAAP that appear on federal or state threatened and endangered species lists. The historic details regarding the number and date of species sightings are presented in the Caddo Lake Institute (CLI) report (CLI, 1995). Of the 22 animal species that could potentially be present, information received (USFWS, 2003) (Texas Department of Parks and Wildlife, 2003) identified the following list of threatened species and ecological communities of concern that are known or suspected to occur in the vicinity of LHAAP (species that have been confirmed are listed in italics) (Shaw, 2007b).

• Federal Listed Threatened Species:

- Bald Eagle
- Louisiana Black Bear

State Listed Threatened Species:

- Louisiana Black Bear
- Rafinesque's Big-Eared Bat
- Alligator Snapping Turtle
- Timber Rattlesnake
- Bluehead Shiner

State Species of Concern:

Southern Lady's Slipper

• State Special Features/Natural Communities/Managed Areas:

- Colonial Waterbird Rookeries
- Bald Cypress-Water Tupelo Series
- Shortleaf Pine-Oak Series
- Water Oak-Willow Oak Series
- Caddo Lake State Park

Some conflicting evidence is available regarding the potential presence of the Timber Rattlesnake at Longhorn. This State-listed species is described in historical site documents as being confirmed present on the site, but there is no recent documented evidence of this species being present on site (Shaw, 2007b). Therefore, it is assumed for the ARAR evaluation that the Timber Rattlesnake is potentially present, along with the Alligator Snapping Turtle as well as the Bald Eagle and the Rafinesque's Big-Eared Bat. Timber rattlesnakes prefer moist lowland forests and hilly woodlands or thickets near permanent water sources such as rivers, lakes, ponds, streams and swamps where tree stumps, logs and branches provide refuge. Alligator snapping turtles prefer deep waters of ponds, canals, lakes, streams, or swamps where they spend most of their time concealed by mud. Bald eagles in Texas may either represent breeding populations or wintering populations, and tend to roost on large lakes and rivers with tall trees for nesting and unobstructed flight paths to food sources (typically fish). Although Rafinesque's big-eared bats roost in cave entrances, abandoned buildings and under bridges, the preferred roosting sites for these bats are large, dead, hollow trees. Timber Rattlesnakes have not been observed at the Installation by resident wildlife experts, and large water bodies with deep pools required by alligator snapping turtles are not present at this site. Common bat roosting locations, such as dead tree snags and abandoned buildings are not features at this site, and no bald eagle nests are documented as being present in this area. Furthermore, although the site may be used occasionally by bald eagles or Rafinesque's big-eared bats during migration or as part of a foraging territory, this site is too small (85 acres) for regular exposure to occur for these species, which have home ranges of hundreds of acres. The potential for these threatened species to be present at LHAAP-29 is low.

Thus, based on current information, potential remedial action alternatives are not expected to harm any federal- or state-listed threatened or endangered species or their critical habitat. The requirements of the federal Endangered Species Act (16 USC 1531 et seq.), the federal Bald Eagle Protection Act (16 USC 668 et seq.), and the Texas Resource Protection Act (31 TAC 69, Subchapters A and B, and 31 TAC 65, Subchapter G) would be location-specific ARARs in the event that such species or habitats could be impacted by any proposed remedial alternatives. These ARARs are included in **Table 3-2** in the event that such threatened and endangered species/habitats are identified at LHAAP-29 in the future.

3.2.3.4 Sensitive Habitats

A sensitive habitat is defined within the CERCLA hazard ranking system (40 CFR 300, Appendix A) as one that contains an important biological resource or a particularly fragile resource. Wetlands are specifically included as a type of sensitive habitat. Other sensitive habitats include plant communities of unusual or limited distribution and important seasonal-use areas for wildlife (e.g., migration routes, breeding areas, or crucial winter habitat).

The Fish and Wildlife Coordination Act (16 USC 661 et seq.) requires that the effects of water-related projects that modify, divert, or control waters, including drainage activities, be considered with a view to preventing loss of and damage to such resources. This act may provide ARARs if groundwater diversion or treatment activities will impact groundwater-to-surface-water drainage patterns such that fish or wildlife may be adversely affected.

The Caddo Lake National Wildlife Refuge lies adjacent to LHAAP. The expected future use of LHAAP-29 is to be part of that refuge. In light of this future use, the National Wildlife Refuge System Act (50 CFR 35) would be a potential ARAR for impacted areas that will become part of the designated national wildlife refuge system.

Although there are low-lying wetland areas associated with Goose Prairie Creek, Central Creek, Saunder's Branch, and Harrison Bayou, no formal wetlands survey has been conducted at the LHAAP specifically (USACE, 1992; Jacobs, 2001). Nearby Caddo Lake, however, into which LHAAP surface waters flow is part of the Big Cypress Bayou, which is considered a wetland of international significance. Adverse impacts to any identified wetlands located at LHAAP or to the Caddo Lake/Big Cypress Bayou wetland system from remedial actions at LHAAP-29 must be avoided to the extent practicable. If identified wetlands will be impacted and wetland mitigation is required, Title 12, Chapter 221 (*Wetlands Mitigation*) of the Texas Code, as well as the federal standards for wetland mitigation, may provide location-specific ARARs. These requirements will be evaluated during the final ROD stage as further site-specific data are collected and the preferred alternative is proposed and evaluated.

3.2.3.5 Floodplains

Executive Order 11988 (*Floodplain Management*, May 24, 1997) requires evaluation of potential effects of actions in floodplains, consideration of flood hazards, and that floodplain management is ensured. If action is taken in floodplains, the order requires consideration of alternatives that avoid adverse effects and incompatible development and minimize potential harm. This order, as summarized in **Table 3-2**, is TBC guidance for LHAAP-29 remedial activities if such activities should impact identified floodplains.

3.2.4 Potential Action-Specific ARARs

Action-specific ARARs include operation, performance and design requirements or limitations based on the waste types, media, and remedial activities. This section provides a preliminary identification and evaluation of potential federal and state of Texas action-specific ARARs for the proposed remediation of LHAAP-29.

Pursuant to USEPA guidance, there are no action-specific ARARs for the required no action alternative (USEPA, 1991). The action-specific ARARs for the activities common to the

remedial action to be conducted at LHAAP-29 are discussed in **Section 3.2.4.1** below. All action-specific ARARs are listed in **Table 3-3** and are grouped by component action.

Each of the proposed remedial action alternatives will involve several of the following activities: waste generation, characterization, management, storage, and disposal activities; land use controls (LUCs) and long-term monitoring; and water treatment. Action-specific ARARs are discussed here for the activities common to the remedial activities to be proposed for LHAAP-29.

3.2.4.1 Site Preparation, Construction, and Excavation Activities

Certain on-site preparation, construction, and/or excavation activities will be necessary under all remediation actions to prepare the site for remediation, including the soil-moving or site-grading activities. Control of fugitive emissions and storm water runoff during implementation of these activities will be required.

Airborne particulate matter resulting from construction or excavation activities is subject to the fugitive dust and opacity limits listed in 30 TAC 111, Subchapter A. No person may cause, suffer, allow, or permit visible emissions from any source to exceed an opacity of 30 percent for any 6-minute period [30 TAC 111.111(a)]. Reasonable precautions must also be taken to achieve maximum control of dust to the extent practicable, including the application of water or suitable chemicals or the complete covering of materials (30 TAC 111.143 and 30 TAC 111.145).

Texas has also promulgated general nuisance rules for air contaminants mandating that no person shall discharge from any source whatsoever one or more air contaminants, or combinations thereof, in such concentration and of such duration as are or may tend to be injurious to or to adversely affect human health or welfare, animal life, vegetation, or property, or as to interfere with the normal use and enjoyment of animal life, vegetation, or property (30 TAC 101.4).

Storm water discharges from construction activities that disturb equal to or greater than one acre of land must comply with the substantive requirements of a USEPA National Pollutant Discharge Elimination System general permit (40 CFR 122.26; 30 TAC 205, Subchapter A; and 30 TAC 308.121), depending on the amount of acreage disturbed. Substantive requirements include implementation of good construction management techniques; phasing of large construction projects; minimal clearing; and sediment, erosion, structural, and vegetative controls to mitigate runoff and ensure that discharges meet required parameters.

3.2.4.2 Waste Generation, Characterization, Management, Storage, and Disposal Activities

The processes of monitoring, intercepting, or treating contaminated groundwater may generate a variety of primary and secondary waste streams (e.g., soil, personal protective equipment [PPE],

and dewatering and decontamination fluids). These waste streams are expected to be non-hazardous waste. All solid waste (defined as any solid, liquid, semisolid, or contained gaseous material intended for discard [40 CFR 261.2]) generated during remedial activities must be appropriately characterized to determine whether it contains RCRA hazardous waste (40 CFR 262.11; 30 TAC 335.62; 30 TAC 335.503[a][4]; 30 TAC 335.504). All wastes must be managed, stored, treated (if necessary), and disposed of in accordance with the ARARs for waste management listed in **Table 3-3** for the particular type of waste stream or contaminants in the waste.

Excavated environmental media including soil excavated during the installation of monitoring/ extraction wells would be sent off site for disposal or, in the case of non-hazardous trenching or well construction soil, redeposit within the area of contamination (AOC). The USEPA defines "onsite" as the aerial extent of contamination and all suitable areas in close proximity to the contamination necessary for the implementation of the CERCLA response action and notes that such contamination may contain varying types and concentrations of hazardous substances (53 FR 51444; 55 FR 8758). The soil generated from remedial activities at LHAAP-29 is expected to be hazardous. ARARs for the management of such media at the site of generation (i.e., within the AOC) are listed in **Table 3-3**. Other requirements for hazardous waste such as manifesting for off-site disposal (40 CFR 262.20) and planning/implementing off-site response action (40 CFR 300.440) will be complied with even though they are not considered an ARAR.

The USEPA has stated that excavation and redeposition of contaminated soil within an AOC does not constitute "generation"; therefore, the requirements of 40 CFR 262.11 and 268.7 to characterize generated wastes are not applicable (Office of Solid Waste and Emergency Response Directive 9441.1992[16], June 11, 1992). Consolidation of waste between AOCs for treatment or disposal, however, or excavation and treatment with subsequent disposal in the same AOC or off-site disposal constitute "placement." In these situations, RCRA Subtitle C requirements for the generation, handling, treatment, and disposal of such wastes are applicable if the waste/media is determined to contain RCRA hazardous waste (Volume 55, Federal Register [FR], page 8758).

3.2.4.3 Land Use Controls and Long-Term Monitoring

Some combination of restrictive covenants, administrative controls, physical barriers, physical surveillance or other controls, in combination with long-term monitoring of groundwater, would be necessary under all remedial alternatives to restrict access to contamination and protect human health and the environment because none of the actions will completely remove all of contamination to levels that would allow unrestricted access and use of the site.

When engineering or LUC measures are required to protect human health and the environment, 30 TAC 335.565 requires compliance with the identified post-closure care requirements and

deed recordation of the facility in accordance with Sections 335.566(b) through (e). The deed recordation must include a description of post-closure measures required and any LUCs placed on the future use of the property, as well as a metes and bounds description of the tract of land. Since there is no deed for federal land, when the U.S. Army transfers the land to the USFWS, a recordation of the LUC, as required by the State of Texas, will accompany the transfer. If the land is transferred from a federal entity to a non-federal entity, it is transferred by deed. Some or all of these requirements may be ARARs for this remedial action; the specific combination of controls negotiated for this action would be listed in a signed ROD.

3.2.4.4 Well Construction

All of the proposed alternatives, other than the no action alternative, may involve the placement, use, or eventual plugging and abandonment of some type of groundwater monitoring, injection, and/or extraction wells, either for in situ treatment or extraction of the contaminated groundwater or for long-term monitoring of the groundwater. Available standards for well construction and plugging/abandonment would provide ARARs for such actions.

Texas has promulgated technical requirements in Chapter 76 of Title 16 of the TAC applicable to construction, operation, and plugging/abandonment of water wells. In particular, 16 TAC 76.1000 (Locations and Standards of Completion for Wells), 16 TAC 76.1002 (Standards for Wells Producing Undesirable Water or Constituents) (LHAAP-29 contaminated groundwater could be considered "undesirable water" defined pursuant to Section 76.10[36] as "water that is injurious to human health and the environment or water that can cause pollution to land or other waters"), 16 TAC 76.1004 (Standards for Capping and Plugging of Wells and Plugging Wells that Penetrate Undesirable Water or Constituent Zones), and 16 TAC 76.1008 (Pump Installation) may provide ARARs for the placement, construction, and eventual plugging/abandonment of groundwater injection or extraction wells or the placement and long-term operation of groundwater monitoring wells for proposed groundwater remedial strategies.

Texas has promulgated technical requirements in 30 TAC 331 applicable to construction and abandonment of Class V injection wells. The temporary wells to be used in applying chemical oxidants to the plume of MC in the intermediate groundwater zone fit the category of Class V injection wells.

3.2.4.5 Water Treatment

Contaminated groundwater and wastewaters collected during well drilling, groundwater extraction or decontamination activities could be transported to the on-site water treatment facility constructed as a component of the previous interim remedial action at other LHAAP sites (LHAAP-18/24) and would subsequently be discharged in compliance with the CWA outfall limits for the facility as listed in the ROD. Such waters would be characterized, as required, before transport and managed accordingly in compliance with requirements for the type of waste

contaminating the water. To assure compliance with the water treatment plant's discharge limits, the incoming water must meet the waste acceptance criteria for the facility. On-site wastewater treatment units (as defined in 40 CFR 260.10) that are part of a wastewater treatment facility that is subject to regulation under Section 402 or Section 307(b) of the CWA are not subject to RCRA Subtitle C hazardous waste management standards (40 CFR 270.1[c][2][v]; 40 CFR 264.1[g][6]; 30 TAC 335.42[d][1]). The USEPA has clarified that this exemption applies to all tanks, conveyance systems, and ancillary equipment, including piping and transfer trucks, associated with the wastewater treatment unit (53 FR 34079, September 2, 1988).

3.3 Preliminary Cleanup Levels

Cleanup levels are the concentrations for individual chemicals in soil and groundwater above which some response action (e.g., treatment, LUCs) would be required. The cleanup levels for soil, groundwater, and solid residue in the cooling water lines at LHAAP-29 are determined with consideration of the risk to human health, the risk to ecological receptors, and the ARARs identified for the site in **Section 3.2.2**.

3.3.1 Soil

Perchlorate was not identified as a COC in the risk assessment; however, it has been carried forward as a COC in this document because perchlorate is present in groundwater at LHAAP-29 at concentrations that represent a potential non-carcinogenic human health hazard and perchlorate in on-site soils is considered as the primary source. Perchlorate will be remediated to the more stringent of the SAI-Ind and GWP-Ind standards, which is GWP-Ind.

Target COPECs above the risk-based EcoPRGs are co-located with the soil and sediments containing explosives in the cooling water outfall ditch. Removal of the soils at this location will address ecological risk concerns presented in the BERA as well as human health concerns. **Table 3-4** presents the applicable cleanup level for the target contaminants.

3.3.2 Groundwater

The cleanup levels for groundwater at LHAAP-29 are the MCLs (when available) and the TCEQ GW-Ind (TCEQ, 2006) for chemicals without MCLs. Groundwater at LHAAP-29 has unacceptable risk or hazard primarily due to MC, TCE and perchlorate. Some of the chemicals (e.g., TCE) have degradation products with MCLs, and those degradation products have also been identified as COCs. **Table 3-5** summarizes the COCs and the proposed cleanup levels for groundwater using the MCLs and GW-Ind. The metals COCs are retained as provisional COCs based on preliminary data. The extent of these inorganic COCs will be assessed at wells site wide during the Remedial Design.

3.3.3 Cooling Water Lines

The cleanup levels for solid residue in the cooling water lines at LHAAP-29 are the GWP-Ind values. Solid residue in the cooling water lines exceeded the GWP-Ind for 2,4-DNT in manholes 8 and 10. If similar thicknesses and concentrations of solid residue exist in the adjacent pipelines, then 2,4-DNT could potentially leach into groundwater at unacceptable concentrations if the pipe deteriorates. **Table 3-6** summarizes the COCs and the proposed cleanup levels for solid residue in the lines using the GWP-Ind values."

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Table 3-1 Potential Chemical-Specific ARARs/TBCs

Citation	Activity or Prerequisite/Status	Requirement		
Surface/Subsurface Soils				
TCEQ Texas Risk Reduction Rules	Ensures adequate protection of human health and	Near surface (i.e., 0-2 feet bgs) non-residential (industrial) soils shall conform to the non-		
30 TAC 335.558 and 335.559(d)(2)	the environment from potential exposure to contaminants associated with releases – relevant and appropriate for remediation of contaminated soil for cross-media contamination pathways such as soil to groundwater and for hypothetical future maintenance workers.	residential soil MSCs (SAI-Ind) based upon worker ingestion of soil, inhalation of particulates and volatiles and the non-residential soil-to-groundwater cross media protection concentration. The concentration of contamination in soil shall not exceed the non-residential soil-to-groundwater cross media (GWP-Ind). See Table 3-4 for specific numeric criteria.		
	Groundw	ater		
Federal Safe Drinking Water Act MCLs/Non-Zero MCLGs	Applicable to drinking water at the tap—relevant and appropriate for water that could potentially be used for human consumption.	Must not exceed MCLs/non-zero MCLGs for water designated as a current or potential source of drinking water. See Table 3-5 for specific numeric criteria.		
40 CFR 141				
TCEQ Texas Risk Reduction Rules	Applicable to industrial groundwater—relevant and appropriate for hypothetical future	If no maximum contaminant level has been promulgated, groundwater must not exceed the industrial medium-specific concentration. See Table 3-5 for specific numeric criteria.		
30 TAC 335	maintenance worker exposure to groundwater			

Abbreviations:

ARAR	applicable or relevant and appropriate requirement	MSC	medium-specific concentration
bgs	below ground surface	SAI-Ind	soil MSC for industrial use based on inhalation, ingestion, and dermal contact
GWP-Ind	soil MSC for industrial use base on groundwater protection	TAC	Texas Administrative Code
MCL	maximum contaminant level	TBC	to-be-considered [guidance]
MCLG	maximum contaminant level goal	TCEQ	Texas Commission on Environmental Quality

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Table 3-2 Potential Location-Specific ARARs/TBCs

Resource/Citation	Activity or Prerequisite Status	Requirement
Preservation of Archaeological and Paleontological Artifacts National Historic Preservation Act (16 USC 470 et seq.); 43 CFR 7.5(b)(1); 36 CFR 800; 13 TAC 15; 13 TAC 25	archaeological or paleontological resources— applicable if such resources are discovered. No known archeological or paleontological resources	Action must avoid irreparable harm, loss, or destruction of such resources if discovered. Such resources must be surveyed, designated, and protected in accordance with relevant federal rules and regulations, standards, and guidelines, as these are adopted by the Texas Historical Commission.
Preservation of Native American Artifacts Native American Graves Protection and Repatriation Act (25 USC Section 3001); 43 CFR 10.4(c) and (d)	Excavation activities that inadvertently discover such Native American resources—applicable if such resources are discovered. No known Native American resources exist at LHAAP-29.	Activities in the area of the discovery must be stopped and reasonable effort taken to secure and protect the objects discovered.
Protection of Threatened and Endangered Species (as listed in Table 3-5) Endangered Species Act (16 USC 1531 et seq.); 50	Activities that may adversely impact any state- or federally-listed, threatened or endangered species or their habitat—applicable if such species and/or habitats are impacted	Actions that jeopardize the existence of a listed species or result in the destruction or adverse modification of critical habitat must be avoided, or reasonable and prudent mitigation measures must be taken.
CFR 402; Bald Eagle Protection Act (16 USC 668 et seq.); Texas Resource Protection Act, 31 TAC 69 Subchapters A and B, and 31 TAC 65 Subchapter G		No person may take, possess, propagate, transport, export, sell or offer for sale, or ship any species of fish, wildlife, or native plant listed by the Texas Parks and Wildlife Department as endangered or threatened. The Department shall actively seek full restitution for and/or restoration of such a native plant, fish, or wildlife, or habitat loss occurring as a result of human activities.
Protection of Fish and Wildlife Resources Fish and Wildlife Coordination Act (16 USC 661 et seq.)	Action that impounds, modifies, diverts, or controls waters, including navigation and drainage activities—applicable	The effects of water-related projects on fish and wildlife resources and their habitat should be considered with a view to the conservation of fish and wildlife resources by preventing loss of and damage to such resources.
Protection of Caddo Lake National Wildlife Refuge System	Activities that may adversely impact or cause harm/loss of protected fish, wildlife and/or habitat in such protected areas—relevant and appropriate	The taking, disturbance, injury, or damage to any protected plant or animal on a national wildlife refuge is prohibited. The disposal of waste except at designated/approved points or locations or the polluting of any waters, streams, or other areas within any national wildlife refuge is prohibited.
National Wildlife Refuge System Act (16 USC 668dd-668ee); 50 CFR 35; 31 TAC 69.19	to impacted areas that will become part of the designated national wildlife refuge system	Restitution for and/or restoration of fish, wildlife, and habitat loss occurring as a result of human activities is required; appropriate measures include, but are not limited to, direct replacement of fish, wildlife, and/or habitat destroyed.
Protection of Wetlands Section 404 of the Clean Water Act	Actions that involve the discharge of dredged or fill material into jurisdictional wetlands or actions that have a potential adverse impact to, or take place	No discharge of dredged or fill material into an aquatic ecosystem is permitted if there is a practicable alternative that would have less adverse impact.
(33 USC 1344); 40 CFR 230.10(a) and (d); Swampbuster Provision of the Food Security Act; Executive Order 11990, "Protection of Wetlands"	within, wetlands—applicable if delineated wetlands are present at the site and will be adversely impacted by the action. No known delineated wetlands are located at LHAAP-29.	No discharge of dredged or fill material shall be permitted unless appropriate and practicable steps per 40 CFR 230.70 et seq. have been taken, which will minimize potential impacts of the discharge on the aquatic ecosystem.

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Table 3-2 (continued) Potential Location-Specific ARARs/TBCs

Resource/Citation	Activity or Prerequisite Status	Requirement
Protection of Floodplains	Activities which involve federally undertaken,	Action shall be taken to reduce the risk of flood loss, minimize the impact of floods on human
į į	financed, or assisted construction and improvements	safety, health and welfare, and restore and preserve the natural and beneficial values of
Executive Order 11988 (Floodplain Management, May	or which involve conducting federal activities and	floodplains.
24, 1997)	programs affecting land use - applicable if	
		The potential effects of actions in floodplains shall be evaluated, and consideration of flood
	Floodplains should not be impacted by the remedial	hazards and floodplain management ensured. Most of LHAAP-29 is not within the 100-year
	action at LHAAP-29.	floodplain.

Abbreviations:

ARAR

applicable or relevant and appropriate requirement Code of Federal Regulations Texas Administrative Code CFR TACTBC to-be-considered (guidance) USC United States Code

Table 3-3
Potential Action-Specific ARARs/TBCs

Citation	Activity or Prerequisite/Status	Requirement
	General Site Preparation,	Construction, and Excavation Activities
Air Contaminants – General Nuisance Rules 30 TAC 101.4	Emissions of air contaminants—applicable.	No person shall discharge from any source whatsoever one or more air contaminants or combinations thereof, in such concentration and of such duration as are or may tend to be injurious to or to adversely affect human health or welfare, animal life, vegetation, or property, or as to interfere with the normal use and enjoyment of animal life, vegetation, or property.
Opacity Standard 30 TAC 111.111(a)(8)(A)	Fugitive emissions from land-disturbing activities (e.g., excavation, construction)—applicable.	Visible emissions shall not be permitted to exceed opacity of 30% for any 6-minute period from any source.
Fugitive Particulate Matter Standard 30 TAC 111.145	Fugitive emissions from land-disturbing activities (e.g., excavation, construction)—applicable.	No person may cause, suffer, allow, or permit a structure, road, street, alley or parking area to be constructed, altered, repaired, or demolished, or land to be cleared without taking at least the following precautions to achieve control of dust emissions: Use of water or of suitable oil or chemicals for control of dust in the demolition of structures, in construction operations, in work performed on a road, street, alley, or parking area, or in the clearing of land; and Use of adequate methods to prevent airborne particulate matter during sandblasting of structures or similar operations.
Storm water Runoff Controls 40 CFR 122.26; 30 TAC 205, Subchapter A; 30 TAC 308.121	Storm water discharges associated with construction activities—applicable to disturbances of equal to or greater than 1 acre of land.	Good construction management techniques, phasing of construction projects, minimal clearing, and sediment, erosion, structural, and vegetative controls shall be implemented to mitigate storm water run-on/runoff.
	Waste Generation	on, Management, and Storage
Characterization of Solid Waste 40 CFR 262.11 30 TAC 335.62 30 TAC 335.504 30 TAC 335.503(a)(4)	Generation of solid waste, as defined in 30 TAC 335.1—applicable.	Must determine whether the generated solid waste is RCRA hazardous waste by using prescribed testing methods or applying generator knowledge based on information regarding material or process used. If the waste is determined to be hazardous, it must be managed in accordance with 40 CFR 262–268. After making the hazardous waste determination as required, if the waste is determined to be nonhazardous, the generator shall then classify the waste as Class 1, Class 2, or Class 3 (as defined in Section 335.505 through Section 335.507) using one or more of the methods listed in Section 335.503(a)(4) and Section 335.508 and manage the waste in accordance with the requirements of Chapter 335 of the TAC for industrial solid waste.
Characterization of Hazardous Waste 40 CFR 264.13(a)(1); 40 CFR 268.7 30 TAC 335.504(3) 30 TAC 335.509 30 TAC 335.511	Generation of a RCRA hazardous waste for treatment, storage, or disposal—applicable if hazardous waste is generated (e.g., PPE).	Must obtain a detailed chemical and physical analysis of a representative sample of the waste(s) that at a minimum contains all the information that must be known to treat, store, or dispose of the waste in accordance with 40 CFR 264 and 268. Must also determine whether the waste is restricted from land disposal under 40 CFR 268 et seq. by testing in accordance with prescribed methods or use of generator knowledge of waste.

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Table 3-3 *(continued)*Potential Action-Specific ARARs/TBCs

Citation	Activity or Prerequisite/Status	Requirement
National Oil and Hazardous Substances Pollution Contingency Plan	Procedure for planning and implementing off-site response actions.	USEPA will determine the acceptability under the selection of any facility selected for the treatment, storage, or disposal of CERCLA waste.
40 CFR 300.440		
Management of RCRA Hazardous Waters—Wastewater Treatment Unit Exclusion 40 CFR 264.1(g)(6) 40 CFR 270.1(c)(2) 30 TAC 335.41(d)(1)	Treatment/disposal of wastewater containing RCRA hazardous waste—applicable to management of contaminated groundwater if it is determined to contain RCRA characteristically hazardous waste.	On-site wastewater treatment units, as defined in 40 CFR 260.10, that are part of a wastewater treatment facility subject to regulation under Section 402 or Section 307(b) of the CWA are excluded from the requirements of RCRA Subtitle C (Note: USEPA has clarified that this exemption applies to all tank systems, conveyance systems, and ancillary equipment, including transfer trucks, associated with the wastewater treatment unit [53 FR 34079, September 2, 1988]).
Requirements for Temporary Storage of Hazardous Waste in Accumulation Areas 40 CFR 262.34(a) and (c)(1) 30 TAC 335.69(a) and (d)	On-site accumulation of 55 gallons or less of RCRA hazardous waste for 90 days or less at or near the point of generation—applicable if hazardous waste is generated (e.g., PPE) and stored in an accumulation area.	A generator may accumulate hazardous waste at the facility provided that Waste is placed in containers that comply with 40 CFR 264.171 to 264.173 (Subpart I); and Container is marked with the words "hazardous waste"; or Container may be marked with other words that identify the contents.
Requirements for the Use and Management of Containers 40 CFR 264.171–264.173 30 TAC 335.69(e) 30 TAC 335.152(a)(7)	On-site storage/treatment of RCRA hazardous waste in containers for greater than 90 days—applicable if hazardous waste is generated (e.g., PPE) and is stored in containers.	Design and operating standards of 40 CFR 264.175(c) and 40 CFR 264.171, 264.172, and 264.173(a) and (b) must be met for the use and management of hazardous waste in containers.
Well Construction Standards— Monitoring or Injection Wells 16 TAC 76.1000	Construction of water wells—applicable to construction of new monitoring or injection wells, if needed.	Wells shall be completed in accordance with the technical requirements of Section 76.1000, as appropriate.
Class V Injection Wells 30 TAC 331, Subchapter H	Installation, operation, and closure of injection wells for in situ chemical oxidation fall in the category of Class V Injection Wells – relevant and appropriate.	Injection wells shall be constructed to the required specifications for isolation casing, surface completion, prevention of commingling, and confinement of undesirable groundwater to its zone of origin. Closure shall be accomplished by removing all of the removable casing and the entire well shall be pressure filled via a tremie pipe with cement from bottom to the land surface, or closure shall be performed by the alternative method for Class V Wells completed in zones of undesirable groundwater. Groundwater concentrations at time of well closure will determine the appropriate method of abandonment.

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Table 3-3 *(continued)*Potential Action-Specific ARARs/TBCs

Citation	Activity or Prerequisite/Status	Requirement
Well Construction Standards—Extraction Wells	Construction of water wells—applicable to construction of extraction (recovery) wells.	Wells shall be completed in accordance with the technical requirements of Section 76.1000, as appropriate.
16 TAC 76.1000(a) and (c) through (h) 16 TAC 76.1002(a) through (c) 16 TAC 76.1008(a) through (c)	constituction of extraction (recovery) wells.	Water wells completed to produce undesirable water shall be cased to prevent the mixing of water or constituent zones.
		The annular space between the casing and the wall of the borehole shall be pressure grouted with cement or bentonite grout to the land surface. Bentonite grout may not be used if a water zone contains chloride water above 1500 ppm or if hydrocarbons are present.
		Wells producing undesirable water or constituents shall be completed in such a manner that will not allow undesirable fluids to flow onto the land surface.
		During installation of a water well pump, installer shall make a reasonable effort to maintain integrity of groundwater and to prevent contamination by elevating the pump column and fittings, or by other means suitable under the circumstances. Pump shall be constructed so that no unprotected openings into the interior of the pump or well casing exist.
	Tre	eatment/Disposal
Disposal of Wastewater (e.g., contaminated groundwater, dewatering fluids, decontamination liquids)	RCRA-restricted characteristically hazardous waste intended for disposal—applicable if extracted groundwater is determined to be RCRA characteristically hazardous.	Disposal is not prohibited if such wastes are managed in a treatment system subject to regulation under Section 402 of the CWA that subsequently discharges to waters of the United States.
40 CFR 268.1(c)(4)(i) 30 TAC 335.431(c)		
		Closure
Requirements for Closure of a RCRA Container Storage Area 40 CFR 264.111 40 CFR 264.178 30 TAC 335.152(a)(5) 30 TAC 335.152(a)(7)	Closure of a RCRA-permitted container storage area—applicable if hazardous waste is generated (e.g., PPE) and is stored in containers.	post-closure escape of hazardous waste, hazardous constituents, leachate, contaminated runoff, or hazardous waste decomposition products to ground or surface waters or to the atmosphere; and Complies with closure requirements of 40 CFR 178.
		All hazardous waste and residues must be removed from containment system. Remaining containers, liners, bases, and soil containing or contaminated with hazardous waste or residues must be decontaminated or removed.

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Table 3-3 *(continued)*Potential Action-Specific ARARs/TBCs

Citation	Activity or Prerequisite/Status	Requirement
Standards for Plugging Wells that Penetrate Undesirable Water or Constituent Zones	Plugging and abandonment of wells—applicable to plugging and closure of monitoring and/or extraction wells.	If a well is abandoned, all removable casing shall be removed and the entire well pressure filled via a tremie pipe with cement from bottom up to the land surface. In lieu of this procedure, the well shall be pressure-filled via a tremie tube with bentonite grout of a minimum 9.1 lb/gal weight followed by a cement plug extending from land
16 TAC 76.1004(a) through (c)		surface to a depth of not less than 2 feet. Undesirable water or constituents or the freshwater zone(s) shall be isolated with cement plugs.
	Post-Closure	Care and Land Use Controls
Warning Signs in Contaminated Areas	Hazardous substances left in place on contaminated property—relevant and	Placement of warning signs on property contaminated with hazardous substances is required when such contamination presents a danger to public health or safety.
30 TAC 335.443-448	appropriate.	Warning signs can be removed when it is determined that the remedial action on the contaminated property is complete and that no further hazard to the public health and safety exists.
Land Use Controls when Hazardous Substances are Left in Place 30 TAC 335.565	Hazardous substances left in place on contaminated property—relevant and appropriate.	Where engineering or land use control measures are required to protect human health and the environment, they must comply with the identified post-closure care requirements and recordation notification with the county for the facility in accordance with Section 335.566.
30 TAC 335.566		Must make recordation notification with the county or counties in which the activities take place the information specified in Sections 335.566(b) through (e):
		 Description of post-closure measures required, Description of any land use or legal controls placed on the future use of the property, Metes and bounds description of the tract of land, and Statement that pertinent information and documents are available for inspection.

Abbreviations:

ARAR CFR CWA USEPA FR Ib/gal	applicable or relevant and appropriate requirement Code of Federal Regulations Clean Water Act of 1972 U.S. Environmental Protection Agency Federal Register pound per gallon	% PPE ppm RCRA TAC TBC	percent personal protective equipment part per million Resource Conservation and Recovery Act of 1976 Texas Administrative Code to be considered (guidance)
ib/yai	pound per gallon	.50	to 20 contract ou (guillantes)

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Table 3-4
Proposed Cleanup Levels for Target COCs/COPECs in Soil

COCs / COPECs Targeted for Remediation	SAI-Ind (mg/kg)	GWP-Ind (mg/kg)	SS Eco PRG (mg/kg)	TS Eco- PRGs (mg/kg)	Proposed Cleanup Level ^a
Remediation	0-2 feet	Vadose Zone	0 -0.5 feet	0-3 feet	(mg/kg)
2.4./ T-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	F10	F 1	/ 1	4.7	4.7 ^b
2,4,6-Trinitrotoluene	510	5.1	6.1	4.7	5.1c
2,4-Dintrotoluene	4.2	0.042		12	0.042
2,6-Dinitrotoluene	4.2	0.042	2.7	6.8	0.042
2-Amino-4,6-dinitrotoluene	170	1.7			1.7
4-Amino-2,6-dinitrotoluene	170	1.7			1.7
Perchlorate	950	7.2			7.2

Notes and Abbreviations:

^a Unless otherwise noted, cleanup level applies to soil from surface to groundwater interface

^b Applies from 0 to 3 feet below ground surface

^c Applies from 3 feet below ground surface to groundwater interface

COC contaminant of concern

COPEC contaminant of potential ecological concern EcoPRG Ecological Preliminary Cleanup level

GWP-Ind soil medium specific concentration for industrial use based on groundwater protection

mg/kg milligrams per kilogram

SAI-Ind soil medium specific concentration for industrial use based on inhalation, ingestion, and dermal contact

SS surface soil TS total soil

Table 3-5
Proposed Cleanup Levels for Target COCs in Groundwater

COCs Targeted for Remediation	TCEQ RRS2 MSC GW-Ind (μg/L)	MCL (μg/L)		
Explosives				
2,4-Dinitrotoluene	0.42			
2,6-Dinitrotoluene	0.42			
2-Nitrotoluene (o)	1,000			
3-Nitrotoluene (m)	1,000			
4-Nitrotoluene (p)	1,000			
Anions				
Perchlorate 72				
Volatile Organic Compounds				
1,2-Dichloroethane		5		
Methylene Chloride		5		
Trichloroethene (TCE)		5		
1,1-Dichloroethene (TCE degradation product)		7		
1,2-Dichloroethene (TCE degradation product)		5		
Vinyl Chloride (TCE degradation product)		2		
Metals				
Arsenic		10		
Mercury		2		
Nickel	2,000			

Notes and Abbreviations:

GW-Ind groundwater MSC for industrial use MSC medium specific concentration

MCL Safe Drinking Water Act maximum contaminant level μg/L micrograms per liter MSC medium specific concentration

RRS2 Risk Reduction Rule Standard No. 2

TCEQ Texas Commission on Environmental Quality

Table 3-6 Proposed Cleanup Levels for Target COCs in Cooling Water Lines

Explosive	GWP-Ind (mg/kg)
2,4,6-Trinitrotoluene	5.1
2,4-Dinitrotoluene	0.042
2,6-Dinitrotoluene	0.042
2-amino-4,6-Dinitrotoluene	1.7
4-amino-2,6-Dinitrotoluene	1.7

Abbreviations:

mg/kg GWP-Ind milligrams per kilogram

soil MSC for industrial use based on groundwater protection

MSC medium-specific concentration

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4.0 Identification and Screening of Technologies and Process Options

The primary objective of identifying, screening, and evaluating potentially applicable technology types and process options for the LHAAP-29 FS is to identify an appropriate range of remedial technologies and process options to be developed into remediation alternatives. This screening process consists of a series of analytical steps that include the following:

- Identify volumes or areas of media of concern, and the associated COCs (Section 4.1)
- Identify GRAs (Section 4.2)
- Identify and screen remedial technologies and process options (Section 4.3)
- Evaluate and select representative process options (Section 4.4)

These steps are outlined in the USEPA RI/FS guidance (USEPA, 1988b) and the NCP.

4.1 Contaminants and Media Volumes of Concern

Section 2.0 presents detailed site conditions at LHAAP-29. Based on available sampling data, soil, sediment, groundwater, and residual contamination in the former wastewater and cooling water lines at LHAAP-29 have been identified as media of concern because these media pose an unacceptable carcinogenic risk and non-carcinogenic hazard to a hypothetical future maintenance worker. These contaminated media include:

- TNT in soils adjacent to the foundation of the former process buildings 802-A (29SB08), 806-A (stained) and 806-D (29DLineWHW01) are contributing to ecological risks as well as having the potential for migration into groundwater. Contamination in this area is primarily present in the top one (1) foot of soil with an estimated volume of 230 cy.
- Residual explosive compounds remain in the former TNT wastewater and cooling water drain lines and manholes.
- Explosives in sediment and surface soils in the cooling water outfall ditch (29SD46) and immediately adjacent to the north of Avenue D (29SD13, 29SB15, and GPS-12) that are contributing to unacceptable health and ecological risks, respectively. The maximum depth of contamination is 7 feet bgs. Maximum depths of excavation will be 3 feet bgs for an ecological receptor for a total volume of 760 cy.
- Isolated perchlorate-containing soils in the northeastern portion of LHAAP-29 (sample location 29SB86) at a maximum depth of 8 feet bgs or approximately 2,900 cy.
- Dissolved plumes of VOCs, explosive compounds, and perchlorate contamination
 exist in groundwater at LHAAP-29 that pose an unacceptable cancer risk and health
 hazard. The extent of the contamination has been determined. Perchlorate, VOCs,
 and nitrotoluene contamination exists in the shallow zone and has contaminated

approximately 9 million gallons. A VOC plume in the intermediate zone is approximately 21 million gallons (based on MC).

4.2 General Response Actions

GRAs are large groups of remedial actions that typically satisfy the RAOs. The GRAs include no action, LUCs, containment, removal, treatment, and disposal. These GRAs may be combined to form remediation alternatives that meet the RAOs. The following are descriptions of the GRAs:

- **No Action**—The no action GRA is retained throughout the FS process as required by the NCP. The no action alternative provides a comparative baseline against which other alternatives can be evaluated. Under this alternative no remedial action will be taken. The site is considered to be left "as is," with no LUCs, containment, removal, treatment, or other mitigating actions.
- Land Use Controls—LUCs include institutional and administrative controls that would reduce or eliminate access to the site. The volume, mobility, and toxicity of the contaminants are not reduced through the application of LUCs. LUCs are generally combined with other GRAs to meet the RAOs.
- Containment—Another method of reducing risk to receptors is through containment, which reduces access to the contaminated medium or the migration potential of the contaminated medium. The contaminated medium must be isolated from the primary transport mechanisms such as precipitation migration through the soil column and groundwater flow. This isolation may be accomplished through capping of contaminated soils or the installation of subsurface barriers to prevent groundwater migration.
- **Removal**—Removal GRAs extract the contaminated medium from its present location and move it to an alternative location for treatment and/or disposal. These removal technologies can be selected to reduce exposure to receptors and can be used in conjunction with treatment processes.
- In Situ Treatment—In situ treatment GRAs or process options reduce the toxicity, mobility, or volume of the contaminated medium. Chemicals are added, physical properties of the medium are changed, or biological activity of the medium is modified without removal.
- Ex Situ Treatment—Ex situ treatment GRAs involve the reduction of toxicity, mobility, or volume of contaminated medium. Ex situ treatment processes are typically coupled with removal and disposal process options.
- Disposal—Disposal GRAs involve the discharge of the contaminated medium.
 Disposal process options are typically coupled with removal and treatment process options.

4.3 Screening of Technologies

This section presents the approach to technology and process option screening. In the technology screening process, GRAs are identified that, by themselves or in combination with other GRAs, could be implemented to meet the RAOs established for LHAAP-29. Technologies associated with each GRA and process options associated with each technology are identified. Process options that are not technically feasible for the site are eliminated (screened out) from further consideration. If all of the process options under a given technology are screened out, the entire technology is eliminated.

The technologies and process options are initially screened for technical applicability to identify those to be carried forward for further evaluation. The screening process reduces the number of possible process options for a given technology to a number that is appropriate for consideration at LHAAP-29. The following are the two general criteria used to determine if a technology or process option should be retained for further evaluation:

- Applicability to the type and combination of contaminants
- Applicability to the site's physical conditions

Figures 4-1 and **4-2** present the technologies and process options considered for LHAAP-29 soil and groundwater, respectively. Process options not considered technically applicable were not retained for further evaluation; the rationale for their elimination is shown in these figures.

4.4 Evaluation and Selection of Representative Process Options

In this section, each of the process options retained from the initial screening in **Section 4.3** (**Figures 4-1** and **4-2**) are further evaluated and screened, further reducing the list of process options that are developed into alternatives in **Section 5.0**. Process options are evaluated using three criteria: effectiveness, implementability, and cost. Based on these criteria, representative process options are selected for each technology. The representative process options provide a basis for developing alternatives in the FS.

The general descriptions of the process options retained from the screening, along with the relevant aspects of effectiveness, implementability, and cost, are discussed. The effectiveness evaluation considers the following: (1) the potential effectiveness of process options in handling the estimated areas or volumes of the medium; (2) the contribution toward meeting any of the goals identified in the RAOs; (3) the potential impacts to humans and the environment during the construction and implementation phase; and (4) how proven and reliable the process is with respect to the contaminants and conditions at the site.

The implementability evaluation considers both the technical and administrative feasibility of implementing a process option. Implementability concentrates on the difficulty of implementing the option, including the number of treatability studies required, the extent of innovative design

required, and the extent of site preparation needed. Unusual equipment or unusual conditions for standard equipment may decrease the ease of implementation. The institutional aspects of implementability such as permitting and availability of services are also considered.

The cost evaluation focuses on the relative capital and operation and maintenance (O&M) costs required. A ranking of high, medium, or low relative to other similar process options is given; each ranking considers both capital and O&M costs. Based on this evaluation, one or more representative process options are selected for each response action to be carried forward into the development of alternatives. The selection of representative process options for the development of alternatives does not eliminate the remaining process options from future consideration. Those process options not carried forward may be reconsidered during the development of the PP, ROD, or remedial design.

4.4.1 Soil/Sediment

The soil process options will be evaluated to address residual explosives in the drain lines, soil, and sediment, and perchlorate in the soil. The risks and hazards posed to hypothetical future maintenance workers and ecological receptors as well as the potential migration of contaminants to groundwater from residual contamination will be addressed.

4.4.1.1 No Action

The "no action" process option does not provide additional remediation, maintenance, or security activities at contaminated soil or sediment areas at LHAAP-29. The lack of a remedial action can lead to receptor exposure to the contaminated soil or sediment. This process option is retained as a baseline with which other remediation alternatives are compared.

- **Effectiveness**—This response action could have negative long-term impacts on human health and the environment. Industrial use at LHAAP-29 would result in risks to humans from exposure to contaminated soil and sediment.
- **Implementability**—No implementation is required.
- **Cost**—None.

4.4.1.2 Land Use Controls

LUCs would be implemented to regulate access to soil and groundwater and include covenants/deed restrictions, administrative controls, and physical mechanisms. This process option controls exposure by restricting access and use of the contaminated soil and groundwater and also provides information needed to assess future conditions at the site. The LUC process option is applicable to the soil and groundwater at LHAAP-29. Notification of industrial/recreational use will accompany all transfer documents and will be recorded in the County Courthouse. Five-year reviews will be performed to document that the land use remains consistent with the industrial/recreational exposure scenario evaluated in the risk assessment.

4.4.1.2.1 Access Controls

Access controls would be implemented to regulate access to the contaminated soil and sediment areas. The process options for access controls include covenants, administrative controls, and physical barriers/security.

Covenants. To protect human health, restrictions can be placed on the use of the contaminated site through modifications to the property deed or transfer documents. Deed restrictions would be needed only if the U.S. Army releases the property to a non-federal entity. These restrictions are only effective as long as they are enforced by the property owners and local authorities. The U.S. Army is ultimately responsible for the enforcement of LUCs.

- **Effectiveness**—Covenants are effective, if enforced, in controlling human activities such as construction activities. These actions can limit or prevent exposure to contaminants remaining on the site after remediation and can be implemented on a temporary basis. However, their effectiveness declines with time as institutional knowledge is lost.
- **Implementability**—These options can be readily implemented.
- Cost—Low.

Administrative Controls. Administrative controls consist of the use of procedures to limit access to sites to control access to both surface and subsurface contamination. Permits for subsurface penetration or excavation can be used. Notices can be filed with local authorities defining the presence of hazardous waste. These are controls the U.S. Army can use while they maintain control of the site.

- Effectiveness—Administrative controls are effective in controlling human intrusion into contaminated areas during and after remediation. Procedures that limit certain activities in the vicinity of the wastes and access to the site which limits exposure. However, it is not effective for controlling the soil-to-groundwater pathway or for ecological receptors. Administrative controls can be used in conjunction with barriers and deed restrictions. This option is effective only while the administrative controls are enforced.
- **Implementability**—Procedures are readily available and implemented. They may need to be modified for LHAAP-29.
- Cost—Low.

Physical Mechanisms. Physical mechanisms include physical barriers intended to limit access to property, such as fences or signs. However, the future use of the site is to be a part of a national wildlife refuge under the USFWS. It is anticipated that restrictions and administrative

controls will be adequate to control access to the contaminated groundwater and physical mechanisms will not be required.

- Effectiveness—Physical barriers and security are effective in controlling human intrusion into contaminated areas during and after remediation. This option is effective only as long as the barriers and security mechanisms are maintained. However, it is not effective for controlling the soil-to-groundwater pathway or for ecological receptors.
- **Implementability**—This option is readily implemented with available equipment and personnel.
- Cost Low.

4.4.1.2.2 Monitoring

Monitoring is used to assess the performance of remedial actions and verify compliance with the established RAOs. Process options for monitoring are physical surveillance and long-term media monitoring.

Physical Surveillance. Visual and physical inspections of engineered remedial action components can detect physical changes (e.g., cracks in caps, erosion, unwanted vegetation, holes in fences, etc.) that may ultimately lead to the failure or unsatisfactory performance of that component. Repairs and/or revised maintenance activities can be implemented as a result of these inspections. However, it is not effective for controlling the soil-to-groundwater pathway or for ecological receptors.

- **Effectiveness**—Physical surveillance is effective in determining the continued integrity of engineered systems and the need for repairs and/or replacement. Physical surveillance needs to be used with contaminant monitoring to assess the impact of integrity failure.
- **Implementability**—Physical surveillance is easily implemented. It requires experienced, but readily available, personnel to make regular visits to the site for inspections. Existing engineered controls at LHAAP are currently being inspected.
- **Cost**—Low.

4.4.1.2.3 Summary of Land Use Control Process Options

Since LUCs will not prevent soil-to-groundwater contamination or exposure of ecological receptors, LUCs are not retained as a process option.

4.4.1.3 Containment

The containment GRA consists of technologies that limit the migration of contaminants and the associated potential for exposure, but they do not reduce contaminant mobility, toxicity, or volume. The technologies considered are soil, asphalt or multilayer capping.

4.4.1.3.1 Capping

The capping technology is intended to minimize (1) infiltration of surface water/precipitation and subsequent leachate generation caused by percolation of water through the waste, (2) mobilization of contaminants through wind or water erosion, or (3) direct contact with surface or subsurface contamination by intruders or biota. The capping process options considered are soil covers, asphalt caps, and multilayer caps.

Soil Cover. Soil covers consist of a layer of soil placed over contamination. Vegetation is generally encouraged to limit erosion. The purpose of the cover is to prevent access or exposure to the contamination, but the cover does not control infiltration of water through the contamination. It is best used on contamination that is relatively insoluble or in combination with a treatment technology that renders the contamination insoluble.

- **Effectiveness**—A soil cover can be very effective at preventing access to explosives in surface soil. It is not applicable to deeper soil that already has a layer of clean soil between the contamination and the receptor.
- Implementability—Soil covers are easy to implement. Standard earthmoving equipment can move local soil over the contaminated areas. Portions of LHAAP-29 may require some initial clearing. Soil cover maintenance to limit large vegetative growth that could disrupt the cover and to control erosion would be needed. Frequent maintenance (mowing) would be required.
- Cost—Low.

Asphalt Cap. Asphalt caps control infiltration of rainwater or run-on water through the installation of impermeable asphalt. This process option is particularly useful if the site is to be used as a parking lot or other light industrial use.

- **Effectiveness**—Asphalt caps can be effective at reducing infiltration if sufficient maintenance occurs. Asphalt can quickly develop cracks and holes that need to be filled, and maintenance will be needed to repair them as they occur. These caps are most effective if the area needs to be asphalted for another use that will promote its long-term maintenance.
- Implementability—Asphalt caps are easy to install. As with other caps to control infiltration, they need to be sloped to encourage runoff during rain events. Frequent maintenance is less necessary than with multilayer caps as the asphalt does not require

mowing. However, asphalt cracks easily and this must be controlled to maintain effectiveness.

• Cost—Low.

Multilayer Cap. A multilayer cap is an engineered cover that can consist of various layers of soil, clay, membranes and other materials. Multilayer caps control infiltration of rainwater or run-on water through the installation of impermeable layer materials and can prevent access or exposure to the contamination.

- **Effectiveness**—Multilayer caps can be effective at reducing infiltration if sufficient maintenance occurs. Long-term maintenance would be required for ensure cracks and holes do not develop. Maintenance will be needed to repair them as they occur.
- Implementability—A multilayer cap is more difficult to implement than a soil or asphalt cap due to the design and installation requirements. As with other caps to control infiltration, they need to be sloped to encourage runoff during rain events. More maintenance is necessary with a multilayer cap than an asphalt cap as frequent mowing is required. The multilayer cap must be inspected and maintained to ensure its long-term effectiveness.
- **Cost**—High.

Plug and Abandon Lines. Plugging and abandoning lines consists of completely filling the piping or plugging the inlets and outlets (e.g., with a cementitious grout). Plugging and abandoning can prevent migration of solid residue from the lines, minimize contact between contaminants and surrounding groundwater, and prevent access or exposure to the contamination.

- **Effectiveness**—Plugging and abandoning lines can be effective against migration and leaching if occasional maintenance is performed. Maintenance would be required to ensure the inlets and outlet plugs remain intact, or to repair them as needed.
- Implementability—Plugging and abandoning lines is relatively simple to implement. Inlets and outlets may be filled in and/or covered with clean local soil or concrete. For greater resistance to leaching, some form of grout or flowable material may be used to fill the interior of the pipe lines before plugging the inlets and outlets.
- **Cost**—Moderate.

4.4.1.3.2 Summary of Containment Process Options

The soil cover alternative is a representative process option for addressing the relatively insoluble explosive contamination in the surface soil and sediments. It provides the least expensive option that meets the needs of a containment option. However, the capping options do not prevent the contaminated soil from continuing to impact groundwater and thus would be less

protective of human health and the environment than other alternatives. Therefore, the containment process options for soil and sediment are removed from further consideration.

Plugging and abandoning lines is a generally effective and efficient method of addressing buried piping. Therefore, the containment process option of plugging and abandoning lines is retained for further consideration.

4.4.1.4 Removal

The removal GRA consists of technologies that remove contaminated media or waste material to either relocate it or prepare it for treatment and/or disposal. The removal technology considered is excavation with a process option of conventional excavation.

4.4.1.4.1 Excavation

Conventional Excavation. This excavation method uses a variety of conventional excavation equipment to remove debris, soil, and other buried waste. The equipment can include excavators, track loaders, bulldozers, and tool carriers of differing sizes with attachments or manipulators suitable for dealing with a varied waste profile. This equipment can be used individually or together as circumstances dictate. It is considered applicable to the pipelines and contaminated soil and sediments at LHAAP-29. It can be used for both shallow and deep soil.

• Effectiveness—Conventional excavation equipment is applicable to the LHAAP-29 soils. The equipment has consistently proven reliable and effective for soil and other media in hazardous and non-hazardous applications for decades. Various attachments can increase the versatility of the equipment, allowing their use with a wide range of wastes. Ancillary equipment for screening, sorting, and segregation can be effectively integrated with conventional excavation equipment.

The hazards to operators, in addition to the normal excavation hazards, come from exposure to contaminated media. Misting or fixative agents can reduce fugitive dust emissions during excavation. Buried piping and any residual contents in the piping, can also pose hazards to both human health and the environment when pipes are broken or disturbed during excavation. PPE can reduce or eliminate exposure from inhalation/ingestion or dermal contact. The potential for releasing contamination (from residual contamination inside the lines, clay pipe with asbestos wicking, and transite asbestos containing pipe) during removal of the pipelines is likely.

- **Implementability**—Conventional excavation is readily implemental, and the equipment, attachments, and operators are widely available. The equipment can be readily adapted to the material and conditions at the site. Special handling and disposal considerations would apply to any transite piping that is excavated.
- **Cost**—Moderate.

4.4.1.4.2 Summary of the Removal Process Option

Conventional excavation equipment is carried forward as the representative process option for soil removal because of its effective application for a wide range of wastes, its equipment availability, and its widespread use in environmental restoration activities. Excavation of piping is not carried forward due to potential to disturb the asbestos containing materials during removal.

4.4.1.5 Ex Situ Treatment

Ex situ treatment technologies provide varying levels of waste treatment following removal of the waste. These technologies are applied to reduce the volume, mobility, or toxicity of the waste. The ex situ treatment technologies considered are physical/chemical, thermal, and biological treatment. Ex situ treatment could be considered if excavated material requires treatment before disposal to meet waste acceptance criteria or if complete treatment could be achieved so remaining material is clean.

4.4.1.5.1 Thermal Treatment

Thermal treatment destroys and/or removes organic and volatile metal contaminants. The process option considered is incineration.

Incineration. Incineration is an ex situ thermal destruction process in which organic compounds is destroyed by exposure to extremely high temperatures. It is considered applicable to the source problems at LHAAP-29. Many different systems are available: rotary dryer systems, indirect-fired systems, direct-fired systems, screw-type systems, and asphalt plant aggregate driers. Each system uses the same basic principle of operation, which is a furnace to remove and destroy organic compounds in the waste feed. One of the more common systems, a rotary kiln incinerator, feeds the waste material into the upper end of a sloped rotating kiln. The slope and the rotating action conveys the waste to the low end of the kiln, exposing the waste to the heated gases (up to 1,800 degrees Fahrenheit [°F]) in the kiln and vaporizing and destroying the contaminants. The combustion gases are then drawn through an afterburner (2,200°F) and scrubbing system before discharge to the atmosphere.

• Effectiveness—Incinerators have been effectively used for years on organic-contaminated media and are the Best Demonstrated Available Technology for many RCRA organics. It is applicable to most, if not all, of the organic- and explosives-contaminated wastes at LHAAP-29. The destruction capabilities of an incinerator allow the achievement of relatively low cleanup levels. Incineration is a robust technology that can handle a wide variety of organic compounds and concentrations because of its high temperatures. The disadvantages of incineration are that some organics generate toxic products of incomplete combustion, some materials are not incinerable, the capital and operating costs are high, and supplemental fuel is often required. If the ash contains heavy metals, the ash may have to be stabilized before disposal as a RCRA waste.

- Implementability—Incineration systems are available for both on- and off-site use. The off-gas stream may require additional treatment and may produce a residue that requires disposal. Thermal treatment systems are generally not well received by the public because of concerns with air emissions.
- **Cost**—High.

4.4.1.5.2 Biological Treatment

Biological treatment process options use biological processes to degrade or destroy contaminants. The ex situ process evaluated is composting.

Composting. Composting is a controlled biological process by which organic contaminants (e.g., VOCs) are converted by microorganisms (under aerobic and anaerobic conditions) to innocuous, stabilized byproducts. Typically, thermophilic conditions (54–65 degrees Celsius [°C]) must be maintained to properly compost soil contaminated with hazardous organic contaminants. The increased temperatures result from heat produced by microorganisms during the degradation of the organic material in the waste. In most cases, this is achieved by the use of indigenous microorganisms. Soil is excavated and mixed with bulking agents and organic amendments, such as wood chips, and animal and vegetative wastes, to enhance the porosity of the mixture to be decomposed. Maximum degradation efficiency is achieved through maintaining oxygenation (e.g., daily windrow turning), irrigation as necessary, and closely monitoring moisture content and temperature. There are three process designs used in composting: aerated static pile composting (compost is formed into piles and aerated with blowers or vacuum pumps), mechanically agitated in-vessel composting (compost is placed in a reactor vessel where it is mixed and aerated), and windrow composting (compost is placed in long piles known as windrows and periodically mixed with mobile equipment). Windrow composting is usually considered to be the most cost-effective composting alternative. Meanwhile, it may also have the highest fugitive emissions. If VOC or SVOC contaminants are present in soil, off-gas control may be required.

- Effectiveness—The composting process may be applied to soil contaminated with biodegradable organic compounds. Pilot and full-scale projects have demonstrated that aerobic, thermophilic composting is able to reduce the concentration of VOCs, polyaromatic hydrocarbons, and explosives [TNT, hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX), and octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX)]. The addition of amendments will increase the volume of the waste. Windrow composting has been demonstrated as an effective technology for treatment of explosives-contaminated soil.
- **Implementability**—All materials and equipment used for composting are commercially available. Substantial space may be required for composting.
- Cost—Low.

4.4.1.5.3 Summary of Ex Situ Treatment Process Options

Currently the chemicals at LHAAP-29 that are considered to potentially require treatment are the explosives in soil and sediment (potential characteristic hazardous waste). Perchlorate contaminated soils have not been considered for ex situ treatment since it is non-hazardous. The thermal treatment option is effective for permanent destruction of explosives in the soil and is carried forward for consideration. Biological treatment by composting is less developed for LHAAP-29 conditions and is removed from further consideration.

4.4.1.6 Disposal

The disposal GRA consists of those technologies that provide for the disposal of removed wastes at new or existing, permitted disposal facilities. Both on-site and off-site facilities are evaluated. A selection of on-site facilities versus off-site facilities is made for developing alternatives.

4.4.1.6.1 Off-Site Disposal

Off-site disposal options include off-site treatment and disposal facilities, a RCRA disposal facility, or an industrial landfill. The selection of the disposal facility depends on the waste characteristics and although all are evaluated here, none are selected to represent other off-site options.

Treatment, Storage, Disposal Facility. A Treatment, Storage, Disposal (TSD) facility is a commercial, permitted, off-site facility that is licensed to treat, store, and/or dispose of a variety of waste streams. There are numerous such facilities all over the country offering broad ranges of treatment options, many of which could effectively treat and dispose of the LHAAP-29 waste and soils. This option would be used if treatment before disposal is needed to meet ARARs.

- **Effectiveness**—A TSD facility is effective at treating and disposing of treated wastes in a permitted, off-site disposal facility.
- Implementability—Numerous facilities exist that have and are treating wastes similar to those found at LHAAP-29. These facilities are already permitted and licensed to operate. Wastes have to meet the waste acceptance criteria of the receiving TSD facility.
- **Cost**—Moderate.

RCRA Disposal Facility. This process option consists of any number of existing disposal facilities that use engineered features such as multilayer liners and caps, leachate detection and collection systems, run-on/-off controls, and intrusion barriers to isolate wastes from human and environmental receptors.

• **Effectiveness**—Disposal involves permanent disposition of the RCRA-generated contaminated soil in a manner that protects human health and the environment. Off-

site disposal would include the transportation of excavated soils to an approved and licensed facility.

- **Implementability**—Implementation is moderate if the waste acceptance criteria can be met.
- Cost—Moderate.

Industrial Landfill. An existing industrial landfill can be used to dispose of that debris or refuse that is not a RCRA waste or has been decontaminated to acceptable levels. Such a facility is a Class II lined facility permitted to receive industrial, commercial, institutional, land-clearing, and construction/demolition waste. The facility does not accept RCRA-hazardous waste or free liquids. This option would be used to dispose of waste that is considered hazardous to human health and the environment but is not a RCRA-hazardous waste.

- **Effectiveness**—Industrial landfills are effective in isolating low hazard wastes from the environment and human receptors because the waste acceptance criteria severely restrict the type and concentrations of waste that may be disposed.
- **Implementability**—Disposal of the excavated clean wastes or treated wastes would involve transportation and compliance with waste acceptance criteria.
- Cost—Moderate.

4.4.1.6.2 On-Site Disposal

On-site consolidation is considered as the technology process option for on-site disposal.

Consolidation. Consolidation involves placing treated LHAAP-29 soil and sediment back into LHAAP areas. The waste is excavated, partially treated on the site if needed, and then placed elsewhere on LHAAP. The contaminants in the treated waste would have to have been rendered immobile, making the treated waste better suited for placement. This option precludes the need to transport the treated waste to an off-site disposal facility. A single or multilayer cap would then be placed over the waste. If the waste is fully treated, no special disposal process option is needed.

- **Effectiveness**—Consolidation is effective in isolating the very low hazard wastes from human receptors and the environment. It can limit the area requiring long-term institutional controls.
- Implementability—Consolidation is used at other hazardous waste sites around the country where off-site disposal options are unavailable or undesirable and where the continued on-site presence of treated waste is not problematic. Given the potential future land uses at the LHAAP, there may be regulatory and public reluctance to moving the waste around the LHAAP.
- **Cost**—Low compared to off-site disposal.

4.4.1.6.3 Summary of Disposal Process Options

All off-site disposal process options are carried forward for additional consideration until waste streams and volumes are more clearly identified in the alternative development process. The onsite disposal option of consolidation is not retained because of the potential regulatory and public concerns about leaving waste on the site after having already removed it, the potential future land uses, and the widespread availability of off-site treatment and disposal facilities.

4.4.1.7 Summary of Representative Soil/Sediment Process Options

Figure 4-3 is presented to illustrate the process options that have been selected for remedial alternative development for soils at LHAAP-29. The following remedial alternatives are developed from the retained representative GRAs, technologies or process options:

- No action
- Removal, off-site disposal
- Plug and abandon pipe lines

Detailed analyses of these remedial alternatives are included in **Section 5.0**.

4.4.2 Groundwater

In the following subsections, process options are evaluated to address shallow groundwater contaminated with VOCs, explosives and perchlorate; and intermediate groundwater contaminated with MC.

4.4.2.1 No Action

The "no action" process option provides no groundwater remedial activities. No monitoring of the groundwater or surface water conditions occurs under this process option. This process option is retained as a baseline with which other remediation alternatives are compared.

- **Effectiveness**—Without access controls or remediation, the groundwater from LHAAP-29 could result in a future unacceptable risk to humans if the groundwater is ingested.
- Implementability—No implementation is required.
- Cost—None.

4.4.2.2 Land Use Controls

This LUC process option would be implemented to regulate access and use of the contaminated groundwater at LHAAP-29. The U.S. Army will perform notification of industrial/recreational use which will accompany all transfer documents and will be recorded in the Harrison County Courthouse. Five-Year Reviews will be performed to document that the land use remains consistent with the industrial/recreational exposure scenario evaluated in the risk assessment.

4.4.2.2.1 Access Controls

Access controls would be implemented to regulate access to the groundwater. The process options for access controls include covenants/deed restrictions, administrative controls, and physical mechanisms.

Covenants/Deed Restrictions. Restrictions to the groundwater can be accomplished through modifications to the property deed or agreements about land use. Legal restrictions can be placed on the installation of groundwater extraction wells not only to prevent access to the contamination, but also to minimize the possibility of moving the contamination toward a future user. A recordation of the LUCs (including restriction to groundwater use) will accompany the transfer documentation from the U.S. Army to the USFWS. Deed restrictions would be needed only if the U.S. Army releases the property to a non-federal entity. These restrictions are effective only as long as the property owners and local authorities enforce them. The U.S. Army is ultimately responsible for the enforcement of the LUCs.

- **Effectiveness** Covenants/deed restrictions are effective, if enforced, in controlling human activities such as potable well construction. These actions can limit or prevent exposure to contaminants remaining on the site after remediation and can be implemented on a temporary basis. The 5-year reviews will ensure that the covenants/deed restrictions are enforced and remain effective.
- **Implementability** These options can be readily implemented.
- Cost Low.

Administrative Controls. Administrative controls consist of the use of training or procedures to limit access to the site and reduce the risk to human health posed by site contamination at LHAAP-29. These measures may include internal notices and site inspections to serve as a reminder of the existence of LUCs, a site approval process to review land-use changes at LHAAP-29 to ensure the LUCs are followed, training of site personnel regarding the existence and care of the LUCs, and regular inspection and maintenance of the LUCs. These are controls the U.S. Army can use while it maintains control of the site.

- **Effectiveness** Administrative controls are effective in controlling human intrusion into contaminated areas during and after remediation. The training required for access to the site limits potential exposure to the contaminated groundwater. Administrative controls can be used in conjunction with physical mechanisms and deed restrictions. This option is effective only while LUCs are maintained.
- **Implementability** Training and procedures are readily available and implemented. They may need to be modified for LHAAP.
- Cost Low.

Physical Mechanisms. Physical mechanisms include various engineered remedies to contain or reduce contamination and/or physical barriers intended to limit access to property, such as fences or signs. It is anticipated that covenants and administrative controls will be adequate to control access to the contaminated groundwater and physical mechanisms will not be required.

4.4.2.2.2 Monitoring

Monitoring and surveillance are used to assess the performance of remedial actions and verify compliance with the established RAOs. Process options for monitoring are physical surveillance and long-term media monitoring.

Physical Surveillance. Visual and physical inspections of engineered remedial action components can detect physical changes (e.g., iron deposition and pipeline cracks) that may ultimately lead to the failure or unsatisfactory performance of that component. Repairs and/or revised maintenance activities can be implemented as a result of these inspections.

- **Effectiveness** Physical surveillance is effective in determining the continued integrity of engineered systems and the need for repairs and/or replacement. Physical surveillance needs to be used with contaminant monitoring to assess the impact of integrity failure.
- **Implementability** Physical surveillance is easily implemented and requires experienced, but readily available personnel to make regular visits to the site for inspections.
- Cost Low.

Long-Term Media Monitoring. Environmental media (e.g., groundwater) can be monitored after the implementation of the remedial action to determine the effect the remedy has had on the level of contamination. Long-term media monitoring can detect a potential failure of the action to meet the RAOs. Monitoring can also be used to detect changes in expected site conditions or changes in the expected effectiveness of the remedy, and indicate whether additional actions should be implemented.

- **Effectiveness** Long-term media monitoring would be successful in evaluating the effectiveness of a remedial alternative. The effectiveness of the monitoring system depends on the design of the monitoring plan.
- Implementability Equipment and personnel are readily available. The site is readily accessible, and most monitoring techniques have already been implemented at LHAAP. Multiple groundwater-monitoring wells are already in place, and there is a reasonable baseline of groundwater conditions.
- Cost Moderate due to labor and analytical costs.

4.4.2.2.3 Summary of Land Use Controls Process Options

Covenants, administrative controls, physical surveillance, and long-term media monitoring are carried forward as representative process options for the LUCs GRA. Notification of industrial/recreational use will accompany all transfer documents and will be recorded in the Harrison County Courthouse. The covenants would only be used if the U.S. Army releases the land to a non-federal entity. All of these process options could be combined with other process options to meet the RAOs.

4.4.2.3 Removal

The removal GRA consists of technologies that remove groundwater to either relocate it or prepare it for treatment. The removal technology considered is groundwater collection/removal.

4.4.2.3.1 Groundwater Collection/Removal

Groundwater collection and removal is accomplished by either extraction wells, interception trenches, or horizontal wells.

Extraction Wells. These are vertically installed wells designed to collect and extract clean or contaminated groundwater to contain a plume or to reduce contaminant mass in the plume.

- **Effectiveness**—Extraction wells are considered the most effective groundwater removal technology applicable over a wide range of site conditions. However, proper locations need to be selected to provide for effective extraction and long-term operation.
- Implementability—This process is the single most commonly used method to remove groundwater in a very wide range of conditions. Some site predesign characterization may be needed to site new wells. Extraction wells are easy to install at all depths that might be required at LHAAP-29. Existing monitoring wells at LHAAP-29 could be converted to extraction wells.
- **Cost**—Low to moderate.

Interception Trenches. An interception trench is a high permeability subsurface trench that collects contaminated groundwater. It is constructed and operates very much like a vertical French drain with the exception that the collected groundwater is actively pumped from the trench for ex-situ treatment. The trench can be installed across the entire width of a shallow plume to more effectively capture contaminated groundwater.

- **Effectiveness**—Interception trenches are very effective at collecting groundwater. The trench functions like a continuous line of extraction wells. The trenches are also only applicable to shallow zone contamination.
- Implementability—Interception trenches are relatively easy to install with conventional construction equipment. The process requires long-term maintenance to

ensure that the permeable media and collection piping do not become clogged. Interception trenches are difficult to install at depths to intercept the intermediate flow zone.

• **Cost**—Moderate.

Horizontal Wells. Horizontal wells are similar to vertical wells with the exception that they are installed horizontally and are typically screened their entire length. They function like drains and offer a water removal capability that exceeds that of a similarly sized vertical well. Horizontal wells could be installed under source areas to remove contaminated groundwater or collect migrating leachate.

- **Effectiveness**—Horizontal wells are very effective at removing large volumes of contaminated groundwater in applications where vertical wells cannot be used. Wells up to 12 inches in diameter and 10–500 feet deep can be installed over 1,000-foot lengths. A single horizontal well is generally equivalent to five vertical wells in sandy soil and ten vertical wells in clayey soil.
- **Implementability**—Although this process is commonly used in the oil industry, it is still in the demonstration phase in environmental restoration. It would likely be used underneath a source area to collect contaminated groundwater or leachate.
- Cost—High.

4.4.2.3.2 Summary of Removal Process Options

Horizontal wells are not retained as a representative groundwater removal process option because of their limited use in environmental restoration actions and because of their high costs. Interception trenches are effective at removing groundwater though typically at a higher cost than extraction wells. Because extraction well systems are flexible, robust, and effective in a wide range of hydrogeologic conditions, the extraction well process option will be retained for remedial alternative development in this FS. This option may be used to extract the localized, highly contaminated groundwater from the intermediate zone. Interception trenches could be considered during the implementation of the remedial action, should the results of pre-design studies warrant their use.

4.4.2.4 In Situ Treatment

In situ treatment technologies provide varying levels of groundwater treatment without prior removal of the groundwater, and reduce the mobility or toxicity of the contaminants in groundwater. The in situ treatment technologies under consideration are physical/chemical and biological treatments.

4.4.2.4.1 Physical/Chemical Treatment

MNA, air sparging/soil vapor extraction, in situ oxidation, and permeable reactive barriers are process options considered potentially applicable to the groundwater at LHAAP-29.

Monitored Natural Attenuation. MNA is a remedial process option that will achieve the cleanup levels over time. Natural subsurface processes such as dilution, volatilization, biodegradation, adsorption, and chemical reactions with subsurface materials are monitored to confirm their progress in reducing contaminant concentrations. **Appendix C** provides an evaluation of the ongoing natural attenuation at LHAAP.

The VOCs and perchlorate are amenable to MNA.

- Effectiveness—MNA is considered under CERCLA on a case-by-case basis. USEPA guidance has been developed to aid in the selection of this process option for VOCs. MNA has been selected for a number of CERCLA sites. MNA is effective when source term releases have been mitigated, off-site releases of contaminants at unacceptable levels are not occurring, and it can be demonstrated that natural attenuation mechanisms are occurring. Regular monitoring must be conducted throughout the process to confirm that attenuation is occurring in accordance with cleanup objectives. The MNA evaluation for LHAAP-29 (see **Appendix C**) demonstrated that natural attenuation was occurring and is effectively controlling COCs in the shallow groundwater zone. Vinyl chloride, a common degradation product of TCE has been detected in the intermediate zone at well 29WW16 where the highest VOC concentrations have been detected indicating that natural attenuation is occurring. However, the high MC concentration at 29WW16 (7,110,000 µg/L) exceeds the tolerant range for microorganism activities and limits the effectiveness of the natural attenuation in the intermediate zone.
- **Implementability**—Significant groundwater sampling and analyses must be performed to confirm that conditions are suitable for natural attenuation and to establish a monitoring network. It must also be confirmed that additional source releases and unacceptable off-site releases are not occurring.
- **Cost**—Low to moderate.

Air Sparging/Soil Vapor Extraction. This process option is designed to remove VOCs from the groundwater by volatilizing these contaminants through the introduction of air. Air is introduced into the groundwater, assisting in the volatilization of those organics in solution in the groundwater. Extraction wells are installed into the vadose zone and a vacuum is drawn on these wells. The extraction system draws off the organic-laden air that was bubbled through the groundwater in addition to any vapors that exist in the soil pore spaces. The volatilized contaminants can then be drawn from these extraction wells and treated. This process can be used in those areas where VOCs exist in the groundwater and the vadose zone above this groundwater is relatively permeable.

- **Effectiveness**—This process is very effective on highly volatile contaminants (e.g., TCE) and highly permeable formations. It is incompatible with certain soil types, and high humic content inhibits volatilization of contaminants. Implementation at LHAAP-29 is complicated by high clay content soil that may limit the effectiveness of air sparging by retarding the movement of air and vapors through the soil column. The presence of discontinuous high-permeability zones can result in preferential air flow paths, limiting the effectiveness.
- Implementability—Vapor extraction and air sparge equipment is readily available and commercial vendors are available to design and operate these systems. This process has been used at many hazardous waste sites in relatively homogeneous media. Organics that are removed from the vapor extraction wells require ex situ treatment. Site characterization and modeling are required to determine the proper location of the injection and extraction wells and extraction rates.
- **Cost**—Low to moderate.

In Situ Oxidation. Contaminated media are treated through the addition of oxidizers, such as potassium permanganate, hydrogen peroxide or activated persulfate, which convert the contaminants to a less mobile or toxic form. This process option is applicable to VOCs such as MC and TCE. A treatability study was conducted at LHAAP-29 to evaluate the effectiveness of in situ chemical oxidation (see **Appendix B**) using activated sodium persulfate to treat the MC and concluded that combined heat and alkaline activated persulfate oxidation appeared to be the best treatment option.

- Effectiveness—In situ oxidation is effective on contaminants in a relatively homogeneous and porous medium. The approximately 17 to 45-foot clay to silty-clay layer between the shallow and the intermediate zones constitutes a barrier that will keep the passive reduction process of the shallow zone from being affected by the oxidative process occurring in the intermediate zone. Based on the treatability study (see Appendix B), combined heat (40°C) and alkaline persulfate oxidation appeared to the best treatment option of the MC in the intermediate zone; however, the long-term effectiveness is uncertain as a change in chemistry could mobilize or change the chemical behavior of the previously oxidized or reduced constituents. Chemical oxidation is most effective for VOCs (particularly TCE) and is considered a suitable approach for the primary COC at LHAAP-29, MC. Chemical oxidation is not effective for treatment of chlorinated alkanes such as 1,2-DCA.
- Implementability—This process option may be difficult to implement in situ because of concerns regarding delivery and sufficient exposure of the contaminants to the chemical agents. An additional concern is the release of excess reactants or byproducts to the environment. There have been limited applications of these processes, which are generally more readily implemented in the ex situ mode. A recent USEPA evaluation by their Technology Innovation Office concluded that the application of in situ oxidation is highly dependent upon the delivery system.
- **Cost**—Low to moderate.

Permeable Reactive Barriers. Permeable reactive barriers can be a physical/chemical or biological treatment option. A reactive barrier or gate is a permeable wall containing reactive media that is constructed across the path of a contaminant plume. As contaminated water passes through the wall, the contaminants are removed or degraded, allowing uncontaminated water to emerge on the downgradient side. Reactive barriers are usually installed through adaptation of conventional construction methods for impermeable barriers such as open trenches, polymer slurry trenches, and overlapping caissons. Reactive barriers may be constructed from a variety of materials including zero-valence metals (ZVM), granulated activated carbon (GAC), biological material, and other sorbents. These materials treat contaminants through a combination of mechanisms, including adsorption, chemical reduction, and biodegradation.

ZVM works by chemically reducing contaminants, thus either causing their degradation or limiting their mobility. A variety of metals can be used as reducing agents such as silver, gold, palladium, copper, zinc, aluminum, manganese, and iron. In situ reactive gates require high volumes of ZVM, making the application of precious metals such as silver, gold, and palladium impractical. The most practical metal for this technology is iron, because of its relative abundance, low cost, and low toxicity. However, more effective and more expensive forms of iron (palladized iron) may be necessary, depending on the contaminant.

GAC is the most widely used adsorbent and filter medium because of its effectiveness on a variety of contaminants. GAC is chemically stable and will not produce secondary contaminants. The surface area of the carbon and the pH of the solution flowing through the medium determine the rate and effectiveness of GAC in adsorbing contaminants. In addition, different contaminants are adsorbed according to different ionic natures and kinetics.

- **Effectiveness**—The effectiveness of this process depends greatly on the contaminants, the reactive media, site hydrology, and site geochemistry. Reactive media clogging and exhaustion causes the need for periodic replacement. The gates are generally limited to shallower applications because of the difficulties in installing and monitoring the media at depth. There are concerns over the longevity of the reactive media given uncertain and changing chemical and physical conditions.
- Implementability—Permeable reactive barriers require adequate site and contaminant characterization and monitoring to determine effectiveness. This process requires treatability testing before full-scale implementation to determine potential physical and chemical interactions with surrounding materials, location within the aquifer, and criteria for replacement. Long-term maintenance requirements may be significant.
- **Cost**—Moderate.

4.4.2.4.2 Biological Treatment

Biological treatment process options use living organisms such as bacteria or fungi to detoxify or immobilize contaminants in waste. These process options are primarily used to convert organic contaminants into nontoxic products.

Enhanced Bioremediation. This general process option covers a wide range of individual biological process options that rely on microbial transformation of organic contaminants under aerobic or anaerobic conditions into benign forms to obtain energy or carbon. Excessively high concentrations of contaminants could be toxic to microbes. Many organic contaminants, including some of the COCs at LHAAP-29, can be biodegraded under anaerobic (without oxygen) conditions. The activity of microorganisms is greatly affected by pH, redox potential, temperature, oxygen content, and most importantly, nutrient availability. These conditions can be manipulated to achieve optimal conditions for microbial activity, accelerating the biodegradation of the target contaminants. The conditions are manipulated through the addition of nutrients or electron acceptors or donors.

- Effectiveness—In situ biodegradation is effective in either low oxygen conditions or high oxygen and methane conditions in a permeable media that enhances the continuing delivery of nutrients to the bacteria. The primary challenge for in situ biological treatment is to effectively introduce the bacteria and nutrients to the affected areas and ensure adequate mixing and contact. The rate of destruction is typically slower than other competing processes, but fewer and less toxic byproducts result. The vast amount of chloride ions that would be produced through enhanced bioremediation would likely reduce the effectiveness of biodegradation.
- **Implementability**—Enhancing the biological activity may be difficult in some of the low permeability soil at LHAAP-29 because of complications associated with the delivery of nutrients and oxygen. Equipment and expertise are readily available, but significant treatability testing would be required.
- Cost—Low to moderate.

4.4.2.4.3 Summary of In Situ Treatment Process Options

There are numerous in situ groundwater treatment process options available. In the shallow zone, a significant reduction in perchlorate, explosives and VOC concentrations detected during the various rounds of groundwater monitoring indicates that natural attenuation is effectively occurring. However, that is not currently the case for the intermediate groundwater zone at LHAAP-29 primarily due to the high MC concentration at well location 29WW16. Therefore, MNA alone is not expected to be effective in the intermediate zone. MNA is retained as a remediation option in the shallow zone and for further consideration for the post-treatment period in the intermediate zone. The effectiveness of the air sparging/soil vapor extraction and permeable reactive barrier process options for treatment of LHAAP-29 groundwater may be limited by site geology or hydraulic conditions, contaminant characteristics, or the degree of

required long-term maintenance. In situ chemical oxidation is considered a fast and efficient process with respect to the COCs in LHAAP-29 groundwater and a treatability study performed for the groundwater at the site identified this option as a viable alternative and in situ oxidation will, therefore, be retained for remedial alternative development. Although enhanced bioremediation will not be retained for remedial alternative development due to the excessive MC concentrations which could ultimately be toxic to the microbes introduced through the bioremediation process; this option may be considered an alternative to chemical oxidation once MC concentrations are reduced.

4.4.2.5 Ex Situ Treatment

Ex situ treatment technologies provide varying levels of water treatment following extraction or collection of the water. These technologies are applied to reduce the volume, mobility, or toxicity of recovered groundwater. Although ex situ treatment technologies considered are physical/chemical, thermal, and biological, they have been grouped into two process options under an on-site treatment technology – the existing treatment system and a new mobile or skid-mounted system near the extraction point.

4.4.2.5.1 New Treatment Plant

A small, skid-mounted or mobile treatment plant could be built near the point of groundwater extraction. The treatment system would be designed for removal of the COCs from the extracted groundwater. GAC or air stripping could remove the COCs. The new treatment plant may require a pretreatment system (e.g., precipitation) if iron and other interfering metals are present in the groundwater.

- **Effectiveness**—All of the considered technologies are proven effective and are even used at an existing treatment plant at LHAAP. Smaller units have less operational flexibility and may expect deviations more often. However, this option would be effective.
- **Implementability**—The implementation of this option is more difficult than that of the existing treatment plant. A few studies would be needed to design the plant to meet the site conditions. This option is still reasonably easy to implement.
- **Cost**—Moderate. The capital costs of this option are considerably greater than that of the existing plant. However, there is a potential that the operational costs could be minimized.

4.4.2.5.2 Burning Ground No. 3 Groundwater Treatment Plant

This facility, which is currently processing contaminated groundwater from other LHAAP sites (LHAAP-18/24 and LHAAP-16), includes unit operations such as neutralization, precipitation, and air stripping. The effluent from the plant is discharged to Harrison Bayou.

- **Effectiveness**—The existing plant is currently treating groundwater. The hydraulic capacity of the plant has not been met yet, so additional flow could be effectively handled. The discharge requirements are routinely met, indicating an effective operation.
- Implementability—The existing plant is already operational. It is operating below current design capacity. Depending on the composition of the site water sent to the plant, it is possible that no revisions to the plant would be necessary. However, LHAAP-29 is located approximately 1.5 miles from the existing plant and that distance makes the implementability of direct pumping to the plant impractical. A series of on-site holding tanks would be required.
- **Cost**—Frequent transport of the contaminated groundwater from on-site holding tanks to the plant makes this option cost moderate to high in comparison to other alternatives.

4.4.2.5.3 Summary of Ex Situ Treatment Process Options

The utilization of the existing LHAAP groundwater treatment plant will be retained for remedial alternative development. It is already effectively operational, and the capital costs for construction of the plant have already been spent. Currently, groundwater from other LHAAP sites provides the majority of the water that is treated by the plant. Because of its proven effectiveness and lower costs, the current treatment system is used to develop alternatives.

4.4.2.6 Summary of Representative Groundwater Process Options

Figure 4-4 is presented to illustrate the process options that have been selected for remedial alternative development. The following representative GRAs, technologies or process options are retained.

- No action
- LUCs
- Groundwater extraction and follow-up in situ chemical oxidation in the intermediate groundwater zone
- Groundwater extraction and ex situ treatment
- MNA (shallow groundwater zone and intermediate groundwater zone after in situ or ex situ treatment)

Development of the remedial alternatives is included in **Section 5.0**.

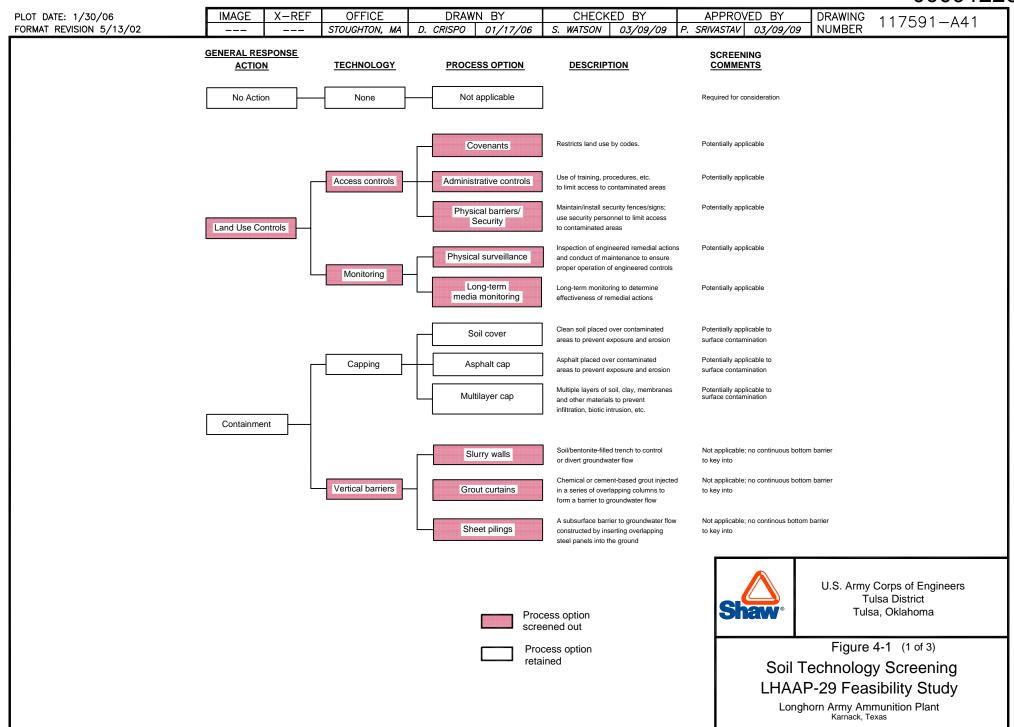
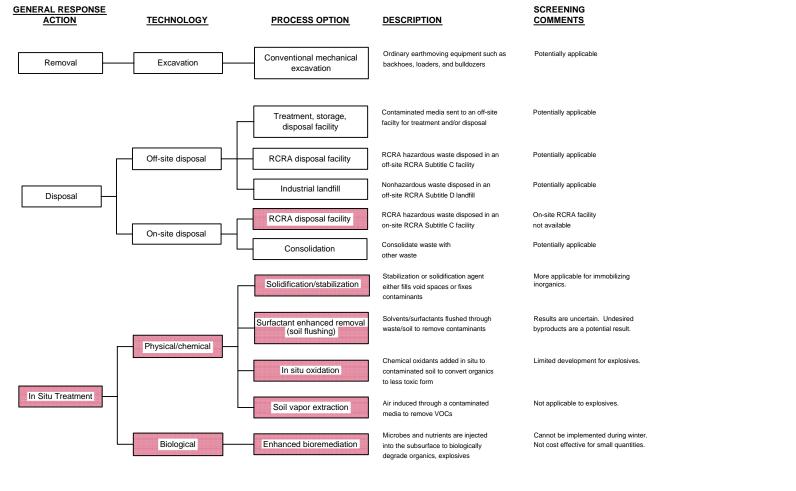


IMAGE X-REF **OFFICE** DRAWN BY CHECKED BY APPROVED BY **DRAWING** PLOT DATE: 10/16/08 117591-A34 NUMBER FORMAT REVISION 5/13/02 R. DUFFIELD 10/16/08 P. SRIVASTAV 03/09/09 STOUGHTON, MA D. CRISPO 01/17/06





Process option retained

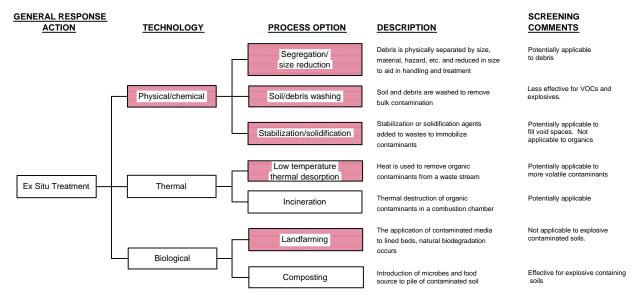


U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

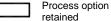
Figure 4-1 (2 of 3)

Soil Technology Screening LHAAP-29 Feasibility Study

IMAGE X-REF OFFICE DRAWN BY CHECKED BY APPROVED BY **DRAWING** PLOT DATE: 10/16/08 117591-A35 NUMBER FORMAT REVISION 5/13/02 R. DUFFIELD 10/16/09 P. SRIVASTAV 03/09/09 STOUGHTON, MA D. CRISPO 01/17/06







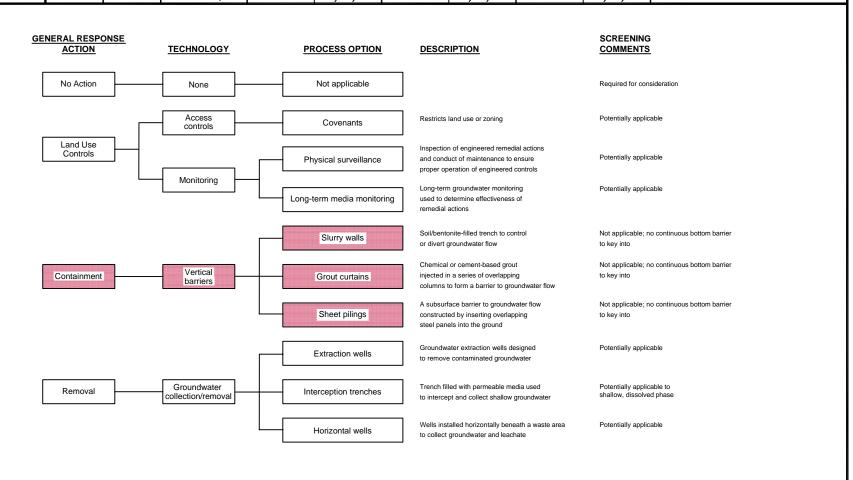


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Figure 4-1 (3 of 3)

Soil Technology Screening LHAAP-29 Feasibility Study

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retained



U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

Figure 4-2 (1 of 2)

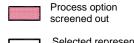
Groundwater Technology Screening LHAAP-29 Feasibility Study

Karnack, Texas

IMAGE X-REF OFFICE DRAWN BY CHECKED BY APPROVED BY PLOT DATE: 10/16/08 DRAWING 117591-A37 FORMAT REVISION 5/13/02 NUMBER STOUGHTON, MA D.CRISPO 01/17/06 R. DUFFIELD | 10/16/09 P. SRIVASTAV 03/09/09 **GENERAL RESPONSE** SCREENING **TECHNOLOGY** PROCESS OPTION DESCRIPTION COMMENTS ACTION Potentially applicable to dissolved phase The monitored degradation of Monitored natural contaminants through natural biological attenuation and chemical processes Air injected into saturated matrices to remove Potentially applicable to Air sparging dissolved VOCs contaminants through volatilization Chemical oxidants or reducers added Potentially applicable Physical/ In situ oxidation/ in situ to convert organics to less chemical reduction toxic form Injection of chemicals that cause Not applicable to VOCs Precipitation contaminants to precipitate in place A trench filled with a reactive or sorbent Potentially applicable to both In Situ Permeable reactive barrier material designed to treat groundwater dissolved VOCs and perchlorate Treatment as it passes through the trench Microbes and nutrients are injected Potentially applicable to both Enhanced into the subsurface to biologically VOCs and perchlorate bioremediation degrade organics Biological Plants are used to remove, transfer, Takes too long and contaminated Phytoremediation stabilize, or destroy contaminants groundwater is too deep Mobile or skid-mounted system Potentially applicable New treatment plant near extraction point On-site Ex Situ treatment Treatment Treatment processes at existing water Potentially applicable Burning Ground No. 3 treatment plant are precipitation, Groundwater Treatment Plant air stripping, and fluidized bed reactor On-site Discharge of treated groundwater to Potentially applicable Disposal Surface water discharge disposal surface water after treatment U.S. Army Corps of Engineers Tulsa District Process option Tulsa, Oklahoma screened out Process option Figure 4-2 (2 of 2) retained **Groundwater Technology Screening** LHAAP-29 Feasibility Study Longhorn Army Ammunition Plant

PLOT DATE: 1/30/06 FORMAT REVISION 5/13/02 IMAGE X-REF OFFICE DRAWN BY CHECKED BY APPROVED BY DRAWING 117591-A40 NUMBER STOUGHTON, MA 01/17/06 03/09/09 P. SRIVASTAV 03/09/09 D. CRISPO S. WATSON

GENERAL RESPONSE ACTION	TECHNOLOGY	PROCESS OPTION	EFFECTIVENESS	<u>IMPLEMENTABILITY</u>	COST
No Action	- None -	Not applicable	Does not achieve RAOs.	Not acceptable to USEPA	None
Land Use Controls	Access controls	Covenants	Effective as long as property owners and local authorities enforce them. Does not reduce contamination and is not effective to protect groundwater or ecological receptor.	Readily implemented but has legal and authority requirements	Low cost to document land use restrictions
		Administrative controls	Effective as long as LUCs are implemented. Does not reduce contamination and is not effective to protect groundwater or ecological receptor.	Training and procedurs are available and readily implemented.	Low cost to implement training and routine inspection and maintenance of LUCs.
		Physical barriers/ Security	Effective as long as physical mechanisms are maintained. Does not reduce contamination and is not effective to protect groundwater or ecological receptor.	Readily implemented. Fencing and signs are commercially available items.	Low cost to install fences and signage.
		Physical surveillance	Effective but needs to be used with contaminant monitoring to assess impact of integrity failure. Does not reduce contamination and is not effective to protect groundwater or ecological receptor.	Readily implemented but requires experienced persons to make routine inspections.	Low cost to implement; however, depends on frequency of inspections.
	Monitoring	Long-term media monitoring	Effectiveness depends on the design of the monitoring plan. Does not reduce contamination and is not effective to protect groundwater or ecological receptor.	Readily implemented. The site is accessible and groundwater monitoring wells exist onsite.	Moderate costs due to labor and analytica costs.
Containment	Capping	Soil cover	Effective, susceptible to cracking, but has self healing properties. Requires maintenance and long-term monitoring	Easily implemented. Restrictions on future land use in capped areas.	Medium capital, low maintenance.
		Asphalt cap	Effective but susceptible to weathering and cracking. Requires maintenance and long-term monitoring.	Easily implemented. Restrictions on future land use in capped areas.	Medium capital, high maintenance.
		Multilayer cap	Effective, least susceptible to cracking.	Moderate implementability. Restrictions on future land use in capped areas.	High capital, high maintenance.
Removal	Excavation	Conventional mechanical	Effective for permanent removal of contaminants. Removed solids require treatment or disposal.	Easily implemented. Conventional soil removal equipment is widely available.	Medium capital, no maintenance.
		excavation		Squipmont to mady artifaction	



Selected representative process option



U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

Figure 4-3 (1 of 2) Selection of Representative Soil Process Options LHAAP-29 Feasibility Study Longhorn Army Ammunition Plant Karnack, Texas

IMAGE X-REF OFFICE DRAWN BY CHECKED BY APPROVED BY PLOT DATE: 10/16/08 **DRAWING** 117591-A38 NUMBER FORMAT REVISION 5/13/02 R. DUFFIELD 10/16/08 P. SRIVASTAV 03/09/09 STOUGHTON, MA D. CRISPO 01/17/06 **GENERAL RESPONSE EFFECTIVENESS IMPLEMENTABILITY ACTION TECHNOLOGY** PROCESS OPTION COST Effective at treating and disposing of treated wastes Easily implemented. Numerous facilities Medium capital, no maintenance. Treatment, storage exist that treat similar site waste. in a permitted, off-site dispoal facility. disposal facility Effective at isolating wastes from the environment Moderate implementability if the waste criteria Medium capital, no maintenance. Off-site disposal RCRA disposal facility due to engineering design requirements. can be met. Requires frequent waste sampling. Effective at isolating low hazard wastes from the environment Easily implemented if waste criteria is below Medium capital, no maintenance. Industrial landfill Disposal due to waste restrictions. acceptable levels for landfill disposal. Effective for low hazard waste only. Difficult to implement due to regulatory and Low cost, high maintenance. On-site disposal Consolidation public reluctance to dispose waste at LHAAP. Readily implemented; however, offgas High capital, no maintenance. Effective for permanent destruction of VOCs and Incineration Ex Situ Treatment Thermal may require additional treatment. Public explosives. may have concerns with emissions. U.S. Army Corps of Engineers Process option **Tulsa District** screened out Tulsa, Oklahoma Selected representative process option

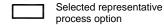
Figure 4-3 (2 of 2) Selection of Representative Soil Process Options LHAAP-29 Feasibility Study

PLOT DATE: 1/30/06 FORMAT REVISION 5/13/02

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GENERAL RESPONSE ACTION	TECHNOLOGY	PROCESS OPTION	<u>EFFECTIVENESS</u>	<u>IMPLEMENTABILITY</u>	COST
No Action	None	Not applicable	Does not achieve RAOs.	Not acceptable to USEPA	None
Natural Attenuation	Natural attenuation	Monitored natural attenuation	Effective when sources have been mitigated and a determination that MNA is occurring.	Requires significant groundwater sampling. No significant detection of degradation products (cis-1,2-DCE or vinyl chloride).	Moderate cost due to sample requirements.
	Access controls	Covenants	Effective as long as propery owners and local authorities enforce them. Does not reduce contamination.	Readily implemented but has legal and authority requirements	Low cost to document land use restrictions
Land Use Controls		Physical surveillance	Effective but needs to be used with contaminant monitoring to assess impact of integrity failure.	Readily implemented but requires experienced to make routine inspections.	Low cost to implement; however, depends on frequency of inspections.
	Monitoring	Long-term media monitoring	Effectiveness depends on the design of the monitoring plan.	Readily implemented. The site is accessible and groundwater monitoring wells exist onsite.	Moderate costs due to labor and analytica cost
	Г	Extraction wells	Considered most effective groundwater removal method.	Easily implemented. Extraction wells are easy to install and existing wells are easily modified.	Low to moderate capital.
Removal	Groundwater collection/removal	Interception trenches	Effective at collecting groundwater in shallow groundwater zone.	Difficult to implement. May be difficult to install and requires long-term maintenance.	Medium capital, high maintenance.
	L	Horizontal wells	Effective at removing large volumes of contaminmated groundwater.	Medium difficulty to implement but this method is still in the demonstration phase in environmental restoration.	High capital, high maintenance.





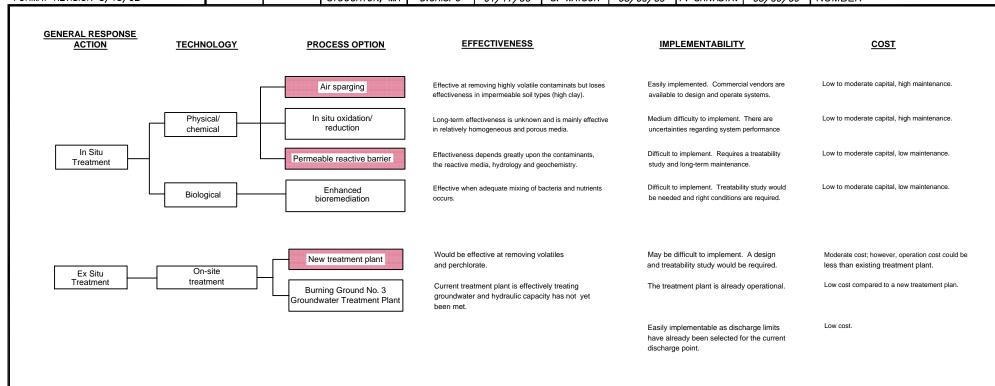


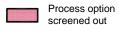
U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

Figure 4-4 (1 of 2)

Selection of Representative Groundwater Process Options LHAAP-29 Feasibility Study Longhorn Army Ammunition Plant Karnack, Texas

PLOT DATE: 10/16/08 FORMAT REVISION 5/13/02 **IMAGE** X-REF OFFICE DRAWN BY CHECKED BY APPROVED BY DRAWING 117591-A39 NUMBER P. SRIVASTAV STOUGHTON, MA D.CRISPO 01/17/06 S. WATSON 03/09/09 03/09/09





Process option retained



U.S. Army Corps of Engineers Tulsa District Tulsa, Oklahoma

Figure 4-4 (2 of 2)

Selection of Representative Groundwater Process Options LHAAP-29 Feasibility Study

5.0 Development and Description of Alternatives

Section 5.1 presents the development of a range of alternatives based on the key assumptions regarding site and contaminant conditions (**Section 2.0**), the RAOs and applicable ARARs (**Section 3.0**), and the representative process options (**Section 4.0**). **Section 5.2** presents the detailed description of the alternatives.

5.1 Development of Alternatives

5.1.1 Requirements and Preferences

The CERCLA process, as defined in the NCP, develops a remedy that protects human health and the environment, complies with ARARs (unless a statutory waiver is justified and granted), is cost-effective, and uses permanent solutions and alternative treatment or resource recovery technologies to the maximum extent practicable. A statutory preference for remedies that would result in permanent and significant decreases in toxicity, mobility, or volume through treatment and provide long-term protection is stated in Section 121 of CERCLA, as amended.

The NCP defines the following preferences in developing remedial action alternatives:

- Use of treatment to address the "principal threats" posed by a site, wherever practical.
- Use of engineering controls, such as containment, for waste that poses a relatively low, long-term threat and for which treatment is not practical.
- Implementation of a combination of actions, as appropriate, to achieve protection of human health and the environment. For example, in appropriate site situations, treatment of principal threats would be combined with engineering controls, such as containment, and LUCs for treatment residuals and untreated waste.
- Use of LUCs, such as drinking water supply controls and covenants, to supplement engineering controls for short- and long-term management to prevent or limit exposures to hazardous substances.
- Selection of an innovative technology when the technology offers the following: the potential for comparable or better treatment performance or implementability, fewer or lesser magnitude adverse impacts than other technologies, or lower costs than demonstrated technologies for similar levels of performance.
- Usable groundwater is expected to be returned to beneficial uses, whenever
 practicable, within a time frame that is reasonable given the particular circumstances
 of the site. When such restoration is not practicable, the prevention of further
 migration of the plume and of exposure to the contaminated groundwater are expected.

These statutory requirements and preferences were given due consideration in the development of alternatives for LHAAP-29.

5.1.2 Development using Remediation Strategies and Process Options

The media at LHAAP-29 presenting an unacceptable risk or hazard are groundwater, soil at isolated areas, sediment in the outfall ditch, and solid residue in the cooling water lines and manholes. Thus, the purpose of the remedial alternatives is to present the decision maker with technical and economic options for remediation of soil, sediment, residual contamination in pipe lines, and groundwater at LHAAP-29. Although all of the action alternatives have been designated to achieve the RAOs and the statutory requirements under CERCLA, each alternative must also be sufficiently unique in its strategy and approach that the range of alternatives represents a reasonable spectrum of final site conditions in the view of the decision makers.

The process options that remain after screening were grouped and combined into alternatives to meet the RAOs as indicated on **Table 5-1**.

A number of process options are common to both action alternatives (Alternatives 2 and 3):

- Long-term LUCs to restrict groundwater use are common to all action alternatives. The proposed groundwater remedy for each of the action alternatives necessitates that groundwater LUCs be maintained until cleanup levels are achieved. The LUCs include access controls and monitoring as discussed in **Section 4.4.2.2**.
- The process option for the shallow groundwater is MNA. MNA was evaluated (**Appendix C**) and is a viable option.
- The process option selected for the residual contamination in the lines and manholes is to plug the inlets and outlets. This will minimize contact from hypothetical future maintenance workers and prevent water from infiltrating and transporting contaminants.

5.2 Description of Remedial Alternatives

The following sections describe the remedial alternatives in more detail (see **Table 5-1** for a presentation of the components of each alternative). The details included in the alternative descriptions (e.g., quantities and dimensions) support the evaluation in **Section 6.0** and the cost estimate in **Appendix A**. Quantities and dimensions are provided for cost estimating purposes only and may be changed based on the design. Designs and process options other than those considered here may be substituted once the decision on remedial approach is made.

5.2.1 Alternative 1 - No Action Alternative

As required by the NCP, the "no action" alternative provides a comparative baseline against which the action alternatives can be evaluated. Under this alternative the source units

(contaminated soil, sediment, and residual contamination in pipe lines) and groundwater would be left "as is," without implementing any additional containment, removal, treatment, or other mitigating actions. No other actions would be implemented to reduce existing or potential future exposure to human and ecological receptors.

5.2.2 Alternative 2 – Excavation and Off-site Disposal for Soil; Plug Lines; Extraction, In Situ Chemical Oxidation and MNA for Intermediate Zone Groundwater; MNA and LUCs for Shallow Zone Groundwater

The goals of this alternative are to prevent exposure of the hypothetical future maintenance worker to contaminated soil and groundwater and ecological receptors to surface soil/sediment at LHAAP-29. Soil and sediment that have the potential to pose risk to the human or ecological receptor or impact groundwater or surface water will be removed. To eliminate future impact to on-site surface water and groundwater, the TNT wastewater lines and the cooling water lines will be plugged and abandoned in place. The shallow zone and intermediate zone groundwater have contaminants above MCLs or GW-Ind that will be reduced over time to meet the cleanup levels.

Under this scenario, the highest concentration area in the MC plume in the intermediate groundwater zone will be treated. In situ chemical oxidation treatment is proposed. Extraction will be implemented as part of the in situ treatment to physically remove mass and to control the hydraulic gradient. After in situ treatment, natural attenuation will be monitored and evaluated to confirm that contaminant concentrations are being reduced to cleanup levels over time. LUCs would be maintained until the groundwater is returned to beneficial use.

5.2.2.1 Removal of Soil above Cleanup Levels

The recommended removal action consists of excavation of the nitrotoluene and perchlorate-contaminated soil and off-site disposal at a RCRA Subtitle D-permitted landfill. Excavation of the contaminated soil and disposal in a RCRA-permitted landfill will result in the following: 1) removal of contaminated soil that is a potential source of cross-contamination to groundwater, thereby ensuring that groundwater can ultimately be returned to its beneficial uses; 2) removal of soil that is posing risk to ecological receptors; and 3) removal of soil that is a direct risk to the hypothetical future maintenance worker, thereby protecting human health by preventing inhalation, ingestion, and dermal contact with the COCs. The estimated volume of soil to be removed is approximately 3,900 cubic yards and is based on the cleanup levels in **Table 3-4** and the receptor. The excavation locations are highlighted on **Figure 2-1**. The removal of soil contamination will be verified by collecting confirmation samples from the walls and floors of the excavation area and submitting them for laboratory analysis for the COCs of interest. Clean borrow soil will be used as needed to backfill the excavations so they can be graded for proper drainage.

With the removal of the contaminated surface soil and sediment at LHAAP-29, plugging of the former TNT wastewater and cooling water lines and abandoning the manholes associated with the cooling water lines, health and ecological risks as well as the potential migration of soil to surface water and groundwater will be eliminated and long-term operations for soil will not be required.

5.2.2.2 Plug and Abandon Lines

The transite TNT wastewater line will be flushed with water to remove visual residue. The rinsate water will be containerized. Appropriate rinsate handling procedures will be followed based on its waste classification. The inlets and outlets of the transite TNT wastewater line will be plugged with a bentonite slurry mix or equivalent.

The cooling water lines showed no significant contamination except for 2,4-DNT in the solid residue in manholes 8 and 10. The cooling water lines will be inspected to determine if there is contaminated solid residue in the lines adjacent to manholes 8 and 10. An attempt will be made to sample and analyze the residue and water in the cooling water lines as part of the RD phase. If there is not enough residue volume to sample or the concentrations in the sample are less than the GW-Ind (water) or GWP-Ind (solid) and the residue is nonhazardous, the pipe will be plugged and abandoned. No solid residue or liquid will be left in the pipe if the explosive constituents exceed the GWP-Ind (residue), the GW-Ind (water) or the solid or liquid is determined to be hazardous (residue or water). If explosive concentrations are above the GWP-Ind (residue) or GW-Ind (water) or the material is found to be hazardous, the line will be flushed before plugging and abandoning. The rinsate will be characterized for waste handling. The manholes will then be plugged with a bentonite slurry mix or equivalent.

5.2.2.3 In Situ Chemical Oxidation for Intermediate Zone VOC Groundwater Plume

In situ chemical oxidation in groundwater is a technology that oxidizes most organic constituents in the saturated zone to carbon dioxide and mineral products. The proposed oxidant is activated persulfate. The persulfate ion $(S_2O_8^{-2})$ is a strong oxidant that reacts with organic compounds primarily by the sulfate anion radical. The persulfate reagent is very soluble in water to concentrations of 30 to 40 percent and the solutions are relatively stable at concentrations as low as 1 to 10 percent. These properties allow for optimum delivery and distribution to the subsurface matrix without being limited by solubility of the oxidant. Persulfate activation by adjusting the pH to alkaline conditions and/or applying heat is effective for chlorinated methanes, such as MC, the primary COC in the groundwater intermediate zone at LHAAP-29. A treatability study was conducted at LHAAP-29 to evaluate the effectiveness of in situ chemical oxidation using activated sodium persulfate to treat the MC and concluded that combined heat and alkaline activated persulfate oxidation appeared to be the best treatment option (**Appendix B**).

In general, the components of the in situ chemical oxidation action include:

- **Installation of injection wells.** Four intermediate zone injection wells (88 feet bgs) will be installed around existing intermediate monitoring well 29WW16, where MC was detected at the highest concentration. The four wells will be arranged in a square with well 29WW16 in the center of the square. The new wells will be spaced approximately 50 feet apart, creating a treatment zone with an aerial coverage of 2,500 square feet. The spacing may be adjusted based on actual field conditions.
- **Injection of oxidation solution.** One pore volume of heat activated (40°C) combined persulfate and sodium hydroxide solution at 60 grams per liter (g/L) and 15 g/L, respectively, will be injected into four wells while simultaneously extracting groundwater from well 29WW16. Temporary piping will be used for the injection array. Based on the estimated volume of the treatment zone (50' × 50' × 40') and a porosity of 25 percent, a total of 25,000 cubic feet (187,000 gallons) of activated persulfate and sodium hydroxide solution will be injected into the subsurface. An estimated 94,000 pounds of persulfate reagent and 23,500 pounds of sodium hydroxide will be injected into the subsurface. A second round of injection may be required if monitoring indicates COCs are not being effectively reduced from the initial round. For costing purposes, it is assumed a second round will be required. If contaminant concentrations do not decrease as anticipated, the method will be modified.
- **Simultaneous extraction of groundwater.** Well 29WW16 will be converted to an extraction well. Prior to conversion, a pump test will be conducted and hydrogeologic parameters will be measured to assess aquifer conditions. Groundwater flow in the vicinity of 29WW16 and the injection wells will be modeled to determine the scope of the modifications needed at 29WW16 and to assess the time required to extract one pore volume.

A temporary piping system will be used to convey the extracted water to three 5,000-gallon on-site storage tanks. The on-site tanks will be interconnected and will be equipped with a high level shut off to the extraction pump. Once every two days, water will be pumped into a tank truck and transported to the LHAAP groundwater treatment plant for treatment and discharge. A 20-foot by 50-foot gravel pad will be prepared for the tanks, and a 6-inch layer of gravel would be placed to upgrade the road to the tanks. The estimated quantities are for costing purposes only and will be revised during the design.

• Monitor effectiveness. To monitor the effectiveness of the in situ chemical oxidation, six wells will be monitored biweekly for three sampling events. The six wells will include one new monitoring well, four injection wells, and 29WW16. The effect of the first chemical injection should be evident within a few weeks. It is anticipated that a second injection will be needed after approximately 2 months. Following in situ treatment, groundwater monitoring will be implemented for well 29WW16 and three additional wells to demonstrate continued reductions through MNA.

Based on the Treatability Study (included in **Appendix B**), the MC concentrations will be reduced by approximately 75% through heat-activated persulfate application. MNA will be initiated after the formation has recovered from the oxidation treatment activities.

5.2.2.4 Monitored Natural Attenuation

In both the shallow and intermediate groundwater zones, MNA will be used to complete the remediation. MNA will reduce contaminant levels to MCL/GW-Ind concentrations and return these zones to beneficial uses.

The MNA evaluation in **Appendix C** has shown that MNA has been effective in the shallow zone in reducing contaminant concentrations. Based on the findings of that evaluation, the time necessary to return the shallow aquifer is driven by 1,2-DCA, which may require approximately 70 years.

A monitoring program will be developed as part of the remedial design phase and will define the MNA expectations. The objectives of the monitoring program will include the demonstration that MNA is occurring, verification that there has been no unacceptable impact to downgradient receptors, verification that the plume is not expanding, and verification of the attainment of RAOs. The sampling program design will be based on the current plume, seasonal variations, groundwater direction, and velocity. MNA monitoring will be conducted for eight quarters. The MNA samples will be collected for VOC and MNA parameter analysis. An MNA report will be prepared to document the effectiveness of MNA in each groundwater zone. If MNA performance is adequate, performance monitoring will continue semi-annually for the next 3 years, then annually until the next 5-year review. The sampling frequency may then be changed to once every 5 years if the data suggest less frequent sampling is appropriate. For costing purposes, a 30-year monitoring program is assumed. Sampling frequency, reporting frequency, or analytical suite may be modified based on the results of the sampling program. Additional monitoring is recommended once every five years after reduction of the COCs and demonstration of MNA effectiveness to support 5-year reviews until cleanup levels are met.

The MNA evaluation in **Appendix C** has also shown that MNA in the intermediate zone will not be effective in reducing the high MC concentrations in the vicinity of 29WW16. However, in this alternative, MNA will be implemented following chemical oxidation, which will have reduced the MC concentrations to levels that are amenable to remediation by MNA. However, the introduction of the chemical oxidant may result in conditions in the intermediate groundwater zone that are not optimal for biological degradation, which is a significant mechanism of natural attenuation. Therefore, it may be necessary to inject a carbon source and specialized microorganisms into the intermediate zone to enhance biological degradation of the remaining chlorinated organics. Aquifer conditions will be evaluated following the injection to determine if

this is necessary. If required, the carbon source and microorganisms would be injected via the four wells installed for the oxidant injection.

An evaluation of the site-wide extent of arsenic, mercury and nickel will be made during remedial design. During subsequent monitoring events, it is expected that groundwater will be tested for metals, including arsenic, mercury and nickel, to monitor cleanup levels, and potential mobilization of metals due to changed subsurface conditions during remediation.

5.2.2.5 Land Use Controls

Land use controls will be maintained until the proposed cleanup levels are achieved in both the shallow and intermediate zones. The LUCs will consist of a restriction on groundwater use at LHAAP-29. If at some time in the future property ownership is transferred from a federal agency to the private sector, a deed restriction for the use of groundwater will be developed. The U.S. Army will record a notice of LUCs with Harrison County and will include the notice with any transfer letter to the USFWS for the intended future use as a national wildlife refuge.

5.2.3 Alternative 3 – Excavation and Off-site Disposal for Soil; Plug Lines; and Extraction, MNA, and LUCs for Groundwater

The goals of this alternative are to prevent exposure of the hypothetical future maintenance worker to contaminated soil and groundwater and ecological receptors to surface soil/sediment at LHAAP-29. Soil and sediment that have the potential to impact groundwater will be removed. To eliminate future impact to on-site surface water and groundwater, the TNT transite wastewater lines and the cooling water lines will be plugged and abandoned in place. The shallow zone groundwater have contaminants above MCLs or GW-Ind that will be reduced over time via MNA to meet the cleanup levels. This alternative uses groundwater extraction followed by MNA to return the groundwater in the intermediate zone to the cleanup levels. The extracted groundwater would be piped to a series of on-site storage tanks, and then pumped to trucks and transported to the existing LHAAP groundwater treatment plant for treatment and discharge.

5.2.3.1 Removal of Soil above Cleanup Levels

As in Alternative 2, the recommended removal action consists of excavation of the nitrotoluene and perchlorate-contaminated soil and off-site disposal at a RCRA Subtitle D-permitted landfill. Excavation of the contaminated soil and disposal in a RCRA-permitted landfill will result in the following: 1) removal of contaminated soil that is a potential source of cross-contamination to groundwater, thereby ensuring that groundwater can ultimately be returned to its beneficial uses; 2) ecological receptors, thereby protecting the deer mouse and shrew; and 3) removal of soil that is a direct risk to the hypothetical future maintenance worker, thereby protecting human health by preventing inhalation, ingestion, and dermal contact with the COCs. The estimated volume of soil to be removed is approximately 3,900 cubic yards and is based on the cleanup levels in **Table 3-4** and the receptor. The excavation locations are highlighted on **Figure 2-1**. The

removal of soil contamination will be verified by collecting confirmation samples from the walls and floors of the excavation area and submitting them for laboratory analysis for the COCs of interest. Clean borrow soil will be used as needed to backfill the excavations so they can be graded for proper drainage.

With the removal of the contaminated surface soil and sediment at LHAAP-29, plugging of the former TNT wastewater and cooling water lines and abandoning the manholes associated with the cooling water lines, health and ecological risks as well as the potential migration of soil to surface water and groundwater will be eliminated and long-term operations for soil will not be required.

5.2.3.2 Plug and Abandon

The transite TNT wastewater line will be flushed with water to remove visual residue. The rinsate water will be containerized. Appropriate rinsate handling procedures will be followed based on its waste classification. The inlets and outlets of the transite TNT wastewater line will be plugged with a bentonite slurry mix or equivalent.

The cooling water lines showed no significant contamination except for 2,4-DNT in the solid residue in manholes 8 and 10. The cooling water lines will be inspected to determine if there is contaminated solid residue in the lines adjacent to manholes 8 and 10. An attempt will be made to sample and analyze the residue and water in the cooling water lines as part of the RD phase. If there is not enough residue volume to sample or the concentrations in the sample are less than the GW-Ind (water) or GWP-Ind (solid) and the residue is nonhazardous, the pipe will be plugged and abandoned. No solid residue or liquid will be left in the pipe if the explosive constituents exceed the GWP-Ind (residue), the GW-Ind (water) or the solid or liquid is determined to be hazardous (residue or water). If explosive concentrations are above the GWP-Ind (residue) or GW-Ind (water) or the material is found to be hazardous, the line will be flushed before plugging and abandoning. The rinsate will be characterized for waste handling. The manholes will then be plugged with a bentonite slurry mix or equivalent.

5.2.3.3 Groundwater Extraction and Treatment for Intermediate Groundwater Zone

The groundwater remediation component of this alternative involves the extraction of VOC-contaminated groundwater by means of recovery wells, temporary storage in on-site ASTs, pumping of the stored water into trucks to be transported for treatment at the existing LHAAP water treatment plant. The purpose of this "pump and treat" system is to reduce VOC concentrations in the intermediate zone groundwater to levels that can subsequently be reduced through natural attenuation (typically levels in the 1,000s of $\mu g/L$). The anticipated duration of extraction is 3 years.

This action will begin with a pre-design study. A pump test will be conducted and hydrogeologic parameters will be measured to better design the system. Groundwater flow will be modeled to set performance evaluation parameters and to assess the likely time required for remediation.

Groundwater contamination in the intermediate zone at LHAAP-29 primarily consists of a MC plume. A minimum of five additional wells (four extraction and one monitoring) are proposed to be installed in the intermediate zone within the region of greatest MC contamination in order to provide a more effective extraction process. Several groundwater monitoring wells are located throughout the site and some of these could also be converted to extract contaminated groundwater if needed.

A piping system will be constructed to transport the extracted water from five extraction wells (four new wells and 29WW16) to three 5,000-gallon storage tanks to be located on-site at LHAAP-29. The tanks will be interconnected and will be equipped with a high level shut off to the pump. Once every two days, the water will be pumped out to a tank truck and transported to the existing groundwater treatment plant for treatment and discharge. A 20-foot by 50-foot gravel pad will be prepared for the tanks plus a 6-inch layer of gravel will be placed to upgrade the road to the tanks. This will require approximately 19,000 tons of base stone at LHAAP-29. The alternative will also require the installation of approximately 2,350 feet of 2-inch high-density polyethylene piping for pumping the water to the tanks. The piping will be installed at approximately three feet bgs to prevent disturbance. These estimates are for costing purposes only and will be revised during the design.

During extraction, samples will be collected from the five extraction wells plus the new monitoring well to monitor the effectiveness of the action. During startup of the extraction system (until the system is operating properly), bimonthly sampling will be conducted. Startup is estimated to be approximately six months. After startup, monitoring will be reduced to quarterly for the remaining 2.5 years.

Water Treatment. The extracted groundwater from LHAAP-29 will be treated at the LHAAP groundwater treatment plant, which was originally built to treat groundwater containing VOCs and metals extracted from other LHAAP sites. The plant uses air stripping, carbon adsorption, and thermal oxidation. Perchlorate treatment using a fluidized bed reactor was added in April 2001 to the treatment plant. Figure 5-1 shows a simplified flow diagram of the primary treatment components in the existing plant. The extracted water from LHAAP-29 would be discharged from the tank truck into the existing 300,000-gallon equalization tank. This tank receives water from other LHAAP sites and is stored in this tank until treatment. After the water is treated, the effluent would be discharged in accordance with plant procedures. The plant presently operates at a fraction of its maximum capacity of 1 to 1.5 million gallons of water per

month. The original groundwater treatment plant components have adequate capacity to accommodate the increase in volume that will be introduced to the system when the contaminated groundwater is transported from LHAAP-29 to the plant.

Extraction System. Operation and maintenance will include groundwater extraction system maintenance, groundwater treatment plant operations, and environmental media monitoring. In three years, the extraction wells are anticipated to remove the highest concentrations of VOCs from the groundwater intermediate zone at LHAAP-29, thus reducing the contaminant mass to make conditions favorable for MNA (estimate assumes 3 years). For MNA, four wells will be selected for use as monitoring wells, and monitoring will be implemented to demonstrate that any remaining VOCs are attenuated by natural processes (see Section 5.2.3.4). During the groundwater extraction operations, the extraction wells will require regular maintenance to prevent fouling of well screens, and the extraction pumps will require routine maintenance and may also require replacement. Cleaning of the pipelines, refurbishing pumps and other maintenance activities will be needed on the groundwater collection and transport system during full-scale operation. O&M costs will include the addition of chemicals, power, and labor; equipment cleaning, tank cleaning, general system maintenance, and replacement; and regulatory monitoring and reporting. O&M activities will also be conducted at the LHAAP plant location as part of the routine plant O&M activities.

5.2.3.4 Monitored Natural Attenuation

In both the shallow and intermediate groundwater zones, MNA will be utilized to complete the remediation. MNA will reduce contaminant levels to MCL or GW-Ind concentrations and return these zones to beneficial uses.

The MNA evaluation in **Appendix C** has shown that MNA can be effective in the shallow zone. Based on the findings of that evaluation, the time necessary to return the shallow aquifer is driven by 1,2-DCA, which may require approximately 70 years.

The MNA evaluation in **Appendix C** has also shown that MNA in the intermediate zone will not be effective in handling the high MC concentrations in the vicinity of 29WW16. However, in this alternative, MNA will be implemented following three years of groundwater extraction, which will have reduced the MC concentrations to levels that are amenable to remediation by MNA.

A monitoring program will be developed as part of the remedial design phase and will define the MNA expectations. The objectives of the monitoring program will include the demonstration that MNA is occurring, verification that there has been no unacceptable impact to downgradient receptors, verification that the plume is not expanding, and verification of the attainment of

RAOs. The sampling program design will be based on the current plume, seasonal variations, groundwater direction, and velocity.

MNA quarterly monitoring will be conducted for eight quarters. For the estimate, 12 existing wells and 1 new well will be selected for MNA in the shallow groundwater zone. Four wells will be selected in the intermediate groundwater zone. The MNA samples will be collected for VOC and MNA parameter analysis. An MNA report will be prepared to document the effectiveness of MNA in each groundwater zone. If MNA performance is adequate, performance monitoring will continue semi-annually for the next 3 years, then annually until the next 5-year review. The sampling frequency may then be changed to once every 5 years if the data suggest less frequent sampling is appropriate. For costing purposes, a 30-year monitoring program is assumed. Sampling frequency, reporting frequency, or analytical suite may be modified based on the results of the sampling program. CERCLA 5-year reviews will be performed at LHAAP-29 as required until ARARs are achieved.

An evaluation of the site-wide extent of arsenic, mercury and nickel will be made during remedial design. During subsequent monitoring events, it is expected that groundwater will be tested for metals, including arsenic, mercury and nickel, to monitor cleanup levels, and potential mobilization of metals due to changed subsurface conditions during remediation.

5.2.3.5 Land Use Controls

Land use controls will be maintained until the proposed cleanup levels are achieved in both the shallow and intermediate zones. The LUCs will consist of a restriction on groundwater use at LHAAP-29. If at some time in the future property ownership is transferred from a federal agency to the private sector, a deed restriction for the use of groundwater will be developed. The U.S. Army will record a notice of LUCs with Harrison County and will include the notice with any transfer letter to the USFWS for the intended future use as a national refuge.

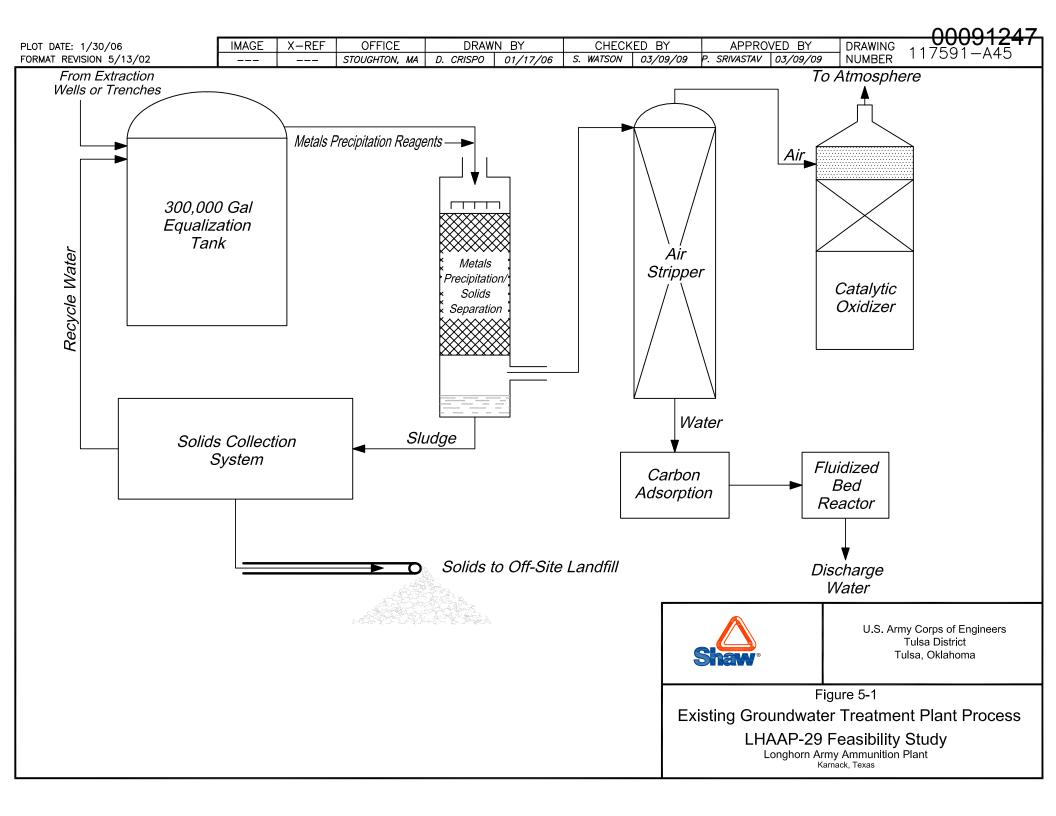
Shaw Environmental, Inc.

Table 5-1
Alternative Development

Contaminated Media	Process Option	Selected for Alternative Grouping		
		1 (No Action)	2	3
SOLIDS				
Soil / Sediment	Excavate media above cleanup levels, off-site disposal.	_	Yes	Yes
Residue in TNT Waste Water and Cooling Water Pipe Lines	Plug inlets and outlets including manholes.	_	Yes	Yes
GROUNDWATER				
Shallow Zone	Monitored Natural Attenuation (MNA) and LUCs until goals achieved.	_	Yes	Yes
Intermediate Zone	In situ treatment, MNA, LUCs until goals achieved.	_	Yes	_
	Ex-situ treatment, MNA, LUCs until goals achieved	_	_	Yes

Abbreviations:

TNT trinitrotoluene LUCs land use controls



6.0 Detailed Analysis of Alternatives

6.1 Introduction

This section presents and assesses relevant information that provides the basis for selecting an alternative. **Section 6.2** provides an overview of the evaluation criteria. The detailed analysis begins with an individual analysis in **Section 6.3** in which each alternative is individually evaluated according to the evaluation criteria identified in the NCP (40 CFR 300.430). Following the individual analyses, the alternatives are compared in relation to the two threshold criteria and then the alternatives are assessed regarding the five balancing criteria, highlighting the key advantages, disadvantages, and trade-offs that are considered as part of the evaluation process.

6.2 Overview of the Evaluation Criteria

CERCLA, Section 121, as amended, specifies statutory requirements for remedial actions. These requirements include protection of human health and the environment, compliance with ARARs, a preference for permanent solutions that incorporate treatment as a principal element to the maximum extent practicable, and cost-effectiveness. To assess whether alternatives meet the requirements, the USEPA has identified nine criteria in the NCP (40 CFR 300.430) that must be evaluated for each alternative considered for selection (Section 300.430[e][9][iii]). Provided here are summaries of the nine criteria and an overview of the approach taken by this FS to evaluate each alternative with regard to these criteria.

6.2.1 Criterion 1: Overall Protection of Human Health and the Environment

This evaluation criterion assesses whether the alternative achieves and maintains adequate protection of human health and the environment in accordance with the RAOs established in **Section 3.0**. Because the scope of this criterion is broad, it also reflects the discussions of the subsequent criteria, including long-term effectiveness and permanence, and short-term effectiveness. Evaluation of this criterion describes how site risks associated with each pathway are eliminated, reduced, or mitigated through treatment, engineering, or LUCs. This criterion also considers whether an alternative poses an unacceptable short-term or cross-media affect.

6.2.2 Criterion 2: Compliance with ARARs

This criterion addresses compliance with promulgated federal and state environmental requirements. The detailed analysis summarizes which requirements are applicable or relevant and appropriate to an alternative and how the alternative meets these requirements. If an alternative cannot meet a requirement, a determination can be made that a waiver under CERCLA may be appropriate, and a basis for justifying the waiver is presented. ARARs consist

of two sets of requirements – those that apply and those that are relevant and appropriate. In certain cases, standards may not exist that address the proposed action or the COCs. In such cases, nonpromulgated advisories, criteria, or guidance developed by the USEPA or other federal agencies or states can be TBCs. There are three types of ARARs; chemical-specific, location-specific, and action-specific. The chemical-, location- and action-specific ARARs are presented in **Section 3.2**.

6.2.3 Criterion 3: Long-Term Effectiveness and Permanence

This criterion evaluates the extent to which an alternative achieves an overall reduction in risk to human health and the environment after the RAOs are met. The criterion considers the degree to which the alternative provides sufficient long-term controls and reliability to prevent exposures that exceed protective levels for human and environmental receptors. The principal factors addressed by this criterion include magnitude of residual risk and the adequacy and reliability of controls to address such risk. This criterion also addresses the uncertainties associated with these factors.

The evaluation of adequacy and reliability of controls assesses the effectiveness of any treatment, containment, or institutional measures that are part of the alternative. Factors considered include performance characteristics, maintenance requirements, and expected durability. Information and data from past performance and similar technology applications are incorporated appropriately into the evaluation. LUCs are considered where they have the potential to improve the effectiveness of engineered measures.

6.2.4 Criterion 4: Reduction of Toxicity, Mobility, or Volume through Treatment

This criterion reflects the statutory preference that remedial alternatives contain a principal component that substantially reduces toxicity, mobility, or volume of hazardous substances through treatment. The evaluation regarding this criterion considers the extent to which alternative technologies can effectively and permanently fix, transform, immobilize, or reduce the volume of waste materials and contaminated media.

6.2.5 Criterion 5: Short-Term Effectiveness

This criterion addresses the effects of the construction and implementation phases of the alternative until the RAOs are achieved. The evaluation regarding this criterion considers the effect on human health and the environment posed by operations conducted during the remedial action phases. Both the potential effect and associated mitigative measures are examined for maintaining protectiveness for the community, remediation workers, and environmental receptors throughout the duration of remedial activities.

Potential short-term risks to the public include inhalation of constituents that may be released during waste removal and treatment operations, and contaminant exposure and physical injury

during waste transport off site. Potential short-term risks to workers include direct contact and exposure during construction, waste handling, and transportation; physical injury or death during construction and transportation activities; and nonremediation worker exposures to airborne contaminants during waste and soil removal operations. Alternative analyses also include a description of mitigating measures such as engineering and LUCs that are expected to minimize potential risks to the public and workers. This evaluation also addresses the anticipated duration of remedial activities.

6.2.6 Criterion 6: Implementability

This criterion examines the technical and administrative factors affecting implementation of an alternative and considers the availability of services and materials required during implementation. Technical factors to be assessed include the ease and reliability of construction and operations, the prospects for implementing a future action, and the adequacy of monitoring systems to detect failures. Administrative factors include permitting and coordination requirements between the lead agency and regulatory agencies. Service and material considerations include TSD capacities, equipment and operator availability, and prospective technology applicability or development requirements.

The assessment of technical feasibility examines the performance history of the technologies in direct applications or considers the expected performance for similar applications. Uncertainties associated with construction, operation, and performance monitoring are also addressed.

The evaluation of administrative feasibility includes a discussion of those actions required to coordinate with regulatory agencies to establish the framework for complying with key substantive technical requirements that must be met by an alternative. Additionally, those alternatives that include off-site transportation of waste are reviewed to assess the feasibility of off-site disposal.

The availability of services and materials is addressed by analyzing the material components of the proposed technologies to determine the locations and quantities of those materials, and by reviewing process operations to identify special services, operator skills, or training required to readily implement the process.

The NCP requires that the evaluation of the relative administrative feasibility of each alternative include "...activities needed to coordinate with other offices and agencies, and the ability and time required to obtain any necessary approvals and permits from other agencies (for off-site actions). CERCLA, Section 121(e), stipulates that no deferral, state, or local permit shall be required for the portion of any removal or remedial action conducted entirely on site." An action must satisfy the substantive requirements of the permits that will otherwise be required.

6.2.7 Criterion 7: Cost

Cost estimates are included for each remedial alternative. The estimates are based on feasibility level scoping and are intended to aid in making project evaluations and comparisons among alternatives. The estimates have an expected accuracy of +50 to -30 percent for the scope of the action described in **Section 5.0** for each alternative. The estimates are divided into capital cost and O&M cost and are developed according to an assumed schedule for the various activities based on similar project experience.

Capital costs are defined as those expenditures required to initiate and install an alternative. These are short-term costs and are exclusive of costs required to maintain the action throughout the project lifetime. Capital costs consist of direct and indirect costs. Direct costs include construction costs (material, labor, and equipment to install an action), service equipment, process and new process buildings, utilities, and waste disposal costs. Indirect costs include design engineering, inspection, project integration, project administration and management, and project contingencies.

O&M costs are long-term costs associated with ongoing remediation at a site. These costs occur after construction and installation are completed. The costs include labor, materials, utilities, and services required to monitor, operate, and maintain the facilities for a period of up to 30 years.

The estimated present worth of each remedial alternative is determined on a discount rate of 2.8 percent and a base O&M and monitoring period of up to 30 years, unless the alternative evaluated is expected to be complete in less than 30 years.

Appendix E presents detailed cost estimates and the major assumptions used to develop the cost estimates for each remedial alternative.

6.2.8 Criterion 8: State Acceptance

State acceptance of an alternative will be evaluated in the PP issued for public comment. Therefore, this criterion is not considered in this FS.

6.2.9 Criterion 9: Community Acceptance

Community acceptance of each alternative will be evaluated after a PP is issued for public comment. Therefore, this criterion is not considered in this FS.

6.3 Individual Analysis of Alternatives

6.3.1 Alternative 1 - No Action Alternative

Under the "no action" alternative, no further action will be taken at LHAAP-29 to control human exposure to contaminated groundwater or to monitor potential groundwater impacts to surface water. The contaminated waste and cooling water lines, soil, sediment and groundwater will

remain in place without the implementation of any contaminant removal, treatment, or containment. The LUCs to prevent groundwater access at the site will not be established or will be discontinued. No environmental monitoring will occur. It is assumed that the public and ecological receptors could access the waste. This alternative provides a baseline for comparison purposes.

6.3.1.1 Overall Protection of Human Health and the Environment

The "no action" alternative does not achieve the RAOs for LHAAP-29. This alternative provides no control of exposure to the contaminated waste and cooling water lines, soil, sediment, and groundwater and no reduction in the risks to human and ecological receptors for current and future land use scenarios. Risks to receptors will exceed the USEPA-established threshold for acceptable incremental lifetime cancer risk of 1×10^{-4} for carcinogens or an HI of 1 for noncarcinogens. The greatest risk will come from ingestion of groundwater although risk from exposure to surface soil is possible. The contaminants causing the greatest amount of risk are VOCs in the intermediate groundwater zone and perchlorate and explosive compounds in the shallow groundwater zone. The EEQ is greater than 1 for the deer mouse and short-tailed shrew. Explosive compounds in the soil are located at isolated areas of the site and pose a human health and ecological hazard. Additionally, the residual material in the TNT waste and cooling water lines have the potential to migrate to surface water and groundwater since the lines remain open to the environment.

6.3.1.2 Compliance with ARARs

CERCLA, Section 121, cleanup standards, including compliance with ARARs, apply only to actions the USEPA determines should be taken under CERCLA, Sections 104 and 106 authority. A "no action" decision will be made when no action is deemed necessary to reduce, control, or mitigate exposure because the site does not present a threat to human health and the environment, or because any action taken will worsen the negative effects on human health and the environment. Because no remedial activities are associated with this alternative, compliance with chemical-specific ARARs will not be met. Since no remedial activities will be conducted, action-specific and location-specific ARARs will not apply.

6.3.1.3 Long-Term Effectiveness and Permanence

6.3.1.3.1 Magnitude of Residual Risk

The "no action" alternative will not provide an effective or permanent long-term solution. Soil exposure routes generated an HI of 1.3 for the hypothetical future maintenance worker and an unacceptable EEQ for ecological receptors. The residual risk and toxicity from groundwater exposure under a "no action" alternative will be unacceptable at LHAAP-29. For the hypothetical future maintenance worker, groundwater exposure routes account for over 99 percent of the overall carcinogenic and non-carcinogenic risks, generating a carcinogenic risk of

 3.9×10^{-1} and an HI of 3,000. These risks were conservatively calculated for a hypothetical future maintenance worker ingesting the groundwater. Currently, the groundwater at LHAAP-29 is not used for drinking water, and is not anticipated to be used for drinking water under a national wildlife refuge future use scenario.

6.3.1.3.2 Adequacy and Reliability of Controls

The "no action" alternative will not establish or maintain any LUCs at LHAAP-29 and, therefore, will not reduce the existing site risks.

6.3.1.4 Reduction of Toxicity, Mobility, or Volume through Treatment

Implementation of the "no action" alternative will not reduce toxicity, mobility, or volume of contaminants because this alternative does not employ treatment.

6.3.1.5 Short-Term Effectiveness

Under the "no action" alternative, no remedial action will be taken; therefore, the short-term effectiveness criterion is not applicable to this alternative. The "no action" alternative will not cause any added short-term risks to remediation workers, the community or the environment.

6.3.1.6 Implementability

This alternative is inherently implementable because no remedial action will be taken.

6.3.1.7 Cost

There are no costs associated with the "no action" alternative.

6.3.2 Alternative 2 – Excavation and Off-site Disposal for Soil; Plug Lines; In Situ Chemical Oxidation for Intermediate Zone Groundwater; MNA and LUCs

This alternative consists of the following major components:

- Soil and sediment excavation
- Plugging and abandonment of the former TNT transite wastewater and cooling water lines and cooling water line manholes
- In situ chemical oxidation to address the area of greatest contamination in the intermediate zone groundwater plume
- MNA for the remaining contamination in the intermediate groundwater zone
- MNA for COCs in the shallow groundwater zone
- Long-term LUCs to restrict use of groundwater until proposed cleanup levels are met

6.3.2.1 Overall Protection of Human Health and the Environment

6.3.2.1.1 Protection of Human Health

The actions proposed for this alternative will:

- 1. Prevent exposure to residual wastes in the pipe lines, manholes, soil, and sediment that exceed cleanup levels
- 2. Prevent potential transport of contaminated soil, contaminated sediment, and residual wastes in the pipe lines
- 3. Prevent leaching of contaminants from the soil or the pipe lines into the groundwater at concentrations that exceed cleanup levels
- 4. Directly treat high concentrations of VOCs in the intermediate groundwater zone
- 5. Ultimately return both the intermediate and shallow groundwater zones to cleanup levels
- 6. Prevent inappropriate groundwater usage via LUCs

Therefore, the residual site risk upon completion of these actions will be within the target risk range for the hypothetical future maintenance worker. This alternative is protective of human health and the environment and achieves the RAOs for LHAAP-29.

The field activities planned under this alternative will have some short-term risks requiring the significant reliance on engineering controls to minimize the risk. Exposure to risks that occur during excavation of contaminated soil and sediment and plugging of underground lines will be controlled through the implementation of a health and safety plan in compliance with 29 CFR 1910.120. The plan will establish safe work procedures and appropriate PPE.

6.3.2.1.2 Protection of the Environment

The removal of soil and sediment that exceeds cleanup levels at LHAAP-29 will reduce the risk to ecological receptors from contaminated soil. In the short-term, risks will occur when soils and sediment are removed and staged. Engineering controls will be important to control direct exposure and runoff potential during the field work.

6.3.2.2 Compliance with ARARs

6.3.2.2.1 Chemical-Specific ARARs

This alternative will comply with the chemical-specific ARARs for surface soils and sediment at LHAAP-29. Soil and sediment excavation will remove material that causes exceedances of the target cancer risk range and the non-cancer HI for the hypothetical future maintenance worker in these media. The removal of the source soils and sediment and plugging of the former TNT wastewater and cooling water lines will positively impact groundwater by eliminating the

potential for the leaching of contaminants into groundwater at concentrations exceeding cleanup levels. The remediation of the elevated MC concentrations in the intermediate groundwater zone will target the bulk of the contaminant mass, provide an efficient remedy to arrest potential vertical and horizontal plume migration, and reduce risks of exposure to groundwater that exceeds chemical-specific ARARs.

6.3.2.2.2 Location-Specific ARARs

The activities that will be conducted under this alternative would comply with all location-specific ARARs. No activities would take place in sensitive environments such as wetlands, and no impacts to archeological resources or threatened and endangered species are anticipated.

6.3.2.2.3 Action-Specific ARARs

The activities that will be conducted under this alternative will comply with all action-specific ARARs. Soil remediation will occur in compliance with all transportation and disposal requirements. Runoff controls will be important during soil/sediment excavation. All runoff requirements will be met to protect Goose Prairie Creek and Central Creek.

6.3.2.3 Long-Term Effectiveness and Permanence

6.3.2.3.1 Magnitude of Residual Risks

Upon completion of source removal, the residual site risk will be within the target risk range and below an HI of 1 for the hypothetical future maintenance worker and within risk range for the ecological receptor. The implementation of LUCs under this alternative would prevent direct contact by human receptors with contaminated groundwater at LHAAP-29, thus minimizing the potential risk posed by groundwater contamination.

6.3.2.3.2 Adequacy and Reliability of Controls

The soil exposure risk at LHAAP-29 for a hypothetical future maintenance worker or ecological receptor would be removed by excavating the isolated contaminated soil and sediment areas and plugging the former TNT wastewater and cooling water lines and manholes.

Treatment of high concentrations of VOCs in the intermediate groundwater zone through in situ treatment will be effective for reducing COC concentrations to levels that can be addressed via natural attenuation. In situ treatment includes concurrent groundwater extraction. The extracted water will be treated at the existing LHAAP groundwater treatment plant. That plant has been operating successfully for several years. There are significant issues associated with the effectiveness of groundwater extraction. If hydraulic conductivity in the aquifer is too low, the volumetric flow rate of groundwater to the well will be low and will decrease the effectiveness of extraction. A small capture zone may require excessive time to capture the contamination. There are more pump maintenance issues associated with low flow conditions. If the extraction well goes dry, it causes the pump to overheat and fail to operate.

The layer of clay to silty clay between the shallow and intermediate groundwater zones will provide a barrier that will keep the passive reductive process within the shallow zone from being affected by the chemical oxidation process proposed for the intermediate zone. In addition, the properties of persulfate, the proposed chemical oxidant, allow for optimum delivery and distribution to the subsurface matrix without being limited by solubility as is the case with other oxidants.

MNA will be implemented for groundwater in both the shallow zone and the intermediate zone. In the intermediate zone, it will be initiated after the in situ treatment phase. The MNA evaluation (**Appendix C**) has demonstrated that natural attenuation can be effective in the shallow zone. Effectiveness of natural attenuation in the intermediate zone will depend on successful completion of the in situ treatment. In both zones, long-term success will be verified by monitoring the progress of natural attenuation.

Long-term LUCs for groundwater will prevent exposure to the remaining COCs in both the shallow and intermediate groundwater zones until proposed cleanup levels are met. The reliability of LUCs would depend on the maintenance of the controls. It is not anticipated that groundwater cleanup levels in the shallow zone will be met in the near future.

Consistent with the required 5-year CERCLA review, compliance with the risk-reduction goals will be monitored and performance of the controls will be assessed. The 5-year reviews may indicate the need for components of this alternative to be repaired, modified, or replaced.

6.3.2.4 Reduction of Toxicity, Mobility, or Volume through Treatment

In two ways, this alternative satisfies the USEPA statutory preference for remedial actions that permanently reduce contaminant toxicity, mobility and volume and utilize treatment as a principle element. In the intermediate groundwater zone of LHAAP-29, in situ chemical oxidation will reduce the toxicity and volume of the major contaminants. In both the shallow and intermediate groundwater zones, MNA will reduce the toxicity and volume through natural biological and chemical processes.

6.3.2.5 Short-Term Effectiveness

6.3.2.5.1 Protection of the Community during Remedial Action

This alternative is protective of the surrounding community during remedy implementation primarily because all activities would occur on site with very little disturbance of contaminated material. Truck traffic for equipment and materials, including the shipment of contaminated soil off site for disposal and on-site delivery of borrow material (for backfilling), and chemical oxidant (for in situ treatment) will occur. If a spill of contaminated soils occurs, the spill would be easy to contain and would not impact the surrounding communities. During remediation

activities at LHAAP-29, control of surface runoff will be important to avoid releases of contamination to adjacent surface water bodies.

6.3.2.5.2 Protection of Workers during Remedial Action

Some short-term risks to human health or the environment will exist during implementation of this alternative. The soil excavation activity has the potential for transportation or construction accidents. Additionally, this alternative will involve potential short-term risks to workers associated with the operation of drilling equipment and potential exposure to decontamination fluids, chemical oxidant, contaminated groundwater, and excavated soil. Other risks to workers include those generally associated with construction activities (e.g., slips, trips, and falls).

The implementation of proper engineering controls and safety equipment will minimize potential short-term risks to remediation personnel conducting the installation of the groundwater extraction system and groundwater sampling activities. Measures will be taken to prevent the contact of personnel with the extracted groundwater. Remediation workers will conform to the site health and safety program and will be equipped with the necessary PPE. A site-specific health and safety plan will be prepared prior to implementing this alternative.

6.3.2.5.3 Short-Term Environmental Effects

Minor clearing and grubbing at LHAAP-29 will be required to effectively excavate the soil and sediment and install monitoring wells or injection points for in situ chemical oxidation of groundwater. However, since these areas have been cleared in the past, it is unlikely that there are any sensitive species that will be impacted. If any sensitive areas are found, the appropriate regulation will be followed. The implementation of proper engineering controls will minimize the risk of environmental impacts.

6.3.2.5.4 Duration of Remedial Activities

In six months, in situ treatment is expected to remove the highest concentrations of VOCs in the intermediate zone, thus reducing the contaminant mass to concentrations that can be readily addressed by natural attenuation. At that point, the injection wells will begin to be used as monitoring wells, and monitoring will be implemented to demonstrate that any remaining VOCs are attenuated by natural processes. Perchlorate, VOCs, and explosive compounds detected in the shallow zone are expected to continue to attenuate by natural processes. After the initial eight quarters of MNA performance monitoring in each zone, natural attenuation monitoring will be semiannually for three years, then annually until the next CERCLA 5-year review.

Long-term monitoring, consisting of LUCs surveillance and groundwater monitoring will be implemented every five years thereafter. Until cleanup levels are met, monitoring will be needed to determine trends in groundwater contamination levels and effectiveness of the remedial action. The monitoring time may increase or decrease depending on the effectiveness of the

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treatment method. The amount of time needed to achieve cleanup levels in groundwater will depend on the effectiveness of the natural attenuation. The natural attenuation evaluation (**Appendix C**) estimates that it will take approximately 70 years (due to 1,2-DCA) for complete attenuation to cleanup levels for the shallow zone.

6.3.2.6 Implementability

6.3.2.6.1 Technical Feasibility

The limited amount of soil and sediment excavation is easy to implement once the area requiring excavation is defined and cleared. Plugging and abandonment of the TNT transite wastewater and cooling water lines and the cooling water line manholes can be conducted without extensive intrusive activities. Considering the small quantity of soil with reasonably low levels of contamination requiring disposal, a disposal location will be available. All equipment, services and materials are readily available to conduct the activities for this alternative, and the LHAAP groundwater treatment plant is already operational.

Minimal technical concerns exist that will hinder the implementation of the in situ chemical oxidation. The equipment and materials required for oxidant source delivery are commercially available, but specialized knowledge of in situ chemical oxidation treatment will be required for implementation. This methodology may be difficult to implement in situ because of concerns regarding delivery and sufficient exposure of the contaminants to the chemical agents. An additional typical concern is the release of excess reactants or byproducts to the environment. Low groundwater yield could decrease the effectiveness of the associated extraction.

6.3.2.6.2 Administrative Feasibility

All actions under this alternative would be implemented on the site and thus do not require permits, though substantive provisions of permits that would otherwise be required are considered to be ARARs. By legal agreement (i.e., the FFA), the U.S. Army shall submit to the USEPA and TCEQ a Responsiveness Summary and ROD. Following consideration of any comments by TCEQ, the ROD will be finalized jointly by the U.S. Army and USEPA, or if they are unable to reach agreement about the selection of the remedial action, by the USEPA administrator. By addressing the identified ARARs in the ROD and subsequent documents, it is anticipated that the alternative would adequately address all administrative barriers.

LUCs, although administratively implementable, would require the development of an implementation plan as part of the remedial design, and internal notices to relevant regulatory offices of the existence of the LUCs. Approval by the USEPA and the State of Texas is required prior to the modification or termination of LUCs, implementation actions, or modification of land-use by the U.S. Army. The U.S. Army must also seek concurrence from the USEPA and the State of Texas prior to any action that may disrupt the effectiveness of the LUCs or any action that may alter or negate the need for LUCs.

6.3.2.7 Cost

The total project present worth cost of Alternative 2 is approximately \$3.0 million. The details and a comparison of the cost estimates for all of the alternatives are presented in **Appendix E**.

6.3.2.7.1 Capital Cost

The total capital cost is estimated at approximately \$2.1 million. The direct capital cost includes mobilization of construction activities; excavation of soil material; plugging of underground lines; filling of manholes associated with the cooling water lines; installation and operation of the in situ chemical oxidation system (including the associated groundwater extraction); transportation and disposal of excavated soils; demobilization of construction activities and the activities associated with LUCs. Capital costs also include a work plan, regulatory and remedial design documents and a closure report.

6.3.2.7.2 O&M Cost

The total O&M cost is estimated at approximately \$919,000. This cost includes monitoring for MNA in the shallow and intermediate zones, monitoring to support required CERCLA 5-year reviews, and LUC surveillance to verify groundwater is not used.

6.3.3 Alternative 3 – Excavation and Off-site Disposal for Soil; Plug Lines; Groundwater Extraction for Intermediate Zone; MNA and LUCs

This alternative consists of the following major components:

- Soil and sediment excavation;
- Plugging and abandonment of the former TNT transite wastewater and cooling water lines and the cooling water line manholes;
- Extraction, treatment, and disposal of highly contaminated groundwater from in the intermediate zone
- MNA for the remaining contamination in the intermediate groundwater zone
- MNA for COCs in the shallow groundwater zone
- Long-term LUCs to restrict use of the groundwater until the proposed cleanup levels are met

6.3.3.1 Overall Protection of Human Health and the Environment

6.3.3.1.1 Protection of Human Health

The actions proposed for this alternative will:

1. Prevent exposure to residual wastes in the pipe lines, manholes, soil, and sediment that exceed cleanup levels

- 2. Prevent potential transport of contaminated soil, contaminated sediment, and residual wastes in the pipe lines
- 3. Prevent leaching of contaminants from the soil or the pipe lines into the groundwater at concentrations that exceed cleanup levels
- 4. Extract, treat, and dispose highly contaminated groundwater from the intermediate groundwater zone
- 5. Ultimately return both the intermediate and shallow groundwater zones to cleanup levels
- 6. Prevent inappropriate groundwater usage via LUCs

Therefore, the residual site risk upon completion of these actions would be within the target risk range for the hypothetical future maintenance worker. This alternative is protective of human health and the environment and achieves the RAOs for LHAAP-29.

The field activities planned under this alternative will have some short-term risks requiring significant reliance on engineering controls to minimize the risk. Exposure to risks that occur during excavation of contaminated soil and sediment and plugging of the underground lines will be controlled through the implementation of a health and safety plan in compliance with 29 CFR 1910.120. The plan will establish safe work procedures and appropriate PPE.

6.3.3.1.2 Protection of the Environment

The removal of soil and sediment that exceed cleanup levels at LHAAP-29 will reduce the risk to ecological receptors from contaminated soil. In the short-term, risks will occur when the soil and sediment are removed and staged. Engineering controls will be important to control direct exposure and runoff potential during the field work.

6.3.3.2 Compliance with ARARs

6.3.3.2.1 Chemical-Specific ARARs

This alternative would comply with the chemical-specific ARARs for surface soils and sediment at LHAAP-29. Soil and sediment excavation will remove material that causes exceedance of the target cancer risk range and the non-cancer HI for the hypothetical future maintenance worker in these media. The removal of the source soils and sediment and plugging of the underground TNT wastewater and cooling water lines will positively impact groundwater by eliminating the potential for leaching of contaminants into soils and ultimately to groundwater at concentrations exceeding cleanup levels. Groundwater remediation under this alternative will ultimately achieve cleanup levels in both the shallow and intermediate zone under the industrial user scenario.

6.3.3.2.2 Location-Specific ARARs

The activities that will be conducted under this alternative will comply with all location-specific ARARs. No activities would take place in sensitive environments such as wetlands, and no impacts to archeological resources or threatened and endangered species are anticipated.

6.3.3.2.3 Action-Specific ARARs

The activities that will be conducted under this alternative will comply with all action-specific ARARs. Soil remediation will occur in compliance with all transportation and disposal requirements. Runoff control will be important during soil/sediment excavation. All runoff requirements will be met to protect Goose Prairie Creek and Central Creek.

6.3.3.3 Long-Term Effectiveness and Permanence

6.3.3.3.1 Magnitude of Residual Risks

Upon completion of source removal, the residual site risk will be within the target risk range and below an HI of 1 for the hypothetical future maintenance worker and within risk range for the ecological receptor. The implementation of LUCs under this alternative would prevent direct contact by human receptors with contaminated groundwater at LHAAP-29, thus minimizing the potential risk posed by groundwater contamination.

6.3.3.3.2 Adequacy and Reliability of Controls

The soil exposure risk at LHAAP-29 for a hypothetical future maintenance worker or ecological receptor will be removed by excavating the isolated contaminated soil and sediment areas and plugging the underground TNT wastewater and cooling water lines and abandonment of the cooling water line manholes.

Groundwater extraction and treatment will be effective for reducing COC concentrations to concentrations that can be addressed via natural attenuation. The extracted water will be treated at the existing LHAAP groundwater treatment plant, which has been operating successfully for several years. There are significant issues associated with the effectiveness of groundwater extraction, especially associated with the use of extraction wells. If the hydraulic conductivity is too low in the aquifer, groundwater extraction will be slow and ineffective. Small capture zones may lead to excessive time frames to capture the contamination. There are also maintenance issues associated with low flow conditions. If extraction wells go dry, it causes the pumps to overheat and fail to operate. A pre-design study may be needed to determine the optimum configuration of wells.

MNA will be implemented for groundwater in both the shallow zone and the intermediate zone. In the intermediate zone, it will be initiated after the extraction phase. The MNA evaluation (**Appendix C**) has demonstrated that natural attenuation can be effective in the shallow zone. Effectiveness of natural attenuation in the intermediate zone will depend on successful

completion of the in situ treatment. In both zones, long-term success will be ensured by monitoring that verifies that natural attenuation is actively occurring.

LUCs will prevent exposure to the groundwater COCs exceeding the cleanup levels in the intermediate zone during the time required to remediate the groundwater. The reliability of LUCs will depend on the maintenance of the controls. It is not anticipated that groundwater cleanup levels in either the shallow or intermediate zone will be met in the near future. Compliance with the risk-reduction goals will be monitored and performance of the controls will be assessed throughout the duration of this alternative. The assessment may indicate the need for components of this alternative to be repaired, modified, or replaced.

Consistent with the required 5-year CERCLA review, compliance with the risk-reduction goals would be monitored and performance of the controls will be assessed. The 5-year reviews may indicate the need for components of this alternative to be maintained, modified, or replaced.

6.3.3.4 Reduction of Toxicity, Mobility, or Volume through Treatment

This alternative satisfies the USEPA statutory preference for remedial actions that permanently reduce the toxicity, mobility, and volume of the contaminants and utilize treatment as a principal element. Implementation of groundwater extraction at LHAAP-29 would permanently reduce the toxicity, mobility, and volume of the groundwater contaminants in this area. Use of the current LHAAP plant would provide irreversible destruction of the COCs in the extracted groundwater from the intermediate zone. In both the shallow and intermediate groundwater zones, MNA will reduce the toxicity and volume through natural biological and chemical processes.

6.3.3.5 Short-Term Effectiveness

6.3.3.5.1 Protection of the Community during Remedial Action

This alternative is protective of the surrounding community during remedy implementation primarily because all activities would occur on site with very little disturbance of contaminated material. Truck traffic for equipment and materials, including the shipment of contaminated soil off site for disposal and on-site delivery of borrow material for backfilling, will occur. If a spill of contaminated soils, the spill would be easy to contain and would not impact the surrounding communities. During remediation activities at LHAAP-29, control of surface runoff will be important to avoid releases of contamination to adjacent surface water bodies.

6.3.3.5.2 Protection of Workers during Remedial Action

Some short-term risks to human health or the environment will exist during implementation of this alternative. The soil excavation activity has the potential for transportation or construction accidents. Additionally, this alternative will involve potential short-term risks to workers associated with the operation of drilling equipment and potential exposure to decontamination

fluids, contaminated groundwater, and excavated soil. Other risks to workers include those associated with extended operation of the LHAAP groundwater treatment plant plus risks common to construction activities (e.g., slips, trips, and falls).

The implementation of proper engineering controls and safety equipment will minimize potential short-term risks to remediation personnel conducting the installation of the groundwater extraction system and groundwater sampling activities. Measures will be taken to prevent the contact of personnel with the extracted groundwater. Remediation workers will conform to the site health and safety program and will be equipped with the necessary PPE. A site-specific health and safety plan will be prepared prior to implementing this alternative.

6.3.3.5.3 Short-Term Environmental Effects

Minor clearing and grubbing at LHAAP-29 will be required to effectively excavate the soil and to install extraction wells and pipelines for groundwater recovery. However, since these areas have been cleared in the past, it is unlikely that there are any sensitive species that will be impacted. If any sensitive areas are found, the appropriate regulation will be followed. The implementation of proper engineering controls will minimize the risk of environmental impacts.

6.3.3.5.4 Duration of Remedial Activities

In three years, the groundwater extraction system is expected to remove the highest concentrations of VOCs from LHAAP-29 intermediate groundwater zone, thus reducing the contaminant mass. After three years, the extraction wells will be used as monitoring wells, and monitoring will be implemented to demonstrate that any remaining VOCs in the intermediate zone are attenuated by natural processes. Perchlorate, VOCs, and explosive compounds detected in the shallow zone are also expected to attenuate by natural processes. Natural attenuation in each of the shallow and intermediate zones will be monitored quarterly for two years to evaluate its effectiveness. Then monitoring would continue semiannually for three years, then annually until the next CERCLA 5-year review. Monitoring will continue once every five years until cleanup levels are achieved. The natural attenuation evaluation (**Appendix C**) estimates that it would be approximately 70 years (due to 1,2-DCA) for complete attenuation for the shallow zone.

6.3.3.6 Implementability

6.3.3.6.1 Technical Feasibility

The limited amount of soil and sediment excavation is easy to implement once the area requiring excavation is defined and cleared. Plugging of the TNT transite wastewater and cooling water lines can be conducted without extensive intrusive activities. All equipment, services and materials are readily available to conduct the activities for this alternative. Considering the small quantity of soil with reasonably low levels of contamination requiring disposal, a disposal location will be available.

Minimal technical concerns exist that will hinder the implementation of this alternative. Routine inspection and maintenance of the LUCs would be required. All equipment, services and materials are readily available to conduct the activities for this alternative, and the LHAAP groundwater treatment plant is already operational. Low groundwater yield could decrease the effectiveness of the extraction system. A detailed pre-design study would be needed to determine the optimum configuration of wells for effective extraction of the LHAAP-29 groundwater.

6.3.3.6.2 Administrative Feasibility

All actions under this alternative would be implemented on the site and thus do not require permits, though substantive provisions of permits that would otherwise be required are considered to be ARARs. By legal agreement (i.e., the FFA), the U.S. Army shall submit to the USEPA and TCEQ a Responsiveness Summary and ROD. Following consideration of any comments by TCEQ, the ROD will be finalized jointly by the U.S. Army and USEPA, or if they are unable to reach agreement about the selection of the remedial action, by the USEPA administrator. By addressing the identified ARARs in the ROD and subsequent documents, it is anticipated that the alternative would adequately address all administrative barriers.

LUCs, although administratively implementable, would require the development of an implementation plan as part of the remedial design, and internal notices to relevant regulatory offices of the existence of the LUCs. Approval by the USEPA and the State of Texas is required prior to the modification or termination of LUCs, implementation actions, or modification of land-use by the U.S. Army. The U.S. Army must also seek concurrence from the USEPA and the State of Texas prior to any action that may disrupt the effectiveness of the LUCs or any action that may alter or negate the need for LUCs.

6.3.3.7 Cost

The total project present worth cost of Alternative 3 is approximately \$2.9 million. The details and a comparison of the cost estimates for all of the alternatives are presented in **Appendix E**.

6.3.4.7.1 Capital Cost

The total capital cost is estimated at approximately \$1.3 million. The capital costs include mobilization, excavation of soil material, plugging the underground pipes, installing the groundwater extraction system and on-site storage system, transportation and disposal of excavated soils, demobilization of construction activities and the activities associated with LUCs.

The capital costs also include a work plans, remedial design document, pre-design study and a closure report.

6.3.4.7.2 O&M Cost

The total O&M cost is estimated at approximately \$1.6 million. The O&M cost includes O&M for of the groundwater extraction and storage system for the intermediate groundwater zone, monitoring for MNA in the shallow and intermediate zones, monitoring to support the required CERCLA 5-year review process, and LUC surveillance to verify groundwater is not used until proposed cleanup levels are met.

6.4 Comparative Analysis of Alternatives

6.4.1 Introduction

This section presents a comparative analysis of the remedial alternatives for LHAAP-29 according to the CERCLA evaluation criteria described in **Section 6.2**. This analysis is the second stage of the detailed evaluation process and provides information that forms the basis for selecting a preferred remedy.

This comparative analysis considers two of the three criteria categories, the threshold criteria and primary balancing criteria. The threshold category contains two criteria that must be satisfied by the selected alternative:

- Overall protection of human health and the environment and
- Compliance with ARARs.

These criteria are important because they reflect the key statutory mandates of CERCLA. If an alternative does not satisfy both of these criteria, it is not eligible to be selected.

The primary balancing category contains five criteria under which the relative advantages and disadvantages of the alternatives are compared to determine the most appropriate remedy. The five criteria are the following:

- Long-term effectiveness and permanence;
- Reduction of toxicity, mobility, or volume through treatment;
- Short-term effectiveness:
- Implementability; and
- Cost

The comparison of these five criteria for the alternatives forms the basis of the comparative analysis. The first and second balancing criteria address the statutory preference for treatment as a principal element of the remedy. Together with the third and fourth criteria, they form the basis for determining the general feasibility of each alternative and for determining whether costs are proportional to the overall effectiveness.

The two modifying criteria, state and community acceptance, must be satisfied if the alternative is to be accepted. The modifying criteria of state and community acceptance are typically not evaluated until the public has had an opportunity to comment on the PP. Because specific alternatives have not been presented to the state and community, these two criteria are not formally compared in the FS.

A comparative analysis under the threshold and primary balancing criteria is presented in **Sections 6.4.2** and **6.4.3**, respectively, and is consistent with the format of the individual analysis of alternatives in **Section 6.3**.

6.4.2 Threshold Criteria

6.4.2.1 Overall Protection of Human Health and the Environment

The three alternatives provide varying levels of human health protection. The "no action" alternative (Alternative 1) would not be protective of human health or the environment as no remedial activities or LUCs would be conducted. Alternative 1 does not achieve RAOs and provides the least protection of all the alternatives; it provides no reduction in risks to human health or the environment because no measures would be implemented to eliminate pathways for human and ecological exposure.

Alternatives 2 and 3 both satisfy the RAOs for LHAAP-29 and provide access and use restrictions for residual contamination. Alternatives 2 and 3 rely heavily on LUCs to prevent access to the shallow groundwater zone until cleanup levels are achieved. Both Alternatives 2 and 3 provide treatment of the primary COC for human health in the intermediate zone.

6.4.2.2 Compliance with ARARs

Alternative 1 does not comply with chemical-specific ARARs as no remediation of groundwater will be conducted. Alternatives 2 and 3 comply with all chemical-specific ARARs for soil and groundwater, as well as the location-specific and action-specific ARARs.

6.4.3 Primary Balancing Criteria

6.4.3.1 Long-Term Effectiveness and Permanence

Alternative 1 would be the least effective and permanent in the long term. Under this alternative, no contaminant removal or treatment would take place and no measures would be implemented to control exposure risks posed by contaminated surface soil and groundwater at LHAAP-29.

Alternatives 2 and 3 would significantly and permanently reduce groundwater contaminant concentrations to the applicable cleanup levels and, therefore, provide long-term effectiveness and permanence. Should in situ chemical oxidation or groundwater extraction be considered ineffective after implementation, the remedy or the cleanup levels may need to be re-evaluated.

Alternatives 2 and 3 both rely on MNA and LUCs until the proposed cleanup levels are achieved.

Alternative 2 provides a slightly higher level of effectiveness than Alternative 3 since the intermediate groundwater zone would reach concentrations amenable to natural attenuation in a shorter time frame. By requiring a shorter time frame, Alternative 2 allows the opportunity to evaluate the impact of the in situ treatment and re-inject if necessary.

6.4.3.2 Reduction of Toxicity, Mobility, or Volume through Treatment

Alternatives 2 and 3 both provide a large degree of permanent reduction in toxicity and volume of the groundwater contaminants while Alternative 1 provides no attempt at reduction.

6.4.3.3 Short-Term Effectiveness

Because Alternative 1 does not involve remedial measures, no short-term risk to remediation workers, the local community, or the environment would exist. Alternatives 2 and 3 involve material excavation and off-site disposal, which represent a greater exposure potential to remediation workers, a greater potential for runoff releases to the environment, and the potential for off-site traffic accidents and impacts on communities between LHAAP and the disposal facility. Additionally, Alternatives 2 and 3 both involve potential short-term risks to workers associated with exposure to contaminated groundwater from monitoring and/or operation of drilling/construction equipment.

Alternative 2 has short-term risks due to remediation workers constructing and operating an in situ treatment system, including the handling of chemical oxidants. Both Alternatives 2 and 3 have short-term risks associated with increased operations at the LHAAP groundwater treatment system, which includes chemical handling (caustic acids) and operation of a high-temperature catalytic oxidizer. However, Alternative 3 is estimated to have a longer operation period (3 years) than Alternative 2 (6 months).

By planning the construction, excavation, and transportation activities in accordance with industry and OSHA codes and requirements, risks from contaminant exposure and construction operations would be controlled to acceptable levels. Sediment deposition into adjacent surface water bodies can be controlled during earthwork and construction activities. Erosion control measures would include surface grading; emplacement of silt fences; covering surfaces with straw, mulch, riprap, and/or geotextile fabrics. Following completion of all construction and excavation, disturbed areas would be regraded with clean backfill and revegetated with native grasses.

6.4.3.4 Implementability

Administratively, all of the alternatives are implemental. Under Alternative 1, no remedial action would be taken. Therefore, no difficulties or uncertainties would be associated with its implementation.

For Alternatives 2 and 3, soil excavation would require coordination between excavation, sampling, transportation, and disposal. For groundwater, Alternatives 2 and 3 are also technically implementable, but there are uncertainties associated with hydrogeologic conditions that may impact the ability of in situ chemical oxidation or groundwater extraction to lower contaminant levels sufficiently to reach concentrations amenable to MNA. Alternative 3 would be somewhat more difficult to implement than Alternative 2 from a technical standpoint due to the increased duration (six months for Alternative 2 compared to three years for Alternative 3) that would be required to convey the contaminated groundwater to the existing LHAAP groundwater treatment plant.

6.4.3.5 Cost

Cost estimates are used in the CERCLA FS process to eliminate those remedial alternatives that are significantly more expensive than competing alternatives without offering commensurate increases in performance or overall protection of human health or the environment. The cost estimates developed are preliminary estimates with an intended accuracy range of +50 to -30 percent. Final costs will depend on actual labor and material costs, actual site conditions, productivity, competitive market conditions, final scope, final schedule, final engineering design, and other variables.

Costs developed are capital costs (including fixed-price remedial construction) and long-term O&M costs (post-remediation). Overall 30-year present worth costs are developed for each alternative assuming a discount rate of 2.8 percent. Total project present worth costs for each alternative is presented in **Appendix E**.

The progression of present worth costs from the least expensive alternative to the most expensive alternative is as follows: Alternative 1, Alternative 3, and Alternative 2. No costs are associated with Alternative 1 because no remedial activities would be conducted. Alternative 3 has the highest O&M costs associated with the estimated 3-year extraction period. Alternative 2 has the highest present worth and capital costs primarily due to the activities associated with the injection phase of the in situ chemical oxidation. Alternative 3 costs would be higher if there was no existing LHAAP groundwater treatment system.

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Appendix A

Investigation Results – 2004 and 2005

Appendix A Investigation Results – December 2004 and February 2005

1.0 Introduction

Shaw Environmental, Inc. (Shaw) performed additional field investigation activities at LHAAP-29 in December 2004 and February 2005 to further define the extent of perchlorate and explosives in soil, sediment, and water. Also in February 2005, the USACE collected soil samples near building foundations for explosives analysis. The numbers of samples and the types of analyses are summarized in **Table A-1** and the sample locations are provided in **Figures A-1** and **A-2**.

2.0 Shaw Investigation Activities

In December 2004 and February 2005, Shaw collected ten soil, 3 sediment, 8 solid residue, and 15 water samples at various locations to assess the affect of explosives in or near former wastewater drainage lines, ditches, and a pond. The ten soil samples were collected at five separate locations (29SB81 through 29SB85) at depth intervals of 4 to 5, and 8 to 9 feet below ground surface (bgs). These locations were adjacent to wash house sumps at five of the six previously active former 2,4,6-trinitrotoluene (TNT) production lines. Twelve soil samples (two from each of the six sump locations) were initially proposed, in accordance with the Addendum 3, Additional Investigation, LHAAP-29 and LHAAP-49, Final Work Plan, Groundwater Data Gaps Investigation Groups 2 and 4 (Addendum 3, Additional Investigation) (Shaw, 2004a). One soil boring location, however, was submerged in water and drilling at this location was not practical. Eight solid residue and twelve water samples were collected from manholes around the site. Originally, a total of 12 manholes were proposed to be sampled for solid residue and surface water; however, one manhole (MH-04) was collapsed and no samples were collected from this location. Additionally, no solid residue samples were collected from manholes MH-01, MH-03, and MH-11 due to a lack of solid residue. Due to dry conditions during the December 2004 sampling activities, water samples were collected only from manholes MH-01, MH-02, and MH-09. In February 2005, additional water samples were collected from MH-03, and MH-05 through MH-12. One sediment sample and one surface water sample were collected from the outfall ditch that received water from the cooling water drain lines. The remaining two sediment and two surface water samples were collected from the pond that exists at the location of the former pump house for the wastewater (red/yellow liquor) collection system.

Shaw also collected 12 soil samples (three in each of four soil borings) to examine the vertical and horizontal extent of perchlorate contamination in two areas in the northern portion of LHAAP-29. Two of the four borings, 29SB88 and 29SB89, were advanced through the slab at the location of the former rocket motor washout building. Three samples were collected from each boring. One sample was collected from immediately beneath the slab, one sample was collected from a depth of 4 to 5 feet beneath the previous sample, and one sample was collected immediately above the water table. Borings 29SB86 and 29SB87 were advanced in an area approximately 600 feet southwest of the former rocket motor washout building where perchlorate had been detected in the soil during earlier investigations. Samples from these borings were collected at depth intervals of 0 to 0.5 feet bgs, 6 to 8 feet bgs, and immediately above the water table.

The analytical results for the December 2004 and February 2005 investigations at LHAAP-29 are provided in **Tables A-2**, **A-3**, and **A-4**, for soil, sediment and solid residue, and water, respectively. Results for one explosive analyte (TNT) are also presented on **Figure A-1**, and results for perchlorate are presented on **Figure A-2**.

2.1 Sampling and Analysis

This section describes the sampling and analysis procedures applicable to water, sediment, solid residue, and soil samples collected. Samples were collected and handled in accordance with TERC Standard Operating Procedure 1111, Sample Handling (IT Corporation/OHM Remediation Services Corp., 2002). Samples were analyzed on a 7-day turnaround time. Health and safety procedures, including screening methods, are described in the Site Safety and Health Plan, Appendix A of the Final Work Plan (Shaw, 2004b).

2.1.1 Soil Sampling

Soil samples were collected at the boring locations identified in **Figures A-1** and **A-2**. Two to three soil samples were collected from each boring location. Soil borings were advanced using a direct push technology (DPT) rig. The DPT method involved the use of a high-capacity hydraulic ram mounted on an all-terrain vehicle to advance a drive sampler attached to steel push rods. At two locations (29SB88 and 29SB89), concrete slabs were penetrated using a concrete boring tool. Soil samples were collected continuously during DPT operation using a 24- to 36-inch-long sampler with a disposable liner. The depths of the borings were based on Addendum 3, Additional Investigation (Shaw, 2004a).

Boring locations were marked with a stake, where practical, and a Global Positioning System (GPS) device was used to obtain location coordinates. Site personnel covered the tailgate of a pick-up truck with plastic sheeting and used it as a sample preparation area. Field analytical and health and safety instruments were calibrated and recorded within the field logbook. New

disposable gloves were donned between each sampling interval to prevent cross-contamination. The sampling equipment was decontaminated as described in Section 4.5 in the Chemical Data Acquisition Plan, Appendix C of the Final Work Plan (Shaw, 2004b). The drilling operations observed proper safety, sampling, and drilling methods. When the soil sample was received from the driller, the soil-filled sampler was opened, the sample liner was removed from the barrel, the liner was cut open, and the sample liner was placed on the plastic sheeting. The entire length of material from the barrel was described according to ASTM D2488-93, "Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)" (ASTM International, 2004) and recorded on the standard Drilling Log Form. After verifying the appropriate sampling intervals, composite soil samples were placed in a container. Each sample container was labeled as described in Section 4.6.2 of the Chemical Data Acquisition Plan (Shaw, 2004b), enclosed in a sealable plastic bag, and placed in a cooler containing ice. This procedure was repeated for each interval to the total boring depth. Drilling activities and sampling procedures were recorded on a Field Sampling Report or logbook. COC documentation was completed and a photographic record of sample locations was maintained. Cuttings were disposed into the same borehole and the hole was grouted to surface. Decontamination fluids were disposed at the LHAAP-18/24 groundwater treatment plant. The samples were placed in 4-ounce wide-mouth glass containers, preserved on ice at a temperature of 4 degrees Celsius or less, and delivered to the analytical laboratory for analysis using EPA methods SW 8330 or EPA 314.0 for explosives or perchlorate, respectively.

Field duplicates (quality control samples) were collected and analyzed to assess the precision for the field sampling and laboratory analytical process. Each field duplicate was collected by filling a second sample container in rapid succession after collecting the primary soil sample. Duplicates were collected for samples 29SB85-001 and 29SB85-002.

2.1.2 Sediment and Solid Residue Sampling

Sediment was collected at the locations identified in **Figure A-1**. A sampling site was prepared by laying plastic sheeting on the adjacent ground. Field equipment and instruments were calibrated to verify they were in proper working order and calibration values were recorded in the field logbook. New disposable gloves were donned between samples to prevent cross-contamination. The sampling equipment was decontaminated as described in Section 4.5 in the Chemical Data Acquisition Plan (Shaw, 2004b). Information, deviations from procedures, and rationale for changes were recorded in the field logbook. Coordinates of each sampling location were recorded using a GPS unit.

The sediment sampling interval was 0 to 0.5 feet bgs. In manholes with concrete or masonry floors, the solid residue sample was limited to soil-like material that had collected atop the floor.

One sediment or solid residue sample was collected from each proposed location as stated in Addendum 3, Additional Investigation (Shaw, 2004a).

Sediment was placed into a clean stainless steel bowl and thoroughly mixed with a clean stainless steel spoon. At the manholes, a decontaminated trowel was attached to a 12-foot extension handle. Sediment was retrieved using this device, mixed, and placed in a 4-ounce glass container. An organic vapor meter was used to check for volatile organic compounds and record readings in the field logbook. The sample containers were filled directly from the tray or bowl with the spatula or spoon. As many stones, twigs, grass, etc., were removed from the sample as possible. If the sample was water saturated, the water was carefully decanted from the container with minimal disturbance to the sample. The sample was transferred directly from the sampler to the sample container leaving no headspace. Using wide, clear tape, the label was covered and the container was placed in a sealed plastic bag, and immediately placed in an iced cooler. Location coordinates were obtained using a GPS for the sediment sample locations. The location, sample-depth, and/or field measurements were recorded in the field logbook. COC documentation was completed and a photographic record was maintained. The samples were placed in 4-ounce glass containers, preserved on ice at a temperature of 4 degrees Celsius or less, and delivered to the analytical laboratory for analysis using EPA Method SW 8330 for explosives.

A field duplicate (quality control sample) was collected and analyzed to assess the precision for the field sampling and laboratory analytical process. The field duplicate was collected by filling a second sample container in rapid succession after collecting the primary sample. The duplicate was collected for sample 29SD640-MH09.

2.1.3 Surface Water Sampling

Surface water samples were collected at the locations shown in **Figure A-1**. A sampling site was prepared by laying plastic sheeting on the adjacent ground. Field equipment and instruments were calibrated to verify they were in proper working order and calibration values were recorded in the field logbook. Shaw personnel recorded a description of the site and sampling locations, including the coordinates of the sampling locations based on a GPS unit and/or site maps. Personal protective equipment was donned as required and specified in the Site Safety and Health Plan (Shaw, 2004b). New disposable gloves were donned prior to initializing sampling activities. The water samples were usually collected at locations where sediment samples were also collected. At those locations, the water sample was collected first. Water samples were collected in one of three ways:

• Surface water samples from the pond and the ditch were collected in open containers.

- Manhole water samples were collected in December 2004 using a clean/decontaminated 2-inch-diameter PVC sampler with a valve.
- Manhole water samples were collected in February 2005 using a peristaltic pump with clean/decontaminated tubing.

The sampling procedures were recorded on a field logbook. General water quality parameters (e.g., pH, conductivity, temperature, oxidation/reduction potential, turbidity) were measured using field instruments and recorded on the field logbook. COC documentation was completed and a photographic record was maintained. The sample was placed in a 1-liter amber bottle, preserved on ice at a temperature of 4 degrees Celsius or less, and shipped to the laboratory for analysis. Explosives were analyzed using EPA Method SW 8330.

Two field duplicates were collected and analyzed to assess the precision for the field sampling and laboratory analytical process. The field duplicates were collected by filling two separate 1-liter glass amber containers in rapid succession after collecting the primary water sample. Duplicates were collected for samples 29WL40-MH09 and 29WL40-MH09-02.

2.2 Results

The December 2004 and February 2005 results for explosives and perchlorate in the soil, sediment, and water samples from LHAAP-29 are presented in **Tables A-2**, **A-3**, and **A-4**. The associated data evaluation reports are included as **Attachment 1** of this document.

2.2.1 Explosives Results

Explosives were analyzed in soil, sediment, solid residue, and water samples collected throughout LHAAP-29. The soil samples were associated with the wash house sumps, while the sediment, solid residue, and water samples were associated either with the pond, the cooling water outfall ditch, or the cooling water manholes.

The explosives soil sample results in the soil near the sumps were largely non-detects, with a detection limit of 200 μ g/kg. Of the 14 explosives parameters analyzed in ten primary samples and 2 field duplicates, there were six detected results. These included TNT at 4 to 5 feet bgs at 29SB83 (430 μ g/kg), 2-amino-4,6-dinitrotoluene (DNT) at 4 to 5 feet bgs at 29SB85 (230J μ g/kg), and both 2-amino-4,6-DNT (900 μ g/kg) and 4-amino-2,6-DNT (300J μ g/kg) at 8 to 9 feet bgs at 29SB85. The remaining two detections were in the field duplicate for the 8- to 9-foot-interval at 29SB85.

In the two sediment samples at the pond, the only detection was 410 μ g/kg TNT at 29SD43-MH12 and 29SD45; the detection limit was 200 μ g/kg. The two surface water samples had detections of TNT (0.4J and 0.39J μ g/L), 2-amino-4,6-DNT (0.56J and 0.53J μ g/L), and

4-amino-2,6-DNT (2 and 1.9 μ g/L) at 29SW44 and 29SW45, respectively; the detection limit was 0.2 μ g/L.

The highest results for both sediment and soil during the investigation were at the cooling water outfall ditch. The sediment sample (29SD46) had 26,000,000 μ g/kg TNT and 8,000,000 μ g/kg 2,4-DNT. The associated water sample (29SW46) had 860 μ g/L TNT. Both samples had detections for other explosives, at lower concentrations.

Several explosives (1,3,5-trinitrobenzene; TNT; 2,4-DNT; 2,6-DNT; 2-amino-4,6-DNT; and 4-amino-2,6-DNT) were detected in both the water and solid residue from the cooling water manholes. Explosives were detected at low concentrations in solid residue samples from six of the eight cooling water manholes that were sampled. The highest solid residue result was $11,000 \,\mu\text{g/kg}$ TNT at manhole MH-02. The next highest results were for degradation products (9,000 $\,\mu\text{g/kg}$ 2-amino-4,6-DNT and 7800 $\,\mu\text{g/kg}$ 4-amino-2,6-DNT) at MH-10. The 12 water samples from the manholes had detected results for explosives, though the magnitude of the results varied several orders of magnitude. The highest explosives concentration from the water samples was 5,200 $\,\mu\text{g/L}$ TNT in manhole MH-09, which also had detections of 27 $\,\mu\text{g/L}$, 220 $\,\mu\text{g/L}$, and 290 $\,\mu\text{g/L}$ of 2,6-DNT, 2-amino-4,6-DNT, and 4-amino-2,6-DNT, respectively. MH-09 was sampled again in February 2005 and had a TNT result of 20 $\,\mu\text{g/L}$ at that time.

2.2.2 Perchlorate Results

Perchlorate was detected in five of the 12 soil samples collected at two areas in the northeastern portion of LHAAP-29. The detections at LHAAP-29 varied from 40.3 μ g/kg to 8,600 μ g/kg. However, due to interferences, the detection limits of the non-detect results varied from 114 to 267 μ g/kg. The highest results were not found at the two borings drilled through the slab at the former rocket motor washout facility, but at boring 29SB86. That boring location was chosen because of elevated perchlorate results in earlier investigations. As shown in **Figure A-2**, the results at 29SB86 varied from 40.3 μ g/kg at the surface to 8,600 μ g/kg at 6-8 feet bgs to 689 μ g/kg at 20-21 feet bgs (just above the water table). The 8,600 μ g/kg value exceeds perchlorate results in soil from earlier investigations at LHAAP-29.

3.0 USACE Investigation Activities

Plexus (Plexus, 2005) reported stained soil in the vicinity of wash house Building 806-D, possibly caused by explosives, such as TNT. On February 9 and 10, 2005, the USACE collected samples of soil at the foundation of Wash House 806-D and submitted them for explosives analysis (USACE, 2005). The results are presented in **Table A-5**.

The concrete foundation was cored in two places on the western end of the wash house. The western end of each wash house is the downgradient end and could be expected to have received runoff from settling tanks that were once housed in each wash house. Location 29DLineWHC01 was at a crack in the slab. The second location 29DLineWHC02, was slightly north and downgradient of the first core. The soil beneath the cores was slightly sandy with high clay content. The third sample was collected along the edge of the foundation at the most western end of the wash house slab. The soil was visually inspected at several locations along the foundation, and sample 29DLineWHW01 was collected at the location with the most obvious staining. **Figure A-3** indicates the sample locations.

The soil samples at the cored locations had no detected results for explosives. The sample from the edge of the foundation had detected results for four explosives parameters; the highest result was $27,300 \,\mu\text{g/kg}$ TNT.

4.0 References

ASTM International, 2004, ASTM D2488-00, "Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)" available online at <www.astm.org> (January 2005).

IT Corporation/OHM Remediation Services Corp., 2000, Standard Operating Procedures Manual, USACE – Tulsa District, Total Environmental Restoration Contract, Contract No. DACA56-94-D-0020, Houston, Texas.

Shaw Environmental, Inc. (Shaw), 2004a, *Draft Addendum 3*, *Additional Investigation, LHAAP-29 and LHAAP-49*, *Final Work Plan Groundwater Data Gaps Investigation Groups 2 and 4*, Houston, Texas, September.

Shaw, 2004b, Final Work Plan, Groundwater Data Gaps Investigation, Groups 2 and 4, Houston, Texas, February.

USACE, 2005, Personal Communication (e-mail from C. Murray to R. Zeiler), Subject: Washhouse Soil Sampling, March 28.

Tables

Shaw Environmental, Inc.

Table A-1
December 2004/February 2005 Sampling and Analyses
LHAAP-29

Media	Sample Locations	Primary Samples	Field Duplicates	Analytical Suite	Results Table
Soil					
Soil Near Wash House Sumps	29SB81-29SB85	10	2	Explosives	A-2
Soil in Perchlorate Areas	29SB86-29SB89	12	0	Perchlorate	A-2
Sediment					
Pond Sediment	29SD44, 29SD45	2	0	Explosives	A-3
Outfall Ditch Sediment	29SD46	1	0	Explosives	A-3
Manhole Solid Residue	29SD33, 29SD36-29SD41, 29SD43 (Manholes 2, 5-10, and 12)	8	1	Explosives	A-3
Water	•				
Pond Surface Water	29SW44, 29SW45	2	0	Explosives	A-4
Outfall Ditch Surface Water	29SW46	1	0	Explosives	A-4
Manhole Water	Manholes 1-3 and 5-12	12	2	Explosives	A-4

Table A-2 Soil Sampling Results 2004 Soil Investigation LHAAP-29

Sam	ple Location		2	9SB81				2	9SB81					29SB82					29SB82					29SB83					29SB83		\neg
	Sample ID		295	SB81-001				299	B81-002				29	SB82-001				29	SB82-002	2			29	SB83-001				29	SB83-002		
	Sample Date		16	-Dec-04				16	-Dec-04				1	5-Dec-04				1	5-Dec-04				1	5-Dec-04				1	5-Dec-04		
Si	ample Depth		4-	5 ft bgs				8-	9 ft bgs				4	-5 ft bgs				8	l-9 ft bgs				4	l-5 ft bgs				8	-9 ft bgs		
S	Sample Type			REG					REG					REG					REG					REG					REG		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
1,3-Dinitrobenzene	μg/kg	200	U	U		1	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2,4,6-Trinitrotoluene	μg/kg	200	U	U		1	200	J	U		1	200	U	U		1	200	U	U		1	430				1	200	U	U		1
2,4-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2,6-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2-Amino-4,6-dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
4-Amino-2,6-dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
HMX	μg/kg	200	U	U		1	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
m-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
Nitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
o-Nitrotoluene	μg/kg	200	U	U		1	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
p-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	Ū	U		1	200	U	U		1
RDX	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	Ü	U		1	200	U	U		1
Tetryl	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
Anions																															
Perchlorate	μg/kg																														

Table A-2 Soil Sampling Results 2004 Soil Investigation LHAAP-29

Sa	imple Location		2	9SB84				2	29SB84					29SB85					29SB85					29SB85					29SB85		
	Sample ID		299	SB84-001				29:	SB84-002				29	SB85-001				29S	B85-001-I	-D			29	SB85-002)			29S	B85-002-F	D	
	Sample Date		15	-Dec-04				15	5-Dec-04				1	5-Dec-04				1	5-Dec-04				1	5-Dec-04				1'	5-Dec-04		
	Sample Depth		4	5 ft bgs				8	-9 ft bgs				4	-5 ft bgs				4	l-5 ft bgs				8	3-9 ft bgs				8	3-9 ft bgs		
	Sample Type			REG					REG					REG					FD					REG					FD		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U	<u> </u>	1
1,3-Dinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2,4,6-Trinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U	<u> </u>	1
2,4-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2,6-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2-Amino-4,6-dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	230	J	J	15	1	200	U	U		1	900				1	830				1
4-Amino-2,6-dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	300	J	J	15	1	240	J	J	15	1
HMX	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
m-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U	<u> </u>	1
Nitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
o-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
p-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
RDX	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
Tetryl	μg/kg	200	U	U		1	200	U	U		1	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1
Anions																															
Perchlorate	μg/kg																														

Table A-2 Soil Sampling Results 2004 Soil Investigation LHAAP-29

Sa	mple Location		2'	9SB86				2	9SB86				- 2	9SB86				2	29SB87					29SB87				- 2	29SB87		
	Sample ID		295	B86-001				295	B86-002				29	SB86-003				295	SB87-001	l			29	SB87-002				29	SB87-003		\neg
	Sample Date		14	-Dec-04				14	-Dec-04				14	1-Dec-04				14	1-Dec-04				1	4-Dec-04				14	4-Dec-04		
	Sample Depth		0-0).5 ft bgs				6-	8 ft bgs				20	-21 ft bgs				0-0	0.5 ft bgs				6	-8 ft bgs				19	-20 ft bgs		
	Sample Type			REG					REG					REG					REG					REG					REG		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg																												<u> </u>		
1,3-Dinitrobenzene	μg/kg																													ļ	
2,4,6-Trinitrotoluene	μg/kg																												<u> </u>		
2,4-Dinitrotoluene	μg/kg																												<u> </u>		
2,6-Dinitrotoluene	μg/kg																														
2-Amino-4,6-dinitrotoluene	μg/kg																												1		
4-Amino-2,6-dinitrotoluene	μg/kg																												<u> </u>		
HMX	μg/kg																														
m-Nitrotoluene	μg/kg																												<u> </u>		
Nitrobenzene	μg/kg																												1		
o-Nitrotoluene	μg/kg																														
p-Nitrotoluene	μg/kg																														
RDX	μg/kg																														
Tetryl	μg/kg																												1		i
Anions																															
Perchlorate	μg/kg	40.3	,			1	8600				100	689				2	117	U	U		10	57	U	U		5	122	U	U		10

Table A-2 Soil Sampling Results 2004 Soil Investigation LHAAP-29

S	ample Location		2	9SB88				2	9SB88					29SB88				2	9SB89					29SB89				2	29SB89		
	Sample ID		295	SB88-001				295	B88-002)			29	SB88-003				295	SB89-001				29	SB89-002)			29	SB89-003		
	Sample Date		14	-Dec-04				14	-Dec-04				14	1-Dec-04				15	Dec-04				1	5-Dec-04				1!	5-Dec-04		
	Sample Depth		0-	1 ft bgs				4-	5 ft bgs				15	-16 ft bgs				0-0	0.5 ft bgs				2	1-5 ft bgs				12	-13 ft bgs		
	Sample Type			REG					REG					REG					REG					REG					REG		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg																														
1,3-Dinitrobenzene	μg/kg																														
2,4,6-Trinitrotoluene	μg/kg																														
2,4-Dinitrotoluene	μg/kg																														
2,6-Dinitrotoluene	μg/kg																														
2-Amino-4,6-dinitrotoluene	μg/kg																														
4-Amino-2,6-dinitrotoluene	μg/kg																														
HMX	μg/kg																														
m-Nitrotoluene	μg/kg																														
Nitrobenzene	μg/kg																														
o-Nitrotoluene	μg/kg																														
p-Nitrotoluene	μg/kg																														
RDX	μg/kg																														
Tetryl	μg/kg																														
Anions																															
Perchlorate	μg/kg	74.5				1	133	U	U		10	64.4	U	U		5	60.2	U	U		5	63.9	U	U		5	144				1

Notes:

μg/kg - micrograms per kilogram

DF - dilution factor

FD - field duplicate

ft bgs - feet below ground surface

J - The analyte was positively identified; the reported value is the estimated concentration of the constituent detected in the sample analyzed.

Qual - qualifier

RC - reason code

15 - quantitation

REG - regular

U - Not detected. The analyte was analyzed for, but not detected above the associated reporting limit.

ValQual - validation qualifier

Table A-3 Sediment and Solid Residue Sampling Results 2004 Investigation LHAAP-29

Sample	e Location		29:	SD33-MH	02			299	SD36-MH0)5			299	SD37-MH	06			299	SD38-MH0)7			29S	D39-MH08	3			29S	D40-MH09		
	Sample ID		29	SD33-MH	02			299	SD36-MH0)5			299	SD37-MH	06			299	SD38-MH0)7			29S	D39-MH08	3			29S	D40-MH09	1	
Sai	mple Date		1	17-Dec-04				1	7-Dec-04				1	7-Dec-04				1	6-Dec-04				1	6-Dec-04				17	7-Dec-04		
Sam	ple Depth		0)-0.3 ft bgs	;			0	-0.3 ft bgs				0	-0.3 ft bgs	;			0	-0.3 ft bgs				0-	0.3 ft bgs				0-0	0.3 ft bgs		
Sar	mple Type			REG					REG					REG REG						REG					REG						
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg	440				1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
1,3-Dinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
2,4,6-Trinitrotoluene	μg/kg	11000				5	200	U	U		1	290	J	J	15	1	630				1	5500				1	1200				1
2,4-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	710				1	200	U	U		1
2,6-Dinitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	300	J	J	15	1	200	U	U		1
2-Amino-4,6-dinitrotoluene	μg/kg	3800		J	17	1	200	U	UJ	17	1	290	J	J	17, 15	1	200	U	U		1	1200				1	2400		J	17	1
4-Amino-2,6-dinitrotoluene	μg/kg	2600		J	17	1	200	U	UJ	17	1	260	J	J	17, 15	1	200	U	U		1	880				1	2500		J	17	1
HMX	μg/kg	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	J		1	200	J	U		1
m-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
Nitrobenzene	μg/kg	200	J	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	J		1	200	J	U		1
o-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
p-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1
RDX	μg/kg	200	Ü	U		1	200	Ū	U		1	200	U	Ū		1	200	U	U		1	200	Ü	U		1	200	U	Ü		1
Tetryl	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1

Notes can be found on the last page

Table A-3
Sediment and Solid Residue Sampling Results
2004 Investigation
LHAAP-29

San	nple Location		299	SD40-MH	09			299	SD41-MH1	10			299	SD43-MH	12				29SD44					29SD45				2	9SD46		
	Sample ID		29SE	040-MH09)-FD			299	D41-MH1	10			295	SD43-MH	12				29SD44				:	29SD45				2	9SD46		
	Sample Date		1	17-Dec-04				1	6-Dec-04				1	7-Dec-04				1	9-Dec-04				1'	9-Dec-04				16	5-Dec-04		
S	ample Depth		0	-0.3 ft bgs	S			0-	0.3 ft bgs				0	-0.3 ft bgs				0	-0.5 ft bgs				0-	0.5 ft bgs				0-0	0.5 ft bgs		
	Sample Type			FD					REG					REG					REG	DC DE				REG					REG		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
1,3-Dinitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
2,4,6-Trinitrotoluene	μg/kg	1100				1	7000				1	410				1	200	U	U		1	410				1	26000000				5000
2,4-Dinitrotoluene	μg/kg	200	U	U		1	1100				1	200	U	U		1	200	U	U		1	200	U	U		1	8000000				5000
2,6-Dinitrotoluene	μg/kg	200	U	U		1	240	J	J	15	1	200	U	U		1	200	U	U		1	200	U	U		1	15000				10
2-Amino-4,6-dinitrotoluene	μg/kg	470		J	17	1	9000				10	200	U	UJ	17	1	200	U	U		1	200	U	U		1	48000				10
4-Amino-2,6-dinitrotoluene	μg/kg	460		J	17	1	7800				1	200	U	UJ	17	1	200	U	U		1	200	U	U		1	2000	U	U		10
HMX	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	J		1	2000	U	U		10
m-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
Nitrobenzene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	J		1	2000	U	U		10
o-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
p-Nitrotoluene	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
RDX	μg/kg	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	200	U	U		1	2000	U	U		10
Tetryl	μg/kg	200	Ū	Ü		1	200	U	Ü		1	200	U	U		1	200	U	U		1	200	Ū	U		1	2000	Ü	Ü		10

Notes:

μg/kg - micrograms per kilogram

DF - dilution factor

FD - field duplicate

ft bgs - feet below ground surface

J - The analyte was positively identified; the reported value is the estimated concentration of the constituent detected in the sample analyzed.

Qual - qualifier

RC - reason code

15 - quantitation

17 - field duplicate RPD criteria is exceeded

REG - regula

U - Not detected. The analyte was analyzed for, but not detected above the associated reporting limit.

ValQual - validation qualifier

Table A-4 Water Sampling Results 2004 Investigation/2005 Investigation LHAAP-29

Sample	e Location			29SW44					29SW45					29SW46				29V	/L32-MH0				29W	/L33-MH02)			29V	VL34-MH03	}	
	Sample ID		29S\	N44-0412	219			29S	W45-04121	19			29S\	N46-04121	16			29V	/L32-MH0				29W	/L33-MH02)			29WI	_34-MH03-0	ງ2	
Sai	mple Date		1	9-Dec-04				1	19-Dec-04				1	6-Dec-04				1	5-Dec-04				15	5-Dec-04				2	4-Feb-05		
Sam	ple Depth			-					-					-					-					-					-		
Sar	nple Type			REG					REG					REG					REG					REG					REG		
Parameter	Units	Result	Qual	ValQua	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																															
1,3,5-Trinitrobenzene	μg/L	0.2	U	U		1	0.2	U	U		1	0.73		J	15	1	0.2	\supset	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
1,3-Dinitrobenzene	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	\supset	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
2,4,6-Trinitrotoluene	μg/L	0.4	J	J	15	1	0.39	J	J	15	1	860				100	250				50	0.93	J	J	15	1	23		JL	07A	5
2,4-Dinitrotoluene	μg/L	0.2	U	U		1	0.2	U	U		1	19				10	15				5	0.2	U	U		1	0.263	U	UJL	07A	1
2,6-Dinitrotoluene	μg/L	0.2	U	U		1	0.2	U	U		1	7.6				1	4.1				1	0.2	U	U		1	0.263	U	UJL	07A	1
2-Amino-4,6-dinitrotoluene	μg/L	0.56	J	J	15	1	0.53	J	J	15	1	20				10	16				5	3.4				1	1.19		JL	07A	1
4-Amino-2,6-dinitrotoluene	μg/L	2				1	1.9				1	48				10	33				5	6.1				1	2.13		JL	07A	1
HMX	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	\supset	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
m-Nitrotoluene	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
Nitrobenzene	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	\supset	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
o-Nitrotoluene	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	\supset	U		1	0.2	U	U		1	0.263	U	UJL	07A	1
p-Nitrotoluene	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	Ū	Ü		1	0.2	U	U		1	0.2	U	Ū		1	0.263	Ū	UJL	07A	1
RDX	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	Ū	Ü		1	0.2	Ū	U		1	0.2	Ū	Ü		1	0.263	Ū	UJL	07A	1
Tetryl	μg/L	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.2	U	U		1	0.263	U	UJL	07A	1

Table A-4 Water Sampling Results 2004 Investigation/2005 Investigation LHAAP-29

San	ple Location		29\	NL36-M	H05				29\	NL37-MH0	6			29V	VL38-MH0	7			29\	VL39-MH0	3			29W	/L40-MH09)			29V	VL40-MH09)	
	Sample ID		29W	L36-MH	05-02	2			29W	L37-MH06	-02			29WL	.38-MH07-	02			29WI	L39-MH08-	02			29W	/L40-MH09)			29Wl	_40-MH09-	ე2	
	Sample Date		2	4-Feb-0)5				2	4-Feb-05				2	3-Feb-05				2	3-Feb-05				1	7-Dec-04				2	3-Feb-05		
S	ample Depth			-						-					-					-					-					-		
	Sample Type			REG						REG					REG					REG					REG					REG		
Parameter	Units	Resul	t Qua	ValQu	ial F	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																																
1,3,5-Trinitrobenzene	μg/L	0.26	U	UJL	. 0	7A	1	1.34		JL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
1,3-Dinitrobenzene	μg/L	0.26	U	UJL	. 0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
2,4,6-Trinitrotoluene	μg/L	84.3		JL	0	7A	10	430		JL	07A	100	0.955	J	J	15	1	6.36				1	5200				500	20				5
2,4-Dinitrotoluene	μg/L	0.26	U	UJL	. 0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.8	J	J	15	1	1.13				1
2,6-Dinitrotoluene	μg/L	0.26	U	UJL	0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	27				20	1.27				1
2-Amino-4,6-dinitrotoluene	μg/L	1.82		JL	0	7A	1	6.27		JL	07A	1	0.428	J	J	15	1	1.29				1	220				20	1.68				1
4-Amino-2,6-dinitrotoluene	μg/L	2.74		JL	0	7A	1	8.15		JL	07A	1	0.364	J	J	15	1	1.7				1	290				20	2.42				1
HMX	μg/L	0.26	U	UJL	0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
m-Nitrotoluene	μg/L	0.26	U	UJL	. 0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
Nitrobenzene	μg/L	0.26	U	UJL	0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
o-Nitrotoluene	μg/L	0.26	U	UJL	0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
p-Nitrotoluene	μg/L	0.26	U	UJL	. 0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
RDX	μg/L	0.26	U	UJL	0	7A	1	0.494	J	JL	07A, 15	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1
Tetryl	μg/L	0.26	U	UJL	. 0	7A	1	0.26	U	UJL	07A	1	0.26	U	U		1	0.258	U	U		1	0.2	U	U		1	0.266	U	U		1

Shaw Environmental, Inc.

Table A-4 Water Sampling Results 2004 Investigation/2005 Investigation LHAAP-29

Sam	ple Location		29V	/L40-MH0)9			29\	VL40-MHC)9			29V	/L41-MH1	0			29V	/L42-MH11	1			29W	/L43-MH12)	\neg
	Sample ID		9WL4	0-MH09-0	2-FD			29WI	_40-MH09	-FD			29WL	41-MH10	-02			29WL	.42-MH11-(02			29WL	43-MH12-	02	\neg
S	Sample Date		2	3-Feb-05				1	7-Dec-04				2	3-Feb-05				2	3-Feb-05				2	3-Feb-05		\neg
Sa	mple Depth			-					-					-					-					-		\neg
S	ample Type			FD					FD					REG					REG					REG		
Parameter	Units	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF	Result	Qual	ValQual	RC	DF
Explosives																										
1,3,5-Trinitrobenzene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	U	U		1	0.258	U	U		1	0.275	U	U		1
1,3-Dinitrobenzene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	\supset	U		1	0.258	\supset	U		1	0.275	U	U		1
2,4,6-Trinitrotoluene	μg/L	24				5	5900				500	15				4	18				5	25				5
2,4-Dinitrotoluene	μg/L	1.09				1	0.83	J	J	15	1	1.05				1	0.922	٦	J	15	1	0.934	J	J	15	1
2,6-Dinitrotoluene	μg/L	1.24				1	27				20	1.35				1	1.15				1	1.31				1
2-Amino-4,6-dinitrotoluene	μg/L	1.63				1	210				20	2.01				1	1.29				1	1.75				1
4-Amino-2,6-dinitrotoluene	μg/L	2.36				1	280				20	2.58				1	1.96				1	2.67				1
HMX	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	\supset	U		1	0.258	\supset	U		1	0.275	U	U		1
m-Nitrotoluene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	\supset	U		1	0.258	\supset	U		1	0.275	U	U		1
Nitrobenzene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	\supset	U		1	0.258	\supset	U		1	0.275	U	U		1
o-Nitrotoluene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	U	U		1	0.258	U	Ü		1	0.275	Ū	U		1
p-Nitrotoluene	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	Ü	U		1	0.258	U	U		1	0.275	Ū	U		1
RDX	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	U	U		1	0.258	U	U		1	0.275	Ū	U		1
Tetryl	μg/L	0.258	U	U		1	0.2	U	U		1	0.258	U	U		1	0.258	U	U		1	0.275	U	U		1

Notes:

μg/L - micrograms per liter

DF - dilution factor

FD - field duplicate

J - The analyte was positively identified; the reported value is the estimated concentration of the constituent detected in the sample analyzed.

L - Result may be biased low. Details are provided in the validation report.

Qual - qualifier

RC - reason code

07A - sample

15 - quantitation

REG - regular

U - Not detected. The analyte was analyzed for, but not detected above the associated reporting limit.

ValQual - validation qualifier

Table A-5
Explosives Analytes at Wash House 806-D Foundation^a
2005 Sampling by USACE
LHAAP-29

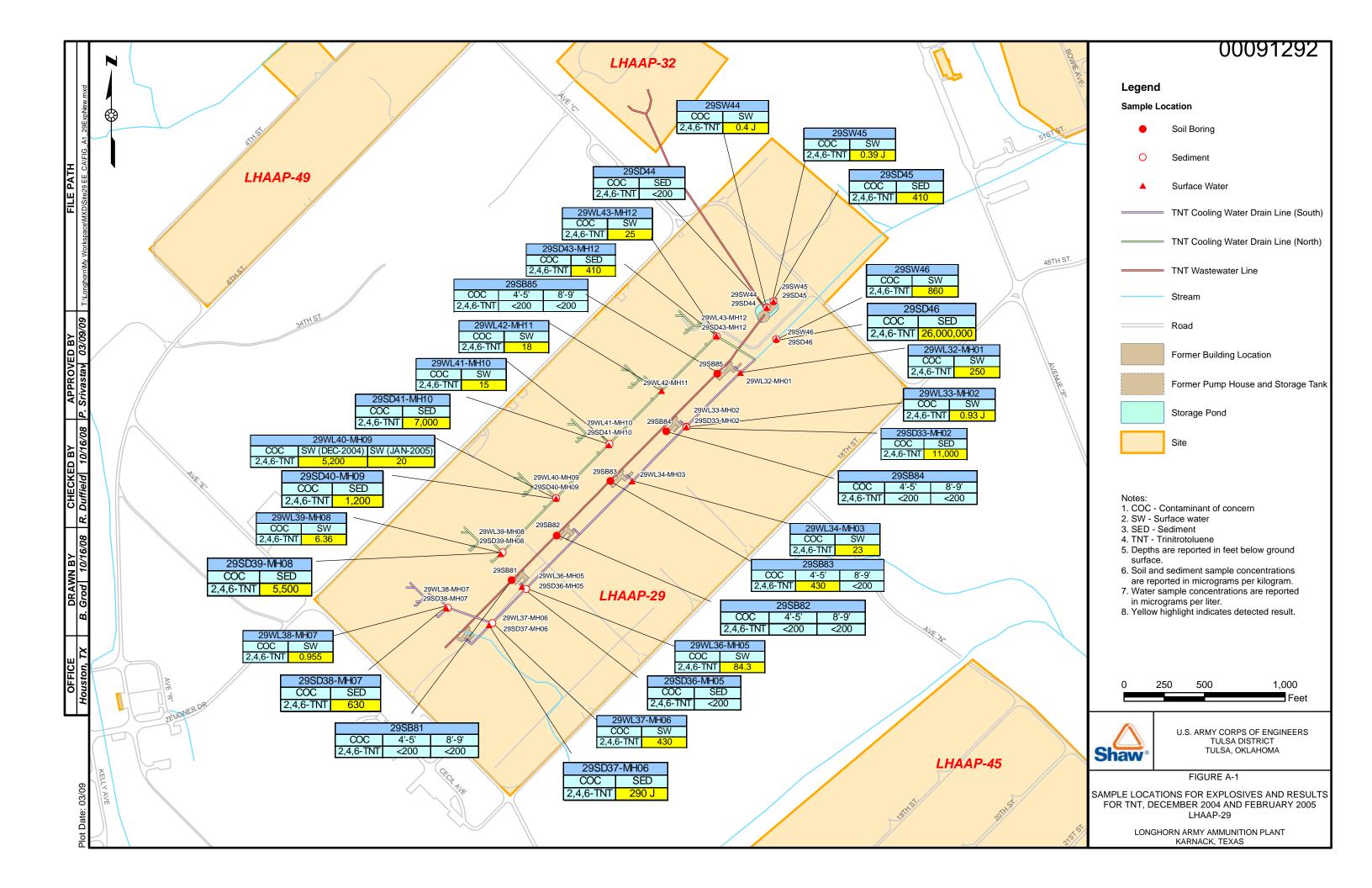
		005 Sampling by USA0 plosives Results (µg/	
Analyte	29DLineWHC01	29DLineWHC02	29DLineWHW01
1,3,5-Trinitrobenzene	< 375	< 375	4,610
2,4,6-Trinitrotoluene	< 375	< 375	27,300
2,4-Dinitrotoluene	< 375	< 375	< 375
2,6-Dinitrotoluene	< 375	< 375	< 375
2-Amino-4,6-dinitrotoluene	< 375	< 375	5,780
4-Amino-2,6-dinitrotoluene	< 375	< 375	2,870
HMX	< 375	< 375	< 375
m-Dinitrobenzene	< 375	< 375	< 375
m-Nitrotoluene	< 375	< 375	< 375
Nitrobenzene	< 375	< 375	< 375
o-Nitrotoluene	< 375	< 375	< 375
p-Nitrotoluene	< 375	< 375	< 375
RDX	< 375	< 375	< 375
Tetryl	< 375	< 375	< 375

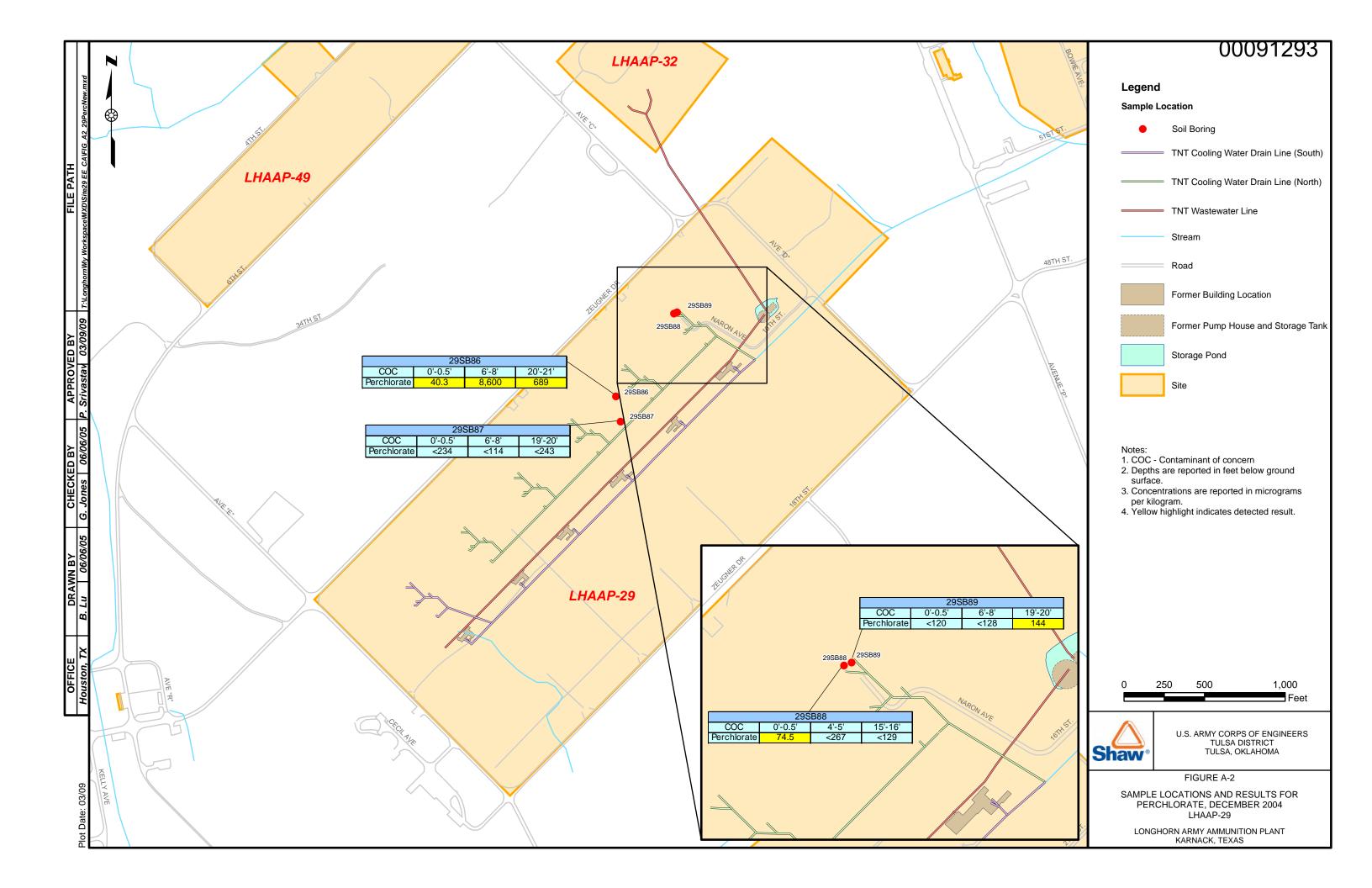
Notes

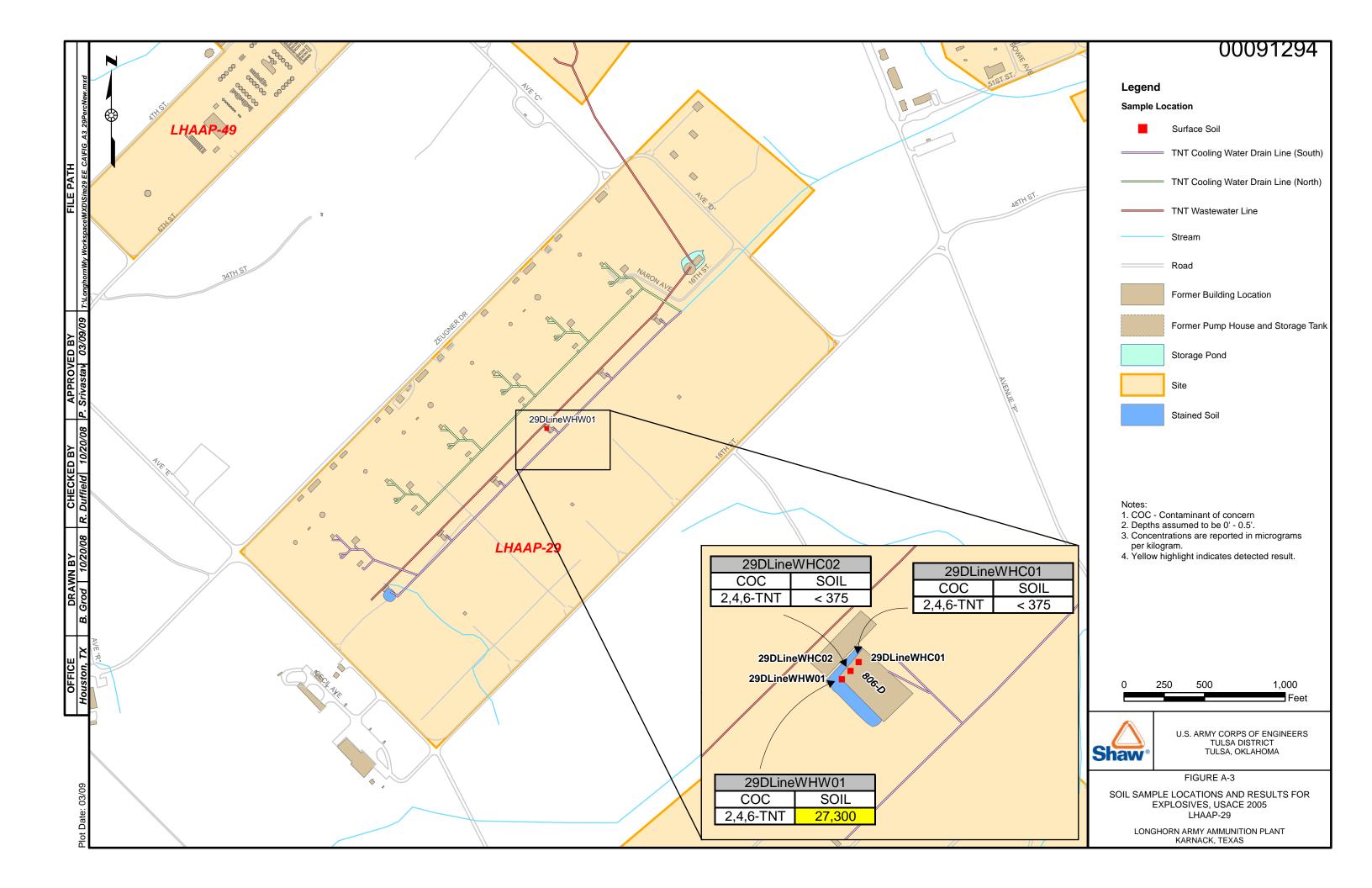
 μ g/kg micrograms per kilogram

^a Reference: USACE, 2005, Personal Communication (e-mail from C. Murray to R. Zeiler), Subject: Wash house soil sampling, March 28.

Figures







Attachment 1 Laboratory Reports

Available on the Attached CD

TABLE OF CONTENTS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L128

SECTION		PAGE
Cover Letter, CO	DC/Sample Receipt Form	1000 – 1006
GC/MS-VOA	**	2000 –
GC/MS-SVOA	**	3000 –
GC-VOA	**	4000 –
GC-SVOA	**	5000 –
HPLC	EPA METHOD 8330	6000 – 6049
METALS	**	7000 –
WET	**	8000 –
OTHERS	**	9000 –
	the state of the s	

^{** -} Not Requested



1835 W. 205th Street Torrance, CA 90501

> Tel: (310) 618-8889 Fax: (310) 618-0818

Date: 01-03-2005 EMAX Batch No.: 04L128

Attn: Diane Meyer

Shaw E&I 1430 Enclave Parkway Houston TX 77077

Subject: Laboratory Report

Project: Longhorn Army Ammunition Plant

Enclosed is the Laboratory report for samples received on 12/16/04. The data reported include:

Sample ID	Control #	Col Date	Matrix	Analysis
29SB85-001	L128-01	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB85-002	L128-02	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB85-001-QC	L128-03	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB85-002-QC	L128-04	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB82-001	L128-05	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB82-002	L128-06	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29SB83-001	L128-07	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29\$B83-002	L128-08	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29sB84-001	L128-09	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29\$B84-002	L128-10	12/15/04	SOIL	NITROAROMATICS & NITRAMINES
29WL32-MH01	L128-11	12/15/04	WATER	NITROAROMATICS & NITRAMINES
29WL32-MH02	L128-12	12/15/04	WATER	NITROAROMATICS & NITRAMINES

The results are summarized on the following pages.

Please feel free to call if you have any questions concerning these results.

Sincerely yours,

Kam Y. Pang, Ph.D. Laboratory Director

Environmental & Infrastructure, Inc.

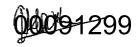
1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-002

041128

L	aborato	ry Name	EMAX	· · · · · · · · · · · · · · · · · · ·					ress:	1835 205th Street Torrance, CA 90501		Conta	act: \) pe	Kel	bley			*	:
		1	AAD				Projec		ition on Are	Area 29 Former TNT					Method I				Remarks	-
Projec	t Name	Longi	horn AAP			Project (JII AIR	Project Telephone No.		0		le sepa	ate con	tamers)		T	Remains	
, , ,		8457	'1 <i>A</i>		Dione Moves 294.269.4404 5 5 6 6 7															
USAC	E Point o	f contact:					diio i	ricyc		t Manager/Supervisor	韥	8 3	by .	l						
l			Cliff Murray	,							ပ္	es	12		·		٠ .			
USAC	E Teleph	one No.								Praveen Srivastav	o Jac	5 E	Ora			1. 7000	** **	1.2	·	
Rem No.		Sample N	umber		Date	Time	Comp	Grab	Matrix	Sample Description, Location	Number of Containers	Nitroaromatics a	Perchlorate							
1	29SB8			12	MH	10.15			SOIL	29SB85	1	х				7.51				,
2	29SB8	5-002				10:22			SOIL	29SB85	1	х								,
3	29SB	85	-001-QC		\	10:15			SOIL	215885	1	х	<u> </u>							٠
4	29SB_	郡	-002-QC		¥	10:22			SOIL	z9 SB85	1	х								,
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		Standard Rush Due: Seals Intact? N Received Good Condition V N Cold S , O C																		
	TAT:	Standard	Rush Du	e:			Se	eals Int	act7	Received Good	Condition	-1-8	N	c	old 🗐	1,0	C			





Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-001

042128

									4000 0000 00								····	
La	aboratory Name:	EMAX			·····			dress:	Torrance, CA 90501		Con	tact:	Joe	Kel!	bley	·		
Project	t Name Longho					1 1	ect Loc		Area 29 Former INI			Analys	sis and	Method	Desired			
Project		III AAF			Project			on Ar	Project Telephone No.				te sepa	rate con	tainers)		,	Remarks
,		_								en en	2 2	314.0	1			1		
11040		845714 Diane Me				Mey		281-368-4404	Containers	60	, E	. .						
USACE Point of contact: Cliff Murray				Proje			Nitroaromatics and	ate by										
USACE	E Telephone No.					,			Praveen Srivastav	j ja	2 E	Ď						
Item No.	Sample Num	ber	c	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Number of	Nitroa	Perchlorate						
-1-	29SB80-001		_			_		So⊩	29\$B90	1-	L _X							
-2	29 SB80-0 02		+					SOIL	20SB80	1	y							
3	29SD81-001		Ļ					SOIL	29\$B81		L,							
4	293B81-002							COIL	29SB81									
	29SB82-001		121	ıЯμ	14 36	1000	X	SOIL	29SB82	1	X							
6 2	29SB82-002		1	/	4:48	3	X	SOIL	29SB82	1	х							
7 2	29SB83-001				1400	R	X	SOIL	29SB83	1	х							
8 2	29SB83-002				1405	3	X	SOIL	29SB83	1	X							
9 2	29SB84-001				1125	36	X	SOIL	29SB84	1	Х				1			
10 2	9SB84-002		_	1	1130	ญ	X	SOIL	29SB84	1	X					-		
	anafers Relinquished	By (Signatu	ire)			te/Tim			ansfers Accepted By (Signature)	Date		Special Is	nstruction	ıs				
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					··							FedEx A	Airbill No).;				
								Laborati	TY A	12-16	0930	Sample	r's Signa	ature		·		
TA	AT: Standard	Rush Due				Se	eals Inta	ct?	Received Good (N_	Co	d				

Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-0-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-008

044128

Tursa	TERC DACASS-94-D-0020						1835 205th Street									
La	boratory Name: EMAX				Addı	ress:	Torrance, CA 90501		Contac	-						
					t Local		Area 29 Former INI				s and M			•,		Remarks
Pmiec	t Name Longhorn AAP			Prod	uctio	n Are	a				e separ	ate cont	amers)			remarks
Projec		-	Project (Contac	t		Project Telephone No.	p5	2 E	314.0						
•	845714	-	Di	ane l	Vleye	<u> </u>	281-368-4404	aine	s at	131		-				
USAC	E Point of contact: Cliff Murray					Projec	t Manager/Supervisor	of Containers	Nitroaromatics and Nitroamines by 8330	ate by		-				
USAC	E Telephone No.						Praveen Srivastav	Number of	ami	Hor						
Item No.	Sample Number	Date	Time	Comp	Grab	Matrix	Sample Description, Location	N	Nitro Nitro	Perchlorate						
	29WL32-MH01	12/15/04	1330		X	sw	29WL32-MH01	2	х							
	29WL33-MH02	12/15/04	1445		X	sw	29WL33-MH02	2	х							
 	29WL34-MH03					SW	29WL34-MH93 -	-2-	×							
	29WL35-MH04					sw	29WL35-MH04	2	X					,.	<u> </u>	
5	29WL36-MH05				D	sw	29WL36-MLIQ5	2	X							
-6-	29WL37-MH06		1/M	SV	1	SW	29WL37-MH06	2	X						-	
	2 9WL38-MH07	1					29WL38-MH07	2	X		3 5					
8	29WL39-MH08			<u> </u>	 	-sw	29WL39-MH08-	2	X		٠				-	
9		-	-		-			-	┼─		 					
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		1	 	_		_		-		FedE	Airbill l	No.:				
			-			Labor	allery		16-04	Samp	ler's Sig	nature				
- direct	TAT: Standard Rush Due: Seals Intact? Y Received Good Condition Y N Cold															

SAMPLE RECEIPT FORM 1

Туре	of Delivery	Delivered By/Airbill	ECN 04/2128
EMAX Courier			Recepient (10n Luna/ser
Client Delivery			Date 12-16-04
Third Party (UPS	J1787464218	Time 0930
	and the second s		
		COC Inspection	
Client Name	•	Sampler Name	Sampling Date/Time/Location
Address		Courier Signature/Date/Time	Analysis Required
Client PM/FC	and the second second	TAT	Matrix
Tel #/Fax #		Sample ID	Preservative (if any)
Safety Issues	None	High Concentrations expected	Superfund Site Samples
Comments.	Rad Screening Require	ed	
	destruction of the second seco		
	· .	Packaging Inspection	
Container	Cooler	☐ Box ☐	
Condition	Custody Seal	☐ Intact ☐ Dama	ged
Packaging	Bubble Pack	Suffici	ient plastic bad
Temperatures	Cooler 1	☑ Cooler 2 Cooler	
	Cooler 5	Cooler 6 Cooler	7 Cooler 8
	Cooler 9	Cooler 10 Cooler	11 Cooler 12
Comments:			
LSCID	Client ID	Discrepancy	Corrective Action
L128-03	295385-001-6	C LABEL REASTO FOR PERCH.	CORATE called client
		ANALYSIS	IDS with 80; 81, 82
			83, 84 85 > explosives
-04	2958 (05)002- 00		, 86,87,88,897 Perchbrate
		OATE TIME WEDE MATCHED ON	
		COC) REQUETO FOR PER CHORA,	to run these sumples
		MALYSIS	for explosives perclicul
-05		NO COLLECTION ONTE ON LABEL	Deter to chin of expstody
-06		COLLECTION TIME ON WASEL	
		REMPS 1445 (1448 ON COC)	
-09		COLLECTION TIME ON LABER	
		RETURN (1125 ON COC)	J
LOCIDAL			
LSCID : Lab Samp	ie Container ID		
REVIEWS	n water to make the second of the second	Ži.	
Sample Labeling	Contract of the Contract of th	SRF NE	PM amk
Date	12-16-9U	Date 12-17-04	Date 12/17/04
	The state of the s		

UPS Next Day Air UPS Worldwide Express™ Shipping Document	WEIGHT DIMENSIONAL WEIGHT WEIGHT The shipper authorities Unit to be at as forceding agent for expert control and customs purposes. The shipper collises, technology or solvare were aboved to mit to the United States in excordance with the Expert control of the Collision and the Collision of the United States in excordance with the Expert control of the Collision of the Collisi
04L128 } 12-16-04 04L129 } 12-16-04	EXPRESS (INTL) DOCUMENTS ONLY SATURDAY DELIVERY
SHIPMENT FROM ACCOUNT NO HEFERENCE NUMBER	J178 746 421 8. J178 746 421 8
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DELIVERY TO	UPS Next Day Air®
TELEPHONE Residential	J178 746 421 8
บางทำ20ธิถูงw Unite (Parcel Service Ville, KY	JJ.78 745 423 8 DATE OF SHIPMENT

REPORTING CONVENTIONS

DATA QUALIFIERS:

Lab Qualifier	AFCEE Qualifier	Description
J .	F	Indicates that the analyte is positively identified and the result is less than RL but greater than MDL.
N		Indicates presumptive evidence of a compound.
В	В	Indicates that the analyte is found in the associated method blank as well as in the sample at above QC level.
distribution of the second of	J	Indicates that the result is above the maximum calibration range.
*	*	Out of QC limit.

Note: The above qualifiers are used to flag the results unless the project requires a different set of qualification criteria.

ACRONYMS AND ABBREVIATIONS:

CRDL	Contract Required Detection Limit
RI	Reporting Limit
MRL	Method Reporting Limit
PQL	Practical Quantitation Limit
MDL	Method Detection Limit
DO	Diluted out

DATES

The date and time information for leaching and preparation reflect the beginning date and time of the procedure unless the method, protocol, or project specifically requires otherwise.

LABORATORY REPORT FOR

SHAW E&I

LONG HORN ARMY AMMUNITION PLANT

EPA METHOD 8330 EXPLOSIVES

SDG#: 04L128

CASE NARRATIVE

CLIENT:

SHAW E & I

PROJECT:

LONG HORN ARMY AMMUNITION PLANT

EMAX SDG:

04L128

EPA METHOD 8330 EXPLOSIVES

Two (2) water and ten (10) soil samples were received on 12/16/04 for Explosives analysis by EPA Method 8330 in accordance with USEPA-SW846 3rd edition, and EMAX-8330.

1. Holding Time

Analytical holding time was met. Extraction for water samples was started and completed on 12/20/04. Extraction for soil samples was started on 12/20/04 and completed on 12/21/04

2. Calibration

Initial calibration was 5 point. %RSDs were within 20%. All continuing calibrations of the primary column were carried out at 12-hour intervals and the recoveries were within 85-115%.

3. Method Blank

Method blanks were free of contamination at the Reporting Limit.

4. Surrogate recovery

Surrogate recovery for sample L128-11I was diluted out. All other surrogate recoveries were within QC limits.

5. Lab Control Sample / Lab Control Duplicate

All recoveries were within QC limits.

6. Matrix Spike/Matrix Spike Duplicate

Sample L128-02 was spiked. Recoveries were within QC limits.

7. Sample Analysis

Sample analyses were within QC requirements. Quantitation is from the primary column. All positive results above RL were confirmed by LC-CN column and the confirmation is presumptive because it was based on retention time window.

Samples were air-dried prior to extraction; hence, no moisture correction was applied to RL, MDL and results.

SDG NO.

LAB CHRONICLE EXPLOSIVES

: 04L128

: SHAW E&I Client

Instrument ID : T081 Project : LONGHORN ARMY AMMUNITION PLANT

					SOIL				
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio		
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
								EW OOF	Method Blank
MBLK1S	EXL005SB	1	NA	12/21/0417:34	12/20/0417:30	XL21013A	XL21012A	EXL005S	
LCS1S	EXL005SL	1	NA	12/21/0418:03	12/20/0417:30	XL21014A	XL21012A	EXL005S	Lab Control Sample (LCS)
29SB85-001	L128-01	1	NA	12/21/0418:32	12/20/0417:30	XL21015A	XL21012A	EXL005S	Field Sample
29SB85-002	L128-02	1	NA	12/21/0419:01	12/20/0417:30	XL21016A	XL21012A	EXL005S	Field Sample
29SB85-002MS	L128-02M	1	NA	12/21/0419:29	12/20/0417:30	XL21017A	XL21012A	EXL005S	Matrix Spike Sample (MS)
29SB85-002MSD	L128-02\$	1	NA	12/21/0419:58	12/20/0417:30	XL21018A	XL21012A	EXL005S	MS Duplicate (MSD)
29SB85-001-QC	L128-03	1	NA	12/21/0420:27	12/20/0417:30	XL21019A	XL21012A	EXL005S	Field Sample
29SB85-002-QC	L128-04	1	NA	12/21/0421:54	12/20/0417:30	XL21022A	XL21021A	EXL005S	Field Sample
29SB82-001	L128-05	1	NA	12/21/0422:22	12/20/0417:30	XL21023A	XL21021A	EXL005S	Field Sample
29SB82-002	L128-06	1	NA	12/21/0422:51	12/20/0417:30	XL21024A	XL21021A	EXL005S	Field Sample
29SB83-001	L128-07	1	NA	12/21/0423:20	12/20/0417:30	XL21025A	XL21021A	EXL005S	Field Sample
29SB83-002	L128-08	1	NA	12/21/0423:49	12/20/0417:30	XL21026A	XL21021A	EXL005S	Field Sample
29SB84-001	L128-09	i	NA.	12/22/0400:18	12/20/0417:30	XL21027A	XL21021A	EXL005S	Field Sample
29SB84-002	L128-10	i	NA.	12/22/0400:46	12/20/0417:30	XL21028A	XL21021A	EXL005S	Field Sample
295804-002	L 120-10		1471	12,22,0100112	1			V	
					WATER		•	· ·	
01:	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio	n Prep.	
Client	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
Sample ID	Sample 10	ractor	MOISC	DOTESTING					
	EXL004WB	1	NA	12/20/0418:27	12/20/0413:00	XL20004A	XL20003A	EXL004W	Method Blank
MBLK1W	EXLOO4WL	<u>,</u>	NA NA	12/20/0418:56	12/20/0413:00	XL20005A	XL20003A	EXL004W	Lab Control Sample (LCS)
LCS1W		4	NA.	12/20/0419:24	12/20/0413:00	XL20006A	XL20003A	EXL004W	LCS Duplicate
LCD1W	EXL004WC	i-		12/20/0419:53	12/20/0413:00	XL20007A	XL20003A	EXL004W	Field Sample
29WL32-MH01	L128-11	ļ	NA		12/20/0413:00	XL21004A	XL21002A	EXL004W	Diluted Sample
29WL32-MH01DL1	L128-11T	5	NA	12/21/0413:15		XL21004A XL21003A	XL21002A	EXLOC4W	Diluted Sample
29WL32-MH01DL2	L128-11I	50	NA	12/21/0412:46	12/20/0413:00		XL21002A XL20003A	EXLOC4W	Field Sample
29WL32-MH02	L128-12	1	NA	12/20/0420:22	12/20/0413:00	XL20008A	ALZUUUSA	CALUU4W	rieta sampte

- Filename

% Moist - Percent Moisture

SAMPLE RESULTS

EPA METHOD 8330 EXPLOSIVES

Client : SHAW E&I Date Collected: 12/15/04 Date Received: 12/16/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L128 Date Extracted: 12/20/04 17:30 Sample ID: 29SB85-001 Date Analyzed: 12/21/04 18:32 Lab Samp ID: L128-01 Dilution Factor: 1 Lab File ID: XL21015A Matrix : SOIL Ext Btch ID: EXLO058 % Moisture : NA Calib. Ref.: XL21012A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	230J	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	101	63-143	

Note: All positive results are confirmed by CN column

EPA METHOD 8330 EXPLOSIVES

Client : SHAW E&I Date Collected: 12/15/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L128 Date Received: 12/16/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SB85-002 Date Analyzed: 12/21/04 19:01 Lab Samp ID: L128-02 Dilution Factor: 1 Lab File ID: XL21016A Matrix : SOIL Ext Btch ID: EXLO05S % Moisture : NA Calib. Ref.: XL21012A Instrument ID : T-081 ______

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
in a serie in a serie and a	1-11-11		
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	300J	400	200
2-AM-4,6-DNT	900	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
* * * * * * * * * * * * * * * * * * * *			

63-143

Note: All positive results are confirmed by CN column

3,4-DINITROTOLUENE

EPA METHOD 8330 EXPLOSIVES

Client : SHAW E&I Date Collected: 12/15/04 Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L128 Date Received: 12/16/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SB85-001-QC Date Analyzed: 12/21/04 20:27 Lab Samp ID: L128-03 Dilution Factor: 1 Lab File ID: XL21019A Matrix : SOIL Ext Btch ID: EXLO05S % Moisture : NA Calib. Ref.: XL21012A Instrument ID : T-081 -----

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
HMX	=,=,= = =,= NB		200
	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	NĎ	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	104	63-143	

Note: All positive results are confirmed by CN column

Client : SHAW E&I
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L128 Date Collected: 12/15/04 Date Received: 12/16/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SB85-002-QC Date Analyzed: 12/21/04 21:54 Lab Samp ID: L128-04 Dilution Factor: 1 : SOIL Lab File ID: XL21022A Matrix Ext Btch ID: EXLO05S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL21021A

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	240J	400	200
2-AM-4,6-DNT	830	400	200
2,6-DNT	ND	400	200
2,4-DNT	NĎ	400	200
2-NITROTOLUENE	ND	.400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	101	63-143	

Note: All positive results are confirmed by CN column

15

Client :	SHAW E&I	Date Collected: 12/15/04	
	LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/16/04	
Batch No. :	04L128	Date Extracted: 12/20/04 17:30	
Sample ID:	29SB82-001	Date Analyzed: 12/21/04 22:22	
Lab Samp ID:		Dilution Factor: 1	
Lab File ID:		Matrix : SOIL	,
Ext Btch ID:		% Moisture : NA	
Calib. Ref.:	XL21021A	Instrument ID : T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
	=,= ='= = = =		
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	[*] 400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	100	63-143	

Client : SHAW E&I	Date Collected: 12/15/04				
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/16/04				
Batch No. : 04L128	Date Extracted: 12/20/04 17:30				
Sample ID: 29SB82-002	Date Analyzed: 12/21/04 22:51				
Lab Samp ID: L128-06	Dilution Factor: 1				
Lab File ID: XL21024A	Matrix : SOIL				
Ext Btch ID: EXLO05S	% Moisture : NA				
Calib. Ref.: XL21021A	Instrument ID : T-081				

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	~400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		
3,4-DINITROTOLUENE	100	63-143	

Client : SHAW E&I Date Collected: 12/15/04 Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L128 Date Received: 12/16/04 Date Extracted: 12/20/04 17:30 Sample ID: 29\$B83-001 Date Analyzed: 12/21/04 23:20 Lab Samp ID: L128-07 Dilution Factor: 1 Lab File ID: XL21025A : SOIL Matrix Ext Btch ID: EXLO05S % Moisture : NA Calib. Ref.: XL21021A Instrument ID : T-081

PARAMETERS	RESÚLTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)	
НМХ	ND	400	200	
RDX	ND	400	200	
1,3,5-TNB	ND	400	200	
1,3-DNB	ND	400	200	
TETRYL	ND	400	200	
NITROBENZENE	ND	400	200	
2,4,6-TNT	430	400	200	
4-AM-2,6-DNT	ND	400	200	
2-AM-4,6-DNT	NĎ	400	200	
2,6-DNT	ND	400	200	
2,4-DNT	ND	400	200	
2-NITROTOLUENE	ND	<b></b> 400	200	
3-NITROTOLUENE	ND	400	200	
4-NITROTOLUENE	ND	400	200	
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT		
3,4-DINITROTOLUENE	102	63-143		

Client : SHAW E&I
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L128 Date Collected: 12/15/04 Date Received: 12/16/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SB83-002 Date Analyzed: 12/21/04 23:49 Lab Samp ID: L128-08 Dilution Factor: 1 Lab File ID: XL21026A Matrix : SOIL Ext Btch ID: EXLO05S % Moisture : NA Calib. Ref.: XL21021A Instrument ID : T-081 ______

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	100	63-143	

Client :	SHAW E&I	Date Collected: 12/15/04	
Project :	LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/16/04	
Batch No. :	04L128	Date Extracted: 12/20/04 17:30	
Sample ID:	29SB84-001	Date Analyzed: 12/22/04 00:18	
Lab Samp ID:	L128-09	Dilution Factor: 1	
Lab File ID:	XL21027A	Matrix : SOIL .	1
Ext Btch ID:	EXL005s	% Moisture : NA	
Calib. Ref.:	XL21021A	Instrument ID : T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	101	63-143	

			==
Client :	SHAW E&I	Date Collected: 12/15/04	
Project :	LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/16/04	
Batch No. :	04L128	Date Extracted: 12/20/04 17:	30
Sample ID:	29SB84-002	Date Analyzed: 12/22/04 00:4	46
Lab Samp ID:	L128-10	Dilution Factor: 1	
Lab File ID:	XL21028A	Matrix : SOIL	1
Ext Btch ID:	EXL005S	% Moisture : NA	
Calib. Ref.:	XL21021A	Instrument ID : T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
			======
НМХ	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	105	63-143	

Client : SHAW E&I Date Collected: 12/15/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L128 Date Received: 12/16/04 Date Extracted: 12/20/04 13:00 Sample ID: 29WL32-MH01 Date Analyzed: 12/20/04 19:53 Lab Samp ID: L128-11 Dilution Factor: 1 Lab File ID: XL20007A Matrix : WATER Ext Btch ID: EXLOO4W % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL20003A 

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
нмх	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	240E	1	.2
4-AM-2,6-DNT	34E	1	.2
2-AM-4,6-DNT	17E	1	.2
2,6-DNT	4.1	1	.2
2,4-DNT	17E	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	~ i	.2
4-NITROTOLUENE	ND	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

3,4-DINITROTOLUENE 90 63-143

Client :	SHAW E&I	Date Collected:	12/15/04	
	LONGHORN ARMY AMMUNITION PLANT	Date Received:	12/16/04	
Batch No. :	04L128	Date Extracted:	12/20/04 13:00	
Sample ID:	29WL32-MH01DL1	Date Analyzed:	12/21/04 13:15	
Lab Samp ID:	L128-11T	Dilution Factor:	5	
Lab File ID:	XL21004A	Matrix :	WATER	1
Ext Btch ID:	EXL004W	% Moisture :	NA	
Calib. Ref.:	XL21002A	Instrument ID :	T-081	
			the state of the s	

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
HMX	ND	5	1
RDX	ND	5	1
1,3,5-TNB	ND	5	1
1,3-DNB	ND	5	1
TETRYL	ND	5	1
NITROBENZENE	ND	5	1
2,4,6-TNT	240E	5	1
4-AM-2,6-DNT	33	5	1
2-AM-4,6-DNT	16	5	1
2,6-DNT	2.7J	5	1
2,4-DNT	15	5	1
2-NITROTOLUENE	ND	5	1
3-NITROTOLUENE	ND	´´ 5	1
4-NITROTOLUENE	ND	5	1

SURROGATE PARAMETERS	% RECOVERY	QC LIMIT
3,4-DINITROTOLUENE	84	63-143

Client : SHAW E&I Date Collected: 12/15/04 Date Received: 12/16/04

Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L128 Date Extracted: 12/20/04 13:00 Sample ID: 29WL32-MH01DL2 Date Analyzed: 12/21/04 12:46

Lab Samp ID: L128-11I Dilution Factor: 50 Lab File ID: XL21003A : WATER Matrix Ext Btch ID: EXLOO4W % Moisture : NA Calib. Ref.: XL21002A Instrument ID : T-081

______

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
HMX	ND	50	10
RDX	ND	50	10
1,3,5-TNB	ND	50	10
1,3-DNB	ND	50	10
TETRYL	ND	50	10
NITROBENZENE	ND	50	10
2,4,6-TNT	250	50	10
4-AM-2,6-DNT	36J	50	10
2-AM-4,6-DNT	17J	50	10
2,6-DNT	ND	50	10
2,4-DNT	15J	50	10
2-NITROTOLUENE	ND	50	10
3-NITROTOLUENE	ND	[~] 50	10
4-NITROTOLUENE	ND	50	10

SURROGATE PARAMETERS % RECOVERY QC LIMIT -------------3,4-DINITROTOLUENE DO 63-143

Note: All positive results are confirmed by CN column

DO : Diluted out

Client :	SHAW E&I	Date Collected:	12/15/04	
Project :	LONGHORN ARMY AMMUNITION PLANT	Date Received:	12/16/04	
Batch No. :	04L128	Date Extracted:	12/20/04 13:00	
Sample ID:		Date Analyzed:	12/20/04 20:22	
Lab Samp ID:		Dilution Factor:	1	
Lab File ID:		Matrix :	WATER	
Ext Btch ID:		% Moisture :	NA	a
Calib. Ref.:	XL20003A	Instrument ID :	T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
нмх	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	.93J	1	.2
4-AM-2,6-DNT	6.1	1	.2
2-AM-4,6-DNT	3.4	1	.2
2,6-DNT	ND	1	.2
2,4-DNT	ND	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	ຶ 1	.2
4-NITROTOLUENE	ND	1	.2

SURROGATE PARAMETERS	% RECOVERY	QC LIMIT
3,4-DINITROTOLUENE	95	63-143

Note: All positive results are confirmed by CN column  $\frac{1}{2}$ 

# QC SUMMARIES

Client :	SHAW E&I	Date Collected: N	A Î
	LONGHORN ARMY AMMUNITION PLANT	Date Received: 1	2/20/04
Batch No. :	04L128	Date Extracted: 1	2/20/04 13:00
Sample ID:	MBLK1W	Date Analyzed: 1	2/20/04 18:27
Lab Samp ID:	EXL004WB	Dilution Factor: 1	
Lab File ID:	XL20004A	Matrix : W	ATER 🗻
Ext Btch ID:	EXL004W	% Moisture : N	A
Calib. Ref.:	XL20003A	Instrument ID : T	-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
HMX	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	ND	1	.2
4-AM-2,6-DNT	ND	1	.2
2-AM-4,6-DNT	ND	1	.2
2,6-DNT	ND	1	.2
2,4-DNT	ND	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	~ i	.2
4-NITROTOLUENE	ND	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

100

63-143

Note: All positive results are confirmed by CN column

3,4-DINITROTOLUENE

### EMAX QUALITY CONTROL DATA LCS/LCD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.: METHOD:

04L128 EPA 8330

MATRIX: DILUTION FACTOR: 1

WATER

MBLK1W

1

% MOISTURE:

NA

LAB SAMP ID: LAB FILE ID:

SAMPLE ID:

EXL004WB

XL20004A

EXL004WL XL20005A

EXL004WC XL20006A

DATE EXTRACTED: 12/20/0413:00 12/20/0413:00 12/20/0413:00

DATE COLLECTED: NA

DATE ANALYZED: PREP. BATCH:

EXL004W

12/20/0418:27 12/20/0418:56 12/20/0419:24 EXL004W

EXL004W

DATE RECEIVED: 12/20/04

CALIB. REF:

XL20003A

XL20003A /

XL20003A

ACCESSION:

PARAMETER	BLNK RSLT (ug/L)	SPIKE AMT (ug/L)	BS RSLT (ug/L)	BS % REC	SPIKE AMT (ug/L)	BSD RSLT (ug/L)	BSD % REC	RPD (%)	QC LIMIT	MAX RPD
										,
HMX	ND	4	3.84	96	4	3.99	100	4	70-130	30
RDX	ND	4	3.31	83	4	3.19	v 80	4	60-130	30
1,3,5-TNB	ND	4	4.03	101	4	4.06	101	1	70-130	30
1,3-DNB	ND	4	3.85	96	4	3.86	96	0	70-130	30
Tetryl	ND	4	4.08	102	4	4.1	102	0	50-140	30
Nitrobenzene	ND	4	3.62	90	4	3.64	91	1	60-130	30
2,4,6-TNT	ND	4	4.18	105	4	4.22	105	1	70-140	30
4-AM-2,6-DNT	ND	4	3.92	98	4	3.92	98	0	70-130	30
2-AM-4,6-DNT	ND	4	4.01	100	4	4.04	101	1	70-130	30
2,6-DNT	ND	4	4.03	101	4	4.07	102	1	70-130	30
2,4-DNT	ND	4	4.13	103	4	4.12	103	0	70-130	30
2-Nitrotoluene	ND	4	3.81	95	4	3.81	95	0	70-130	30
3-Nitrotoluene	ND	4	3.99	< 100	4	4.02	100	1	70-130	30
4-Nitrotoluene	ND	4	4.02	100	4	4.07	102	1	70-130	30

<u>#</u>

<i>A</i>	SPIKE AMT	BS RSLT	BS	SPIKE AMT	BSD RSLT	BSD	QC LIMIT	
SURROGATE PARAMETER	(ug/L)	(ug/L)	% REC	(ug/L)	(ug/L)	% REC	(%)	
3,4-Dinitrotoluene	4	4.09	102	4	4.27	107	70-130	

Client : SHAW E&I	Date Collected: NA						
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/20/04						
Batch No. : 04L128	Date Extracted: 12/20/04 17:30						
Sample ID: MBLK1S	Date Analyzed: 12/21/04 17:34						
Lab Samp ID: EXLO05SB	Dilution Factor: 1						
Lab File ID: XL21013A	Matrix : SOIL						
Ext Btch ID: EXLO05S	% Moisture : NA						
Calib. Ref.: XL21012A	Instrument ID : T-081						

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
нмх	ND	400	200
RDX	ND ND	400	200
1,3,5-TNB	·		
* *	ND	400	200
1,3-DNB	ŅD	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	<b>~400</b>	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
7 / DINITROTOLUCUE	407	/7 6/7	
3,4-DINITROTOLUENE	103	63-143	

### EMAX QUALITY CONTROL DATA LCS ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L128 EPA 8330

METHOD: 

MATRIX: DILUTION FACTOR: 1 SAMPLE ID:

SOIL

MBLK1S

EXL005SB

EXL005SL XL21014A

1

LAB SAMP ID: LAB FILE ID:

XL21013A

DATE EXTRACTED: 12/20/0417:30 12/20/0417:30

% MOISTURE:

DATE COLLECTED: NA DATE RECEIVED: 12/20/04

DATE ANALYZED: 12/21/0417:34 12/21/0418:03 PREP. BATCH:

CALIB. REF:

EXL005S XL21012A EXL005S

XL21012A

ACCESSION:

PARAMETER	BLNK RSLT (ug/kg)	SPIKE AMT (ug/kg)	BS RSLT (ug/kg)	BS % REC	QC LIMIT
HMX	ND	2000	2110	106	70-140
RDX	ND	2000	2100	105	70-140
1,3,5-TNB	ND	2000	2180	109	70-130
1,3-DNB	ND	2000	2180	109	70-130
Tetryl	ND	2000	2080	104	60-140
Nitrobenzene	ND	2000	2190	109	70-130
2,4,6-TNT	ND	2000	2180	109	70-140
4-AM-2,6-DNT	ND	2000	2160	108	70-130
2-AM-4,6-DNT	ND	2000	2170	109	70-130
2,6-DNT	ND	2000	2120	106	70-140
2,4-DNT	ND	2000	2140	107	70-130
2-Nitrotoluene	ND	2000	2000	100	70-130
3-Nitrotoluene	ND	2000	2090	105	70-130
4-Nitrotoluene	ND	2000	2090	105	70-130

	SPIKE AMT	BS RSLT	BS	QC LIMIT
SURROGATE PARAMETER	(ug/kg)	(ug/kg)	% REC	(%)
			-:	
3.4-Dinitrotoluene	2000	2260	113	70-130

### EMAX QUALITY CONTROL DATA MS/MSD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

1

BATCH NO.: METHOD:

04L128 EPA 8330

MATRIX: DILUTION FACTOR: 1

SOIL

29SB85-002 L128-02

XL21016A

L128-02M XL21017A

DATE EXTRACTED: 12/20/0417:30 12/20/0417:30 12/20/0417:30 12/21/0419:01 12/21/0419:29

12/21/0419:58 EXL005s

DATE COLLECTED: 12/15/04 DATE RECEIVED: 12/16/04

% MOISTURE:

NΑ

CALIB. REF:

SAMPLE ID: LAB SAMP ID:

LAB FILE ID:

DATE ANALYZED:

PREP. BATCH: EXL005S

XL21012A

EXL005S XL21012A

XL21012A

L128-02S

XL21018A

1

ACCESSION:

PARAMETER	SMPL RSLT (ug/kg)	SPIKE AMT (ug/kg)	MS RSLT (ug/kg)	MS % REC	SPIKE AMT (ug/kg)	MSD RSLT (ug/kg)	MSD % REC	RPD (%)	QC LIMIT	MAX RPD (%)
HMX	ND	2000	2250	113	2000	2170	108	4	63-154	50
RDX	ND	2000	1770	88	2000	1760	88	0	63-154	50
1,3,5-TNB	ND	2000	2160	108	2000	2070	104	4	63-143	50
1,3-DNB	ND	2000	2130	107	2000	2130	106	0	63-143	50
Tetryl	ND	2000	2040	102	2000	1960	98	4	54-154	50
Nitrobenzene	ND	2000	2110	105	2000	1980	99	6	63-143	50
2,4,6-TNT	ND	2000	2120	106	2000	2050	102	3	63-154	50
4-AM-2,6-DNT	300J	2000	2400	105	2000	2270	99	6	63-143	50
2-AM-4,6-DNT	900	2000	3130	111	2000	3010	105	4	63-143	50
2,6-DNT	ND	2000	2130	107	2000	2060	103	3	63-154	50
2,4-DNT	ND	2000	2160	108	2000	2130	106	2	63-143	50
2-Nitrotoluene	ND	2000	2000	100	2000	1890	95	5	63-143	50
3-Nitrotoluene	ND	2000	2030	102	2000	1980	99	3	63-143	50
4-Nitrotoluene	ND	2000	2050	102	2000	2040	102	1	63-143	50

SPIKE AMT MS RSLT MS SPIKE AMT MSD RSLT MSD QC LIMIT SURROGATE PARAMETER (ug/kg) (ug/kg) % REC (ug/kg) (ug/kg) % REC (%)

3,4-Dinitrotoluene

2000 2130

106

2000

1950

98

63-143

## INITIAL CALIBRATION

Lab Name : EMAX Inc Instrument ID : HPLC1 81

Instrument ID : HPLC1 81
GC Columm : VARIAN C18
Column size ID : 25CMX4.6MM
LFID & Datetime: XJ19016A 10/19/04 19:08
LFID & Datetime: XJ19017A 10/19/04 19:36
LFID & Datetime: XJ19013A 10/19/04 17:41
LFID & Datetime: XJ19015A 10/19/04 18:10
LFID & Datetime: XJ19015A 10/19/04 18:39
CONCLUNIT: Date

CONC UNIT: ppb

	CONC	CALI	BRATION FA	ACTORS (A	REA or HE	IGHT)/UNI	T	Ī
COMPOUND	Х	1.00X	5.00x	10.00X	20.00X	40.00X	MEAN	%RSD
		=======		1			=======	====
HMX	20.00				72.87	71.66	70.79	3.1
RDX	20.00	80.55	89.55	93.32	92.82	91.48	89.54	5.8
1,3,5-TNB	20.00	212.60	206.29	208.40	210.28	208.06	209.13	1.1
1,3-DNB	20.00	284.05	289.17	293.78	291,57	290.36	289.79	1.3
Tetryl	20.00		165.60	171.93	171.00	171.53	169.94	1.5
Nitrobenzene	20.00	196.75	195.67	202.54	203.55	201.64	200.03	1.8
2,4,6-TNT	20.00	206.40	200.92	203.90	208,44	205.06	204.94	1.4
4-AM-2,6-DNT	20.00	156.75	144.28	146.21	146.58	146.43	148.05	3.3
2-AM-4,6-DNT	20.00	229.95	205.98	210.31	215.07	216.25	215.51	4.2
2,6-DNT	20.00	137.60	131.99	135.36	140.29	135.29	136.11	2.3
2,4-DNT	20.00	276.20	270.64	273.11	277.46	281.68	275.82	1.5
2-Nitrotoluene	20.00	130.40	127.75	127.93	129.28	128.10	128.69	0.9
4-Nitrotoluene	20.00	104.40	103.10	107.11	109.25	110.43	106.86	2.9
3-Nitrotoluene	20.00	132.95	130.43	138.71	137.68	140.89	136.13	3.2
SURROGATE	X	1.00x	5.00x	10.00x		40.00x	MEAN	%RSD
3,4-Dinitrotoluene	20.00	1	1	124.62		1	123.33	į.

EX81J19.MET

Lab Name : EMAX Inc Instrument ID : HPLC1 81 GC Columm : VARIAN C18 Column size ID : 25CMX4.6MM

LFID & Datetime: XJ19016A 10/19/04 19:08 LFID & Datetime: XJ19017A 10/19/04 19:36 LFID & Datetime: XJ19013A 10/19/04 17:41 LFID & Datetime: XJ19014A 10/19/04 18:10 LFID & Datetime: XJ19015A 10/19/04 18:39

		RT OF S	TANDAR	S (MI)	1)	MEAN	RT W	MOOM	RTWINDOW
COMPOUND	1.0X	5.0X	10.0X	20.0X	40.0X	RT	FROM	TO	WIDTH
	=====	=====	=====	=====		=====	=====	=====	
HMX	4.300	4.292	4.292	4.292	4.275	4.290	4.240	4.340	0.050
RDX	6.433	6.383	6.367	6.375	6.333	6.378	6.240	6.516	0.138
1,3,5-TNB	8.650	8.617	8.600	8.633	8.575	8.615	8.462	8.768	0.153
1,3-DNB	10.492	10.450	10.417	10.483	10.400	10.448	10.219	10.677	0.229
Tetryl	11.358	11.308	11.250	11.342	11.250	11.302	11.014	11.590	0.288
Nitrobenzene	12.117	12.092	12.042	12.108	12.033	12.078	11.677	12.479	0.401
2,4,6-TNT	13.675	13.642	13.567	13.642	13.575	13.620	13.219	14.021	0.401
4-AM-2,6-DNT	14.433	14.392	14.292	14.383	14.308	14.362	13.857	14.867	0.505
2-AM-4,6-DNT	14.967	14.983	14.867	14.950	14.883	14.930	14.382	15.478	0.548
2,6-DNT	15.817	15.825	15.742	15.800	15.758	15.788	15.325	16.251	0.463
2,4-DNT				16.367					0.477
2-Nitrotoluene	19.467	19.525	19.442	19.458	19.467	19.472	18.881	20.063	0.591
4-Nitrotoluene	21.192	21.225	21.150	21.175	21.142	21.177	20.520	21.834	0.657
3-Nitrotoluene	22.658	22.717	22.592	22.633	22.600	22.640	21.888	23.392	0.752
SURROGATE	1.0X					***	FROM	TO	WIDTH
	T=====		1	=====	1	ı	222526	1	=======
3,4-Dinitrotoluene	12.900	12.858	12.792	12.875	12.792	12.843	12.468	13.218	0.375
	l			l			l	l	I

EX81J19.MET

Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column

: VARIAN C18

Column size ID

: 25CMX4.6MM

Conc Cont LFID & Datetime: XJ19018A 10/19/2004 20:05

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

CONC UNIT

: ppb

	RT	RT W	MDOM	TRUE	AVERAGE	RESL	JLT	:		%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	=  ======	======	======		========				==	=====
нмх	_  4.300					31158	440.13	10	[	15
RDX	_ 6.400	6.262	6.538	400.0	89.500	38533	430.32	8	1	15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	91920	439.54	10		15
1,3-DNB	_ 10.483	10.254	10.712	400.0	289.800	127403	439.64	10		15
Tetryl	11.342	11.054	11.630	400.0	169.900	71202	418.98	5	l	15
Nitrobenzene	12.108	11.707	12.509	400.0	200.000	86805	433.96	8		15
2,4,6-TNT	13.625	13.224	14.026	400.0	204.900	88599	432.31	.8		15
4-AM-2,6-DNT	14.400	13.895	14.905	400.0	148.100	60914	411.44	3	l	15
2-AM-4,6-DNT	14.950	14.402	15.498	400.0	215.500	91200	423.18	6		15
2,6-DNT	15.800	15.337	16.263	400.0	136.100	56248	413.27	3	1	15
2,4-DNT	16.383	15.906	16.860	400.0	275.800	117421	425.72	6	l	15
2-Nitrotoluene	19.475	18.884	20.066	400.0	128.700	53460	415.40	4.		15
4-Nitrotoluene	21.192	20.535	21.849	400.0	106.900	1 .	435.89	9	1	15
3-Nitrotoluene	22.667	21.915	23.419	400.0	136.100		422.93	6	l	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
					========			=====	==	=====
3,4-Dinitrotoluene	_ 12.875	12.500	13.250	400.0	123.300	52174	423.04	6	ľ	15
		<u> </u>			<u> </u>	l		l	I	-

EX81J19.MET

### ANALYSIS RUN LOG FOR HPLC

SOP D EMAX-8330 Rev. No: 2 D EMAX-8310 Rev. No: 4 D EMAX-8332 Rev. No: 0 D

Book # A81-02-005

	Preparation		Data	T			T	Ma	ıtrix	T				T
	Batch		File Name		Lab San	iple ID	DF	(W)		Notes	•	I	nstrument Number	81
		X1	19.001	TE	6t							INIT	IAL CALIBRATION REFERE	ENCE
		ļ.,	2				<u> </u>						or the second	
		-	3								and the same of th	Date	10/19/04	
		-	4	1-1			-					Method	EX81719	
			5	+			1	<u> </u>				Mid Point	XJ19014A (4/5)	
<u> </u>		<del>                                     </del>	6				-					ICAL ID		(800ppb
NA.		+	7			THE STATE OF THE S	<b> </b>					ICV ID	SHIB-03-36-2	(10ppm)
LYT	***		9				1					DCC ID		· · · · · · · · · · · · · · · · · · ·
ANALYTICAL			10	IB	81 TG14	<del></del>	1							
LB	RIA		l (		3171901	20				) Alofevalu	rated			
BATCH			12		02	100				] RF Shifted	)			<del>~</del>
Œ			13		03	200				7			Solvents ID	
1			14		04	doo				8330 I	cal	Acetonitrile		
			15	ļ	05	8 <i>0</i> 0				(Primary	col.)	Methanol	43206332	
Z			16		01	20						Water	43189	
*			17		02	100								
	<u> </u>		18	IEX	BIJ1901	400				J			Electronic Data Archival	<del></del>
													Location	Date
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		<u> </u>										Comments:	Samples disposed off	- 10/20/0
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			***************************************		<del>/</del>	XP 10/19/0	Ų						vice and the second	
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										<u></u>		Analyzed By:	KP.	
								_		**************************************		I Mary 200 Dy.	PT.	
										······································		· •	This page is checked during the data	neview nro

BM4XLaboratories, Inc. 1835 W. 205th St. Tourside, CA 90501

Lab Name : EMAX Inc Instrument ID : HPLC1 LCT001(T017) GC Columm : LUNA 5U PHENYL-HEXYL Column size ID : 25CMX4.6MM

LFID & Datetime: PH17007A 08/17/04 16:21 LFID & Datetime: PH17003A 08/17/04 13:35 LFID & Datetime: PH17004A 08/17/04 14:16 LFID & Datetime: PH17005A 08/17/04 14:58 LFID & Datetime: PH17006A 08/17/04 15:39

CONC UNIT: ppb

	CONC	CALIE	BRATION FA	CTORS (/	AREA or HE	IGHT)/UN	ΙΤ	Ī
COMPOUND	X	1.00X						%RSD
	=======				=======	=======		====
HMX	20.00	265.05	223.86	243.86	247.42	244.74	244.99	6.0
RDX	20.00	315.15	255.37	260.41	253.93	258.37	268.65	9.7
Nitrobenzene	20.00	359.70	349.71	329.86	323.97	326.71	337.99	4.7
1,3-DNB	20.00	514.05	508.34	520.54	516.70	515.48	515.02	0.9
2-Nitrotoluene	20.00	238.50	278.15	281.94	287.52	281.20	273.46	7.3
4-Nitrotoluene	20.00	287.00	275.75	289.34	288.21	284.04	284.87	1.9
4-AM-2,6-DNT	20.00	276.50	256.61	256.86	264.78	254.15	261.78	3.5
3-Nitrotoluene	20.00	353.75	380.73	345.64	344.94	337.55	352.52	4.8
2-AM-4,6-DNT	20.00	464.60	447.94	400.02	400.57	393.79	421.38	7.7
1,3,5-TNB	20.00	368.85	364.11	349.42	354.06	340.07	355.30	3.2
2,6-DNT	20.00	258.20	256.25	261.51	248.39	253.99	255.67	1.9
2,4-DNT	20.00	433.50	511.11	524.55	509.46	513.54	498.43	7.4
Tetryl	20.00	511.65	504.42	558.66	520.24	525.23	524.04	4.0
2,4,6-TNT	20.00	421.55	507.22	574.38	536.85	548.40	517.68	11.4
SURROGATE	Х	1.00X	1	10.00X				%RSD
3,4-DNT	20.00	288.40	260.85	245.15	244.29	241.54	1 .	ì

EX17H17C.MET

Lab Name : EMAX Inc

Lab Name : EMAX ITC
Instrument ID : HPLC1 LCT001(T017)
GC Columm : LUNA 5U PHENYL-HEXYL

Column size ID : 25CMX4.6MM

LFID & Datetime: PH17007A 08/17/04 16:21 LFID & Datetime: PH17003A 08/17/04 13:35 LFID & Datetime: PH17004A 08/17/04 14:16 LFID & Datetime: PH17005A 08/17/04 14:58 LFID & Datetime: PH17006A 08/17/04 15:39

		RT OF S	STANDARI	OS (MI	V)	MEAN	RT W	MOOM	RTWINDOW
COMPOUND	1.0x	5.0X	10.0X	20.0X	40.0X	RT	FROM	то	WIDTH
	=====	=====		=====	=====	=====	=====	=====	=======
HMX	6.025	6.050	6.042	6.058	6.033	6.042	5.962	6.122	0.080
RDX	7.800	7.817	7.817	7.833	7.792	7.812	7.708	7.916	0.104
Nitrobenzene	10.633	10.675	10.667	10.692	10.633	10.660	10.556	10.764	0.104
1,3-DNB	15.183	15.258	15.258	15.292	15.175	15.233	14.872	15.594	0.361
2-Nitrotoluene							15.497		
4-Nitrotoluene	16.225	16.342	16.342	16.375	16.258	16.308	16.018	16.598	0.290
4-AM-2,6-DNT	16.950	17.108	17.108	17.150	17.000	17.063	16.500	17.626	0.563
3-Nitrotoluene	17.700	17.800	17.775	17.825	17.700	17.760	17.393	18.127	0.367
2-AM-4,6-DNT	18.925	19.125	19.125	19.175	19.025	19.075	18.317	19.833	0.758
1,3,5-TNB	20.142	20.267	20.267	20.317	20.200	20.239	19.626	20.852	0.613
2,6-DNT	21.517	21.642	21.650	21.683	21.558	21.610	20.886	22.334	0.724
2,4-DNT	22.733	22.825	22.892	22.942	22.800	22.838	22.041	23.635	0.797
Tetryl	31.667	31.808	31.850	31.875	31.617	31.763	30.113	33.413	1.650
2,4,6-TNT	33.233	33.367	33.358	33.375	33.150	33.297	31.954	34.640	1.343
**********************	-,,-								
SURROGATE	1.0x	5.0X	10.0X	20.0x	40.0X	RT	FROM	то	WIDTH
			=====		======	=====		=====	=======
3,4-DNT	18.492	18.650	18.600	18.675	18.525	18.588	18.055	19.121	0.533

EX17H17C.MET

### DAILY CALIBRATION

Lab Name Instrument ID : EMAX

Instrument ID GC Column : HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL20003A 12/20/2004 17:58

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======				========	======	=======	=====	==	=====
HMX	4.292	4.242	4.342	400.0		28461	402.03	1		15
RDX	6.300	6.162	6.438	400.0	89.500	35641	398.02	-0		15
1,3,5-TNB	8,500	8.347	8.653	400.0	209.100	83199	397.84	-1	İ	15
1,3-DNB	10.250	10.021	10.479	400.0	289.800	115929	400.05	0		15
Tetryl	11.000	10.712	11.288	400.0	169.900	68123	400.86	0		15
Nitrobenzene	11.792	11.391	12.193	400.0	200.000	80732	403.60	1	İ	15
2,4,6-TNT	13.300	12.899	13.701	400.0	204.900	80648	393.51	-2		15
4-AM-2,6-DNT	13.875	13.370	14.380	400.0	148.100	60372	407.78	2	İ	15
2-AM-4,6-DNT	14.408	13.860	14.956	400.0	215.500	86596	401.82	0	ĺ	15
2,6-DNT	15.358	14.895	15.821	400.0	136.100	55446	407.37	2	İ	15
2,4-DNT	15.908	15.431	16.385	400.0	275.800	111329	403.63	1 1	İ	15
2-Nitrotoluene	18.875	18.284	19.466	400.0	128.700	51626	401.15	0		15
4-Nitrotoluene	20.425	19.768	21.082	400.0	106.900	45124	422.27	6	:	15
3-Nitrotoluene	21.842	21.090	22.594	400.0	136.100	57301	420.92	5	ĺ	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	_======					=======		======	==	_=====
3,4-Dinitrotoluene	12.517	12.142	12.892	400.0	123.300	50724	411.28	3		15
			<u> </u>	<u> </u>	<u> </u>		l. <del></del>	<u> </u>	<u> </u>	

Lab Name Instrument ID : EMAX

Instrument ID GC Column : HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL20015A 12/20/2004 23:44

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT		Ì	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======			=======	======	=====	==	=====
HMX	4.333	4.283	4.383	400.0	70.800	29272	413.49	3		15
RDX	6.408	6.270	6.546	400.0	89.500	38105	425.54	6		15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	85122	407.03	2	İ	15
1,3-DNB	10.467	10.238	10.696	400.0	289.800	119721	413.14	3		15
Tetryl	11.275	10.987	11.563	400.0	169.900	69968	411.72	3	İ	15
Nitrobenzene	12.042	11.641	12.443	400.0	200.000	82996	414.92	4	Ì	15
2,4,6-TNT	13.592	13.191	13.993	400.0	204.900	84236	411.02	.3	Ì	15
4-AM-2,6-DNT	14.333	13.828	14.838	400.0	148.100	61879	417.96	4	Ì	15
2-AM-4,6-DNT	14.875	14.327	15.423	400.0	215.500	87276	404.97	1		15
2,6-DNT	15.750	15.287	16.213	400.0	136.100	57777	424.50	6	İ	15
2,4-DNT	16.325	15.848	16.802	400.0	275.800	113421	411.21	3		15
2-Nitrotoluene	19.358	18.767	19.949	400.0	128.700	52495	407.90	2		15
4-Nitrotoluene	20.983	20.326	21.640	400.0	106.900	46819	438.13	10	l	15
3-Nitrotoluene	22.450	21.698	23.202	400.0	136.100	57711	423.93	6		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	========			=====	==	=====
3,4-Dinitrotoluene	12.850	12.475	13.225	400.0	123.300	51463	417.27	4		15

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XL21002A 12/21/2004 12:17 CONC UNIT

1	RT	RT W	MDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======		=======	=======	=======	=====	==	
HMX	4.308	4.258	4.358	400.0	70.800	28235	398.84	-0		15
RDX	6.342	6.204	6.480	400.0	89.500	36063	402.74	1		15
1,3,5-TNB	8.550	8.397	8.703	400.0	209.100	82108	392.62	-2	l	15
1,3-DNB	10.325	10.096	10.554	400.0	289.800	115534	398.69	-0	۱.	15
Tetryl	11.108	10.820	11.396	400.0	169.900	67938	399.77	-0		15
Nitrobenzene	11.875	11.474	12.276	400.0	200.000	79947	399.67	-0	İ	15
2,4,6-TNT	13.400	12.999	13.801	400.0	204.900	80421	392.40	-2	İ	15
4-AM-2,6-DNT	14.033	13.528	14.538	400.0	148.100	59823	404.07	1	İ	15
2-AM-4,6-DNT	14.558	14.010	15.106	400.0	215.500	84462	391.91	-2		15
2,6-DNT	15.492	15.029	15.955	400.0	136.100	54767	402.38	1		15
2,4-DNT	16.033	15.556	16.510	400.0	275.800	110265	399.77	-0	i	15
2-Nitrotoluene	19.008	18.417	19.599	400.0	128.700	51046	396.64	-1	İ	15
4-Nitrotoluene	20.592	19.935	21.249	400.0	106.900	45322	424.12	6	İ	15
3-Nitrotoluene	22.008	21.256	22.760	400.0	136.100	56862	417.70	4	İ	15
									[ <b></b> :	
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
			======	======	=======	=======	=======		==	=====
3,4-Dinitrotoluene	12.633	12.258	13.008	400.0	123.300	49767	403.52	1		15

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XL21012A 12/21/2004 17:05

	RT	RT W	NDOW	TRUE	AVERAGE	RESULT				%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======			======			=======	=====	==	=====
HMX	4.300	4.250	4.350	400.0	70.800	28637	404.52	1	1	15
RDX	6.325	6.187	6.463	400.0	89.500	35492	396.36	- 1	1	15
1,3,5-TNB	8.525	8.372	8.678	400.0	209.100	83787	400.65	0	1	15
1,3-DNB	10.283	10.054	10.512	400.0	289.800	116602	402.37	1	1	15
Tetryl	11.033	10.745	11.321	400.0	169.900	68756	404.58	1	į	15
Nitrobenzene	11.833	11.432	12.234	400.0	200.000	81307	406.47	2	i	15
2,4,6-TNT	13.350	12.949	13.751	400.0	204.900	80995	395.20	-1	1	15
4-AM-2,6-DNT	13.925	13.420	14.430	400.0	148.100	61989	418.70	5	l	15
2-AM-4,6-DNT	14.442	13.894	14.990	400.0	215.500	85780	398.03	-0	Ì	15
2,6-DNT	15.417	14.954	15.880	400.0	136.100	55335	406.56	2	1	15
2,4-DNT	15.950	15.473	16.427	400.0	275.800	111179	403.09	1	İ	15
2-Nitrotoluene	18.933	18.342	19.524	400.0	128.700	51488	400.08	i o	l	15
4-Nitrotoluene	20.508	19.851	21.165	400.0	106.900	44634	417.68	4	ĺ	15
3-Nitrotoluene	21.917	21.165	22.669	400.0	136.100	57110	419.52	5	l	15
SURROGATE	MINUTES	FROM	то	TRUECON	C'F	AREA	CONC	%D	QL	LIMITS
7 / Dividental cons	43 575	43 300	42 050		403 700	54457	/4/ 70	=====	==	======
3,4-Dinitrotoluene	12.575	12.200	12.950	400.0	123.300	51157	414.79	4		15

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM

Conc Cont LFID & Datetime: XL21021A 12/21/2004 21:25

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE					%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	=======	======	=======			=====	==	=====
IMX	4.333	4.283	4.383	400.0	70.800	29529	417.12	4.	l	15
RDX	6.408	6.270	6.546	400.0	89.500	36651	409.30	2	İ	15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	83931	401.34	0	İ	15
1,3-DNB	10.458	10.229	10.687	400.0	289.800	118138	407.67	2		15
Tetryl	11.258	10.970	11.546	400.0	169.900	68631	403.85	1		15
litrobenzene	12.033	11.632	12.434	400.0	200.000	81515	407.51	2		15
2,4,6-TNT	13.583	13.182	13.984	400.0	204.900	82418	402.15	1	İ	15
4-AM-2,6-DNT	14.300	13.795	14.805	400.0	148.100	60872	411.15	3	l	15
2-AM-4,6-DNT	14.850	14.302	15.398	400.0	215.500	85539	396.91	-1		15
2,6-DNT	15.733	15.270	16.196	400.0	136.100	56026	411.63	3	İ	15
2,4-DNT	16.308	15.831	16.785	400.0	275.800	111103	402.81	1	1	15
2-Nitrotoluene	19.342	18.751	19.933	400.0	128.700	52850	410.66	3	Ι.	15
4-Nitrotoluene	20.992	20.335	21.649	400.0	106.900	43058	402.94	1		15
3-Nitrotoluene	22.442	21.690	23.194	400.0	136.100	56680	416.36	4		15
SURROGATE	MINUTES	FROM	ТО	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
3,4-Dinitrotoluene	12.833	12.458	13.208	400.0	123.300	50526	409.68	2	==	1:

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XL21030A 12/22/2004 01:44
IC UNIT : ppb

CONC UNIT

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COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======		======		=======	=======	======	=====	==	=====
HMX	4.358	4.308	4.408	400.0	70.800	28761	406.27	2	1	15
RDX	6.475	6.337	6.613	400.0	89.500	36851	411.54	3		15
1,3,5-TNB	8.717	8.564	8.870	400.0	209.100	85213	407.47	2		15
1,3-DNB	10.583	10.354	10.812	400.0	289.800	118482	408.86	2		15
Tetryl	11.425	11.137	11.713	400.0	169.900	68419	402.60	1		15
Nitrobenzene	12.183	11.782	12.584	400.0	200.000	82651	413.19	3		15
2,4,6-TNT	13.758	13.357	14.159	400.0	204.900	84235	411.01	3		15
4-AM-2,6-DNT	14.583	14.078	15.088	400.0	148.100	60816	410.78	3	ĺ	15
2-AM-4,6-DNT	15.158	14.610	15.706	400.0	215.500	86030	399.19	-0		15
2,6-DNT	15.992	15.529	16.455	400.0	136.100	57301	421.00	5		15
2,4-DNT	16.567	16.090	17.044	400.0	275.800	111937	405.83	1	1	15
2-Nitrotoluene	19.650	19.059	20.241	400.0	128.700	51783	402.37	1	İ	15
4-Nitrotoluene	21.333	20.676	21.990	400.0	106.900	44795	419.19	5		15
3-Nitrotoluene	22.808	22.056	23.560	400.0	136.100	55798	409.88	2		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
3,4-Dinitrotoluene	13.025	12.650	13.400	400.0	123.300	50569	410.02	3	==	15
3,4-Dinitrotoluene	13.025	12.650	13.400	400.0	123.300	50569	410.02	3	MANAGE AND ADDRESS OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY	

Lab Name

: EMAX

Instrument ID GC Column

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL21002A 12/21/2004 14:29

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESL	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======		=====					=====	==	=====
HMX	6.125	6.045	6.205	400.0			397.31	-1	1	15
RDX	7.933	7.829	8.037			100692	374.81	-6		15
Nitrobenzene	10.725	10.621	10.829	400.0	338.000	131155	388.04	-3	Ì	15
1,3-DNB	15.442	15.081	15.803	400.0	515.000	191677	372.17	-7		15
2-Nitrotoluene	15.850	15.590	16.110	400.0	273.500	107744	394.00	-2		15
4-Nitrotoluene	16.450	16.160	16.740	400.0	284.900	117212	411.46	3	l	15
4-AM-2,6-DNT	17.433	16.870	17.996	400.0	261.800	89732	342.78	-14		15
3-Nitrotoluene	17.883	17.516	18.250	400.0	352.500	145090	411.58	3	l	15
2-AM-4,6-DNT	19.600	18.842	20.358	400.0	421.400	157332	373.37	-7	i -	15
1,3,5-TNB	20.467	19.854	21.080	400.0	355.300	135909	382.52	-4	1	15
2,6-DNT	21.867	21.143	22.591	400.0	255.700	96515	377.50	-6		15
2,4-DNT	23.225	22.428	24.022	400.0	498.400	200257	401.77	0	1	15
Tetryl	32.650	31.000	34.300	400.0	524.000	188547	359.79	-10	İ	15
2,4,6-TNT	33.833	32.490	35.176	400.0	517.700	227459	439.38	10		15
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SURROGATE	MINUTES	FROM	ТО	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
3,4-DNT	18.908	18.375	19.441	400.0	256.000	92885	362.77	-9	==	15
	-								ابدا]

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

GC Column Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL21013A 12/21/2004 22:06 IC UNIT : ppb

CONC UNIT

	RT	RT W	MDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	=======			======	========	=======	======	=====	==	=====
HMX	6.200		6.280				4			15
RDX	8.042	7.938	8.146			100724		_		15
Nitrobenzene	10.883	10.779	10.987	400.0	338.000	129845	384.17			15
1,3-DNB	15.733	15.372	16.094	400.0	515.000	200479	389.26	-3	1	15
2-Nitrotoluene	16.150	15.890	16.410	400.0	273.500	105320	385.14	-4.	1	15
4-Nitrotoluene	16.767	16.477	17.057	400.0	284.900	119340	418.93	5		15
4-AM-2,6-DNT	18.058	17.495	18.621	400.0	261.800	93293	356.38	-11		15
3-Nitrotoluene	18.250	17.883	18.617	400.0	352.500	142248	403.51	1	İ	15
2-AM-4,6-DNT	20.108	19.350	20.866	400.0	421.400	160422	380.70	-5	ļ	15
1,3,5-TNB	20.933	20.320	21.546	400.0	355.300	139700	393.19	-2		15
2,6-DNT	22.450	21.726	23.174	400.0	255.700	98773	386.33	-3	İ	15
2,4-DNT	23.783	22.986	24.580	400.0	498.400	207335	415.97	4	Ι.	15
Tetryl	33.750	32.100	35.400	400.0	524.000	184486	352.04	-12	l	15
2,4,6-TNT	34.808	33.465	36.151	400.0	517.700	238090	459.92	15	l	15
SURROGATE	MINUTES	FROM	ТО	TRUECON	CF	AREA	CONC	%D		LIMITS
3,4-DNT	19.358	18.825	19.891	400.0	256.000	93389	364.74	-9	==	1:
3,4-DNT	19.358	18.825	19.891	400.0	256.000	93389	364.74	-9	_	

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017)

GC Column : LUNA 5U PHENYL-HEXYL
Column size ID : 25CMX4.6MM
Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL23002A 12/23/2004 13:31

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESI	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
*********************	======		*** *** *** *** *** *** ***			=======	======		==	=====
HMX	6.150	6.070	6.230	400.0	245.000	96411	393.54			15
RDX	7.975	7.871	8.079	400.0	268.600	99473	370.27	-7		15
Nitrobenzene	10.817	10.713	10.921	400.0	338.000	128532	380.28	-5		15
1,3-DNB	15.583	15.222	15.944	400.0	515.000	188524	366.05	-8		15
2-Nitrotoluene	16.017	15.757	16.277	400.0	273.500	108923	398.31	-0		15
4-Nitrotoluene	16.600	16.310	16.890	400.0	284.900	114247	401.05	0		15
4-AM-2,6-DNT	17.642	17.079	18.205	400.0	261.800	91953	351.26	-12		15
3-Nitrotoluene	18.083	17.716	18.450	400.0	352.500	133535	378.80	-5		15
2-AM-4,6-DNT	19.750	18.992	20.508	400.0	421.400	149389	354.52	-11		15
1,3,5-TNB	20.700	20.087	21.313	400.0	355.300	127994	360.24	-10		15
2,6-DNT	22.158	21.434	22.882	400.0	255.700	88146	344.77	-14		15
2,4-DNT	23.458	22.661	24.255	400.0	498.400	195937	393.11	-2	İ	15
Tetryl	33.050	31.400	34.700	400.0	524.000	186616	356.11	-11	ĺ	15
2,4,6-TNT	34.250	32.907	35.593	400.0	517.700	227296	439.07	10	ĺ	15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
		======	======					=====		=====
3,4-DNT	19.067	18.534	19.600	400.0	256.000	88738	346.57	-13		15
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Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

GC Column

CONC UNIT

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COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======		========	=======		=====	==	=====
HMX	6.092	6.012	6.172	400.0	245.000	100956	412.09	3	l	15
RDX	7.892	7.788	7.996	400.0	268.600	106815	397.60	-1	İ	15
Nitrobenzene	10.725	10.621	10.829	400.0	338.000	137424	406.59	2	1	15
1,3-DNB	15.433	15.072	15.794	400.0	515.000	190308	369.52	-8	İ	15
2-Nitrotoluene	15.683	15.423	15.943	400.0	273.500	120478	440.57	10	İ	15
4-Nitrotoluene	16.433	16.143	16.723	400.0	284.900	131083	460.16	15	l	15
4-AM-2,6-DNT	17.467	16.904	18.030	400.0	261.800	89560	342.12	-14	İ	15
3-Nitrotoluene	17.933	17.566	18.300	400.0	352.500	156892	445.05	11	İ	15
2-AM-4,6-DNT	19.500	18.742	20.258	400.0	421.400	186947	443.65	11	İ	15
1,3,5-TNB	20.517	19.904	21.130	400.0	355.300	140781	396.23	-1	İ	15
2,6-DNT	21.958	21.234	22.682	400.0	255.700	100508	393.12	-2	İ	15
2,4-DNT	23.267	22.470	24.064	400.0	498.400	210136	421.59	5	l	15
Tetryl	32.625	30.975	34.275	400.0	524.000	197217	376.34	-6	l	15
2,4,6-TNT	33.950	32.607	35.293	400.0	517.700	237840	459.43	15	ĺ	15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======		======	======				=====	==	=====
3,4-DNT	18.925	18.392	19.458	400.0	256.000	77807	303.88	-24	*	15
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ANALYTICAL LOGS

6043

ANALYSIS RUN LOG FOR HPLC

ting Date:	12/20/04	Time: (り(のひ				g Date: 12/10/07	f Time: 2	3144	
Preparation Batch	Data File Name	Lab Sample ID		(W)	rix (S)	Notes	Ir	astrument Number	81
Daton	File Name 10) 2/2/04 XE XL20.001	TEST		(17)	(-)		INITI	AL CALIBRATION REFERE	NCE
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	3	CEX81J19664				800	Date	10/19/04	
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	5	1 L					Mid Point	XJ19074A (4/5))
	5	↓ e					ICAL ID		
:	7	OUL128-11				E	ICV ID		
	8	1 12					DCC ID	SHIC-03-54-2	
	9	046142-07				E			
EXLORIW	10	04145-01	V	 		Sat.			
	11	Ringe							
EXLORIN	12	046145-02	V	/		gat.			
10,000	13	Ringe						Solvents ID	
•	14						Acetonitrile		
3	15	CEX81779665				800	Methanol	43206332	
							Water	44168	
5									
22								Electronic Data Archival	
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							□ EZC_5_HPL	C	_
		XP 121	18752	,			D		
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ANALYSIS RUN LOG FOR HPLC

EMAX-8330 Rev. No: 2 □ EMAX-8310 Rev. No: 4 □ EMAX-8332 Rev. No: 0 □ SOP Book # A81-02-005

Startin	g Date:	12/21/04	Time:	ોા:48		Endin	g Date:	12/22/04	Time: Olic	1 4		
	Preparation Batch	Data File Name	Lab Sample ID	DF	Ma (W)	trix (S)		Notes	I	nstrument Number	81	
		XL21.001	IB81L666						INITI	INITIAL CALIBRATION REFERENCE		
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	EXLOUGU	3	O4L128-11I	50	V				Date	16/19/04	with the second second	
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		5	04445-01I	500				ر روز الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري الماري	Mid Point	XJ19014 A (4/8)	<i>)</i>	
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AL)		8	J 02 T	20		ļ			DCC ID	SHIC-03-54-Z		
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ANALYTICAL BATCH		10	+ 07T	10	1			·····				
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177		12	exx81719667				800					
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		14	+ L						Acetonitrile			
C									Methanol	43206332		
10		16	02						Water	44168		
XC21007A		17	0214								****	
1 4		18	025							Electronic Data Archival		
		19	1 03			V				Location	Date	
		10	IB						DEZC_5_HPLO			
		21	CEX81T19668				800		0			
	EXLOUSS	22	046128-04			V			Comments:	Samples disposed	N	
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		<u>₹ 30</u>	CEX81719669				800			This page is checked during the data r	eview process.	

 $m{J}$ MAXLaboratories, Inc. 1833 W. 20* St. Tombres, C45(15))

ANALYSIS RUN LOG FOR HPLC

Book # A17-010

Starting			Time: 13:47				2/21/04	Time: 27 ! C	TÇ	
	Preparation Batch	Data File Name	Lab Sample ID	DF		ntrix W	Notes	1	nstrument Number	17
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Ī	EXLOUGE	3	04L128-11T	5		V	hup. RR	met.	EX17H17C	
		¥	+ 11T	1			,	т.р	PH17005A (45)
		5	12	1						
		6	04L145-01T	20				<u> </u>	Standards	*
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ANALYTICAL BATCH		8	OZT	20			·	DCC ID	841C-03-54-Z	80 400
AL)		9	1 01	1						
		10	04L142-07T	10			3			
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r_{C}		1 13	Ex x17H17C695				800		Solvent ID	-
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PL9/002								Acetonitrile		
g.									Electronic Data Archival	
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									This page is checked during	the data review process.

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ANALYSIS RUN LOG FOR HPLC cony. SOP MEMAX-8350 Rev. No: 2 II EMAX-8310 Rev. No: 4 II EMAX-8332 Rev. No: 0 II Book # A17-010 Starting Date: 12/23/64 Time: 12:49 **Ending Date:** 12/24/04 02:5 Time: Data File Matrix Preparation Batch Lab Sample ID DF Notes **Instrument Number** 17 Name S W P [23 001 13176700 Initial Calibration CUX 17 H17 C700 Date 400 007 08/17/19 EXLOGS SEMALI 046128.03 met. CCA EX17417C -04 COOK PHITOURA m.p - OL bus ON Standards -67 Name TD 007 Conc. (µg/L) -10 ANALYTICAL DCC ID OOK SHIC-03 16-2 -0210 400 - U W (00)

	010	100 7 11 KBD
	oil	764
excoors	viz	046145-03

1013

ON

OLS

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018

019 020

4.021

- 05 -07

- 06

COXITHITCTOX

-0X - OL T

140 3

Location ERC. 5- APIC

12/27/0x/H

Date

Comments:

Methanol

Acetonitrile

Water

Analyzed By:

Solvent ID

Electronic Data Archival

43306 332

44168

Surpres disposed off 12/27 log &

NS

This page is checked during the data review process

MAXLABORATORIES, INC. 1815 W. 20th St. Todrame, CA 90501

BATCH

0

00

EXTRACTION LOGS

EXTRACTION LOG FOR EXPLOSIVES

Matrix:	,	-8330 Rev.No.: <u>3</u> = Start Date:	12/20/04	Time: /7:30	End Date	e: /2/2//04 Time:	//:00 B	ook # EEX-010
	Sample	Lab	Sample	Extract		Standards	D D	Amount Added (ml)
	Prep	Sample ID	Amount	Volume	Notes	Surrogate	54113-03-36-1	0.4
	ID		(g ml)	(ml)		LCS/MS	SHIB-03-36-2	0.4
	*01	EXL005-8B	2.00	20				
	*02	JV 12/20/4 SL	2.0/	20				
	*03	04L/28 -801	2.03	20		Reagent	Lot#/ID	
	*04	-02	2.01	20		Acetonitrile	43080	
	*05	- 02A	2.02	20		NaCl	· ·	
]	*06	-028	2.03	20		CaCl ₂	SP/B- e/ 4228924	1-267
	*07	- 03	2.01	20		Silica Sand	4228924	9
P	*08	- 04	2.00	20	3.			
REI	*09	- 05	2.03	20				
AR	*10	-06	2.03	20	r .			
PREPARATION BATCH:	*11	-07	2.02	20		SDG#	Extract Location	n
<u>Ş</u> ∣	*12	- 08	2.02	20				
BA	*13	- 09	2.01	2c			SEO4#1	
TC	*14	-10	2.02	20				
H:	*15	04/142 - 01	2.02	20		Comments:		
E	*16	- 02	2.00	20		-		
EXL	*17	- 03	2.01	20				
005-	*18	-04	2.03	20				
2-0	*19	- 05	2,03	20	A Company of the Comp			
	*20	- 06	2.02	20	-			
	*21							
	*22	12/20/04	! Jr			Prepared By:	Jr	
	*23					Standard Added By:	JV/YK	
1	*24				<u> </u>	MLIYU/07 Checked By:	YK-ML	
ŀ	*25				· · ·	Extract Received By:	Driver	· · · · · · · · · · · · · · · · · · ·
ľ	*26					Disposal Date:		

EXTRACTION LOG FOR EXPLOSIVES

SOP: Matrix:	WATE		12/20/04	Time: /3:00	End Dat	te: /2/20/04/ Time:	+4-15:30 Boo	ok#EEX-010
	Sample Prep ID	Lab Sample ID	Sample Amount (g ml)	Extract Volume (ml)	Notes	Standards Surrogate LCS/MS	SHIB-03-36-1 SHIB-03-36-2	Amount Added (ml) 6 · c g
	*01	EXLOOK - WB	200	4				
	*02	1 - WL	200	4				
	*03	· - WC	200	4		Reagent	Lot#/ID	
,	*04	04L128 - 11	200	4		Acetonitrile	13080	
	*05	+ -12	200	4		NaCl	SWIA- 02-14 SP/B-02-14	78
	*06	04 L 142 -07	200	4		CaCl ₂	SP/B-50-12/20/4	0/-267
	*07	04 L 145 - 01	200	4		Silica Sand	42289249	Jo 12/20/
Ę	*08	-02	200	4	3		A	
REI	*09							
AR	*10	Tr 12/	20/04		s .			
PREPARATION BATCH:	*11					SDG#	Extract Location	
NO N	*12							
BA	*13						SECH #1	
TC.	*14							
н:	*15					Comments:		
EXĹ	*16							
1.	*17							
-400	*18							
1-7	*19							
28	*20							
	*21							
	*22					Prepared By:	Jr.	
	*23		Andrewski and Andrewski and Andrewski and Andrewski and Andrewski and Andrewski and Andrewski and Andrewski and			Standard Added By:	JV/EG	
	*24					Checked By:	ML	<u></u>
	*25	,	anamanan da anaman da anaman da anaman da anaman da anaman da anaman da anaman da anaman da anaman da anaman da 			Extract Received By:		
İ	*26					Disposal Date:		

TABLE OF CONTENTS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L129

SECTION		PAGE
Cover Letter, CO	DC/Sample Receipt Form	1000 – 1005
GC/MS-VOA	**	2000 –
GC/MS-SVOA	**	3000 –
GC-VOA	**	4000 –
GC-SVOA	**	5000 –
HPLC	**	6000 –
METALS	**	7000 –
WET	METHOD 314.0	8000 – 8021
OTHERS	**	9000 –
HIRACO, CO.	the state of the s	the state of the s

^{** -} Not Requested



1835 W. 205th Street Torrance, CA 90501

Tel: (310) 618-8889 Fax: (310) 618-0818

Date: 01-07-2005 EMAX Batch No.: 04L129

Attn: Diane Meyer

Shaw E&I 1430 Enclave Parkway Houston TX 77077

Subject: Laboratory Report

Project: Longhorn Army Ammunition Plant

Enclosed is the Laboratory report for samples received on 12/16/04. The data reported include:

Control #	Col Date	Matrix	Analysis
L129-01	12/14/04	SOIL	PERCHLORATE BY IC
L129-02	12/14/04	SOIL	PERCHLORATE BY IC
L129-03	12/14/04	SOIL	PERCHLORATE BY IC
L129-04	12/14/04	SOIL	PERCHLORATE BY IC
L129-05	12/14/04	SOIL	PERCHLORATE BY IC
L129-06	12/14/04	SOIL	PERCHLORATE BY IC
L129-07	12/14/04	SOIL	PERCHLORATE BY IC
L129-08	12/14/04	SOIL	PERCHLORATE BY IC
L129-09	12/14/04	SOIL	PERCHLORATE BY IC
L129-10	12/15/04	SOIL	PERCHLORATE BY IC
L129-11	12/15/04	SOIL	PERCHLORATE BY IC
L129-12	12/15/04	SOIL	PERCHLORATE BY IC
	L129-01 L129-02 L129-03 L129-04 L129-05 L129-06 L129-07 L129-08 L129-09 L129-10	L129-01 12/14/04 L129-02 12/14/04 L129-03 12/14/04 L129-04 12/14/04 L129-05 12/14/04 L129-06 12/14/04 L129-07 12/14/04 L129-08 12/14/04 L129-09 12/14/04 L129-10 12/15/04 L129-11 12/15/04	L129-01 12/14/04 SOIL L129-02 12/14/04 SOIL L129-03 12/14/04 SOIL L129-04 12/14/04 SOIL L129-05 12/14/04 SOIL L129-06 12/14/04 SOIL L129-07 12/14/04 SOIL L129-08 12/14/04 SOIL L129-09 12/14/04 SOIL L129-10 12/15/04 SOIL L129-11 12/15/04 SOIL

The results are summarized on the following pages.

Please feel free to call if you have any questions concerning these results.

Sincerely yours,

Kam Y. Pang, Ph.D. Laboratory Director



Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-003

La	boratory Name: El	MAX						ress:	1835 205th Street Torrance, CA 90501		Conta	oct:) _{oe}	(R)	bley	<i>!</i>			
	1	AAD				Projec		tion on Are	Area 29 Former INI				is and N te separ					Remarks	
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. rojec					-				281-368-4404	ers.	333	314.0							ı
HEAC	845714 E Point of contact:				יט	ane f	меуе		t Manager/Supervisor	擅	8 3	χ 3							l
USAC		Murray						liojes	- 4°	Number of Containers	Nitroaromatics and Nitroamines by 8330	ate by				,			
USAC	E Telephone No.								Praveen Srivastav	ق	2 2	٥			~~ p.gr				
Item No.	Sample Number		Da	ıte	Time	Сотр	Grab	Matrix	Sample Description, Location	NUN	Nitro Nitro	Perchlorate							
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2	29SB86-002		1		q:23		χ	SOIL	29SB86	1		Х							
3	29SB86-003				15.70		X	SOIL	29SB86	1		х						-	-
4	29SB87-001		1		13:10		χ	SOIL	29\$887	1		Х							
5	29SB87-002		ot	·	B:25		χ	SOIL	29SB87	1		Х							
6	29SB87-003				13:47		X	SOIL	29SB87	1		X					ļ		
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8	29SB88-002 + F DC	295838-	oze		H*40		x	SOIL	29SB88	1		Х							
9	29SB88-003 1FD/2	id 2188 ≈0	¥ <u>۳۹۰</u>		15:05		χ,	SOIL	29SB88	2		Х							
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Received Sax



Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

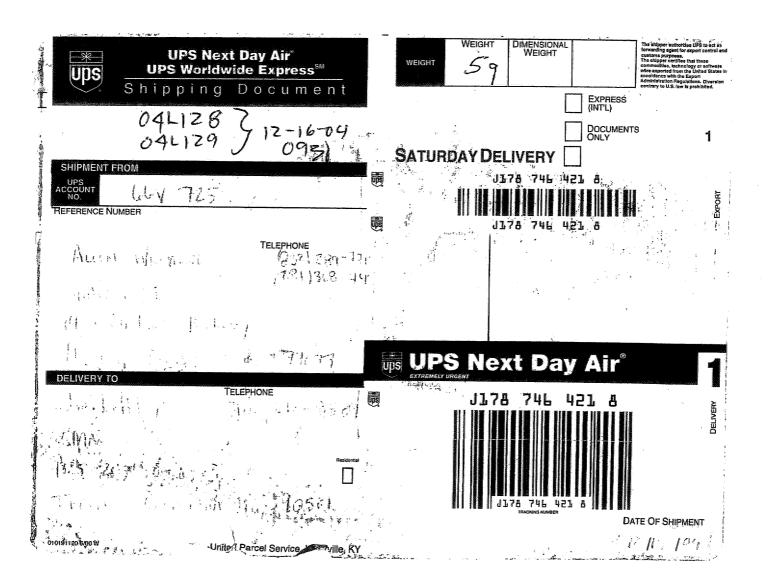
No. 29-EMAX-DEC04-004

	La	boratory Name:	EMAX				Add	ress:	1835 205th Street Torrance, CA 90501		Conta	ict:()c	e \	kello ^l	ley			
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Ī	ISAC	E Point of contact: C	liff Murray					Projec	t Manager/Supervisor	Number of Containers	Nitroaromatics and Nitroamines by 8330	Perchlorate by						
L	SAC	E Telephone No.							Praveen Srivastav	훁	a Te	2					-	
	No.	Sample Num	ber	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Ž	Ziro	Perc						
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SAMPLE RECEIPT FORM 1

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Parties and the same of the sa	of Delivery	Delivered By/Airbill	ECN	044129
EMAX Courier	Control of the Contro		Recepient	jon SERGEY
Client Delivery	- Control of the Cont			12-16-04
Third Party C	PS	J1787464218	Time	0980
		COC Inspection	_	
Gjent Name		Sampler Name	Sampling	Date/Time/Location
Address		Courier Signature/Date/Time	Analysis I	Required
Client PM/FC		□ JAT	Matrix	•
Tel #/Fax #	م خبر	Sample ID	Preservat	ive (if any)
Safety Issues	None	High Concentrations expected	-	d Site Samples
Comments:	Rad Screening Require			
			mandi nisami saut	
				ALCONOMIC TO THE PROPERTY OF T
		Packaging Inspection	·	
Container	Cooler	Box -		
Condition	Custody Seal	☐ Intact ☐ Damag	ned	니 - ' '
Packaging	Bubble Pack	Styrofoam Suffici	yeu oot	plastic bag
Temperatures	- Cooler 1 3.0°C		erit ,	The brasse of
	Cooler 5	Cooler 2 Cooler		Cooler 4
			7	Cooler 8
Comments:	Cooler 9	Cooler 10 Cooler	11	Cooler 12
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LOOID	<u> </u>			
LSCID	Client ID	Discrepancy	(Corrective Action
1129-07	2958(88)001-00	LABEL REDSTO FOR 8330		d Client
(008)		AN ALYSIS		with 80, 81, 82,
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-08	2958(88)002-00	LABEL REASTO FOR B330,	86, 1	87,88, 59, - people
(010)		MMYSIS		*
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				A CONTRACTOR OF THE PARTY OF TH
				A MARINE
LSCID : Lab Samp	le Container ID			
REVIEWS	١			
Sample Labeling	nl	SRF Ho-	PM	am «
Date		Date 12-17-04		12/17/09
MANAGEMENT AND ASSAULT				01-71-0



REPORTING CONVENTIONS

DATA QUALIFIERS:

Lab Qualifier	AFCEE Qualifier	Description
. ل	F	Indicates that the analyte is positively identified and the result is less than RL but greater than MDL.
N		Indicates presumptive evidence of a compound.
В	В	Indicates that the analyte is found in the associated method blank as well as in the sample at above QC level.
E	J	Indicates that the result is above the maximum calibration range.
* .	*	Out of QC limit.

Note: The above qualifiers are used to flag the results unless the project requires a different set of qualification criteria.

ACRONYMS AND ABBREVIATIONS:

CODI	Contract Required Detection Limit
CRDL	Reporting Limit
MRL	Method Reporting Limit
PQL	Practical Quantitation Limit
MDL	Method Detection Limit
DO	Diluted out

DATES

The date and time information for leaching and preparation reflect the beginning date and time of the procedure unless the method, protocol, or project specifically requires otherwise.

LABORATORY REPORT FOR

SHAW E&I

LONGHORN ARMY AMMUNITION PLANT

METHOD 314.0 PERCHLORATE

SDG#: 04L129

CASE NARRATIVE

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L129

METHOD 314.0 PERCHLORATE

Twelve (12) soil samples were received on 12/16/04 for Perchlorate analysis by Method 314.0 in accordance with "Method for Determination of Perchlorate by Ion Chromatography", EPA 600/98-118.

1. Holding Time

Analysis met holding time criteria.

2. Method Blank

Method blank was free of contamination at half the Method Reporting Limit.

3. Lab Control Sample

Lab control sample results were within QC limits.

4. Duplicate

Samples L129-01 and -08 were analyzed for Duplicate. % RPD's were within QC limit.

5. Matrix Spike

Sample L129-01 was spiked. % Recovery was within QC limit.

6. Sample Analysis

Samples were analyzed according to the prescribed QC procedures. All criteria were met.

Non-dilution runs of samples L129-04 to 06, and 08 to 11 could not be evaluated due to matrix interference. The samples were reported from dilution runs.

SAMPLE RESULTS

Matrix

Client : SHAW E&I

Project : LONGHORN ARMY AMMUNITION PLANT

Instrument ID : TI057

Batch No. : 04L129

SAMPLE ID	EMAX SAMPLE ID	RESULTS (ug/kg)	DLF	MOIST	RL (ug/kg)	MDL (ug/kg)	Analysis DATETIME	Extraction DATETIME	LFID	CAL REF	PREP BATCH	Collection DATETIME	Received DATETIME
MBLK1S	PCL007SB	ND	1	NA	20	10	12/29/0418:46	12/28/0416:00	JL29-2	JL29-1	PCL007S	NA	12/28/04
LCS1S	PCL007SL	109	1	NA	20	10	12/29/0419:27	12/28/0416:00	JL29-4	JL29-1	PCL007S	NA	12/28/04
LCD1S	PCL007SC	108	1	ΝA	20	10	12/29/0419:47	12/28/0416:00	JL29-5	JL29-1	PCL007S	NA	12/28/04
29SB86-001	L129-01	40.3	1	16.6	24	12	12/29/0420:07	12/28/0416:00	JL29-6	JL29-1	PCL007S	12/14/04	12/16/04
29SB86-001DUP	L129-01D	39.4	1	16.6		12	12/29/0420:27	12/28/0416:00	JL29-7	JL29-1	PCL007S	12/14/04	12/16/04
29SB86-001MS	L129-01M	164	1	16.6		12	12/29/0420:47	12/28/0416:00	JL29-8	JL29-1	PCL007S	12/14/04	12/16/04
29SB86-002	L129-02	8600	100	15.7	2370	1190	01/04/0515:52	12/28/0416:00	JA04-6	JA04-1	PCL007S	12/14/04	12/16/04
29SB86-003	L129-03	689	2	20.2		25.1	01/04/0516:12	12/28/0416:00	JA04-7	JA04-1	PCL007S	12/14/04	12/16/04
29SB87-001	L129-04	ND	10	14.4		117	01/04/0520:04	12/28/0416:00	JA04-18	JA04-12	PCL007S	12/14/04	12/16/04
29SB87-002	L129-05	ND	5	12.3		57	01/04/0516:53	12/28/0416:00	JA04-9	JA04-1	PCL007S	12/14/04	12/16/04
29SB87-003	L129-06	ND	10	17.7	243	122	01/04/0520:24	12/28/0416:00	JA04-19	JA04-12	PCL007S	12/14/04	12/16/04
29SB88-001	L129-07	74.5	1	10.6	22.4	11.2	01/04/0519:43	12/28/0416:00	JA04-17	JA04-12	PCL007S	12/14/04	12/16/04
29SB88-002	L129-08	ND	10	25.0		133	01/04/0520:44	12/28/0416:00	JA04-20	JA04-12	PCL007S	12/14/04	12/16/04
29SB88-002DUP	L129-08D	ND	10	25.0	267	133	01/04/0521:04	12/28/0416:00	JA04-21	JA04-12	PCL007S	12/14/04	12/16/04
29SB88-003	L129-09	ND	5	22.4		64.4	01/04/0518:14	12/28/0416:00	JA04-13	JA04-12	PCL007S	12/14/04	12/16/04
29SB89-001	L129-10	ND	5	16.9		60.2	01/04/0518:34	12/28/0416:00	JA04-14	JA04-12	PCL007S	12/15/04	12/16/04
29SB89-002	L129-11	ND	5	21.8		63.9	01/04/0518:54	12/28/0416:00		JA04-12	PCL007S	12/15/04	12/16/04
29SB89-003	L129-12	144	1	24.5	26.5	13.2	01/04/0519:14	12/28/0416:00	JA04-16	JA04-12	PCL007S	12/15/04	12/16/04

EMAX QUALITY CONTROL DATA MS ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

1

BATCH NO.:

04L129

METHOD: METHOD 314.0

MATRIX:

SOIL

% MOISTURE:

16.6

DILUTION FACTOR: 1

29SB86-001 SAMPLE ID:

LAB SAMP ID:

L129-01 L129-01M

JL29-6

JL29-8

LAB FILE ID:

DATE EXTRACTED: 12/28/0416:00 12/28/0416:00

DATE COLLECTED: 12/14/04

DATE ANALYZED:

12/29/0420:07 12/29/0420:47

PCL007S

DATE RECEIVED: 12/16/04

PCL007S PREP. BATCH:

CALIB. REF:

JL29-1

JL29-1

ACCESSION:

	SMPL RSLT	SPIKE AMT	MS RSLT	MS	QC LIMIT
PARAMETER	(ug/kg)	(ug/kg)	(ug/kg)	% REC	(%)
			2		
Perchlorate	40.3	120	164	103	75-125



EMAX QUALITY CONTROL DATA LCS/LCD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

1

BATCH NO.:

04L129

METHOD 314.0 METHOD:

MATRIX:

SOIL

% MOISTURE:

NA

DILUTION FACTOR: 1

MBLK1S

SAMPLE ID: LAB SAMP ID:

PCL007SB

PCL007SC PCL007SL JL29-4

JL29-2

JL29-5

LAB FILE ID: DATE EXTRACTED:

12/28/0416:00

12/28/0416:00 12/28/0416:00

12/29/0419:47

DATE COLLECTED: NA DATE RECEIVED: 12/28/04

DATE ANALYZED: PREP. BATCH:

12/29/0418:46 PCL007S

12/29/0419:27 PCL007S

1

PCL007S

CALIB. REF:

JL29-1

JL29-1

JL29-1

ACCESSION:

PARAMETER	BLNK RSLT (ug/kg)	SPIKE AMT (ug/kg)	BS RSLT (ug/kg)	BS % REC	SPIKE AMT (ug/kg)	BSD RSLT (ug/kg)	BSD % REC	RPD (%)	QC LIMIT	MAX RPD
Perchlorate	ND	100	109	109	100	108	108	n 1	80-120	20

EMAX QUALITY CONTROL DATA DUPLICATE SAMPLE ANALYSIS

CLIENT:

METHOD:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L129

METHOD 314.0

MATRIX:

SOIL

% MOISTURE:

16.6

DILUTION FACTOR: 1

SAMPLE ID:

29SB86-001DUP

29SB86-001 L129-01

L129-01D

EMAX SAMP ID: LAB FILE ID:

JL29-6

JL29-7

DATE EXTRACTED:

12/28/0416:00 12/28/0416:00

12/29/0420:27

DATE COLLECTED: 12/14/04 DATE RECEIVED: 12/16/04

DATE ANALYZED: PREP. BATCH:

12/29/0420:07 PCL007S

PCL007S

CALIB. REF:

JL29-1

JL29-1

ACCESSION:

	SMPL RSLT	DUPL RSLT	RPD RSLT	QC LIMIT
PARAMETER	(ug/kg)	(ug/kg)	%	(%)
Perchlorate	40.3	39.4	2	. 20

EMAX QUALITY CONTROL DATA DUPLICATE SAMPLE ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L129

METHOD:

METHOD 314.0

MATRIX:

SOIL

10

% MOISTURE:

25.0

DILUTION FACTOR: 10 SAMPLE ID:

29SB88-002

29SB88-002DUP

EMAX SAMP ID:

L129-08

L129-08D

LAB FILE ID: DATE EXTRACTED: JA04-20

JA04-21 12/28/0416:00

12/28/0416:00 01/04/0520:44 01/04/0521:04 DATE COLLECTED: 12/14/04 DATE RECEIVED: 12/16/04

DATE ANALYZED: PREP. BATCH:

PCL007S JA04-12 PCL007S

JA04-12

CALIB. REF:

ACCESSION:

SMPL RSLT (ug/kg)

DUPL RSLT (ug/kg)

ND

RPD RSLT QC LIMIT % (%)

PARAMETER Perchlorate

ND

NA

	IC RESU	JLT FO	DRM
LFID\$	LSID\$	DF\$	PERCHLORATE
JL06-1	IB	1	ND
JL06-2	s-0.0	1	ND
JL06-3	s-2.0	1	101%
JL06-4	s-4.0	1	88.7%
JL06-5	s-10.0	1	91.3%
JL06-6	s-25.0	1	91.2%
JL06-7	s-30.0	1	92.8%
JL06-8	ICV	1	103%
JL06-9	ICB	1	ND
JL06-10	IPCS	1	98.2%
JL06-11	PCL003WB	1	ND
JL06-12	MRL	1	108%
JL06-13	PCL003WL	1	10.8
JL06-14	PCL003WC	1	10.7
JE06-15	L023-01	1	ND
.11.06-16	L023-02	1	ND
JL06-17	L023-01	2	ND
JE06-18	L023-02	2	ND
JL06-19	K208-02	1	ND
JL06-20	K208-03	1	ND
JL06-21	K208-04	1	ND
JL06-22	CCV1-15	1	104%
JL06-23	K208-05	20	289
JL06-24	K208-06	1	ND
JL06-25	K184-02	1	ND
JL06-26	K184-03	5	80.2
JL06-27	K184-05	10	211
JL06-28	K184-07	20	301
JL06-29	K184-08	20	446
.1L06-30	K184-10	20	281
JL06-31	K184-12	1	5.55
JL06-32	CCV2-30	1	107%
JL06-33	PCL004WB	1	ND
11.06-34	PCL004WL	1	10.9
୍ମ L06-35	PCL004WC	1	10.8
JI.06-36	K167-02	10	145
5:.06-37	K167-03	10	245
.06-38	K167-06	10	278
06-39	K167-07	10	138
06-40	K167-10	10	176
	K167-11	4	29.8
ປL06-42	K142-12	2	54.5
JL06-43	CCV3-15	1	103%

			IC SEQUENCE	FORM		
INDX	LSID	LFID	DF	METNAME	SELCOMP	DateTime
1	IB	JL06-1	1	IC57L06	ALL	12/06/0420:29
2,	S-0.0	JL06-2	1	IC57L06	ALL	12/06/0420:50
3	s-2.0	JL06-3	1	IC57L06	ALL	12/06/0421:10
4	S-4.0	JL06-4	1	IC57L06	ALL	12/06/0421:30
5. 7.	S-10.0	JL06-5	1	IC57L06	ALL	12/07/0410:04
6	S-25.0	JL06-6	1	IC57L06	ALL	12/07/0410:24
7.	s-30.0	JL06-7	1	IC57L06	ALL	12/07/0410:45
8	ICV	JL06-8	1	IC57L06	ALL	12/07/0411:04
9	ICB	JL06-9	1	IC57L06	ALL	12/07/0414:31
10	IPCS	JL06-10	1	IC57L06	ALL	12/07/0414:52
11	PCL003WB	JL06-11	1	IC57L06	ALL	12/07/0415:12
12	MRL	JL06-12	1	1C57L06	ALL	12/07/0415:32
13	PCL003WL	JL06-13	1	IC57L06	ALL	12/07/0415:52
14	PCL003WC	JL06-14	1	IC57L06	ALL	12/07/0416:12
15	L023-01	JL06-15	1	IC57L06	ALL	12/07/0416:32
16	L023-02	JL06-16	1	IC57L06	ALL	12/07/0416:53
17	L023-01	JL06-17	2	IC57L06	ALL	12/07/0417:13
18	L023-02	JL06-18	2	IC57L06	ALL	12/07/0417:33
19	K208-02	JL06-19	· 1	IC57L06	ALL	12/07/0418:13
20	K208-03	JL06-20	1	IC57L06	ALL	12/07/0418:33
21	K208-04	JL06-21	i	IC57L06	ALL	12/07/0418:53
22	CCV1-15	JL06-22	i	IC57L06	ALL	12/07/0419:13
23	K208-05	JL06-23	20	IC57L06	ALL	12/07/0419:33
24	K208-06	JL06-24	1	IC57L06	ALL	12/07/0419:53
25	K184-02	JL06-25	i	IC57L06	ALL	12/07/0420:13
:6	K184-03	JL06-26	Š	IC57L06	ALL	12/07/0420:15
27	K184-05	JL06-27	10	IC57L06	ALL	12/07/0420:54
-3	K184-07	JL06-28	20	IC57L06	ALL	12/07/0420:34
	K184-08	JL06-29	20	IC57L06	ALL	12/07/0421:14
30 ·	K184-10	JL06-30	20	IC57L06	ALL	12/07/0421:54
1	K184-12	JL06-31	1	IC57L06	ALL	12/07/0422:14
*2	CCV2-30	JL06-32	i	1C57L06	ALL	12/07/0422:14
33	PCL004WB	JL06-33	i	IC57L06	ALL	12/07/0422:55
34	PCL004WL	JL06-34	i	IC57L06	ALL	12/07/0423:15
35	PCL004WC	JL06-35	i	1C57L06	ALL	12/07/0423:15
36	K167-02	JL06-36	10	IC57L06	ALL	12/07/0423:55
37	K167-02	JL06-37	10	IC57L06		
38	K167-05	JL06-37	10		ALL	12/08/0400:15
39				1C57L06	ALL	12/08/0400:35
	K167-07	JL06-39	10	IC57L06	ALL	12/08/0400:56
40	K167-10	JL06-40	10	IC57L06	ALL	12/08/0401:16
41	K167-11	JL06-41	4	IC57L06	ALL	12/08/0401:36
42	K142-12	JL06-42	2	IC57L06	ALL	12/08/0401:56
43	CCV3-15	JL06-43	1	IC57L06	ALL	12/08/0402:17

	IC RESU	UT F	ORM
LFID\$	LSID\$	DF\$	PERCHLORATE
JL29-1	IPCS	1	102%
JL29-2	PCL007SB	1	.411
JL29-3	MRL	i	117%
	PCL007SL	1	
JL29-4			10.9
JL29-5	PCL007SC	1	10.8
JL29-6	L129-01	1	3.36
JL29-7	L129-01D	1	3.29
JL29-8	L129-01M	1	13.7
JL29-9	L129-02	1	66.9
JL29-10	L129-03	1	62.4
.: 29-11	L129-04	1	ND
₹L29-12	L129-05	1	ND
JL29-13	CCV7-15	1	95.3%
.t .29-14	В	1	ND
· 29-15	L129-06	1	ND
∂9-16	L129-07	1	ND
27-17	L129-08	1	ND
-29-18	L129-09	1	ND
L29-19	L129-10	1	9.7
L29-20	L129-11	1	ND
/L29-21	L129-12	1	12.2
JL29-22	CCV8-30	1	42.3%*
JL29-23	L129-02	25	1800
JL29-24	L129-03	2	ND
JL29-25	L129-04	1	ND
JL29-26	L129-05	1	ND
JL29-27	L129-06	1	ND
JL29-28	CCV9-15	i	ND
1129-29	L129-05	5	ND
JL29-30	L129-06	5	ND
JL29-31	L129-08	5	ND
JL29-31	L129-08	5	ND ND
1L29-33	L129-09	5	
	L129-10	5	ND 313
129-34) 1	
SL29-35	CCV10-30	1	111%*
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		-	IC SEQUENCE	FORM		
XCE	LSID	LFID	DF	METNAME	SELCOMP	DateTime
2.1	IPCS	JL29-1	1	IC57L06	ALL	12/29/0418:26
7	PCL007SB	JL29-2	1	IC57L06	ALL	12/29/0418:46
3	MRL	JL29-3	1	IC57L06	ALL	12/29/0419:07
- L	PCL007SL	JL29-4	1	IC57L06	ALL	12/29/0419:27
ڗ	PCL007SC	JL29-5	1	IC57L06	ALL	12/29/0419:47
6	L129-01	JL29-6	1	IC57L06	ALL	12/29/0420:07
7	L129-01D	JL29-7	1	1C57L06	ALL	12/29/0420:27
3	L129-01M	JL29-8	1	IC57L06	ALL	12/29/0420:47
,	L129-02	JL29-9	1	IC57L06	ALL	12/29/0421:07
10	L129-03	JL29-10	1	IC57L06	ALL	12/29/0421:28
11	L129-04	JL29-11	1	IC57L06	ALL	12/29/0421:48
12	L129-05	JL29-12	1	IC57L06	ALL	12/29/0422:08
13	CCV7-15	JL29-13	1	IC57L06	ALL	12/29/0422:28
14	В	JL29-14	1	IC57L06		12/29/0422:48
15	L129-06	JL29-15	1	1C57L06	ALL	12/29/0423:08
16	L129-07	JL29-16	1	IC57L06	ALL	12/29/0423:29
^7	L129-08	JL29-17	1	IC57L06	ALL	12/29/0423:49
-8	L129-09	JL29-18	1	IC57L06	ALL	12/30/0400:09
. 3	L129-10	JL29-19	1	1C57L06	ALL	12/31/0403:14
3.	L129-11	JL29-20	1	IC57L06	ALL	12/31/0403:46
1.3	L129-12	JL29-21	1	1C57L06	ALL	12/31/0404:18
	CCV8-30	JL29-22	1	IC57L06	ALL	12/31/0404:51
, P. L.	L129-02	JL29-23	25	IC57L06	ALL	12/31/0405:23
24	L129-03	JL29-24	2	IC57L06	ALL	12/31/0405:55
5	L129-04	JL29-25	1	IC57L06	ALL	12/31/0406:27
ି6	L129-05	JL29-26	1	IC57L06	ALL	12/31/0406:59
:7	L129-06	JL29-27	1	IC57L06	ALL	12/31/0407:31
28	CCV9-15	JL29-28	1	IC57L06	ALL	12/31/0408:03
29	L129-05	JL29-29	.5	IC57L06	ALL	12/31/0408:36
30	L129-06	JL29-30	5	IC57L06	ALL	12/31/0409:08
31	L129-08	JL29-31	5	IC57L06	ALL	12/31/0409:40
32	L129-09	JL29-32	5	1C57L06	ALL	12/31/0410:12
33	L129-10	JL29-33	5	1C57L06	ALL	12/31/0410:44
34	L129-11	JL29-34	5	I C57L06	ALL	12/31/0411:16
35	CCV10-30	JL29-35	1	IC57L06	ALL	12/31/0411:48

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	IC RESUL	T FOR	RM
LFID\$	LSID\$	DF\$	PERCHLOR
JA04-1	IPCS	1	13.3
JA04-2	PCL007SQ	1	ND
JA04-3	MRL	1	2.21
JA04-4	PCL007SX	1	10.9
JA04-5	PCL007SY	1	10.9
JA04-6	L129-02	100	725
JA04-7	L129-03	2	54.9
JA04-8	L129-04	5	ND
404-9	L129-05	5	ND
JA04-10	L129-06	5	ND
,:A04-11	L129-08	5	ND
∂ 04-12	CCV11-15	1	108%
.:. J4-13	L129-09	5	ND
.<:04 -1 4	L129-10	5	ND
。 34 - 15	L129-11	5	ND
:A04-16	L129-12	1	10.9
JA04-17	L129-07	1	6.66
JA04-18	L129-04	10	ND
JA04-19	L129-06	10	ND
JA04-20	L129-08	10	ND
JA04-21	L129-08D	10	ND
JA04-22	L129-08A	10	116
JA04-23	BL	1	ND
JA04-24	CCV12-30	1	114%
JA04-25	CCV12-30	1	114%

JA. JAC JAC JAC

An IAS SAN IA IAS SAN

		-		,		
INDX	LSID	LFID	DF	METNAME	SELCOMP	DateTime
1	IPCS	JA04-1	1	IC57L06	ALL	01/04/0513:03
2	PCL007SQ	JA04-2	1	IC57L06	ALL	01/04/0514:31
7	MRL	JA04-3	1	IC57L06	ALL	01/04/0514:51
4	PCL007SX	JA04-4	1	1C57L06	ALL	01/04/0515:11
57	PCL007SY	JA04-5	1	IC57L06	ALL	01/04/0515:32
δ	L129-02	JA04-6	100	IC57L06	ALL	01/04/0515:52
	L129-03	JA04-7	2	IC57L06	ALL	01/04/0516:12
3	L129-04	JA04-8	5	1C57L06	ALL	01/04/0516:32
Ġ	L129-05	JA04-9	5	IC57L06	ALL	01/04/0516:53
" 0	L129-06	JA04-10	5	IC57L06	ALL	01/04/0517:13
11	L129-08	JA04-11	5	IC57L06	ALL	01/04/0517:33
12	CCV11-15	JA04-12	1	IC57L06	ALL	01/04/0517:53
13	L129-09	JA04-13	5	1C57L06	ALL	01/04/0518:14
14	L129-10	JA04-14	5	IC57L06	ALL	01/04/0518:34
15	L129-11	JA04-15	5	IC57L06	ALL	01/04/0518:54
16	L129-12	JA04-16	1	IC57L06	ALL	01/04/0519:14
17	L129-07	JA04-17	1	IC57L06	ALL	01/04/0519:43
18	L129-04	JA04-18	10	IC57L06	ALL	01/04/0520:04
1.9	L129-06	JA04-19	10	IC57L06	ALL	01/04/0520:24
30	L129-08	JA04-20	10	IC57L06	ALL	01/04/0520:44
21	L129-08D	JA04-21	10	1C57L06	ALL	01/04/0521:04
22	L129-08A	JA04-22	10	IC57L06	ALL	01/04/0521:25
23	BL	JA04-23	1	IC57L06	ALL	01/04/0521:45
24	CCV12-30	JA04-24	1	IC57L06	ALL	01/04/0522:05
°5	CCV12-30	JA04-25	1	1C57L06	ALL	01/04/0522:25

IC SEQUENCE FORM

ANALYSIS RUN LOG FOR IC - PERCHLORATE

A.	EMAX	-314.0	Revision N	o. 2		,						_	<u> </u>	Book # A57-0
	12	129	1/04	Time	182	<u> </u>	7			Ending Date	12/3//0	Y	Time 1/48	
	- 1	D	ata File	7.	h Samale ID	DF	Ma	trix	Conductivity,	N	otes	Instru	ment Number	57
	- 1	1	Name	1	o campic its	Di	S	W	(us/cm)					<u>~</u>
*	1	JL	29-1			ĺ	•		2060			INIT	AL CALIBRATION REFEREN	Œ
*	2		2	Pe	LOUTSB		S		·			Method File	1057106. Me	7
*	3		3						<u> </u>			ICAL ID		
	4	,	4	PCI			Ş					ICV ID	1 - 0.	54
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*	1			C			1		771			ICV	10	
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*	6		16	í	-07		П		16.0	bace	elise	LCS	662	10
*	7		17		-08				90.1	rean	alyt (MS	-651	1000
*	/8		18		-09				1244	San	mples	IPC		30/10
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	20		20		-11	<u></u>	\coprod					Comments:	*	T
·	1			4	-12.	<i>V</i>	<u></u>		89			CMC Reading,	QC Criteria	Тетр.
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	Sam Pro H	/2 Sample Prep ID	/2 2 9							$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				

$oldsymbol{E}_{MAXLaboratories}$, Inc. 1835 W. 20 $^{\circ}$ 31 Towards, CA 90501

ANALYSIS RUN LOG FOR IC - PERCHLORATE

•	M		-314.0 Revision	No. 2		_					. .		Book # A57-008
t Date			4/05	Time	/3!0	<u> </u>				Ending Date 1/4	105	Time	
	I	mple Prep ID	Data File Name	L	ab Sample ID	DF	M S	atrix W	Conductivity, (us/cm)	Notes	In	strument Number	57
	*	1	JA 04-1		pes				2680			NITIAL CALIBRATION REFERE	INCE
	*	2	2	2	CLD7SQ 1 KL	L,	ζ				Method File	1057200.	
L	*	3	3_								ICAL ID	SW8 B - 02-	652
L	*	4	4	PC	LOOTSX	1	5				ICV ID	- L	ac ci
	*	5			V SY	1	1						
-	*	6	6	ol 1	29-02	100			Refer b			Standards	
_	*	7	7		- 13	2	Ш		PP		Name	ID	Conc. (ug/L)
	*	8	8		-04	5			p. 54-008		ICAL	S1	20
-	-	9	9		-05				24			S2 0	JP .
	*	0	10		1-06	J.						S3 A51	
: -	*	1 2			-08	1	,		l			84 0	
îŀ	*	3	12		CV11-15	ı						SS P P I	
-	*	4	13	<u>u i</u>	29-09	Ţ.	ς				ICV	F .	
%	*	5	14		- 10	<u> </u>					CCV-15	SW8B-02-660 -661	15
-	*	6	15		-4	5	+				CCV-30	-661	
-	*	7	16		-12 -07	7	-				LCS	508 B-02 - 565 SW3B-02 - 565	10
\ <u> </u>	*	8	18		- 04	_	+				MS/A	7051	10,
┢	*	19	19			10	\dashv				IPC	SW8B-02-063	300 pp 10 pp
-	*	10	20	\dashv	-06	+	+				СМС	SU3B-02 -568	1413 M
	*	1	21		-08	- - -	+	\dashv	+		Comments:		1
H	*	2	22	\dashv	-08h	IO	H.				CMC Reading,	QC Criteria	Temp.
	*	3	23	<u>'</u>	re se	1	~	\dashv	· F		(us/cm) /4/1	(us/cm) ±30	(°)
	*	4	24	-7	32 CV 12-30						1411	Electronic Data Archival	<u> ας</u>
	*	5	25	7	CV12-SUP	力		\dashv		Tanana di di di		Location Location	Date
	*	, 6	20							111			Date
	*	7	27							the plant	{ 		
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	* .	29	29				\dashv	_				Analyzed Ru	: LBIJA
-	*	み 0	30							_/	 	This page is checked during the	

Book # A57-008

57

This page is checked during the data review process.

Instrument Number

MAXLABORATORIES, INC. 1835 W. 20° St. Towards, CA 91301

SOP

Start Date

Sample

Prep

D

EMAX-314.0 Revision No. 2

104

Data File

Name

Time

Lab Sample ID

1824

DF

Matrix

	111			Lameston and the same	1		1 "					
	* <	<u>31</u>	1129-31	2128-08	5	1				INF	TIAL CALIBRATION REFEREN	CE
	*	2	32	-09	I					Method File	SAME AS 9	o rel
	*	3	33	- 10						ICAL ID		
	*	4	34	//	7	1				ICV ID	1	
	*	5	36	CCV10-30								
	*	6				***************************************			1_1		Standards	
BATCH *	*	7		·					17/0	Name	ID	Conc. (ug/L)
C	*	8							W. I.I.	ICAL S	SAME AS	D24
#	**	9	-						14,	S		
\mathcal{R}	*	0							9	S	3	
173	*	1								S4		
Ô	*	2								S		
<u> </u>	*	3						. 1/		ICV		
IN I	*	4								CCV-15		
	*	5								CCV-30		
	*	6					/			LCS		
*	* .	7				1				MS		
	*	8								IPC	/	
	*	9								СМС		
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ANALYSIS RUN LOG FOR IC - PERCHLORATE

Conductivity,

(us/cm)

Ending Date

Notes

ANALYSIS RUN LOG FOR IC - PERCHLORATE

Date	10/	104		Time 2:24					Ending Date	-	Time	
	Sampl		Data File		T	T	trix	Conductivity,		Inet	rument Number	57
	Prep ID		Name	Lab Sample ID	DF	S	W	(us/cm)	Notes	21135	tument Number	1 0,
-		777	06-1	B	1		χ	4		IN	ITIAL CALIBRATION REFEREN	CE
	*		1 2	3-0.0	1-1-		l î			Method File	1657 JOG MET	
	*		3	5-2.0						ICAL ID	SWBB-02-639	
	* .		4	3-4.0	TT					ICV ID	V 640	
	*	;	5	5-10.0								·····
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, [*	L									34	25
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	*	5					-			CCV-30		
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	*	3						720	16/04	IPC		
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	*)			-				*		Analyzed By:	2

B MAX LABORATORIES, INC. 1825 W. 20th St. Tomburs, CASSESI

EXTRACTION LOGS

Page 38 00091380

SAMPLE PREPARATION LOG FOR ORGANIC ACID/PERCHLORATE

ς	01	110		Start Date	1/28/2	/ Time	1600	End Da	te / x/ x8/	∂# Ti	me 2000	
	Sample		Lab	Sample	Dilutio		1		Standards		ID	Amount Add (ml)
	Prep ID		Sample ID	Amount	Volum	1		Notes	Acetate	1 /	14	
	ய		Ш	(g)	(ml)	(ml)			Butyrate			
	*01	PC	LOO7 SB	10	lou	100			Lactate		<u>'</u>	
	*02		1 52	10					Perchlorate	3W8B-	12-651	1.0
	*03		SC	10					Propionate		16	
	*04	0421	29 - 01	10.01			Clear	extrad	Pyruvate		<u>l</u>	
	*05		-010	10.02							-	
	*06		-014	10,01								
•	*07		-02	10.00		in the same	Bn	ITd	Reagent		Lot #/ID	
	*08		- 03	10.00				:	H ₂ SO ₄		US	
)	*09		-04 -0T	10.00					Nanopure	N	anguno	
	*10		-05	10.03			·		Ke	8W 3B	U 12- anguno v 2-565, 14	13 µmhos/
	*11		- 06	10.02				<i>V</i>			,	· · · · · · · · · · · · · · · · · · ·
	*12		-07	10.01			Cle	eu	Legend:			
9400	*13		-08	10.01			Pon	/Til	Color	Texture	Clarity	Artifacts
d (*14		-09	10,02			de	ai	Bu = Blue Bl = Black	Cs = Coarse	Cr = Clear	Rk = Rocks
	*15		- D	10.00			10,	17d	Bn = Brown Gn = Green	Md = Medium	Cy = Cloudy	Sl = Shale
3	*16		- 11	10,00	1			V.	Og = Orange Rd = Red	Fn = Fine	Td = turbid	Vg= Vegetati
٥.	*17	/	- 12	10.60		V V	Cle	rai ,	Yw = Yellow			
	*18				<u></u>			1/4/0	Comments			
	*19							7 7		;		
	*20							/				
	*21											
	*22	1	•									
	*23	``						,		Prepared I	By: <i>VK</i>	1k
	*24									Standard Added	By: JR/,	ls
	*25									Checked I		

RETENTION TIME WINDOW

PERCHLORATE

Lab name:

EMAX

Method:

EMAX-314.1

Instrument ID:

DX500IC57

IC column:

AS16

Column size:

4X250NM

Sample ID	CCV10-30	CCV11-15	MRL			
Analysis Date	1/7/04	1/8/04	1/9/04	AVERAGE RETENTION	SD	RETENTION TIME WINDOW
Analysis Time	18:14	18:15	13:01	TIME	UD	3*SD
COMPOUND	JA06-24	JA08-13	JA09-3			
PERCHLORATE	12.363	12.355	12.278	12.332	0.047	0.141

TABLE OF CONTENTS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L142

SECTION		PAGE
Cover Letter, CO	DC/Sample Receipt Form	1000 – 1007
GC/MS-VOA	**	2000 –
GC/MS-SVOA	**	3000 –
GC-VOA	**	4000 –
GC-SVOA	**	5000 –
HPLC	EPA METHOD 8330	6000 - 6051
METALS	**	7000 –
WET	**	8000 –
OTHERS	**	9000 –

^{** -} Not Requested



1835 W. 205th Street Torrance, CA 90501

Tel: (310) 618-8889 Fax: (310) 618-0818

Date: 12-27-2004 EMAX Batch No.: 04L142

Attn: Diane Meyer

Shaw E&I 1430 Enclave Parkway Houston TX 77077

Subject: Laboratory Report

Project: Longhorn Army Ammunition Plant

Enclosed is the Laboratory report for samples received on 12/17/04. The data reported include:

Sample ID	Control #	Col Date	Matrix	Analysis
, *,* *,* *,* *				
29SB81-001	L142-01	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29SB81-002	L142-02	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29SD38-MH07	L142-03	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29SD39-MH08	L142-04	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29SD41-MH10	L142-05	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29SD46	L142-06	12/16/04	SOIL	NITROAROMATICS & NITRAMINES
29\$W46	L142-07	12/16/04	WATER	NITROAROMATICS & NITRAMINES

The results are summarized on the following pages.

Please feel free to call if you have any questions concerning these results.

Sincerely yours,

Kam Y. Pang, Ph.D. Laboratory Director 1430 Enclave Parkway Houston, TX 77077 (281) 368-4000

CHAIN-OF-CUSTODY

No. 29-EMAX-DEUL

										~ ~ /	7	-		
Laboratory Name: EN	/iAX				ldress	Forrance, CA 90501		Cont	act: Jos	, Val	bley			***************************************
			Proje	ect Loc	cation	Area 29 Former INI								
Project Name Longhorn A	AAP		Pro	ducti	ion Ar				Anaiysis (Indicato	and Metho	d Desire	ď		
Project No.		Project				Project Telephone No.			(indicate	separate co	ontainers	<u>;) </u>		Remarks
845714		,	liono	hear.		1	బ్	and 8330	314.0				1	
JSACE Point of contact:			лапе	e Meyer 281-368-4404			_] <u>=</u>	8 8	3	İ				
	lurray				Proje	ct Manager/Supervisor	Number of Containers	atics	e by					
JSACE Telephone No.			<u> </u>			Praveen Srivastav	er of	lo m	orat					
Sample Number	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Numb	Nitroaromatics and Nitroamines by 833	Perchlorate					-
1 29SB80-001		-		ļ	SOIL	293B80	1	V				 	+	
0.000000		 	1		+	130100		 X				-		-
2 29SB80-002		A STATE OF THE PARTY OF THE PAR	-	Na Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Carlos Ca	SOIL	29SB80	11	x						
ਤੇ 29SB81-001	17/1409			X	SOIL	29SB81	1	х						
4- 29SB81-002	12/16/6	0905		X	SOIL	29SB81	1	х					-	
5 29SB82 001					SOIL	Z9SB8Z					+		_	
6 29SB82-002					SOIL	295B82	+-	X						
7 29SB83-001					SOIL	29SB83		×						
8 29SB83-002					SOIL	29SB83		×				ANGERICA TOTAL		
9 29SB84-001					SOIL	29SB84		-X					***************************************	
10 29SB84 002					SOIL	293B84		X		***************************************			-	AND THE PROPERTY OF THE PROPER
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11 10/1	<u> </u>			-	116	nsfers Accepted By (Signature)	Date/		Special Instru	ictions				
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							1777							
								F	edEx Airbi	II No.:	. , , .	<u> </u>		
						Laboratory Sampler's Signature				**************************************				
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	1 (100	1	Jes	as intac	t? <u> </u>	Y N Received Good	Condition _	<u> </u>	N	Cold	3.4	00		
												-		



Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-005

La	aboratory Name:	EMAX					lress:	1835 205th Street Torrance, CA 90501		Conta	ect:						
			~			ct Loca		Area 29 Former INI				is and N					
		orn AAP		In. last			on Ar	<u> </u>	4			te separ	ate con	tainers)			Remarks
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	84571	4	Diane Meye				Meyer 281-368-4404			8 8	314.0						
	USACE Point of contact: Cliff Murray JSACE Telephone No.						er of Containers	Nitroaromatics and Nitroamines by 8330	orate by		1				Managara da da da da da da da da da da da da da		
Item No.	Sample Num	ıber ·	Date	Time	Сощр	Grab	Matrix	Sample Description, Location	Number of	Nitroar Nitroar	Perchlorate						
1-0	29SD32-MH01			<u> </u>			SED-	298D32-MH01	1	-X-							
2	29SD33-MH02						SED	29SD33-MH02	_1_	_x_							
<u>_3</u>	29SD34-MH03						SED	29SD34-MH03		<u> </u>	and chicken which the state of	and and the same	-A-TT	SECTION SEC. NAMES OF SEC.	**Continuent metholyanus		
-4-	29SD35-MH04						SED	29SD35-MH04	1	-X-	***************************************			****************			
5	29SD36-MH05						-SED	29SD36-MH05	1	_X_							
-6-	29SD37-MH06						SED	29SD37-MH06	1	X	-				-		
-7	29SD38-MH07		17/14/14	12:45			SED	29SD38-MH07	1	Х							
8-	29SD39-MH08	warenar	12/14/64	1307			SED	29SD39-MH08	1	х							
அ	<u> </u>																
10																	
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M. tellin _ 13/11/04 1600																	
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Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-006

L	aboratory Name:	EMAX					dress:	Torrance, CA 90501		Conta	act:	UQ	lelt	ley				
						ct Loca		Area 29 Former INI			•	is and M						
	ct Name Longho	orn AAP		Torsions	1		on Ar	Project Telephone No.	-	<u> </u>		e separa	ite con	tainers) I	r		Remarks	
Proje				Project				Project releprione No.	စ္	and 8330	314.0					ŀ		
	84571	4		Diane Meyer				er 281-368-4404		and 833	3							
	ACE Point of contact: Cliff Murray						of Containers	Nitroaromatics Nitroamines by	erchlorate by									
USAC	E Telephone No.			,			<u> </u>	Praveen Srivastav	ğ	12 5	흗							
Item No.	Sample Num	ber	Date	Time	Сощр	Grab	Matrix	Sample Description, Location	Number of	Nitro Nitro	Perch							
4	29SD40-MH09		 				SED	29SD40-WH09	 1	-x-							—	
2	29SD41-MH10		12/16/0	1315		Х	SED	29SD41-MH10	1	х								
-3	20SD42-MH11-						SED	29SD42-MH11	1_1_	X								-
4	29SD43-MH12						SED	29 9D43-MH12		-x-								
<u>-</u> چ	29SD44						SED	293D44		_x_								_
-6-	29SD45							29SD45	1	v								コ
	29SD46		12/16/04	1515		χ.		29SD46	1	X								\neg
-8	29SDMH	QC	14/6/01			*	SED	29SD MH QC	1	_ж_								
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10																	,	
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Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-007

L	.aboratory Name:	EMAX					lress:	Forrance, CA 90501		Conta	act:)oe 1	rell	ley			
Proie	ct Name Longh	orn AAP				ct Loca ductio		Area 29 Former INI					Method I				Remarks
Proje				Project			Project Telephone No.			F 8		Сосра	10.000	Lancis,		<u> </u>	Tromano.
	84571	4		Diane Meyer				er 281-368-4404		and 8330	Perchlorate by 314.0						
	CE Point of contact: (CE Telephone No.	Cliff Murray					Project Manager/Supervisor Praveen Srivastav		Number of Containers	Nitroaromatics a							
Item No.		nber ·	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Numbe	Nitroar Nitroar	Perchi						
-	29SW44						CIVI	29SW44		×							
2	29SW45							29SW45	<u>-</u>	X							
3	29SW46		12/11/04	15.10				29SW46	2	x							
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garanta.							Laborat	on on	12/16/0	430	Sample	r's Signa	- 5/	Un	HUC	· \	
C TAT: 7 du Standard Rush Due: 7 dou'S Seals intact? N Received Good Condition LY N Cold 3.4°C																	

SAMPLE RECEIPT FORM 1

	4			
	of Delivery	Delivered By/Airbill	ECN	
EMAX Courier	en en en en e		Recepient	The state of the s
L Client Delivery			Date	12-17-04
Third Party	UPS	J1787464227	Time	0930
		COC Inspection		
Client Name		Sampler Name	Sampling	Date/Time/Location
Address	_	Courier Signature/Date/Time	Analysis I	Required
Gient PM/FC		TAT	Matrix	
Tel #/Fax #	ŕ	Sample ID	Preservat	ive (if any)
Safety Issues	None	High Concentrations expected		d Site Samples
Comments:	Rad Screening Require			· · · · · · · · · · · · · · · · · ·
			, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	· · · · · · · · · · · · · · · · · · ·			
		Packaging Inspection		
Container	Cooler	□ Box		
Condition	Custody Seal		amaged	
Packaging	Bubble Pack		ufficient	plastic bag
Temperatures	Cooler 1 3.42° c		,	Plastic bug
	Cooler 5	The state of the s	oler 3	Cooler 4
		generally and the second secon		Cooler 8
Comments:	Cooler 9	Cooler 10 Cool	oler 11	Cooler 12
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	The state of the s			
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<u> </u>				
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United Parcel Service, Louisville, KY	DATE OF SHIPMENT

REPORTING CONVENTIONS

DATA QUALIFIERS:

Lab Qualifier	AFCEE Qualifier	Description
. J	F	Indicates that the analyte is positively identified and the result is less than RL but greater than MDL.
N	and the state of t	Indicates presumptive evidence of a compound.
E	В	Indicates that the analyte is found in the associated method blank as well as in the sample at above QC level.
97000 97000 97000 97000 97000		Indicates that the result is above the maximum calibration range.
Ř	*	Out of QC limit.

Note: The above qualifiers are used to flag the results unless the project requires a different set of qualification criteria.

ACRONYMS AND ABBREVIATIONS:

CRDL	Contract Required Detection Limit
RL	Reporting Limit
MRL.	Method Reporting Limit
PQL	Practical Quantitation Limit
MDL,	Method Detection Limit
DO	Diluted out

DATES

The date and time information for leaching and preparation reflect the beginning date and time of the procedure unless the method, protocol, or project specifically requires otherwise.

LABORATORY REPORT FOR

SHAW E&I

LONGHORN ARMY AMMUNITION PLANT

EPA METHOD 8330 EXPLOSIVES

SDG#: 04L142

CASE NARRATIVE

CLIENT:

SHAW E&I

PROJECT:

LONG HORN ARMY AMMUNITION PLANT

EMAX SDG:

04L142

EPA METHOD 8330 EXPLOSIVES

One (1) water and six (6) soil samples were received on 12/17/04 for Explosives analysis by EPA Method 8330 in accordance with USEPA-SW846 3rd edition, and EMAX-8330.

1. Holding Time

Analytical holding time was met. Extraction for water samples was started and completed on 12/20/04. Extraction for soil samples was started on 12/20/04 and completed on 12/21/04

2. Calibration

Initial calibration was 5 point. %RSDs were within 20%. All continuing calibrations of the primary column were carried out at 12-hour intervals and the recoveries were within 85-115%.

3. Method Blank

Method blanks were free of contamination at the Reporting Limit.

4. Surrogate recovery

Surrogate recoveries in samples L142-05T, 06T, 06J, 07T and 07I were diluted out. All surrogate recoveries in other samples were within QC limits.

5. Lab Control Sample / Lab Control Duplicate

All recoveries were within QC limits.

6. Matrix Spike/Matrix Spike Duplicate

No sample was spiked.

7. Sample Analysis

Sample analyses were within QC requirements. Quantitation is from the primary column. All positive results above RL were confirmed by LC-CN column and the confirmation is presumptive because it was based on retention time window.

Samples were air-dried prior to extraction; hence, no moisture correction was applied to RL, MDL and results.

Sample L142-06 could only be analyzed as a dilution due to dark discoloration of sample extract.

SDG NO.

LAB CHRONICLE EXPLOSIVES

: 04L142

: SHAW E&I Client

Instrument ID : T081 Project : LONGHORN ARMY AMMUNITION PLANT -

					SOIL				
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio	n Prep.	
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
				10.04.00/47.7/	12 (20 (0) 17-70	XL21013A	XL21012A	EXL005S	Method Blank
MBLK1S	EXL005SB	1	NA	12/21/0417:34	12/20/0417:30			EXLOOSS	Lab Control Sample (LCS)
LCS1S	EXL005SL	1	NA	12/21/0418:03	12/20/0417:30	XL21014A	XL21012A		•
29SB81-001	L142-01	1	NA	12/22/0402:13	12/20/0417:30	XL21031A	XL21030A	EXL005S	Field Sample
29SB81-002	L142-02	1	NA	12/22/0402:42	12/20/0417:30	XL21032A	XL21030A	EXL005S	Field Sample
29SD38-MH07	L142-03	1	NA	12/22/0407:59	12/20/0417:30	XL21043A	XL21042A	EXL005S	Field Sample
29SD39-MH08	L142-04	1	NA	12/22/0408:57	12/20/0417:30	XL21045A	XL21042A	EXL005S	Field Sample
29SD41-MH10	L142-05	1	NA	12/22/0409:26	12/20/0417:30	XL21046A	XL21042A	EXL005S	Field Sample
29SD41-MH10DL	L142-05T	10	NA	12/22/0405:35	12/20/0417:30	XL21038A	XL21030A	EXL005S	Diluted Sample
29SD46	L142-06T	10	NA	12/22/0406:32	12/20/0417:30	XL21040A	XL21030A	EXL005S	Diluted Sample
29SD46DL	L142-06J	5000	NA	12/22/0410:23	12/20/0417:30	XL21048A	XL21042A	EXL005S	Diluted Sample
					· · · · · · · · · · · · · · · · · · ·			~	
					WATER		0-136	D	
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio	•	
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
MANUAL MA	EXL004WB	1	ΝA	12/20/0418:27	12/20/0413:00	XL20004A	XL20003A	EXL004W	Method Blank
MBLK1W	EXLOO4WL	i	NA.	12/20/0418:56	12/20/0413:00	XL20005A	XL20003A	EXL004W	Lab Control Sample (LCS)
LCS1W		1	NA NA	12/20/0410:30	12/20/0413:00	XL20006A	XL20003A	EXL004W	LCS Duplicate
LCD1W	EXL004WC				12/20/0413:00	XL20000A	XL20003A	EXLOG4W	Field Sample
29SW46	L142-07	1	NA	12/20/0420:51	• •				Diluted Sample
29SW46DL1	L142-07T	10	NA	12/21/0416:08	12/20/0413:00	XL21010A	XL21002A	EXLO04W	
29SW46DL2	L142-07I	100	NA	12/21/0415:39	12/20/0413:00	XL21009A	XL21002A	EXL004W	Diluted Sample

- Filename

% Moist - Percent Moisture

SAMPLE RESULTS

Client : SHAW E&I Date Collected: 12/16/04 Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SB81-001 Date Analyzed: 12/22/04 02:13 Lab Samp ID: L142-01 Dilution Factor: 1 Lab File ID: XL21031A Matrix : SOIL Ext Btch ID: EXLO05S : NA % Moisture Instrument ID : T-081 Calib. Ref.: XL21030A

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	NĎ	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	_400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	101	63-143	

Client : SHAW E&I
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L142 Date Collected: 12/16/04 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 298881-002 Date Analyzed: 12/22/04 02:42 Lab Samp ID: L142-02 Dilution Factor: 1 Lab File ID: XL21032A Matrix : SOIL Ext Btch ID: EXLO05S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL21030A

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TÉTRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	.400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	102	63-143	

______ Client : SHAW E&I Date Collected: 12/16/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SD38-MH07 Date Analyzed: 12/22/04 07:59 Lab Samp ID: L142-03 Dilution Factor: 1 Lab File ID: XL21043A : SOIL Matrix Ext Btch ID: EXLO05S % Moisture : NA Calib. Ref.: XL21042A Instrument ID : T-081

RESULTS **PARAMETERS** (ug/kg) (ug/kg) (ug/kg) 400 200 **KMX** ND 400 200 RDX ND 1,3,5-TNB ND 400 200 200 400 1,3-DNB ND TETRYL ND 400 200 200 NITROBENZENE ND 400 400 200 2,4,6-TNT 630 4-AM-2,6-DNT ND 400 200 200 400 2-AM-4,6-DNT ND 2,6-DNT 400 200 ND 2,4-DNT ND 400 200 400 200 2-NITROTOLUENE ND 3-NITROTOLUENE ND 400 200 400 200 ND 4-NITROTOLUENE % RECOVERY QC LIMIT SURROGATE PARAMETERS 3,4-DINITROTOLUENE 102 63-143

			====
Client : SHAW E&I	Date	Collected: 12/16/04	
Project : LONGHORN ARMY AMMUNIT		Received: 12/17/04	
Batch No. : 04L142	Date	Extracted: 12/20/04 1	7:30
Sample ID: 29SD39-MH08	Date	Analyzed: 12/22/04 0	8:57
Lab Samp ID: L142-04	Diluti	on Factor: 1	
Lab File ID: XL21045A	Matri	: SOIL	
Ext Btch ID: EXLO05S	% Mois	sture : NA	
Calib. Ref.: XL21042A	Instru	ment ID : T-081	
. NA SAO ESSA AS ESSAS AS ESSAS			

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	5500	400	200
4-AM-2,6-DNT	880	400	200
2-AM-4,6-DNT	1200	400	200
2,6-DNT	300J	400	200
2,4-DNT	710	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	[~] 400	200
4-NITROTOLUENE	ND	400	200
n 1			
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

3,4-DINITROTOLUENE	104	63-143	

Date Collected: 12/16/04 Client : SHAW E&I Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SD41-MH10 Date Analyzed: 12/22/04 09:26 Lab Samp ID: L142-05 Dilution Factor: 1 Lab File ID: XL21046A : SOIL Matrix Ext Btch ID: EXLO05S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL21042A

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
	'= = ='='= = =		
НМХ	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	7000 ′	400	200
4-AM-2,6-DNT	7800	400	200
2-AM-4,6-DNT	9200E	400	200
2,6-DNT	240J	400	200
2,4-DNT	1100	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	NĎ	ິ400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	101	63-143	

_______ Client : SHAW E&I
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L142 Date Collected: 12/16/04 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SD41-MH10DL Date Analyzed: 12/22/04 05:35 Lab Samp ID: L142-05T Dilution Factor: 10 Lab File ID: XL21038A Matrix : SOIL : NA Ext Btch ID: EXLO05S % Moisture Instrument ID : T-081 Calib. Ref.: XL21030A _______

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
НМХ	ND	4000	2000
RDX	ND	4000	2000
1,3,5-TNB	ND	4000	2000
1,3-DNB	ND	4000	2000
TETRYL	ND	4000	2000
NITROBENZENE	ND	4000	2000
2,4,6-TNT	7300	4000	2000
4-AM-2,6-DNT	7800	4000	2000
2-AM-4,6-DNT	9000	4000	2000
2,6-DNT	ND	4000	2000
2,4-DNT	ND	4000	2000
2-NITROTOLUENE	ND	4000	2000
3-NITROTOLUENE	ND	4000	2000
4-NITROTOLUENE	ND	4000	2000
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
11-1-1-1-1-1-1-1-1	No. 400 400 100 400 800 800 800 800		
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column DO: Diluted Out

Date Collected: 12/16/04 Client : SHAW E&I Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 17:30 Sample ID: 29SD46 Date Analyzed: 12/22/04 06:32 Lab Samp ID: L142-06T Dilution Factor: 10 Lab File ID: XL21040A : SOIL Matrix Ext Btch ID: EXL005S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL21030A

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
	-,,		
НМХ	ND	4000	2000
RDX	ND	4000	2000
1,3,5-TNB	ND	4000	2000
1,3-DNB	ND	4000	2000
TETRYL	ND	4000	2000
NITROBENZENE	ND	4000	2000
2,4,6-TNT	11000000E	4000	2000
4-AM-2,6-DNT	ND	4000	2000
2-AM-4,6-DNT	48000	4000	2000
2,6-DNT	15000	4000	2000
2,4-DNT	3500000E	4000	2000
2-NITROTOLUENE	ND	4000	2000
3-NITROTOLUENE	ND	4000	2000
4-NITROTOLUENE	ND	4000	2000
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column DO: Diluted Out $\,$

IN

Client : SHAW E&I	Date Collected: 12/16/04
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/17/04
Batch No. : 04L142	Date Extracted: 12/20/04 17:30
Sample ID: 29SD46DL	Date Analyzed: 12/22/04 10:23
Lab Samp ID: L142-06J	Dilution Factor: 5000
Lab File ID: XL21048A	Matrix : SOIL
Ext Btch ID: EXLO05S	% Moisture : NA
Calib. Ref.: XL21042A	Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
	=========		
нмх	ND	2000000	1000000
RDX	ND	2000000	1000000
1,3,5-TNB	ND	2000000	1000000
1,3-DNB	ND	2000000	1000000
TETRYL	ND	2000000	1000000
NITROBENZENE	ND	2000000	1000000
2,4,6-TNT	26000000	2000000	1000000
4-AM-2,6-DNT	' `ND	2000000	1000000
2-AM-4,6-DNT	ND	2000000	1000000
2,6-DNT	ND	2000000	1000000
2,4-DNT	8000000	2000000	1000000
2-NITROTOLUENE	ND	2000000	1000000
3-NITROTOLUENE	ND	2000000	1000000
4-NITROTOLUENE	ND	2000000	1000000
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column DO: Diluted Out $\footnote{\footnote{Note of the confirmed of the column$

Client : SHAW E&I Date Collected: 12/16/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 13:00 Sample ID: 29SW46 Lab Samp ID: L142-07 Date Analyzed: 12/20/04 20:51 Dilution Factor: 1 Lab File ID: XL20009A : WATER Matrix Ext Btch ID: EXLOO4W % Moisture : NA Calib. Ref.: XL20003A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
нмх	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	.73	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	820E	1	.2
4-AM-2,6-DNT	49É	1	.2
2-AM-4,6-DNT	21E	1	.2
2,6-DNT	7.6	1	.2
2,4-DNT	20E	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	ຶ 1	.2
4-NITROTOLUENE	ND	1	.2
SUPPOCATE DADAMETERS	% DECOVEDY	OC LIMIT	

Note: All positive results are confirmed by CN column

Client : SHAW E&I	1	Date Collected	1: 12/16/04	
Project : LONGHORN ARMY AMMUNITIO	ON PLANT I	Date Received	1: 12/17/04	
Batch No. : 04L142	1	Date Extracted	1: 12/20/04	13:00
Sample ID: 29SW46DL1		Date Analyze	1: 12/21/04	16:08
Lab Samp ID: L142-07T	-1	Dilution Factor	r: 10	
Lab File ID: XL21010A	i	Matrix	: WATER	ø.
Ext Btch ID: EXLOO4W	:	% Moisture	: NA	
Calib. Ref.: XL21002A		Instrument ID	: T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
HMX	ND	10	2
RDX	ND	10	2
1,3,5-TNB	ND	10	2
1,3-DNB	ND	10	2
TETRYL	ND	10	2 2 2 2
NITROBENZENE	ND	10	
2,4,6-TNT	780E	10	2
4-AM-2,6-DNT	48	10	2
2-AM-4,6-DNT	20	10	2
2,6-DNT	7.1J	10	2
2,4-DNT	19	10	2
2-NITROTOLUENE	ND	ຼ 10	2
3-NITROTOLUENE	ND	10	2
4-NITROTOLUENE	ND	10	2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column DO: Diluted Out

Client : SHAW E&I Date Collected: 12/16/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L142 Date Received: 12/17/04 Date Extracted: 12/20/04 13:00 Sample ID: 29SW46DL2 Date Analyzed: 12/21/04 15:39 Dilution Factor: 100 Lab Samp ID: L142-071 Lab File ID: XL21009A : WATER Matrix Ext Btch ID: EXLO04W % Moisture : NA Calib. Ref.: XL21002A Instrument ID : T-081 ______

RESULTS RL MDL **PARAMETERS** (ug/L) (ug/L) (ug/L) ____ 20 HMX ND 100 RDX ND 100 20 1,3,5-TNB ND 100 20 1,3-DNB ND 20 100 TETRYL ND 100 20 20 NITROBENZENE ND 100 20 860 100 2,4,6-TNT 4-AM-2,6-DNT 47J 100 20 20 2-AM-4,6-DNT ND 100 ND 100 20 2,6-DNT 2,4-DNT ND 100 20

ND

ND

100

~100

20

20 20

4-NITROTOLUENE ND 100
SURROGATE PARAMETERS % RECOVERY QC LIMIT
3,4-DINITROTOLUENE DO 63-143

Note: All positive results are confirmed by CN column DO: Diluted Out

2-NITROTOLUENE

3-NITROTOLUENE

QC SUMMARIES

Client :	SHAW E&I	Date Collected: NA
Project :	: LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/20/04
Batch No. :	: 04L142	Date Extracted: 12/20/04 13:00
Sample ID:	: MBLK1W	Date Analyzed: 12/20/04 18:27
Lab Samp ID:	: EXLOO4WB	Dilution Factor: 1
Lab File ID:	: XL20004A	Matrix : WATER
Ext Btch ID:	: EXLOO4W	% Moisture : NA
Calib. Ref.:	: XL20003A	Instrument ID : T-081

DIDINETEDO	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
НМХ	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	ND	1	.2
4-AM-2,6-DNT	ND	1	.2
2-AM-4,6-DNT	ND	1	.2
2,6-DNT	ND	1	.2
2,4-DNT	ND	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	ຶ 1	.2
4-NITROTOLUENE	NĎ	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	100	63-143	

EMAX QUALITY CONTROL DATA LCS/LCD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L142

METHOD: EPA 8330

MATRIX: DILUTION FACTOR: 1

WATER

NA

SAMPLE ID:

MBLK1W

EXL004WB

EXL004WL

EXL004WC

XL20004A

XL20005A

XL20006A

DATE EXTRACTED: 12/20/0413:00 12/20/0413:00 12/20/0413:00 12/20/0418:27 12/20/0418:56 12/20/0419:24 DATE COLLECTED: NA DATE RECEIVED:

% MOISTURE:

12/20/04

DATE ANALYZED: PREP. BATCH:

LAB SAMP ID:

LAB FILE ID:

EXL004W

EXL004W

EXL004W

CALIB. REF:

XL20003A

XL20003A

/ XL20003A

ACCESSION:

	BLNK RSLT	SPIKE AMT	BS RSLT	BS	SPIKE AMT	BSD RSLT	BSD	RPD	QC LIMIT	MAX RPD
PARAMETER	(ug/L)	(ug/L)	(ug/L)	% REC	(ug/L)	(ug/L)	% REC	(%)	(%)	(%)
	,,-									
нмх	ND	4	3.84	96	4	3.99	100	4	70-130	30
RDX	ND	4	3.31	, 83	4	3.19	80	4	60-130	30
1,3,5-TNB	ND	4	4.03	101	4	4.06	101	1	70-130	30
1,3-DNB	ND	4	3.85	96	4	3.86	. 96	Ó	70-130	30
Tetryl	ND	4	4.08	102	4	4.1	102	0	50-140	30
Nitrobenzene	ND	4	3.62	90	4	3.64	91	1	60-130	30
2,4,6-TNT	DN	4	4.18	105	4	4.22	105	1	70-140	30
4-AM-2,6-DNT	ND	4	3.92	98	4	3.92	98	0	70-130	30
2-AM-4,6-DNT	ND	4	4.01	100	4	4.04	101	1	70-130	30
2,6-DNT	ND	4	4.03	101	4	4.07	102	1	70-130	30
2,4-DNT	ND	4	4.13	103	4	4.12	103	Ö	70-130	30
2 ² Nitrotoluene	ND	4	3.81	95	4	3.81	95	0	70-130	30
3-Nitrotoluene	ND	4	3.99	100	4	4.02	100	1	70-130	30
4-Nitrotoluene	ND	4	4.02	100	4	4.07	102	1	70-130	30

	SPIKE AMT	BS RSLT	BS	SPIKE AMT	BSD RSLT	BSD	QC LIMIT	
SURROGATE PARAMETER	(ug/L)	(ug/L)	% REC	(ug/L)	(ug/L)	% REC	(%)	
-,								
3,4-Dinitrotoluene	4	4.09	102	4	4.27	107	70-130	

=========			
Client : S	SHAW E&I	Date Collected:	NA
Project : l	LONGHORN ARMY AMMUNITION PLANT	Date Received:	12/20/04
Batch No. : (04L142	Date Extracted:	
Sample ID: N	MBLK1S	Date Analyzed:	12/21/04 17:34
Lab Samp ID: E	EXL005SB	Dilution Factor:	1
Lab File ID:)	XL21013A	Matrix :	SOIL
Ext Btch ID: 8	EXL005S	% Moisture :	NA –
Calib. Ref.:)	XL21012A	Instrument ID :	T-081

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	˝400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	103	63-143	

EMAX QUALITY CONTROL DATA LCS ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L142

EPA 8330 METHOD:

MATRIX: DILUTION FACTOR: 1

SOIL

MBLK1S

EXL005SB

EXL005SL XL21014A

1

LAB SAMP ID: LAB FILE ID: DATE EXTRACTED: 12/20/0417:30 12/20/0417:30

SAMPLE ID:

XL21013A

12/21/0417:34 12/21/0418:03

DATE COLLECTED: NA

% MOISTURE:

DATE RECEIVED: 12/20/04

NA

PREP. BATCH:

DATE ANALYZED: CALIB. REF:

EXL005s XL21012A EXL005s

XL21012A

ACCESSION:

PARAMETER	BLNK RSLT (ug/kg)	SPIKE AMT (ug/kg)	BS RSLT (ug/kg)	BS % REC	QC LIMIT
нмх	ND	2000	2110	106	70-140
RDX	ND	2000	2100	105	70-140
1,3,5-TNB	ND	2000	2180	109	70-130
1,3-DNB	ND	2000	2180	109	70-130
Tetryl	ND	2000	2080	104	60-140
Nitrobenzene	ND	2000	2190	109	70-130
2,4,6-TNT	ND	2000	2180	109	70-140
4-AM-2,6-DNT	ND	2000	2160	108	70-130
2-AM-4,6-DNT	ND	2000	2170	109	70-130
2,6-DNT	ND	2000	2120	106	70-140
2,4-DNT	ND	2000	2140	107	70-130
2-Nitrotoluene	ND	2000	2000	100	70-130
3-Nitrotoluene	ND	2000	2090	105	70-130
4-Nitrotoluene	ND	2000	2090	105	70-130

	SPIKE AMT	BS RSLT	BS	QC LIMIT	
SURROGATE PARAMETER	(ug/kg)	(ug/kg)	% REC	(%)	
3.4-Dinitrotoluene	2000	2260	113	70-130	

INITIAL CALIBRATION

Lab Name : EMAX Inc
Instrument ID : HPLC1 81
GC Columm : VARIAN C18
Column size ID : 25CMX4.6MM
LFID & Datetime: XJ19016A 10/19/04 19:08

LFID & Datetime: XJ19016A 10/19/04 19:36 LFID & Datetime: XJ19017A 10/19/04 17:41 LFID & Datetime: XJ19013A 10/19/04 18:10 LFID & Datetime: XJ19015A 10/19/04 18:39

CONC UNIT: ppb

	CONC	CALI	RATION FA	ACTORS (A	AREA or HE	IGHT)/UN	T	
COMPOUND	Х	1.00X	5.00X	10.00X	20.00X	40.00X	MEAN	%RSD
		=======		=======		=======		====
HMX	20.00	69.25	67.82	72.36	72.87	71.66	70.79	3.1
RDX	20.00	80.55	89.55	93.32	92.82	91.48	89.54	5.8
1,3,5-TNB	20.00	212.60	206.29	208.40	210.28	208.06	209.13	1.1
1,3-DNB	20.00	284.05	289.17	293.78	291.57	290.36	289.79	1.3
Tetryl	20.00	169.65	165.60	171.93	171.00	171.53	169.94	1.5
Nitrobenzene	20.00	196.75	195.67	202.54	203.55	201.64	200.03	1.8
2,4,6-TNT	20.00	206.40	200.92	203.90	208.44	205.06	204.94	1.4
4-AM-2,6-DNT	20.00	156.75	144.28	146.21	146.58	146.43	148.05	3.3
2-AM-4,6-DNT	20.00	229.95	205.98	210.31	215.07	216.25	215.51	4.2
2,6-DNT	20.00	137.60	131.99	135.36	140.29	135.29	136.11	2.3
2,4-DNT	20.00	276.20	270.64	273.11	277.46	281.68	275.82	1.5
2-Nitrotoluene	20.00	130.40	127.75	127.93	129.28	128.10	128.69	0.9
4-Nitrotoluene	20.00	104.40	103.10	107.11	109.25	110.43	106.86	2.9
3-Nitrotoluene	20.00	132.95	130.43	138.71	137.68	140.89	136.13	3.2
SURROGATE	Х	1.00X	5.00X	10.00X	20.00X	40.00X	MEAN	%RSD
		=======		=======	======	=======		====
3,4-Dinitrotoluene	20.00	117.40	121.21	124.62	126.61	126.82	123.33	3.2
			<u> </u>	l		<u></u>		I

EX81J19.MET

: EMAX Inc Lab Name Instrument ID : HPLC1 81

Instrument ID : HPLC1 81
GC Column : VARIAN C18
Column size ID : 25CMX4.6MM
LFID & Datetime: XJ19016A 10/19/04 19:36
LFID & Datetime: XJ19017A 10/19/04 17:41
LFID & Datetime: XJ19013A 10/19/04 17:41
LFID & Datetime: XJ19014A 10/19/04 18:10
LFID & Datetime: XJ19015A 10/19/04 18:39

		RT OF STANDARDS (MIN)						MDOW	RTWINDOW
COMPOUND	1.0X	5.0X	10.0X	20.0X	40.0X	RT	FROM	TO	WIDTH
	=====	=====	======	=====	=====	=====	=====	=====	
HMX	4.300	4.292	4,292	4.292	4.275	4.290	4.240	4.340	0.050
RDX	6.433	6.383	6.367	6.375	6.333	6.378	6.240	6.516	0.138
1,3,5-TNB	8.650	8.617	8.600	8.633	8.575	8.615	8.462	8.768	0.153
1,3-DNB	10.492	10.450	10.417	10.483	10.400	10.448	10.219	10.677	0.229
Tetryl	11.358	11.308	11.250	11.342	11.250	11.302	11.014	11.590	0.288
Nitrobenzene	12.117	12.092	12.042	12.108	12.033	12.078	11.677	12.479	0.401
2,4,6-TNT	13.675	13.642	13.567	13.642	13.575	13.620	13.219	14.021	0.401
4-AM-2,6-DNT	14.433	14.392	14.292	14.383	14.308	14.362	13.857	14.867	0.505
2-AM-4,6-DNT	14.967	14.983	14.867	14.950	14.883	14.930	14.382	15.478	0.548
2,6-DNT	15.817	15.825	15.742	15.800	15.758	15.788	15.325	16.251	0.463
2,4-DNT	16.383	16.425	16.317	16.367	16.350	16.368	15.891	16.845	0.477
2-Nitrotoluene	19.467	19.525	19.442	19.458	19.467	19.472	18.881	20.063	0.591
4-Nitrotoluene	21.192	21.225	21.150	21.175	21.142	21.177	20.520	21.834	0.657
3-Nitrotoluene	22.658	22.717	22.592	22.633	22.600	22.640	21.888	23.392	0.752
									[
SURROGATE	1.0x	5.0x	10.0X	20.0X	40.0X	RT	FROM	ТО	WIDTH
	22222			=====				1	
3,4-Dinitrotoluene	12.900	12.858	12.792	12.875	12.792	12.843	12.468	13.218	0.375
	l	l	<u> </u>	l	l				

EX81J19.MET

SECOND SOURCE

Lab Name Instrument ID

GC Column

: EMAX

: HPLC1 81 VARIAN C18 Column size ID : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XJ19018A 10/19/2004 20:05

CONC UNIT : ppb

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======		======	======	=======	======	======	=====	==	=====
HMX	4.300	4.250	4.350	400.0	70.800	31158	440.13	10	1	15
RDX	6.400	6.262	6.538	400.0	89.500	38533	430.32	8		. 15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	91920	439.54	10	1	15
1,3-DNB	10.483	10.254	10.712	400.0	289.800	127403	439.64	10]	15
Tetryl	11.342	11.054	11.630	400.0	169.900	71202	418.98	5	Ì	15
Nitrobenzene	12.108	11.707	12.509	400.0	200.000	86805	433.96	8		15
2,4,6-TNT	13.625	13.224	14.026	400.0	204.900	88599	432.31	8	l	15
4-AM-2,6-DNT	14.400	13.895	14.905	400.0	148.100	60914	411.44	3	İ	15
2-AM-4,6-DNT	14.950	14.402	15.498	400.0	215.500	91200	423.18	6	1	15
2,6-DNT	15.800	15.337	16.263	400.0	136.100	56248	413.27	3		15
2,4-DNT	16.383	15.906	16.860	400.0	275.800	117421	425.72	6	1	15
2-Nitrotoluene	19.475	18.884	20.066	400.0	128.700	53460	415.40	4		15
4-Nitrotoluene	21.192	20.535	21.849	400.0	106.900	46579	435.89	9	1	15
3-Nitrotoluene	22.667	21.915	23.419	400.0	136.100	57575	422.93	6.		15
						,				
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======				=======	=======	======	==	=====
3,4-Dinitrotoluene	12.875	12.500	13.250	400.0	123.300	52174	423.04	6		15

EX81J19.MET

Lab Name : EMAX Inc

Instrument ID : HPLC1 LCT001(T017)
GC Columm : LUNA 5U PHENYL-HEXYL
Column size ID : 25CMX4.6MM
LFID & Datetime: PH17007A 08/17/04 16:21
LFID & Datetime: PH17003A 08/17/04 13:35
LFID & Datetime: PH17004A 08/17/04 14:16 LFID & Datetime: PH17005A 08/17/04 14:58 LFID & Datetime: PH17006A 08/17/04 15:39

CONC UNIT: ppb

	CONC	CALI	RATION FA	ACTORS (/	AREA or HE	IGHT)/UN	ĪŢ	
COMPOUND	Х	1.00X	5.00X	10.00X	20.00X	40.00X	MEAN	%RSD
			======		=======			====
HMX	20.00	265.05	223.86	243.86	247.42	244.74	244.99	6.0
RDX	20.00	315.15	255.37	260.41	253.93	258.37	268.65	9.7
Nitrobenzene	20.00	359.70	349.71	329.86	323.97	326.71	337.99	4.7
1,3-DNB	20.00	514.05	508.34	520.54	516.70	515.48	515.02	0.9
2-Nîtrotoluene	20.00	238.50	278.15	281.94	287.52	281.20	273.46	7.3
4-Nitrotoluene	20.00	287.00	275.75	289.34	288.21	284.04	284.87	1.9
4-AM-2,6-DNT	20.00	276.50	256.61	256.86	264.78	254.15	261.78	3.5
3-Nitrotoluene	20.00	353.75	380.73	345.64	344.94	337.55	352.52	4.8
2-AM-4,6-DNT	20.00	464.60	447.94	400.02	400.57	393.79	421.38	7.7
1,3,5-TNB	20.00	368.85	364.11	349.42	354.06	340.07	355.30	3.2
2,6-DNT	20.00	258.20	256.25	261.51	248.39	253.99	255.67	1.9
2,4-DNT	20.00	433.50	511.11	524.55	509.46	513.54	498.43	7.4
Tetryl	20.00	511.65	504.42	558.66	520.24	525.23	524.04	4.0
2,4,6-TNT	20.00	421.55	507.22	574.38	536.85	548.40	517.68	11.4
SURROGATE	Х	1.00x		10.00X	20.00X	40.00X		%RSD
3,4-DNT	20.00	288.40	260.85	245.15	į.	241.54	256.04	7.7
		l	l			***************************************	<u> </u>	l

EX17H17C.MET

1/96

Lab Name : EMAX Inc

Instrument ID : HPLC1 LCT001(T017)
GC Column : LUNA 5U PHENYL-HEXYL

GC COLUMN : LUMA 30 FRENTE NEATE
COLUMN size ID : 25CMX4.6MM
LFID & Datetime: PH17007A 08/17/04 16:21
LFID & Datetime: PH17003A 08/17/04 13:35
LFID & Datetime: PH17004A 08/17/04 14:16 LFID & Datetime: PH17005A 08/17/04 14:58 LFID & Datetime: PH17006A 08/17/04 15:39

	<u> </u>	RT OF S	TANDAR	S (MI)	N)	MEAN	RT W	NDOW	RTWINDOW
COMPOUND	1.0x	5.0x	10.0X	20.0X	40.0X	RT	FROM	то	WIDTH
	=====	=====	=====	=====	=====	======	======	=====	=======
HMX	6.025		6.042	6.058	6.033	6.042	5.962	6.122	0.080
RDX	7.800	7.817	7.817	7.833	7.792	7.812	7.708	7.916	0.104
Nitrobenzene		10.675							
1,3-DNB	15.183	15.258	15.258	15.292	15.175	15.233	14.872	15.594	0.361
2-Nitrotoluene	15.725	15.783	15.767	15.817	15.692	15.757	15.497	16.017	0.260
4-Nitrotoluene	16.225	16.342	16.342	16.375	16.258	16.308	16.018	16.598	0.290
4-AM-2,6-DNT	16.950	17.108	17.108	17.150	17.000	17.063	16.500	17.626	0.563
3-Nitrotoluene	17.700	17.800	17.775	17.825	17.700	17.760	17.393	18.127	0.367
2-AM-4,6-DNT		19.125							
1,3,5-TNB	20.142	20.267	20.267	20.317	20.200	20.239	19.626	20.852	0.613
2,6-DNT	21.517	21.642	21.650	21.683	21.558	21.610	20.886	22.334	0.724
2,4-DNT		22.825							
Tetryl	31.667	31.808	31.850	31.875	31.617	31.763	30.113	33.413	1.650
2,4,6-TNT	33.233	33.367	33.358	33.375	33.150	33.297	31.954	34.640	1.343
SURROGATE	1.0X	5.0X	10.0X	20.0X	40.0X	RT :	FROM	то	WIDTH
			======	1	=====	i	=====	1	======
3,4-DNT	18.492	18.650	18.600	18.675	18.525	18.588	18.055	19.121	0.533
						l			ll

EX17H17C.MET

DAILY CALIBRATION

Lab Name Instrument ID : EMAX

GC Column Column size ID

: HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL20003A 12/20/2004 17:58

CONC UNIT

	RT	RT WI	NDON	TRUE	AVERAGE	RESL	II T			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	=======	=======	=======	=====	==	=====
HMX	4.292	4.242	4.342	400.0	70.800	28461	402.03	1		15
RDX	6.300	6.162	6.438	400.0	89.500	35641	398.02	-0		15
1,3,5-TNB	8.500	8.347	8.653	400.0	209.100	83199	397.84	-1		15
1,3-DNB	10.250	10.021	10.479	400.0	289.800	115929	400.05	.01		15
Tetryl	11.000	10.712	11.288	400.0	169.900	68123	400.86	0		15
Nitrobenzene	11.792	11.391	12.193	400.0	200.000	80732	403.60			15
2,4,6-TNT	13.300	12.899	13.701	400.0	204.900		393.51	-2		15
4-AM-2,6-DNT	13.875	13.370	14.380		148.100		407.78	2		15
2-AM-4,6-DNT	14.408		14.956	400.0	215.500		401.82	0		15
2,6-DNT	15.358		15.821	400.0				2	ļ	15
2,4-DNT	15.908	15.431	16.385	400.0	275.800	111329	403.63	1		15
2-Nitrotoluene	18.875	18.284	19.466	400.0	128.700	51626	401.15	0		15
4-Nitrotoluene	20.425	19.768	21.082	400.0	106.900	45124	422.27	6		15
3-Nitrotoluene	21.842	21.090	22.594	400.0	136.100	57301	420.92	5		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	=======	=======		=====	==	=====
3,4-Dinitrotoluene	12.517	12.142	12.892	400.0	123.300	50724	411.28	3		15
				<u></u>	<u> </u>	<u> </u>		<u> </u>	<u> _</u>	<u> </u>

Lab Name Instrument ID : EMAX

Instrument ID GC Column : HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL20015A 12/20/2004 23:44

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======	======	========		.======		==	=====
HMX	4.333	4.283	4.383	400.0	70.800	29272	413.49	3		15
RDX	6.408	6.270	6.546	400.0	89.500	38105	425.54	6		15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	85122	407.03	2		15
1,3-DNB	10.467	10.238	10.696	400.0	289.800	119721	413.14	3		15
Tetryl	11.275	10.987	11.563	400.0	169.900	69968	411.72	3		15
Nitrobenzene	12.042	11.641	12.443			1 .	414.92	4		15
2,4,6-TNT	13.592	13.191	13.993	400.0	204.900	84236	411.02	3		15
4-AM-2,6-DNT	14.333	13.828	14.838	400.0	148.100			.4		15
2-AM-4,6-DNT	14.875	14.327	15.423	400.0	215.500	87276	404.97	1	1	15
2,6-DNT	15.750	15.287	16.213	400.0	136.100	57777	424.50	6		15
2,4-DNT	16.325	15.848	16.802	400.0	275.800	113421	411.21	3	l	15
2-Nitrotoluene	19.358	18.767	19.949	400.0	128.700	52495	407.90		1	, 15
4-Nitrotoluene	20.983	20.326	21.640	400.0	106.900	46819	438.13	10	1	15
3-Nitrotoluene	22.450	21.698	23.202	400.0	136.100	57711	423.93	6		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	=======				==	=====
3,4-Dinitrotoluene	12.850	12.475	13.225	400.0	123.300	51463	417.27	4		15
	<u> </u>	<u> </u>	l	1	<u> </u>		<u> </u>		١	l ————

Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column

: VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10
Conc Cont LFID & Datetime: XL21002A 12/21/2004 12:17
CONC UNIT : ppb

	RT	RT WI	NDOW	TRUE	AVERAGE	RESI	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======	======		=======	=======	=====	==	=====
HMX	4.308	4.258	4.358	400.0	70.800	28235	398.84	-0	ĺ	15
RDX	6.342	6.204	6.480	400.0	89.500	36063	402.74		١.	15
1,3,5-TNB	8.550	8.397	8.703	400.0	209.100	82108	392.62	-2	1 :	15
1,3-DNB	10.325	10.096	10.554	400.0	289.800	115534	398.69	-0	1	15
Tetryl	11.108	10.820	11.396	400.0	169.900	67938	399.77	-0		15
Nitrobenzene	11.875	11.474	12.276	400.0	200.000	79947	399.67			15
2,4,6-TNT	13.400	12.999	13.801	400.0	204.900	80421	392.40	-2	Ì	15
4-AM-2,6-DNT	14.033	13.528	14.538	400.0	148.100	59823	404.07			15
2-AM-4,6-DNT	14.558	14.010	15.106	400.0	215.500	84462	391.91	-2		15
2,6-DNT	15.492	15.029	15.955	400.0	136.100	54767	402.38	1		15
2,4-DNT	16.033	15.556	16.510	400.0	275.800	110265	399.77	-0		15
2-Nitrotoluene	19.008	18.417	19.599	400.0	128.700	51046	396.64	-1	1	15
4-Nitrotoluene	20.592	19.935	21.249	400.0	106.900	45322	424.12	6	1	15
3-Nitrotoluene	22.008	21.256	22.760	400.0	136.100	56862	417.70	4	1	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
220202020222222222222222222222	======			======			=======	=====	==	======
3,4-Dinitrotoluene	12.633	12.258	13.008	400.0	123.300	49767	403.52	1		15
	1	l	1					1	·	l

Lab Name Instrument ID : EMAX

: HPLC1 81

GC Column Column size ID

: VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10
Conc Cont LFID & Datetime: XL21012A 12/21/2004 17:05
CONC UNIT : ppb

	RT	RT WI	MOOM	TRUE	AVERAGE	RESL	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======		=======	=======	=====	==	=====
HMX	4.300	4.250	4.350	400.0	70.800	28637	404.52	1	1	15
RDX	6.325	6.187	6.463	400.0	89.500	35492	396.36	-1		15
1,3,5-TNB	8.525	8.372	8.678	400.0	209.100	83787	400.65	.0		15
1,3-DNB	10.283	10.054	10.512	400.0	289.800	116602	402.37	1		15
Tetryl	11.033	10.745	11.321	400.0	169.900	68756	404.58	1		15
Nitrobenzene	11.833	11.432	12.234	400.0	200.000	81307	406.47	2		15
2,4,6-TNT	13.350	12.949	13.751	400.0	204.900	80995	395.20	-1		15
4-AM-2,6-DNT	13.925	13.420	14.430	400.0	148.100	61989	418.70	5		15
2-AM-4,6-DNT	14.442	13.894	14.990	400.0	215.500	85780	398.03	-0		15
2,6-DNT	15.417	14.954	15.880	400.0	136.100	55335	406.56	2		15
2,4-DNT	15.950	15.473	16.427	400.0	275.800	111179	403.09	1		15
2-Nitrotoluene	18.933	18.342	19.524	400.0	128.700	51488	400.08	0	1	15
4-Nitrotoluene	20.508	19.851	21.165	400.0	106.900	44634	417.68	4		15
3-Nitrotoluene	21.917	21.165	22.669	400.0	136.100	57110	419.52	5		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	OT.	LIMITS
	======	======	======	======		=======	=======	=====	==	
3,4-Dinitrotoluene	12.575	12.200	12.950	400.0	123.300	51157	414.79	4		15
			<u> </u>	l			l	<u> </u>	 _	<u> </u>

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21021A 12/21/2004 21:25

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESL	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
			======	======	=======	=======	=======	=====	==	=====
HMX	4.333	4.283	4.383	400.0	70.800	29529	417.12	4		15
RDX	6.408	6.270	6.546	400.0	89.500	36651	409.30	2		15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	83931	401.34	0		15
1,3-DNB	10.458	10.229	10.687	400.0	289.800	118138	407.67	2	l	15
Tetryl	11.258	10.970	11.546	400.0	169.900	68631	403.85	1		15
Nitrobenzene	12.033	11.632	12.434	400.0	200.000	81515	407.51	2	1	15
2,4,6-TNT	13.583	13.182	13.984	400.0	204.900	82418	402,15	1		15
4-AM-2,6-DNT	14.300	13.795	14.805	400.0	148.100	60872	411.15	.3		15
2-AM-4,6-DNT	14.850	14.302	15.398	400.0	215.500	85539	396.91	-1	1	15
2,6-DNT	15.733	15.270	16.196	400.0	136.100	56026	411.63	3:	1	15
2,4-DNT	16.308	15.831	16.785	400.0	275.800	111103	402.81	1	1	15
2-Nitrotoluene	19.342	18.751	19.933	400.0	128.700	52850	410.66	.3		15
4-Nitrotoluene	20.992	20.335	21.649	400.0	106.900	43058	402.94	1		15
3-Nitrotoluene	22.442	21.690	23.194	400.0	136.100	56680	416.36	4		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
3,4-Dinitrotoluene	12.833	12.458	13.208		123.300	50526	409.68	2		1:

Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column

: VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21030A 12/22/2004 01:44

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======			======	=======	=======	=======	=====	==	=====
HMX	4.358	4.308		400.0			406.27	2	1	15
RDX	6.475	6.337	6.613	400.0	89.500	36851	411.54	3		15
1,3,5-TNB	8.717	8.564	8.870	400.0	209.100	85213	407.47	2		15
1,3-DNB	10.583	10.354	10.812	400.0	289.800	118482	408.86	2	1	15
Tetryl	11.425	11.137	11.713	400.0	169.900	68419	402.60	1		15
Nitrobenzene	12.183	11.782	12.584	400.0	200.000	82651	413.19	3	1	15
2,4,6-TNT	13.758	13.357	14.159	400.0	204.900	84235	411.01	3		15
4-AM-2,6-DNT	14.583	14.078	15.088	400.0	148.100	60816	410.78	3		15
2-AM-4,6-DNT	15.158	14.610	15.706	400.0	215.500	86030	399.19	-0		15
2,6-DNT	15.992	15.529	16.455	400.0	136.100	57301	421.00	5		15
2,4-DNT	16.567	16.090	17.044	400.0	275.800	111937	405.83	1	1	15
2-Nitrotoluene	19.650	19.059	20.241	400.0	128.700	51783	402.37	1	1	15
4-Nitrotoluene	21.333	20.676	21.990	400.0	106.900	44795	419.19	5	1	15
3-Nitrotoluene	22.808	22.056	23.560	400.0	136.100	55798	409.88	2	j	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======			======		=======	=======	=====	==	=====
3,4-Dinitrotoluene	13.025	12.650	13.400	400.0	123.300	50569	410.02	3	1	15
					2				.	

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21042A 12/22/2004 07:30

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======				======	======	==	=====
HMX	4.367	4.317	4.417	400.0	70.800	28930	408.65	2		15
RDX	6.500	6.362	6.638	400.0	89.500	36558	408.26	2		15
1,3,5-TNB	8.758	8.605	8.911	400.0	209.100	85438	408.55	2		15
1,3-DNB	10.633	10.404	10.862	400.0	289.800	118329	408.33	2		15
Tetryl	11.492	11.204	11.780	400.0	169.900	68305	401.93	0		15
Nitrobenzene	12.242	11.841	12.643	400.0	200.000	81988	409.88	2		15
2,4,6-TNT	13.825	13.424	14.226	400.0	204.900	83467	407.27	2	:	15
4-AM-2,6-DNT	14.692	14.187	15.197	400.0	148.100	60261	407.03	2	1	15
2-AM-4,6-DNT	15.267	14.719	15.815	400.0	215.500	85239	395.52	-1		15
2,6-DNT	16.083	15.620	16.546	400.0	136.100	56754	416.98	4	1	15
2,4-DNT	16.675	16.198	17.152	400.0	275.800	110980	402.36	1	1	15
2-Nitrotoluene	19.758	19.167	20.349	400.0	128.700	52534	408.21	2	1	15
4-Nitrotoluene	21.458	20.801	22.115	400.0	106.900	44762	418.88	5	1	15
3-Nitrotoluene	22.925	22.173	23.677	400.0	136.100	55440	407.25	2		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	1	LIMITS
	47 400	40.777	47 /07		497 700	E0700	/07.0/		==	15
3,4-Dinitrotoluene	13.108	12.733	13.483	400.0	123.300	50300	407.84	2		1 15
	1	I 	ļ	l——			· ———	l	i	I

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21049A 12/22/2004 10:52

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======					=======	=====	==	=====
HMX	4.342	4.292	4.392	400.0	70.800	28491	402.45	1		15
RDX	6.433	6.295	6.571	400.0	89.500	35789	399.68	-0		15
1,3,5-TNB	8.675	8.522	8.828	400.0	209.100	82418	394.10	-1		15
1,3-DNB	10.517	10.288	10.746	400.0	289.800	115799	399.60	-0		15
Tetryl	11.333	11.045	11.621	400.0	169.900	66936	393.88	-2		15
Nitrobenzene	12.108	11.707	12.509	400.0	200.000	81062	405.25	1	Ì	15
2,4,6-TNT	13.667	13.266	14.068	400.0	204.900	82012	400.17	0	1	15
4-AM-2,6-DNT	14.433	13.928	14.938	400.0	148.100	60592	409.26	2	1	15
2-AM-4,6-DNT	14.983	14.435	15.531	400.0	215.500	85034	394.57	-1	1	15
2,6-DNT	15.867	15.404	16.330	400.0	136.100	56030	411.66	3	1	15
2,4-DNT	16.433	15.956	16.910	400.0	275.800	110610	401.02	0	1	15
2-Nitrotoluene	19.500	18.909	20.091	400.0	128.700	51773	402.29	1		15
4-Nitrotoluene	21.158	20.501	21.815	400.0	106.900	43310	405.30	1] .	15
3-Nitrotoluene	22.617	21.865	23.369	400.0	136.100	54824	402.73	1		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	Q٢	LIMITS
	======	======	======	======				=====	==	=====
3,4-Dinitrotoluene	12.933	12.558	13.308	400.0	123.300	50308	407.91	2		15
a 1								<u> </u>	_	

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017)

GC Column

: LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Conc Cont LFID & Datetime: PL21002A 12/21/2004 14:29

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

CONC UNIT

A CONTRACT OF THE PROPERTY OF	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
			=======	======	=======	=======	=======	=====	==	=====
HMX	6.125	6.045	6.205	400.0	245.000	97335	397.31	-1		15
RDX	7.933	7.829	8.037	400.0	268.600			-6		15
Nitrobenzene	10.725	10.621	10.829	400.0	338.000	131155		-3		15
1,3-DNB	15.442	15.081	15.803	400.0	515.000	191677	372.17	-7		15
2-Nitrotoluene	15.850	15.590	16.110	400.0	273.500	107744	394.00	-2		15
4-Nitrotoluene	16.450	16.160	16.740	400.0	284.900	117212	411.46	3		15
4-AM-2,6-DNT	17.433	16.870	17.996	400.0	261.800	89732	342.78			15
3-Nitrotoluene	17.883	17.516	18.250	400.0	352.500	145090	411.58		ļ	15
2-AM-4,6-DNT	19.600	18.842	20.358	400.0	421.400	157332	373.37	•		15
1,3,5-TNB	20.467	19.854	21.080	400.0	355.300	135909	382.52	,		15
2,6-DNT	21.867	21.143	22.591	400.0	255.700	96515	377.50	1		15
2,4-DNT	23.225	22.428	24.022	400.0	498.400		401.77	•		15
Tetryl	32.650	31.000	34.300	400.0	524.000		359.79	,	!	15
2,4,6-TNT	33.833	32.490	35.176	400.0	517.700	227459	439.38	10		15
SURROGATE	MINUTES	FROM	ТО	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
			======	======	=======		=======	22222	==	=====
3,4-DNT	18.908	18.375	19.441	400.0	256.000	92885	362.77	-9		15
	.	l]	<u> </u>		I	

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

GC Column

Column size ID : 25CMX4.6MM
Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58
Conc Cont LFID & Datetime: PL21013A 12/21/2004 22:06
CONC UNIT : ppb

<u> </u>	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	========		======	=====	==	=====
нмх	6.200	6.120	6.280	400.0	245.000	97276		-1		15
RDX	8.042	7.938	8.146	400.0	268.600	100724	374.93	-6		15
Nitrobenzene	10.883	10.779	10.987	400.0	338.000	129845	384.17	-4		15
1,3-DNB	15.733	15.372	16.094	400.0	515.000	200479	389.26	-3	ļ	15
2-Nitrotoluene	16.150	15.890	16.410	400.0	273.500	105320	385.14	-4		15
4-Nitrotoluene	16.767	16.477	17.057	400.0	284.900	119340	418.93	5	i	15
4-AM-2,6-DNT	18.058	17.495	18.621	400.0	261.800	93293	356.38	-11		15
3-Nitrotoluene	18.250	17.883	18.617	400.0	352.500	142248	403.51	1		15
2-AM-4,6-DNT	20.108	19.350	20.866	400.0	421.400	160422	380.70	-5		15
1,3,5-TNB	20.933	20.320	21.546	400.0	355.300	139700	393.19			15
2,6-DNT	22.450	21.726	23.174	400.0	255.700	98773	386.33	-3	1	15
2,4-DNT	23.783	22.986	24.580	400.0	498.400	207335	415.97	1		15
Tetryl	33.750	32.100	35.400	400.0	524.000	184486	352.04			15
2,4,6-TNT	34.808	33.465	36.151	400.0	517.700	238090	459.92	15	1	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======		======	=======		=======	=====	==	=====
3.4-DNT	19.358	18.825	19.891	400.0	256.000	93389	364.74	-9		15
		1	İ						.	

Lab Name

: EMAX

Instrument ID GC Column

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Conc Cont LFID & Datetime: PL22002A 12/22/2004 15:43

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT		l	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	=======		======	======				=====	==	=====
HMX	6.175	6.095	6.255	400.0	245.000	95772	390.93			15
RDX	8.017	7.913	8.121	400.0	268.600	99646	370.92	-7		15
Nitrobenzene	10.892	10.788	10.996	400.0	338.000	128837	381.18	-5		15
1,3-DNB	15.633	15.272	15.994	400.0	515.000	190465	369.82	-8	İ	15
2-Nitrotoluene	16.175	15.915	16.435	400.0	273.500	111705	408.48	2	١.	15
4-Nitrotoluene	16.767	16.477	17.057	400.0	284.900	115471	405.35	1	ĺ	15
4-AM-2,6-DNT	17.750	17.187	18.313	400.0	261.800	90500	345.71	-14		15
3-Nitrotoluene	18.275	17.908	18.642	400.0	352.500	135227	383.60	4	İ	15
2-AM-4,6-DNT	19.900	19.142	20.658	400.0	421.400	151825	360.30	-10	İ	15
1,3,5-TNB	20.792	20.179	21.405	400.0	355.300	132191	372.05	-7		15
2,6-DNT	22.325	21.601	23.049	400.0	255.700	86134	336.90	-16	*	15
2,4-DNT	23.658	22.861	24.455	400.0	498.400	190779	382.76	-4	İ	15
Tetryl	33.350	31.700	35.000	400.0	524.000	174767	333.50	-17	*	15
2,4,6-TNT	34.542	33.199	35.885	400.0	517.700	213536	412.49	3	İ	15
***************************************		-,								
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
3,4-DNT	19.300	18.767	19.833	400.0	256.000	88006	343.71	-14	==	1:

Lab Name

: EMAX

Instrument ID GC Column

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58 Conc Cont LFID & Datetime: PL22006A 12/22/2004 18:29

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT		_	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======	======		=======			==	=====
HMX	6.225	6.145	6.305	400.0	245.000	97161	396.60	-1		15
RDX	8.092	7.988	8.196	400.0	268.600	100361	373.58	-7		15
Nitrobenzene	11.017	10.913	11.121	400.0	338.000	128104	379.02	-5	1	15
1,3-DNB	15.883	15.522	16.244	400.0	515.000	189798	368.52	-8		15
2-Nitrotoluene	16.475	16.215	16.735	400.0	273.500	114963	420.40	5		15
4-Nitrotoluene	17.075	16.785	17.365	400.0	284.900	119765	420.42	.5		15
4-AM-2,6-DNT	18.100	17.537	18.663	400.0	261.800	92040	351.59	-12		15
3-Nitrotoluene	18.608	18.241	18.975	400.0	352.500	147422	418.19	5.	1	15
2-AM-4,6-DNT	20.267	19.509	21.025	400.0	421.400	161108	382.33	-4	1	15
1,3,5-TNB	21.125	20.512	21.738	400.0	355.300	151046	425.12	.6	ĺ	15
2,6-DNT	22.783	22.059	23.507	400.0	255.700	103374	404.33	1		15
2,4-DNT	24.117	23.320	24.914	400.0	498.400	216051	433.46	8		15
Tetryl	34.217	32.567	35.867	400.0	524.000	182304	347.88	-13	İ	15
2,4,6-TNT	35.317	33.974	36.660	400.0	517.700	230791	445.82	11		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
======================================	19.675	19.142	20.208	400.0	256.000	94001	367.13	-8	==	15
						,4001	257115	"]

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017)

GC Column

: LUNA 5U PHENYL-HEXYL : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL22011A 12/22/2004 21:57

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	========	=======	=======	=====	==	=====
HMX	6.383	6.303	6.463	400.0	245.000	95304	389.02	-3		15
RDX	8.333	8.229	8.437	400.0	268.600	100187	372.93	-7	1	15
Nitrobenzene	11.367	11.263	11.471	400.0	338.000	127211	376.37	-6		15
1,3-DNB	16.417	16.056	16.778	400.0	515.000	197822	384.10	-4		15
2-Nitrotoluene	17.108	16.848	17.368	400.0	273.500	116858	427.33	. 7		15
4-Nitrotoluene	17.733	17.443	18.023	400.0	284.900	124307	436.37	9		15
4-AM-2,6-DNT	19.108	18.545	19.671	400.0	261.800	93341	356.56	-11	ĺ	15
3-Nitrotoluene	19.333	18.966	19.700	400.0	352.500	147476	418.34	5	İ	15
2-AM-4,6-DNT	21.242	20.484	22.000	400.0	421.400	157406	373.55	-7		15
1,3,5-TNB	21.908	21.295	22.521	400.0	355.300	139111	391.53	-2		15
2,6-DNT	23.833	23.109	24.557	400.0	255.700	85445	334.20	-16	*	15
2,4-DNT	25.183	24.386	25.980	400.0	498.400	176112	353.33	-12	İ	15
Tetryl	36.167	34.517	37.817	400.0	524.000	173263	330.63	-17	*	15
2,4,6-TNT	37.000	35.657	38.343	400.0	517.700	176240	340.44	-15		15
			-,,	~						,
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======						=====	==	======
3,4-DNT	20.567	20.034	21.100	400.0	256.000	94695	369.84	-8		15

ANALYTICAL LOGS



ANALYSIS RUN LOG FOR HPLC

EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 |

Book # A17-010

_				Time: 12:11		Ending	g Date:	: 48	117/04	Time: 23:5	8	
Ē	tarting		Data File	Lab Sample ID		DF	Ma		Notes		trument Number	17
		Preparation Batch	Name	Lao Sample ID		D1	S	W				
			PH17.001	IB17H658							Initial Calibration	
			2	ex17 H17e-01	20				Not evaluated	Date	08/17/04	
			3	02	100)	met.	EXITHITC	
	Ī		4	63	200				8330 C Feat	m.p	PH17005A	
			5	σγ	yoo				Phonys-hexyl			
	Ī	<u> </u>	6	05	800				celumn		Standards	
	İ		7	4 01	W					Name	ID	Conc. (µg/L)
	>		8	IEXITHITE -01	400				J	DCC ID	SHIC -03-47-2 ************************************	400
	AL T	EXHOUIS	9	04G156-18T		5				Ical Stack		1600
	ANALYTICAL BATCH		lo	18DT		S				Iev	5HIC-03-53-1	400
	2		ų	18								
	LB		12	180		i						
	AT	EXHOOZW	13	046092-247		õ					Solvent ID	
	\mathbf{H}	1	14	1 2405		Į,				Methanol	43206332	
	ŀ		15	24		i				Water	43189	
	F F		16			1				Acetonitrile		
	7	<u> </u>	1 17								Electronic Data Archival	
	PH17 50% A			CEXITHITC658							Location	Date
	S/A		Y -								· · · · · · · · · · · · · · · · · · ·	
										Comments: g	uples disposed of	8/18/04
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ANALYSIS RUN LOG FOR HPLC

OP D EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 |

Book # A81-02-005

10/19/04 Starting Date: Time: 16115 11:27 10/19/04 **Ending Date:** Time: 20:05 Matrix Preparation Data Lab Sample ID DF Notes **Instrument Number** 81 Batch File Name (W) (S) TEST XJ19.001 INITIAL CALIBRATION REFERENCE 2 10/19/04 3 Date 4 EX81719 Method (4/5) 5 XJ19014A Mid Point 5H1B-03-40-3 6 (800 ppb) ICAL ID ANALYTICAL BATCH SHIB-03-36-2 (10ppm) ICV ID 8 DCC ID q IB81 TG14 10 > Alof evaluated EX8171901 MA U 20 REShifted 12 02 100 13 03 200 Solvents ID 8330 Ical 04 400 14 Acetonitrile 15 05 800 (Primary col.) 43206332 Methanol 3 16 01 20 43189 Water 17 02 100 18 IEXBIJ1901 Electronic Data Archival 400 Date Location DEZC_5_HPLC Comments: Samples disposed off 10/20/04 XP 10/19/04 Analyzed By: This page is checked during the data review process.

JMMAXLABORATORIES, INC. 1825 W. 205" St. Tomeros, CASCOL

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ANALYSIS RUN LOG FOR HPLC

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ANALYSIS RUN LOG FOR HPLC

SOP EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 | |

Book # A81-02-005

Startin	ng Date:			ulou		Time:	ો(:4 ફ				g Date:	12/21/04	Time: O[]	44		
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 $m{J}_{MAX}$ Laboratories, INC, 1835 W. 20.45, Torredo, C45(50)

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 $m{b}$ MAXLaboratories, Inc. 1825 W. 205* St. Touring, Ca 91501

					ANALYSIS R	UN L	OG I	OR	HPLC		0009143	8 01
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SOP Starting		2/2/10	<u>ы к</u> м	1AA-0310	Time: 02(13	-		Ending	Bate: plm ou	Time: 1015	2	
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ANALYSIS RUN LOG FOR HPLC

conf. EMAX-8310 Rev. No: 4 D EMAX-8332 Rev. No: 0 D

Book # A17-010

SOP			EMAX-8310 Rev. No: 4 🗆							Book # A17-01
			Time: 13:47	Endi	ng Date		2/2/104	Time: 27 10	TG	
	Preparation Batch	Data File Name	Lab Sample ID	DF	M:	atrix W	Notes	1	nstrument Number	17
		PL21.001	IB171694						Initial Calibration	
		1 2	CEXITHITCGQU				800.	Date	08/17/04	-
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MAXLABORATORIES, INC. 1825 W. 200° St. Torrans, CA 91201

ANALYSIS RUN LOG FOR HPLC

SOP = EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 | |

Book # A17-010

		EMAX-8310 Rev. No: 4 D							Book # A17-0
tarting Date: 12/2210		Time: 15:01	Endi	ng Dat	e: /:	2/22/04	Time: 2/:	57	
Preparation Batch	Data File Name	Lab Sample ID	DF	M S	atrix W	Notes	b	nstrument Number	17
	PL 22, 601	IB176096					N Comment	Initial Calibration	
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	₩ .DII	CEXI7H17C098				400			
									
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MAN DEPORATORIES, INC. 1835 W. 20th St. Tomanna, CA 91301

EXTRACTION LOGS

EXTRACTION LOG FOR EXPLOSIVES

 $oldsymbol{\mathcal{E}}$ MAXlaboratories, Inc. 1835 W. 20. 4 St. Tourance, CA 50531

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latrix:	TUATA	ER Start Date:	12/20/04	Time: /3:00	End Date	: /2/20/04/ Time:	44 15:30 Boo	k# EEX-01
	Sample Prep	Lab Sample ID	Sample Amount	Extract Volume	Notes	Surrogate	SH1B-03-36-1	Amount Adde (ml)
	ID		(g ml)	(ml)		LCS/MS	SHIB-03-36-2	0.08
	*01	EXLOOK - WB	200	4				
1	*02	- WL	200	4			<u>r</u>	
1	*03	+ - WC	200	4		Reagent	Lot#/ID	indus
1	*04	04L128 - 11	200	4		Acetonitrile	13080	the second second second second second second second second second second second second second second second se
	*05	- /2	200	4		NaCl	SW1A-02-14	78
ł	*06	04 L 142 -07	200	4		CaCl ₂	SP/B- 50-10/20/4	
	*07	04 L 145 - 01	200	4		Silica Sand	42289249	JO 12/2
ב	*08	-02	200	4	1			
REP.	*09							
AR	*10	Tr 12/	20/04					· · · · · · · · · · · · · · · · · · ·
PREPARATION BATCH:	*11					SDG#	Extract Location	
NO	*12							
BA	*13						SEC4 #1	
$r_{\rm C}$	*14							· · · · · · · · · · · · · · · · · · ·
H:_	*15					Comments:		
EXĹ	*16							
<u> </u>	*17							
-400	*18							
1-7	*19							
22	*20							
	*21							
	*22					Prepared By:	Jr.	
	*23		<u></u>			Standard Added By:	JV/EG	
1	*24					Checked By:	ML	
ŀ	*25					Extract Received By:		
	*26					Disposal Date:		

EXTRACTION LOG FOR EXPLOSIVES

MAXIABORATORIES, INC. 1835 W. 200th St. Tourance, CA 50531

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in the same

Matrix:	SOIL		12/20/04	Time: /7:30	End Date:	/2/2//04 Time:	11:00	Book # EEX-010
	Sample	Lab Sample	Sample	Extract		Standards	ID	Amount Added (ml)
	Prep	ID	Amount	Volume	Notes	Surrogate	SH113-03-36-	
	ID		(g ml)	(ml)		LCS/MS	SHIB-03-36-	2 0.4
	*01	EXL005-8B		20				
	*02	04L/28 -801	2.0/	20			Timene 1000 de contacto de la contac	
	*03	04L/28 -801	2.03	20		Reagent	Lot#/ID	
	*04	-02	2.01	20		Acetonitrile	¥3080	
	*05	- 02N	2.02	20		NaCl	Per-	
	*06	-028	2.03	20		CaCl ₂	SP/B- 6 422892	1-267
	*07	- 03	2.01	20		Silica Sand	422892	49
P	*08	- 04	2.00	20	1			
RE	*09	- 05	2.03	20				
PAR	*10	- 06	2.03	20	•			
PREPARATION BATCH:	*11	-07	2.02	20		SDG#	Extract Locat	ion
<u>Ş</u>	*12	- 08	2.02	20				
BA	*13	- 09	2.01	20			SEO4#1	
TC	*14	-10	2.02	20				
H:	*15	04/142 - 01	2,02	20		Comments:		
E	*16	- 02	2.00	20	·			
EXL	*17	- 03	2.01	20				
005	*18	-04	2.03	20				
2-0	*19	- 05	2,03	20				
	*20	- 06	2.02	20				
	*21							
	*22	12/20/04	! Jr			Prepared By:	Jr	
	*23	, , , , ,			· · · · · · · · · · · · · · · · · · ·	Standard Added By:	JU/YK	
	*24				***	ML144/07 - Checked By:	YK-ML	
ŀ	*25					Extract Received By:	Do Waley	
	*26					Disposal Date:		

TABLE OF CONTENTS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L145

SECTION		PAGE
Cover Letter, Co	DC/Sample Receipt Form	1000 – 1006
GC/MS-VOA	**	2000 –
GC/MS-SVOA	**	3000 –
GC-VOA	**	4000 –
GC-SVOA	**	5000 –
HPLC	EPA METHOD 8330	6000 - 6055
METALS	**	7000 –
WET	**	8000 –
OTHERS	**	9000
	A situation of the second seco	

^{** -} Not Requested



1835 W. 205th Street Torrance, CA 90501

> Tel: (310) 618-8889 Fax: (310) 618-0818

Date: 12-29-2004

EMAX Batch No.: 04L145

Attn: Diane Meyer

Shaw E&I 1430 Enclave Parkway Houston TX 77077

Subject: Laboratory Report

Project: Longhorn Army Ammunition Plant

Enclosed is the Laboratory report for samples received on 12/20/04. The data reported include:

Sample ID	Control #	Col Date	Matrix	Analysis	
29WL40-MH09	L145-01	12/17/04	WATER	NITROAROMATICS & NITRAMINE	S
29WL40-MH09-QC	L145-02	12/17/04	WATER	NITROAROMATICS & NITRAMINE	Ś
29SD40-MH09	L145-03	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	S
29SD43-MH12	L145-04	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	
29SD40-MH09-QC	L145-05	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	Ś
29SD33-MH02	L145-06	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	S
29SD36-MH05	L145-07	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	S
29SD37-MH06	L145-08	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	S
29SD36-MH05	L145-07	12/17/04	SOIL	NITROAROMATICS & NITRAMINE	S

The results are summarized on the following pages.

Please feel free to call if you have any questions concerning these results.

Sincerely yours,

Kam Y. Pang, Ph.D. Laboratory Director



Environmental & Infrastructure, Inc.

CHAIN-OF-CUSTODY

No. 29-EMAX-DEC04-009

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

Laboratory Name: EMAX

I8

Address:

041145 1835 205th Street Loe Kelbley Contact: Torrance, CA 90501

-			į.	-	t Loca		Area 29 Former IN1	Analysis and Method Desired (Indicate separate containers)								Remarks
	d Name Longhorn AAP		Project C			n Are	a Project Telephone No.				e seuai	ate com	all icis)			remana
Proje								5.5	and 8330	314.0						
	845714		Di	ane i	Vleye		281-368-4404 t Manager/Supervisor	in the	cs a		ľ					
USAC	E Point of contact: Cliff Murray					Fiojec	t wanagerouper race	5	atic ss	9						
	Oilli litalita)							5	STILL STILL	rat						
USAC	CE Telephone No.				 		Praveen Srivastav	Number of Containers	Z E	ž						
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1							29WL41-MH10	 2 -	-x-							
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2 4	29WL43-MH12						29WL43 MH12	2	×	_					<u> </u>	
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	29WL 40 -MH 09 -QC	14141	1315		X	SW	29WL 40 -MH 69 -QC	2	X							
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Environmental & Infrastructure, Inc.

00091447 No. 29-EMAX-DEC04-006

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

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	La	aboratory Name: EMAX					ress:	1835 205th Street Torrance, CA 90501	-	Conta	ct: 🕽	æ	Kelt	pley												
t							Location Area 29 Former IN!			Analysis and Method Desired																
ı	Projec	t Name Longhorn AAP			Prod	uctio	on Area			(Indicate separate containers)							Remarks									
Project No. Proje						t		Project Telephone No.		and 8330	0.			İ												
il.		845714		l n	iane l	Vieve	r	281-368-4404		and 833	314.0															
1	USACE Point of contact:							Project Manager/Supervisor			by 3				1											
ال	30.70	Cliff Murray			i rioject manager/odpervisor					Nitroaromatics Nitroamines by																
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}	<u> </u>	Sample Number	Date				 -	Sample Description, Location	 	diam diam	Bodes			<u> </u>												
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Ŀ	_2_	29SD41-MH10	<u> </u>				SED	296D41-MH10		^					<u> </u>	ļ										
1	3	29SD42-MH11					SED	29SD42-MH11	1	Lx.							-									
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	4	29SD43-MH12	14/1/04	1147		N/	SED	29SD43-MH12	1	Х																
	E	29SD44						29SD44		×																
F		2007					SED	2300	-							 										
-	·6-	29SD45					SED	293D45	1-1-	-x																
r	_							000040		v																
	1	29SD46					SED	298D46		^					<u> </u>											
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1	9_	29SDQC			-		SED	293DQC	1	*				<u></u>												
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Environmental & Infrastructure, Inc.

00091448 No. 29-EMAX-DEC04-005

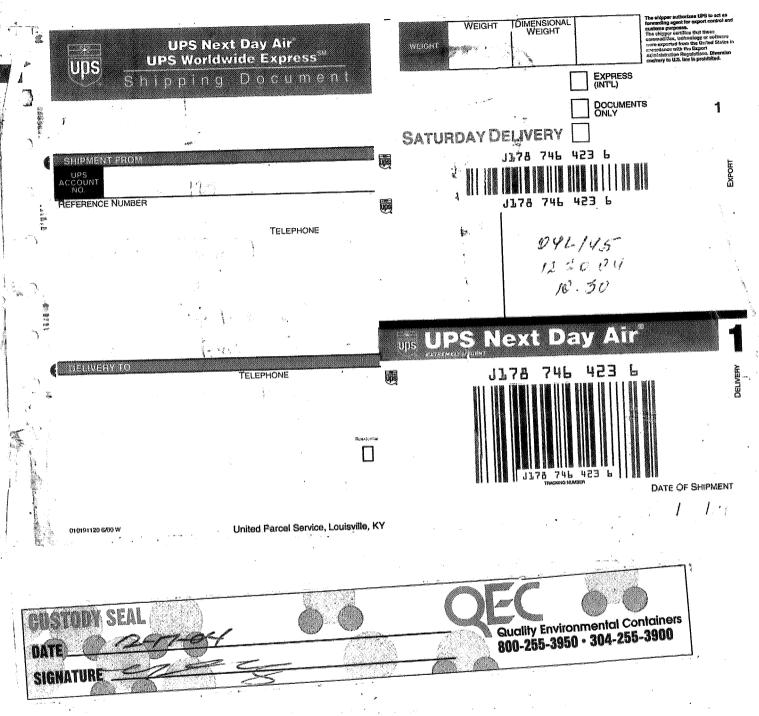
1430 Enclave Parkway Houston, TX 77077 (281) 368-4000 Tulsa TERC DACA56-94-D-0020

CHAIN-OF-CUSTODY

La	aboratory Name		EMAX				Add	ress:	1835 205th Street Torrance, CA 90501		Conta	ıct: ्री	loe k	e/blo	Y			
								Location Area 29 Former INI			Analysis and Method Desired (Indicate separate containers)							
Projec	t Name Long	hori	n AAP					on Area				Remarks						
Project No. Project Contact							Project Telephone No.		<u>ر</u> ا	and 8330	6							
845714 Diane Meye								Meyer 281-368-4404			and 833	314.0						
USACE Point of contact:								Projec	t Manager/Supervisor	Containers	S 5	Ď						
Cliff Murray										lat les	e e							
USAC	E Telephone No.								Praveen Srivastav	Number of	투혈	o e						
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S Fe	Sample N	iumbi	er	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Ž	Nitroaromatics a	Perchlorate						
==				Date		<u> </u>	-	<u> </u>		†								
	29SD32-MH01							SED	293D32-MH01	11	×	<u></u>						
2	29SD33-MH02			1741764	0855	6	X	SED	29SD33-MH02	1	X							
-2-	29SD34-MH03							SED	29SD34-MH03	-4	×							
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.4_	29SD35-MH04							SED	293D35-MH04	1	 							
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•	TAT: Standard		_ Rush Due	9:		Si	eals Inti	act? <u>//</u>	Y N Received Good	Condition	1 _ Y	N	C	old				

SAMPLE RECEIPT FORM 1

Tyro	e of Delivery			
☐ EMAX Courier	a or Delivery	Delivered By/Airbill		042145
Client Delivery				SITPIKOV
Third Party	125	J178-746-4236		12-20-04
PLI Millorary (V118-146-4556	Time	1030
		COC Inspection	· · · · · · · · · · · · · · · · · · ·	
Client Name		COC Inspection Sampler Name	Sampling	Date/Time/Location
Address		Courier Signature/Date/Time	Analysis F	
Client PM/FC		TAT	Matrix	(equired
Tel #/Fax #		Sample ID	-	/2E \
Safety Issues	None	High Concentrations expected		ve (if any)
Comments:	Rad Screening Requir		Superrunc	l Site Samples
		CO.		
		Packaging Inspection	· · · · · · · · · · · · · · · · · · ·	
Container	Cooler	Box		П
Condition	Custody Seal	Intact	amaged	T . 1 .
Packaging	Bubble Pack	☐ Styrofoam ☐ S	ufficient	plastic bag
Temperatures	Cooler 1-4.1°C	☑ Cooler 2		Cooler 4
	Cooler 5	F		Cooler 8
	Cooler 9	entered.		Cooler 12
Comments:				American Addition of the Control of
*	COOLER WAS	SHIPPED ON 12/17/04		
LSCID	Ol' - LID			
LSCID	Client ID	Discrepancy	C	Corrective Action
			7	
				and the state of t
				A CONTRACTOR OF THE CONTRACTOR
1	1			
LSCID : Lab Sam	ple Container ID			
LSCID : Lab Sam	ple Container ID			
		SRF W	PAA	Tay k
REVIEWS Sample Labelin		SRF W- Date (3-10-0 U	PM _	JMK 12/20/04



REPORTING CONVENTIONS

DATA QUALIFIERS:

Lab Qualifier	AFCEE Qualifier	Description
J.	. F	Indicates that the analyte is positively identified and the result is less than RL but greater than MDL.
N		Indicates presumptive evidence of a compound.
В	В	Indicates that the analyte is found in the associated method blank as well as in the sample at above QC level.
and the companion of th	J	Indicates that the result is above the maximum calibration range.
*	*	Out of QC limit.

Note: The above qualifiers are used to flag the results unless the project requires a different set of qualification criteria.

ACRONYMS AND ABBREVIATIONS:

	The state of the s
CRDL	Contract Required Detection Limit
RL	Reporting Limit
MRL	Method Reporting Limit
PQL	Practical Quantitation Limit
MDL	Method Detection Limit
DO	Diluted out

DATES

The date and time information for leaching and preparation reflect the beginning date and time of the procedure unless the method, protocol, or project specifically requires otherwise.

LABORATORY REPORT FOR

SHAW E&I

LONGHORN ARMY AMMUNITION PLANT

EPA METHOD 8330 EXPLOSIVES

SDG#: 04L145

CASE NARRATIVE

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

SDG:

04L145

EPA METHOD 8330 EXPLOSIVES

Two (2) water and six (6) soil samples were received on 12/20/04 for Explosives analysis by EPA Method 8330 in accordance with USEPA-SW846 3rd edition, and EMAX-8330.

1. Holding Time

Analytical holding time was met. Extraction for water samples was started and completed on 12/20/04. Extraction for soil samples was started on 12/22/04 and completed on 12/23/04

2. Calibration

Initial calibration was five points. %RSDs were within 20%. All continuing calibrations of the primary column were carried out at 12-hour intervals and the recoveries were within 85-115%.

3. Method Blank

Method blanks were free of contamination at the reporting limit.

4. Surrogate recovery

Surrogate recoveries in samples L145-01T, -01I, -02T and -02I were diluted out. All surrogate recoveries in other samples were within QC limits.

5. Lab Control Sample / Lab Control Duplicate

All recoveries were within QC limits.

6. Matrix Spike/Matrix Spike Duplicate

Sample L145-04 was spiked. Recoveries were within QC limits.

7. Sample Analysis

Samples were analyzed according to the prescribed QC procedures. Quantitation is from the primary column. All positive results above RL were confirmed by LC-CN column and the confirmation is presumptive because it was based on retention time window.

Samples were air-dried prior to extraction; hence, no moisture correction was applied to RL. MDL and results.

LAB CHRONICLE EXPLOSIVES

SDG NO.

: SHAW E&I Client

Instrument ID : TO81 Project : LONGHORN ARMY AMMUNITION PLANT

				1	JATER				
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio	•	
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
empredit	EXLO04WB	1	NA	12/20/0418:27	12/20/0413:00	XL20004A	XL20003A	EXL004W	Method Blank
MBLK1W	EXLOO4WL	1	NA.	12/20/0418:56	12/20/0413:00	XL20005A	XL20003A	EXL004W	Lab Control Sample (LCS)
LCS1W		, 1	NA NA	12/20/0419:24	12/20/0413:00	XL20006A	XL20003A	EXL004W	LCS Duplicate
LCD1W	EXL004WC	! 4	NA NA	12/20/0417:24	12/20/0413:00	XL20010A	XL20003A	EXL004W	Field Sample
29WL40-MH09	L145-01	20		12/21/0414:12	12/20/0413:00	XL21006A	XL21002A	EXL004W	Diluted Sample
29WL40-MH09DL	L145-01T	20	NA	12/21/0414:12	12/20/0413:00	XL21005A	XL21002A	EXL004W	Diluted Sample
29WL40-MH09DL1	L145-01I	500	NA		12/20/0413:00	XL20012A	XL20003A	EXL004W	Field Sample
29WL40-MH09-QC	L145-02	1	NA	12/20/0422:17	12/20/0413:00	XL21008A	XL21002A	EXLO04W	Diluted Sample
29WL40-MH09-QCDL	L145-02T	20	NA	12/21/0415:10	12/20/0413:00	XL21000A	XL21002A	EXLO04W	Diluted Sample
29WL40-MH09-QCDL1	L145-021	500	NA	12/21/0414:41	12/20/0413:00	ALZIUUTA	ALE TOUEN	LALGOTA	Director compre
					SOIL				
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibratio		
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
				12/23/0411:51	12/22/0417:00	XL23004A	XL23002A	EXL006S	Method Blank
MBLK1S	EXL006SB	ľ	NA	12/23/0411:31	12/22/0417:00	XL23005A	XL23002A	EXL006S	Lab Control Sample (LCS)
LCS1S	EXL006SL	1	NA		12/22/0417:00	XL23005A	XL23002A	EXLOGGS	Field Sample
29SD40-MH09	L145-03	1	NA	12/23/0412:49	12/22/0417:00	XL23007A	XL23002A	EXL006S	Field Sample
29SD43-MH12	L145-04	1	NA	12/23/0413:18	12/22/0417:00	XL23007A	XL23002A	EXLOGOS	Matrix Spike Sample (MS)
29SD43-MH12MS	L145-04M	1	NA.	12/23/0413:46		XL23000A	XL23002A	EXLO06S	MS Duplicate (MSD)
29SD43-MH12MSD	L145-04S	1	NA	12/23/0414:15	12/22/0417:00	XL23009A XL23010A	XL23002A	EXLODGS EXLODGS	Field Sample
29SD40-MH09-QC	L145-05	1	NA	12/23/0414:44	12/22/0417:00		XL23002A	EXLO06S	Field Sample
29SD33-MH02	L145-06	1	NA	12/23/0415:13	12/22/0417:00	XL23011A	XL23002A XL23027A	EXLOGGS EXLOGGS	Diluted Sample
29SD33-MH02DL	L145-06T	5	NA	12/24/0402:44	12/22/0417:00	XL23035A			•
29SD36-MH05	L145-07W	1	NA	12/24/0402:16	12/22/0417:00	XL23034A	XL23027A	EXLO06S	Field Sample Field Sample
29SD37-MH06	L145-08	1	NA	12/23/0416:10	12/22/0417:00	XL23013A	XL23002A	EXL006S	rietu sampte

- Filename

% Moist - Percent Moisture

SAMPLE RESULTS

=========		
Client	· SHAU FRI	Date Collected: 12/17/04

Client : SHAW E&I
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L145 Date Received: 12/20/04

Date Extracted: 12/20/04 13:00 Sample ID: 29WL40-MH09 Lab Samp ID: L145-01 Date Analyzed: 12/20/04 21:20 Dilution Factor: 1

: WATER Lab File ID: XL20010A Matrix Ext Btch ID: EXLO04W % Moisture : NA Calib. Ref.: XL20003A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
НМХ	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	2900E	1	.2
4-AM-2,6-DNT	290E	1	.2
2-AM-4,6-DNT	210E	1	.2
2,6-DNT	27É	1	.2
2,4-DNT	.8J	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	⁻ 1	.2
4-NITROTOLUENE	ND	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

77

63-143

Note: All positive results are confirmed by CN column

3,4-DINITROTOLUENE

Client : SHAW E&I Date Collected: 12/17/04

Date Received: 12/20/04

Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L145 Date Extracted: 12/20/04 13:00 Date Analyzed: 12/21/04 14:12 Sample ID: 29WL40-MH09DL Lab Samp ID: L145-01T Dilution Factor: 20

Lab File ID: XL21006A Matrix : WATER Ext Btch ID: EXLO04W % Moisture : NA Calib. Ref.: XL21002A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
НМХ	ND	20	4
RDX	ND	20	4
1,3,5-TNB	ND	20	4
1,3-DNB	ND	20	4
TETRYL	ND	20	4
NITROBENZENE	ND	20	4
2,4,6-TNT	5000E	20	4
4-AM-2,6-DNT	290	20	4
2-AM-4,6-DNT	220	20	4
2,6-DNT	27	20	4
2.4-DNT	ND	20	4
2-NITROTOLUENE	ND	20	4
3-NITROTOLUENE	ND	ຶ 20	4
4-NITROTOLUENE	ND	20	4
SUDDOCATE DADAMETERS	% DECOVERY	OC LIMIT	

SURROGATE PARAMETERS % RECOVERY QC LIMIT 3,4-DINITROTOLUENE 63-143 DO

Note: All positive results are confirmed by CN column

DO : Diluted out

Client : SHAW E&I Date Collected: 12/17/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L145 Date Received: 12/20/04 Date Extracted: 12/20/04 13:00 Sample ID: 29WL40-MH09DL1 Date Analyzed: 12/21/04 13:43 Dilution Factor: 500 Lab Samp ID: L145-011 Lab File ID: XL21005A : WATER Matrix Ext Btch ID: EXLO04W % Moisture : NA Calib. Ref.: XL21002A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
НМХ	ND	500	100
RDX	ND	500	100
1,3,5-TNB	ND	500	100
1,3-DNB	ND	500	100
TETRYL	NĎ	500	100
NITROBENZENE	ND	500	100
2,4,6-TNT	5200	500	100
4-AM-2,6-DNT	290J	500	100
2-AM-4,6-DNT	190J	500	100
2,6-DNT	ND	500	100
2,4-DNT	ND	500	100
2-NITROTOLUENE	ND	500	100
3-NITROTOLUENE	ND	້500	100
4-NITROTOLUENE	ND	500	100
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column

DO : Diluted out

Client : SHAW E&I Date Collected: 12/17/04

Project : LONGHORN ARMY AMMUNITION PLANT Date Received: 12/20/04
Batch No. : 04L145 Date Extracted: 12/20/04

Batch No. : 04L145 Date Extracted: 12/20/04 13:00 Sample ID: 29WL40-MH09-QC Date Analyzed: 12/20/04 22:17 Lab Samp ID: L145-02 Dilution Factor: 1

 Lab Samp ID: L145-02
 Dilution Factor: 1

 Lab File ID: XL20012A
 Matrix : WATER

 Ext Btch ID: EXL004W
 % Moisture : NA

 Calib. Ref.: XL20003A
 Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
,-,,			
нмх	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	NĎ	1	.2
2,4,6-TNT	2900E	1	.2
4-AM-2,6-DNT	180E	1	.2
2-AM-4,6-DNT	120E	1	.2
2,6-DNT	18E	1	.2
2,4-DNT	.83J	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	´ 1	.2
4-NITROTOLUENE	ND	1	.2

SURROGATE PARAMETERS % RECOVERY QC LIMIT
3,4-DINITROTOLUENE 77 63-143

Mote: All positive results are confirmed by CN column

6007

Client : SHAW E&I Date Collected: 12/17/04
Project : LONGHORN ARMY AMMUNITION PLANT Date Received: 12/20/04
Batch No. : 04L145 Date Extracted: 12/20/04

Batch No. : 04L145 Date Extracted: 12/20/04 13:00 Sample ID: 29WL40-MH09-QCDL Date Analyzed: 12/21/04 15:10

Lab Samp ID: L145-02T Dilution Factor: 20
Lab File ID: XL21008A Matrix : WATER
Ext Btch ID: EXL004W % Moisture : NA
Calib. Ref.: XL21002A Instrument ID : T-081

PARAMETERS	RESULTS (ug/L)	RL (ug/L)	MDL (ug/L)
HMX	ND	20	4
RDX	ND	20	4
1,3,5-TNB	ND	20	4
1,3-DNB	ND	20	4
TETRYL	ND	20	4
NITROBENZENE	ND	20	4
2,4,6-TNT	5000E	20	4
4-AM-2,6-DNT	280	20	4
2-AM-4,6-DNT	210	20	4
2,6-DNT	27	20	4
2,4-DNT	ND	20	4
2-NITROTOLUENE	ND	20	4
3-NITROTOLUENE	ND	໌ 20	4
4-NITROTOLUENE	ND	20	4
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column

DO : Diluted out

Date Collected: 12/17/04 Client : SHAW E&I Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L145 Date Received: 12/20/04

Date Extracted: 12/20/04 13:00 Sample ID: 29WL40-MH09-QCDL1 Date Analyzed: 12/21/04 14:41

Lab Samp ID: L145-021 Dilution Factor: 500 : WATER Lab File ID: XL21007A Matrix Ext Btch ID: EXLOO4W % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL21002A

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
	110101		
НМХ	ND	500	100
RDX	ND	500	100
1,3,5-TNB	ND	500	100
1,3-DNB	ND	500	100
TETRYL	ND	500	100
NITROBENZENE	ND	500	100
2,4,6-TNT	5900	500	100
4-AM-2,6-DNT	290J	500	100
2-AM-4,6-DNT	210J	500	100
2,6-DNT	ND	500	100
2,4-DNT	ND	500	100
2-NITROTOLUENE	ND	500	100
3-NITROTOLUENE	ND	~500	100
4-NITROTOLUENE	ND	500	100
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
7 / 521120000000000		25 4/5	
3,4-DINITROTOLUENE	DO	63-143	

Note: All positive results are confirmed by CN column

DO : Diluted out

Client : SHAW E&I	Date Collected: 12/17/04
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/20/04
Batch No. : 04L145	Date Extracted: 12/22/04 17:00
Sample ID: 29SD40-MH09	Date Analyzed: 12/23/04 12:49
Lab Samp ID: L145-03	Dilution Factor: 1

Lab File ID: XL23006A Matrix : SOIL
Ext Btch ID: EXL006S % Moisture : NA
Calib. Ref.: XL23002A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	1200	400	200
4-AM-2,6-DNT	2500	400	200
2-AM-4,6-DNT	2400	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	~400	200
4 NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	104	63-143	

=========				
Client :	SHAW E&I	Date Collected:	12/17/04	
Project :	LONGHORN ARMY AMMUNITION PLANT	Date Received:	12/20/04	
Batch No. :	04L145	Date Extracted:	12/22/04 17:00	
Sample ID:	29SD43-MH12	Date Analyzed:	12/23/04 13:18	
Lab Samp ID:	L145-04	Dilution Factor:	1	
Lab File ID:	XL23007A	Matrix :	SOIL	,
Ext Btch ID:	EXL006S	% Moisture :	NA	•
Calib. Ref.:	XL23002A	Instrument ID :	T-081	

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	410 🗸	400	200
4-AM-2,6-DNT	ŇD	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	102	63-143	

========	==:		====:		=======				
Client	:	SHAW E&I				Date	Collected:	12/17/04	
	:	LONGHORN	ARMY	AMMUNITION	PLANT		Received:		

Batch No. : 04L145

Sample ID: 29SD40-MH09-QC

Lab Samp ID: L145-05

Date Extracted: 12/22/04 17:00

Date Analyzed: 12/23/04 14:44

Dilution Factor: 1

Lab Samp ID: L143-05
Lab File ID: XL23010A
Ext Btch ID: EXL006S
Calib. Ref.: XL23002A

Dilution Factor: 1
Matrix : SOIL
Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	1100	400	200
4-AM-2,6-DNT	460	400	200
2-AM-4,6-DNT	470	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	103	63-143	

Client : SHAW E&I Date Collected: 12/17/04 Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L145 Date Received: 12/20/04 Date Extracted: 12/22/04 17:00 Sample ID: 29SD33-MH02 Date Analyzed: 12/23/04 15:13 Lab Samp ID: L145-06 Dilution Factor: 1 Lab File ID: XL23011A Matrix : SOIL Ext Btch ID: EXLO06S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL23002A

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	440	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	11000E	400	200
4-AM-2,6-DNT	2600	400	200
2-AM-4,6-DNT	3800	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	97	63-143	

Client : SHAW E&I	Date Collected: 12/17/04
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/20/04
Batch No. : 04L145	Date Extracted: 12/22/04 17:00
Sample ID: 29SD33-MHO2DL	Date Analyzed: 12/24/04 02:44
Lab Samp ID: L145-06T	Dilution Factor: 5
Lab File ID: XL23035A	Matrix : SOIL
Ext Btch ID: EXLO06S	% Moisture : NA
Calib. Ref.: XL23027A	Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
*.************************************	Telephological exp		
НМХ	ND	2000	1000
RDX	ND	2000	1000
1,3,5-TNB	ND	2000	1000
1,3-DNB	ND	2000	1000
TETRYL	ND	2000	1000
NITROBENZENE	ND	2000	1000
2,4,6-TNT	11000	2000	1000
4-AM-2,6-DNT	2500	2000	1000
2-AM-4,6-DNT	4100	2000	1000
2,6-DNT	ND	2000	1000
2,4-DNT	ŃD	2000	1000
2-NITROTOLUENE	ND	2000	1000
3-NITROTOLUENE	ND	2000	1000
4-NITROTOLUENE	ND	2000	1000
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	96	63-143	

Client : SHAW E&I	Date Collected: 12/17/04
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/20/04
Batch No. : 04L145	Date Extracted: 12/22/04 17:00
Sample ID: 29SD36-MH05	Date Analyzed: 12/24/04 02:16
	and a contract of the contract

 Sample ID: 29SD36-MH05
 Date Analyzed: 12/24,

 Lab Samp ID: L145-07W
 Dilution Factor: 1

 Lab File ID: XL23034A
 Matrix : SOIL

 Ext Btch ID: EXL006S
 % Moisture : NA

 Calib. Ref.: XL23027A
 Instrument ID : T-081

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
किसी के किसी के किसी के किसी	***		
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	103	63-143	

Client	:	SHAW E&I	Date	Collected:	12/17/04			
Project	:	LONGHORN ARMY AMMUNITION PLANT	Date	Received:	12/20/04			
Batch No.	2	04L145	Date	Extracted:	12/22/04	17:00		
Sample II	: (29SD37-MH06	Date	Analyzed:	12/23/04	16:10		
Lab Samp II):	L145-08	Dilut	ion Factor:	1			

Lab File ID: XL23013A Matrix : SOIL Ext Btch ID: EXL006S % Moisture : NA Calib. Ref.: XL23002A Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	290J	400	200
4-AM-2,6-DNT	260J	400	200
2-AM-4,6-DNT	290J	400	200
2,6-DNT	ND	400	200
2,4-DNT	ŇD	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	102	63-143	

QC SUMMARIES

Client : SHAW E&I Date Collected: NA Project : LONGHORN ARMY AMMUNITION PLANT Date Received: 12/20/04 Batch No. : 04L145 Date Extracted: 12/20/04 13:0 Sample ID: MBLK1W Date Analyzed: 12/20/04 18:2 Lab Samp ID: EXL004WB Dilution Factor: 1 Lab File ID: XL20004A Matrix : WATER	n
Batch No. : 04L145 Date Extracted: 12/20/04 13:0 Sample ID: MBLK1W Date Analyzed: 12/20/04 18:2 Lab Samp ID: EXL004WB Dilution Factor: 1 Lab File ID: XL20004A Matrix : WATER	n
Sample ID: MBLK1W Date Analyzed: 12/20/04 18:2 Lab Samp ID: EXL004WB Dilution Factor: 1 Lab File ID: XL20004A Matrix : WATER	'n
Lab Samp ID: EXL004WB Dilution Factor: 1 Lab File ID: XL20004A Matrix : WATER	~
tab File ID: XL20004A Matrix : WATER	7
Lab File ID: XL20004A Matrix : WATER	
Ext Btch ID: EXLO04W % Moisture : NA	
Calib. Ref.: XL20003A Instrument ID : T-081	
	; =
RESULTS RL MD	
PARAMETERS (ug/L) (ug/L) (ug/L)	,)
HMX ND 1	~
*****	2
	2
1,3-DNB ND 1	2
TETRYL ND 1	2
NITROBENZENE ND 1	2
2,4,6-TNT ND 1	2
	2
2-AM-4,6-DNT ND 1	2
2,6-DNT ND 1	2
2,4-DNT ND 1 .	2
2-NITROTOLUENE ND 1 .	.2
3-NITROTOLUENE ND 1	2
4-NITROTOLUENE ND 1	2
SURROGATE PARAMETERS % RECOVERY QC LIMIT	
Source Course to We Figure 1	
\$3,4-DINITROTOLUENE 100 63-143	

EMAX QUALITY CONTROL DATA LCS/LCD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.: METHOD:

SAMPLE ID:

LAB SAMP ID:

04L145 EPA 8330

MATRIX: DILUTION FACTOR: 1

WATER

1

MBLK1W EXL004WB EXL004WL

EXL004WC XL20004A XL20005A

LAB FILE ID: XL20006A DATE EXTRACTED: 12/20/0413:00 12/20/0413:00 12/20/0413:00

12/20/0418:27 12/20/0418:56 12/20/0419:24 DATE ANALYZED: PREP. BATCH: EXL004W

XL20003A

EXL004W EXL004W XL20003A XL20003A

1

DATE COLLECTED: NA

% MOISTURE:

DATE RECEIVED: 12/20/04

NA

ACCESSION:

CALIB. REF:

PARAMETER	BLNK RSLT (ug/L)	SPIKE AMT (ug/L)	BS RSLT (ug/L)	BS % REC	SPIKE AMT	BSD RSLT (ug/L)	BSD % REC	RPD (%)	QC LIMIT	MAX RPD
нмх	ND	4	3.84	96	4	3.99	100	4	70-130	30
RDX	ND	4	3.31	83	4	3.19	80	4	60-130	.30
1,3,5-TNB	ND	4	4.03	101	4	4.06	101	1	70-130	30
1,3-DNB	ND	4	3.85	96	4	3.86	96	0	70-130	30
Tetryl	ND	4	4.08	102	4	4.1	102	0	50-140	30
Nitrobenzene	ND	4	3.62	90	4	3.64	91	1	60-130	30
2,4,6-TNT	ND	.4	4.18	105	4	4.22	105	1	70-140	30
4-AM-2,6-DNT	ND	4	3.92	98	4	3.92	98	0	70-130	30
2-AM-4,6-DNT	ND	4	4.01	100	4	4.04	101	1	70-130	30
2,6-DNT	ND	4	4.03	101	4	4.07	102	1	70-130	30
2,4-DNT	ND	4	4.13	103	4	4.12	103	0	70-130	30
2-Nitrotoluene	ND	4	3.81	95	4	3.81	95	0	70-130	30
3 ² Nitrotoluene	ND	4	3.99	100	4	4.02	100	1	70-130	30
4-Nitrotoluene	ND	4	4.02	100	4	4.07	102	1	70-130	30

SURROGATE PARAMETER	SPIKE AMT (ug/L)	BS RSLT (ug/L)	BS % REC	SPIKE AMT (ug/L)	BSD RSLT (ug/L)	BSD % REC	QC LIMIT	
	-							
3,4-Dinitrotoluene	4	4.09	102	4	4.27	107	70-130	

	102						=======	==			
Client	:	SHAW E&I				Date	Collected	d:	NA		
Project	:	LONGHORN	ARMY	AMMUNITION	PLANT	Date	Received	d:	12/22/04		
Batch No.	:	04L145				Date	Extracted	d:	12/22/04	17:00	
Sample ID	2	MBLK1S				Date	Analyzed	d:	12/23/04	11:51	
Lab Samp ID	ï	EXL006SB				Dilut	ion Factor	٠:	1		
Lab File ID	;	XL23004A				Matri	х	:	SOIL		
Ext Btch ID	:	EXL006S				% Mois	sture		NA	Carrie	
Calib. Ref.	:	XL23002A				Instr	ument ID	÷	T-081		

DADAMETEDO	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
НМХ	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	106	63-143	

EMAX QUALITY CONTROL DATA LCS ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.:

04L145

METHOD: EPA 8330 _____

MATRIX: DILUTION FACTOR: 1 SAMPLE ID:

SOIL

1

MBLK1S

EXL006SB XL23004A

EXL006SL XL23005A

LAB SAMP ID: LAB FILE ID:

DATE EXTRACTED: 12/22/0417:00 12/22/0417:00

DATE ANALYZED: 12/23/0411:51 12/23/0412:20

DATE COLLECTED: NA

% MOISTURE:

DATE RECEIVED: 12/22/04

EXL006S

PREP. BATCH: CALIB. REF:

EXL006S XL23002A

XL23002A

ACCESSION:

PARAMETER	BLNK RSLT (ug/kg)	SPIKE AMT	BS RSLT (ug/kg)	BS % REC	QC LIMIT
FANAL PLA	(49/79/		(49/19/	76 KEG	(// /
нмх	ND	2000	2050	102	70-140
RDX	ND	2000	2000	100	70-140
1,3,5-TNB	ND	2000	2160	108	70-130
1,3-DNB	ND	2000	2210	111	70-130
Tetryl	ND	2000	1970	98	60-140
Nitrobenzene	ND	2000	2190	110	70-130
2,4,6-TNT	ND	2000	2140	107	70-140
4-AM-2,6-DNT	ND	2000	2090	104	70-130
2-AM-4,6-DNT	ND	2000	2120	106	70-130
2,6-DNT	ND	2000	2140	107	70-140
2,4-DNT	ND	2000	2150	108	70-130
2-Nitrotoluene	ND	2000	2030	102	70-130
3-Nitrotoluene	ND	2000	2060	103	70-130
4-Nitrotoluene	ND	2000	2210	111	70-130

4	SPIKE AMT	BS RSLT	BS	QC LIMIT
SURROGATE PARAMETER	(ug/kg)	(ug/kg)	% REC	(%)
3.4-Dinitrotoluene	2000	2140	107	70-130

EMAX QUALITY CONTROL DATA MS/MSD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.: METHOD:

04L145 EPA 8330

MATRIX:

SOIL

NA

DILUTION FACTOR: 1 SAMPLE ID:

L145-04

1 29SD43-MH12 L145-04M

XL23007A

L145-04S XL23009A

LAB SAMP ID: LAB FILE ID:

XL23008A DATE ANALYZED: 12/23/0413:18 12/23/0413:46 12/23/0414:15

DATE EXTRACTED: 12/22/0417:00 12/22/0417:00 12/22/0417:00

% MOISTURE:

DATE COLLECTED: 12/17/04 DATE RECEIVED: 12/20/04

PREP. BATCH: CALIB. REF:

EXL006S XL23002A EXL006S

XL23002A

EXL006S XL23002A

ACCESSION:

PARAMETER	SMPL RSLT (ug/kg)	SPIKE AMT (ug/kg)	MS RSLT (ug/kg)	MS % REC	SPIKE AMT (ug/kg)	MSD RSLT (ug/kg)	MSD % REC	RPD (%)	QC LIMIT	MAX RPD
HMX	ND	2000	2110	106	2000	2140	107	1	63-154	50
RDX	ND	2000	1910	95	2000	1930	97	1	63-154	50
1,3,5-TNB	ND	2000	2090	105	2000	2120	106	1	63-143	50
1,3-DNB	ND	2000	2170	108	2000	2170	109	0	63-143	50
Tetryl	ND	2000	2000	100	2000	1990	99	0	54-154	50
Nitrobenzene	ND	2000	2140	107	2000	2140	107	0	63-143	50
2,4,6-TNT	405	2000	2220	91	2000	2250	92	1	63-154	50
4-AM-2,6-DNT	ND	2000	2090	105	2000	2040	102	3	63-143	50
2-AM-4,6-DNT	ND	2000	2140	107	2000	2080	104	Ž	63-143	50
2,6-DNT	ND	2000	2080	104	2000	2020	101	3	63-154	50
2,4-DNT	ND	2000	2140	107	2000	2100	105	Ž	63-143	50
2-Nitrotoluene	ND	2000	1950	98	2000	1970	98	1	63-143	50
3-Nitrotoluene	ND	2000	2090	104	2000	2010	100	4	63-143	50
4-Nitrotoluene	ND	2000	2140	107	2000	2110	106	1	63-143	50

	SPIKE AMT	MS RSLT	MS	SPIKE AMT	MSD RSLT	MSD	QC LIMIT	
SURROGATE PARAMETER	(ug/kg)	(ug/kg)	% REC	(ug/kg)	(ug/kg)	% REC	(%)	
3.4-Dinitrotoluene	2000	2080	104	2000	2040	102	63-143	

INITIAL CALIBRATION

Lab Name : EMAX Inc
Instrument ID : HPLC1 81
GC Columm : VARIAN C18
Column size ID : 25CMX4.6MM
LFID & Datetime: XJ19016A 10/19/04 19:08

LFID & Datetime: XJ19016A 10/19/04 19:08 LFID & Datetime: XJ19017A 10/19/04 19:36 LFID & Datetime: XJ19013A 10/19/04 17:41 LFID & Datetime: XJ19014A 10/19/04 18:10 LFID & Datetime: XJ19015A 10/19/04 18:39

CONC UNIT: ppb

	CONC	CALIE	BRATION FA	ACTORS (A	REA or HE	IGHT)/UNI	T	
COMPOUND	Х	1.00X					MEAN	%RSD
	=======	======					=======	====
HMX	20.00	69.25	67.82	72.36	72.87	71.66	70.79	3.1
RDX	20.00	80.55	89.55	93.32	92.82	91.48	89.54	5.8
1,3,5-TNB	20.00	212.60	206.29	208.40	210.28	208.06	209.13	1.1
1,3-DNB	20.00	284.05	289.17	293.78	291.57	290.36	289.79	1.3
Tetryl	20.00	169.65	165.60	171.93	171.00	171.53	169.94	1.5
Nitrobenzene	20.00	196.75	195.67	202.54	203.55	201.64	200.03	1.8
2,4,6-TNT	20.00	206.40	200.92	203.90	208.44	205.06	204.94	1.4
4-AM-2,6-DNT	20.00	156.75	144.28	146.21	146.58	146.43	148.05	3.3
4-AM-2,6-DNT	20.00	229.95	205.98	210.31	215.07	216.25	215.51	4.2
2,6-DNT	20.00	137.60	131.99	135.36	140.29	135.29	136.11	2.3
2,4-DNT	20.00	276.20	270.64	273.11	277.46	281.68	275.82	1.5
2-Nitrotoluene	20.00	130.40	127.75	127.93	129.28	128.10	128.69	0.9
4-Nitrotoluene	20.00	104.40	103.10	107.11	109.25	110.43	106.86	2.9
3-Nitrotoluene	20.00	132.95	130.43	138.71	137.68	140.89	136.13	3.2
							,	
SURROGATE	X	1.00X	5.00X	10.00X	20.00X	40.00X	MEAN	%RSD
	=======	=======	=======	ı	I	=======	!	====
3,4-Dinitrotoluene	20.00	117.40	121.21	124.62	126.61	126.82	123.33	3.2
**************************************	<u></u> .							

EX81J19.MET

Lab Name : EMAX Inc Instrument ID : HPLC1 81 GC Columm : VARIAN C18 Column size ID : 25CMX4.6MM

Column size ID : 25CMX4.6MM LFID & Datetime: XJ19016A 10/19/04 19:08 LFID & Datetime: XJ19017A 10/19/04 19:36 LFID & Datetime: XJ19013A 10/19/04 17:41 LFID & Datetime: XJ19014A 10/19/04 18:10 LFID & Datetime: XJ19015A 10/19/04 18:39

			TANDARE			MEAN	RT W		RTWINDOW
COMPOUND	1.0X	5.0x		20.0X	40.0X	RT	FROM	TO	WIDTH
	======	======	=====	=====	=====	=====		=====	=======
HMX	4.300	4.292	4.292	4.292	4.275	4.290	4.240	4.340	0.050
RDX	6.433	6.383	6.367	6.375	6.333	6.378	6.240	6.516	0.138
1,3,5-TNB	8.650	8.617	8.600	8.633	8.575	8.615	8.462	8.768	0.153
1,3-DNB	10.492	10.450	10.417	10.483	10.400	10.448	10.219	10.677	0.229
Tetryl	11.358	11.308	11.250	11.342	11.250	11.302	11.014	11.590	0.288
Nitrobenzene	12.117	12.092	12.042	12.108	12.033	12.078	11.677	12.479	0.401
2,4,6-TNT	13.675	13.642	13.567	13.642	13.575	13.620	13.219	14.021	0.401
4-AM-2,6-DNT	14.433	14.392	14.292	14.383	14.308	14.362	13.857	14.867	0.505
2-AM-4,6-DNT	14.967	14.983	14.867	14.950	14.883	14.930	14.382	15.478	0.548
2,6-DNT	15.817	15.825	15.742	15.800	15.758	15.788	15.325	16.251	0.463
2,4-DNT	16.383	16.425	16.317	16.367	16.350	16.368	15.891	16.845	0.477
2-Nitrotoluene	19.467	19.525	19.442	19.458	19.467	19.472	18.881	20.063	0.591
4-Nitrotoluene	21.192	21.225	21.150	21.175	21.142	21.177	20.520	21.834	0.657
3-Nitrotoluene	22.658	22.717	22.592	22.633	22.600	22.640	21.888	23.392	0.752
, 									
SURROGATE	1.0x			1			FROM	TO	WIDTH
	22222	40.050		1	=====	1	1		=======
3,4-Dinitrotoluene	12.900	12.858	12.792	12.875	12.792	12.843	12.468	13.218	0.375

EX81J19.MET

SECOND SOURCE

Lab Name Lab Name Instrument ID : EMAX

: HPLC1 81

GC Column Column size ID : VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XJ19018A 10/19/2004 20:05

CONC UNIT

: ppb

	RT	RT W		TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======		======	======		=======		=====	==	=====
НМХ	4.300		4.350		70.800	31158	440.13	10		15
RDX	6.400	6.262	6.538	400.0	89.500	38533	430.32	8	Ī	15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	91920	439.54	10	İ	15
1,3-DNB	10.483	10.254	10.712	400.0	289.800	127403	439.64	10	Ì	15
Tetryl	11.342	11.054	11.630	400.0	169.900	71202	418.98	5		15
Nitrobenzene	12.108	11.707	12.509	400.0	200,000	86805	433.96	8		15
2,4,6-TNT	13.625	13.224	14.026	400.0	204.900	88599	432.31	8		15
4-AM-2,6-DNT	14.400	13.895	14.905	400.0	148.100	60914	411.44	3	İ	15
2-AM-4,6-DNT	14.950	14.402	15.498	400.0	215.500	91200	423.18	6	İ	15
2,6-DNT	15.800	15.337	16.263	400.0	136.100	56248	413.27	3		15
2,4-DNT	16.383	15.906	16.860	400.0	275.800	117421	425.72	6	l	15
2-Nitrotoluene	19.475	18.884	20.066	400.0	128.700	53460	415.40	4	İ	15
4-Nitrotoluene	21.192	20.535	21.849	400.0	106.900	46579	435.89	9	Ì	15
3-Nitrotoluene	22.667	21.915	23.419	400.0	136.100	57575	422.93	6		15

SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	Q٢	LIMITS
3,4-Dinitrotoluene	12.875	12.500	13.250	400.0	123.300	52174	423.04	6	==	15
	إ ــــــــــــــــــــــــــــــــــــ			<u> </u>	WANTED AND THE STREET				_	

EX81J19.MET

Lab Name : EMAX Inc

Lab Name : EMAX Inc
Instrument ID : HPLC1 LCT001(T017)
GC Columm : LUNA 5U PHENYL-HEXYL
Column size ID : 25CMX4.6MM
LFID & Datetime: PH17007A 08/17/04 16:21
LFID & Datetime: PH17003A 08/17/04 13:35
LFID & Datetime: PH17004A 08/17/04 14:16
LFID & Datetime: PH17005A 08/17/04 14:58
LFID & Datetime: PH17006A 08/17/04 15:39

CONC UNIT: ppb

	CONC	CALIE	BRATION FA	ACTORS (AREA or HE	IGHT)/UN	T	
COMPOUND	Х	1.00X	5.00X	10.00X	20.00X	40.00X	MEAN	%RSD
	=======		======	=======		=======		====
HMX	20.00	265.05	223.86	243.86	247.42	244.74	244.99	6.0
RDX	20.00	315.15	255.37	260.41	253.93	258.37	268.65	9.7
Nitrobenzene	20.00	359.70	349.71	329.86	323.97	326.71	337.99	4.7
1,3-DNB	20.00	514.05	508.34	520.54	516.70	515.48	515.02	0.9
2-Nitrotoluene	20.00	238.50	278.15	281.94	287.52	281.20	273.46	7.3
4-Nitrotoluene	20.00	287.00	275.75	289.34	288.21	284.04	284.87	1.9
4-AM-2,6-DNT	20.00	276.50	256.61	256.86	264.78	254 . 15	261.78	3.5
3-Nitrotoluene	20.00	353.75	380.73	345.64	344.94	337.55	352.52	4.8
2-AM-4,6-DNT	20.00	464.60	447.94	400.02	400.57	393.79	421.38	7.7
1,3,5-TNB	20.00	368.85	364.11	349.42	354.06	340.07	355.30	3.2
2,6-DNT	20.00	258.20	256.25	261.51	248.39	253.99	255.67	1.9
2,4-DNT	20.00	433.50	511.11	524.55	509.46	513.54	498.43	7.4
Tetryl	20.00	511.65	504.42	558.66	520.24	525.23	524.04	4.0
2,4,6-TNT	20.00	421.55	507.22	574.38	536.85	548.40	517.68	11.4
	-,							
SURROGATE	X	1.00x	1	3	1		MEAN	%RSD
3,4-DNT	20.00	288.40	260.85	245.15	244.29	241.54	256.04	7.7
			<u> </u>	l	l	<u> </u>		

EX17H17C.MET

Lab Name : EMAX Inc
Instrument ID : HPLC1 LCT001(T017)
GC Columm : LUNA 5U PHENYL-HEXYL

Column size ID : 25CMX4.6MM

LFID & Datetime: PH17007A 08/17/04 16:21
LFID & Datetime: PH17003A 08/17/04 13:35
LFID & Datetime: PH17004A 08/17/04 14:16
LFID & Datetime: PH17005A 08/17/04 14:58
LFID & Datetime: PH17006A 08/17/04 15:39

				DS (MI		MEAN	RT W	INDOW	RTWINDOW
COMPOUND	1.0x				40.0X		FROM	TO	WIDTH
	=====				=====	=====	=====	=====	=======
HMX	6.025	6.050	6.042	6.058	6.033	6.042	5.962	6.122	0.080
RDX	7.800				7.792			7.916	0.104
Nitrobenzene	10.633	10.675	10.667	10.692	10.633	10.660	10.556	10.764	0.104
1,3-DNB	15.183	15.258	15.258	15.292	15,175	15.233	14.872	15.594	0.361
2-Nitrotoluene	15.725	15.783	15.767	15.817	15.692	15.757	15.497	16.017	0.260
4-Nitrotoluene	16.225	16.342	16.342	16.375	16.258	16.308	16.018	16.598	0.290
4-AM-2,6-DNT	16.950	17.108	17.108	17.150	17.000	17.063	16.500	17.626	0.563
3-Nitrotoluene	17.700	17.800	17.775	17.825	17.700	17.760	17.393	18-127	0.367
2-AM-4,6-DNT	18.925	19.125	19.125	19.175	19.025	19.075	18.317	10 833	0.758
1,3,5-TNB	20.142	20.267	20.267	20.317	20.200	20.239	19-626	20.852	0.613
2,6-DNT	21.517	21.642	21.650	21.683	21.558	21.610	20.886	22.334	0.724
2,4-DNT	22.733	22.825	22.892	22.942	22.800	22.838	22-041	23.635	0.797
Tetryl	31.667	31.808	31.850	31.875	31.617	31.763	30.113	33.413	1.650
2,4,6-TNT	33.233	33.367	33.358	33.375	33.150	33.297	31.954	34.640	1.343
SURROGATÉ	1.0X		10.0X	20.0X	40.0X	RT	FROM	TO	WIDTH
	=====	=====		=====			=====		=======
3,4-DNT	18.492	18.650	18.600	18.675	18.525	18.588	18.055	19.121	0.533
to the second of	.							nau.	

EX17H17C.MET

INITIAL CALIBRATION VERIFICATION METHOD 8330

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017)

GC Column

: LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PH17008A 08/17/2004 17:02

CONC UNIT : ppb

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======				=====	==	=====
HMX	6.033	5.953	6.113	400.0	245.000	96246	392.86	-2		15
RDX	7.800	7.696	7.904	400.0	268.600	97411	362.60	-9		15
Nitrobenzene	10.667	10.563	10.771	400.0	338.000	123928	366.66	-8		15
1,3-DNB	15.258	14.897	15.619	400.0	515.000	198879	386.16	-3		15
2-Nitrotoluene	15.783	15.523	16.043	400.0	273.500	100966	369.21	-8		15
4-Nitrotoluene	16.342	16.052	16.632	400.0	284,900	104969	368.48	-8		15
4-AM-2,6-DNT	17.108	16.545	17.671	400.0	261.800	92990	355.22	-11		15
3-Nitrotoluene	17.808	17.441	18.175	400.0	352.500	124474	353.09	-12		15
2-AM-4,6-DNT	19.167	18.409	19.925	400.0	421.400	152612	362.17	-9		15
1,3,5-TNB	20.333	19.720	20.946	400.0	355.300	129357	364.08	-9		15
2,6-DNT	21.725	21.001	22.449	400.0	255.700	90313	353.24	-12		15
2,4-DNT	22.992	22.195	23.789	400.0	498.400	197715	396.67	-1		15
Tetryl	32.158	30.508	33.808	400.0	524.000	188490	359.68	-10	1	15
2,4,6-TNT	33.675	32.332	35.018	400.0	517.700	212198	409.90	2	l	15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	۵L	LIMITS
	======			======			=======	=====	==	=====
3,4-DNT	18.650	18.117	19.183	400.0	256.000	90360	352.91	-12	1	15
									1	

EX17H17C.MET

DAILY CALIBRATION

Lab Name Instrument ID : EMAX

: HPLC1 81

GC Column Column size ID

: VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10
Conc Cont LFID & Datetime: XL20003A 12/20/2004 17:58
CONC UNIT : ppb

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
						=======			==	=====
HMX	4.292	4.242	4.342	400.0	70.800	28461	402.03	1		15
RDX	6.300	6.162	6.438	400.0	89.500	35641	398.02	-0		15
1,3,5-TNB	8.500	8.347	8.653	400.0	209.100	83199	397.84	-1.	1	15
1,3-DNB	10,250	10.021	10.479	400.0	289.800	115929	400.05	.0	İ	15
Tetryl	11.000	10.712	11.288	400.0	169.900	68123	400.86	0	ĺ	15
Nitrobenzene	11.792	11.391	12.193	400.0	200.000	80732	403.60	1	İ	15
2,4,6-TNT	13.300	12.899	13.701	400.0	204.900	80648	393.51	-2		15
4-AM-2,6-DNT	13.875	13.370	14.380	400.0	148.100	60372	407.78	2	l	15
2-AM-4,6-DNT	14.408	13.860	14.956	400.0	215.500	86596	401.82	0	1	15
2,6-DNT	15.358	14.895	15.821	400.0	136.100	55446	407.37	2	l	15
2,4-DNT	15.908	15.431	16.385	400.0	275.800	111329	403.63	1		15
2-Nitrotoluene	18.875	18.284	19.466	400.0	128.700	51626	401.15	0	l	15
4-Nitrotoluene	20.425	19.768	21.082	400.0	106.900	45124	422.27	6	1	15
3-Nitrotoluene	21.842	21.090	22.594	400.0	136.100	57301	420.92	5		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	OL.	LIMITS
3,4-Dinitrotoluene_	12.517	12.142	12.892	400.0	123.300	50724	411.28	3		15

Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column Column size ID

: VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10

Conc Cont LFID & Datetime: XL20015A 12/20/2004 23:44

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT		-	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======		222272	=======	======	======	=====	==	
HMX	4.333	4.283	4.383	400.0	70.800	29272	413.49	3	l	15
RDX	6.408	6.270	6.546	400.0	89.500	38105	425.54	6		15
1,3,5-TNB	8.642	8.489	8.795	400.0	209.100	85122	407.03	2	l	15
1,3-DNB	10.467	10.238	10.696	400.0	289.800	119721	413.14	3		15
Tetryl	11.275	10.987	11.563	400.0	169.900	69968	411.72	3	İ	15
Nitrobenzene	12.042	11.641	12.443	400.0	200.000	82996	414.92	4		15
2,4,6-TNT	13.592	13.191	13.993	400.0	204.900	84236	411.02	3		15
4-AM-2,6-DNT	14.333	13.828	14.838	400.0	148.100	61879	417.96	4	ł	15
2-AM-4,6-DNT	14.875	14.327	15.423	400.0	215.500	87276	404.97	1	١.	15
2,6-DNT	15.750	15.287	16.213	400.0	136.100	57777	424.50	6	:	15
2,4-DNT	16.325	15.848	16.802	400.0	275.800	113421	411.21	3		15
2-Nitrotoluene	19.358	18.767	19.949	400.0	128.700	52495	407.90	2	1	15
4-Nitrotoluene	20.983	20.326	21.640	400.0	106.900	46819	438.13	10	ĺ	15
3-Nitrotoluene	22.450	21.698	23.202	400.0	136.100	57711	423.93	6	l	15
SURROGATÉ	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======		======		_======		=======	=====	==	=====
3,4-Dinitrotoluene	12.850	12.475	13.225	400.0	123.300	51463	417.27	4		1:
	I		<u> </u>	l				l	I	I

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21002A 12/21/2004 12:17

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESL	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======		======		=======	======	=====	==	
HMX	4.308	4.258	4.358	400.0	70.800	28235	398.84	-0		15
RDX	6.342	6.204	6.480	400.0	89.500	36063	402.74	1		15
1,3,5-TNB	8.550	8.397	8.703	400.0	209.100	82108	392.62	-2		15
1,3-DNB	10.325	10.096	10.554	400.0	289.800	115534	398.69	-0		15
Tetryl	11.108	10.820	11.396	400.0	169.900	67938	399.77	-0	ĺ	15
Nitrobenzene	11.875	11.474	12.276	400.0	200.000	79947	399.67	-0	ĺ	15
2,4,6-TNT	13.400	12.999	13.801	400.0	204.900	80421	392.40	-2	İ	15
4-AM-2,6-DNT	14.033	13.528	14.538	400.0	148.100	59823	404.07	1		15
2-AM-4,6-DNT	14.558	14.010	15.106	400.0	215.500	84462	391.91	-2		15
2,6-DNT	15.492	15.029	15.955	400.0	136.100	54767	402.38	1		15
2,4-DNT	16.033	15.556	16.510	400.0	275.800	110265	399.77	-0	1	15
2-Nitrotoluene	19.008	18.417	19.599	400.0	128.700	51046	396.64	-1	1	15
4-Nitrotoluene	20.592	19.935	21.249	400.0	106.900	45322	424.12	6	1	15
3-Nitrotoluene	22.008	21.256	22.760	400.0	136.100	56862	417.70	4	1	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======		======	=======		=======	=====	==	
3,4-Dinitrotoluene	12.633	12.258	13.008	400.0	123.300	49767	403.52	1	İ	15
		l			l <u></u>			l		

Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column

: VARIAN C18 : 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL21012A 12/21/2004 17:05

CONC UNIT

	RT I	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT		Ī	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======		======	======		======	=======	=====	==	=====
HMX	4.300	4.250	4.350	400.0	70.800	28637	404.52	1	į .	15
RDX	6.325	6.187	6.463	400.0	89.500	35492	396.36	-1		15
1,3,5-TNB	8.525	8.372	8.678	400.0	209.100	83787	400.65	0		15
1,3-DNB	10.283	10.054	10.512	400.0	289.800	116602	402.37	1	1	15
Tetryl	11.033	10.745	11.321	400.0	169.900	68756	404.58	1		15
Nitrobenzene_	11.833	11.432	12.234	400.0	200.000	81307	406.47	2		15
2,4,6-TNT	13.350	12.949	13.751	400.0	204.900	80995	395.20	-1		15
4-AM-2,6-DNT	13.925	13.420	14.430	400.0	148.100	61989	418.70	5	1	15
2-AM-4,6-DNT	14.442	13.894	14.990	400.0	215.500	85780	398.03	-0	1	15
2,6-DNT	15.417	14.954	15.880	400.0	136.100	55335	406.56	2	1	15
2,4-DNT	15.950	15.473	16.427	400.0	275.800	111179	403.09	1	ĺ	15
2-Nitrotoluene	18.933	18.342	19.524	400.0	128.700	51488	400.08	0	1	15
4-Nitrotoluene	20.508	19.851	21.165	400.0	106.900	44634	417.68	4	1	15
3-Nitrotoluene	21.917	21.165	22.669	400.0	136.100	57110	419.52	5		15

SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
			======	======	=======	======	=======	=====	==	22222
3,4-Dinitrotoluene	12.575	12.200	12.950	400.0	123.300	51157	414.79	4		15
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Lab Name

: EMAX

Instrument ID

: HPLC1 81

GC Column Column size ID

: VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL23002A 12/23/2004 10:53

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======		======	======	=====	==	=====
HMX	4.358	4.308	4.408	400.0	70.800	29688	419.36	5		15
RDX	6.492	6.354	6.630	400.0	89.500	34599	386.39	-3		15
1,3,5-TNB	8.742	8.589	8.895	400.0	209.100	80373	384.33	-4		15
1,3-DNB	10.608	10.379	10.837	400.0	289.800	113625	392.10	-2		15
Tetryl	11.467	11.179	11.755	400.0	169.900	65675	386.45	-3	į	15
Nitrobenzene	12.208	11.807	12.609	400.0	200.000	79731	398.59	-0		15
2,4,6-TNT	13.792	13.391	14.193	400.0	204.900	79959	390.15	-2		15
4-AM-2,6-DNT	14.608	14.103	15.113	400.0	148.100	57911	391.15	-2	Ì	15
2-AM-4,6-DNT	15.192	14.644	15.740	400.0	215.500	83017	385.21	-4	İ	15
2,6-DNT	16.025	15.562	16.488	400.0	136.100	55091	404.76	1 1	Ì	15
2.4-DNT	16.600	16.123	17.077			107692	390.44	-2		15
2-Nitrotoluene	19.675	19.084	20.266	400.0	128.700	51328	398.84	-0.		15
4-Nitrotoluene	21.367	20.710	22.024	400.0	106.900	42767	400.21	0		15
3-Nitrotoluene	22.825	22.073	23.577	400.0	136.100	54537	400.62	0	l	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======	=======	======	======	=====	==	=====
3,4-Dinitrotoluene	13.067	12.692	13.442	400.0	123.300	48651	394.47	-1		15
	<u> </u>	l <u></u> .	l <u></u>	1	1	l		l	l	

Lab Name Instrument ID : EMAX

GC Column

: HPLC1 81

Column size ID

: VARIAN C18 : 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10
Conc Cont LFID & Datetime: XL23016A 12/23/2004 17:37
CONC UNIT : ppb

	RT	RT WINDOW		TRUE AVERAGE		RESU			%D	
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	==== ======	======		======	=======		======	=====	==	=====
HMX	4.333	4.283	4.383	400.0			395.25	-1		15
RDX	6.383	6.245	6.521	400.0	89.500	35117	392.17	-2		15
1,3,5-TNB	8.625	8.472	8.778	400.0	209.100	81650	390.43	-2		15
1,3-DNB	10.425	10.196	10.654	400.0	289.800	114830	396.26	-1		15
Tetryl	11.217	10.929	11.505	400.0	169.900	67084	394.75	-1		15
Nitrobenzene	12.017	11.616	12.418	400.0	200.000	80687	403.37	1		15
2,4,6-TNT	13.558	13.157	13.959	400.0	204.900	80222	391.43	-2		15
4-AM-2,6-DNT	14.192	13.687	14.697	400.0	148,100	59942	404.87	1		15
2-AM-4,6-DNT	14.725	14.177	15.273	400.0	215.500	85062	394.70	-1		15
2,6-DNT	15.700	15.237	16.163	400.0	136.100	55098	404.82	1.		15
2,4-DNT	16.250	15.773	16.727	400.0	275.800	110274	399.81	-0	ĺ	15
2-Nitrotoluene	19.308	18.717	19.899	400.0	128.700	51910	403.36	1	1	15
4-Nitrotoluene	20.942	20.285	21.599	400.0	106.900	44073	412.43	3	İ	15
3-Nitrotoluene	22.375	21.623	23.127	400.0	136.100	55859	410.33	3		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D		LIMITS
3,4-Dinitrotoluene	12.800	12.425	13.175	400.0	123.300	50125	406.42	2	==	1:

Lab Name Instrument ID : EMAX

: HPLC1 81 : VARIAN C18

GC Column Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL23027A 12/23/2004 22:54

CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	ILT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D		LIMITS
	======	=====	======		=======	=======	=======	=====	==	=====
HMX	4.375	4.325	4.425	400.0	70.800	29637	418.64	5		15
RDX	6.517	6.379	6.655	400.0	89.500	36080	402.93	1		15
1,3,5-TNB	8.792	8.639	8.945	400.0	209.100	82495	394.47	-1.		15
1,3-DNB	10.675	10.446	10.904	400.0	289.800	116959	403.60	1		15
Tetryl	11.542	11.254	11.830	400.0	169.900	67565	397.58	-1		15
Nitrobenzene	12.308	11.907	12.709	400.0	200.000	82491	412.39	3		15
2,4,6-TNT	13.900	13.499	14.301	400.0	204.900	82087	400.53	.0		15
4-AM-2,6-DNT	14.725	14.220	15.230	400.0	148.100	59400	401.21	0		15
2-AM-4,6-DNT	15.292	14.744	15.840	400.0	215.500	85244	395.54	-1	l	15
2,6-DNT	16.150	15.687	16.613	400.0	136.100	55442	407.34	2	l	15
2,4-DNT	16.742	16.265	17.219	400.0	275.800	109634	397.48	-1	i	15
2-Nitrotoluene	19.883	19.292	20.474	400.0	128.700	52269	406.15	2		15
4-Nitrotoluene	21.592	20.935	22.249	400.0	106.900	43985	411.61	3		15
3-Nitrotoluene	23.092	22.340	23.844	400.0	136.100	55630	408.64	2	ĺ	15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
		.======						=====	==	
3,4-Dinitrotoluene	13.192	12.817	13.567	400.0	123.300	49990	405.33	1		15

Lab Name

: EMAX

Instrument ID GC Columm

: HPLC1 81 : VARIAN C18

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: XJ19014A 10/19/2004 18:10 Conc Cont LFID & Datetime: XL23038A 12/24/2004 04:11

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	ТО	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======	======		======	=======	=====	==	=====
HMX	4.400	4.350					418.15	5		15
RDX	6.592	6.454	6.730	400.0	89.500	37230	415.77	.4		15
1,3,5-TNB	8.892	8.739	9.045	400.0	209.100	84659	404.82	1		15
1,3-DNB	10.825	10.596	11.054	400.0	289.800	120239	414.92	4		15
Tetryl	11.742	11.454	12.030	400.0	169.900	68531	403.26	1		15
Nitrobenzene	12.483	12.082	12.884	400.0	200.000	84709	423.48	6		15
2,4,6-TNT	14.117	13.716	14.518	400.0	204.900	83632	408.07	2		15
4-AM-2,6-DNT	15.067	14.562	15.572	400.0	148.100	59693	403.19	1	İ	15
2-AM-4,6-DNT	15.650	15.102	16.198	400.0	215.500	85801	398.13	-0	İ	15
2,6-DNT	16.458	15.995	16.921	400.0	136.100	57170	420.04	5		15
2,4-DNT	17.058	16.581	17.535	400.0	275.800	111497	404.24	1		15
2-Nitrotoluene	20.267	19.676	20.858	400.0	128.700	53591	416.42	4	i	15
4-Nitrotoluene	22.025	21.368	22.682	400.0	106.900	45028	421.37	5		15
3-Nitrotoluene	23.533	22.781	24.285	400.0	136.100	56965	418.45	5	İ	15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======	======			=======	=====	==	=====
3,4-Dinitrotoluene	13.425	13.050	13.800	400.0	123.300	49777	403.60	1		15

Lab Name

: EMAX

Instrument ID GC Column

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL21002A 12/21/2004 14:29

CONC UNIT

	RT	RT W	MDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======	======	======		=======	=======		=====	==	=====
HMX	6.125	6.045	6.205	400.0	245.000	97335	397.31	- 1		15
RDX	7.933	7.829	8.037	400.0	268.600	100692	374.81	-6		15
Nitrobenzene	10.725	10.621	10.829	400.0	338.000	131155	388.04	-3	İ	15
1,3-DNB	15.442	15.081	15.803	400.0	515.000	191677	372.17	-7	l	15
2-Nitrotoluene	15.850	15.590	16.110	400.0	273.500	107744	394.00	-2	ĺ	15
4-Nitrotoluene	16.450	16.160	16.740	400.0	284.900	117212	411.46	3		15
4-AM-2,6-DNT	17.433	16.870	17.996	400.0	261.800	89732	342.78	-14		15
3-Nitrotoluene	17.883	17.516	18.250	400.0	352.500	145090	411.58			15
2-AM-4,6-DNT	19.600	18.842	20.358	400.0	421.400	157332	373.37	-7	Ì	15
1,3,5-TNB	20.467	19.854	21.080	400.0	355.300	135909	382.52	-4	İ	15
2,6-DNT	21.867	21.143	22.591	400.0	255.700	96515	377.50	-6	'	15
2,4-DNT	23.225	22.428	24.022	400.0	498.400	200257	401.77	0		15
Tetryl	32.650	31.000	34.300	400.0	524.000	188547	359.79	-10	l	15
2,4,6-TNT	33.833	32.490	35.176	400.0	517.700	227459	439.38	10		15
				.=:=====						
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
					=======	222222	3/0 37	======	==	======
3,4-DNT	18.908	18.375	19.441	400.0	256.000	92885	362.77	-9		15
	1	l	l	l]	<u> </u>		l	I	l

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

GC Column

: 25CMX4.6MM

Column size ID

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL21013A 12/21/2004 22:06

CONC UNIT

	RT	RT WI	NDOW	TRUE	AVERAGE	RESU	JLT	<u> </u>	l	%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	======				=======				==	=====
HMX	6.200	6.120	6.280	400.0	245.000	97276	397.07	-1	İ	15
RDX	8.042	7.938	8.146	400.0	268.600	100724	374.93	-6	ĺ	15
Nitrobenzene	10.883	10.779	10.987	400.0	338.000	129845	384.17	-4	İ.	15
1,3-DNB	15.733	15.372	16.094	400.0	515.000	200479	389.26	-3	i :	15
2-Nitrotoluene	16.150	15.890	16.410	400.0	273.500	105320	385.14	-4	1	15
4-Nitrotoluene	16.767	16.477	17.057	400.0	284.900	119340	418.93	5	l	15
4-AM-2,6-DNT	18.058	17.495	18.621	400.0	261.800	93293	356.38	-11	l	15
3-Nitrotoluene	18.250	17.883	18.617	400.0	352.500	142248	403.51	1	1	15
2-AM-4,6-DNT	20.108	19.350	20.866	400.0	421.400	160422	380.70			15
1,3,5-TNB	20.933	20.320	21.546	400.0	355.300	139700	393.19			15
2,6-DNT	22.450	21.726	23.174	400.0	255.700	98773	386.33	-3		15
2,4-DNT	23.783	22.986	24.580	400.0	498.400	207335	415.97	4		15
Tetryl	33.750	32.100	35.400	400.0	524.000	184486	352.04	-12	1	15
2,4,6-TNT	34.808	33.465	36.151	400.0	517.700	238090	459.92	j 15	1	15
*										
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	======	======		======			=======	=====	==	
3,4-DNT	19.358	18.825	19.891	400.0	256.000	93389	364.74	-9	1	15
									<u> </u>	

Lab Name

: EMAX

Instrument ID

: HPLC1 LCT001(T017)

GC Column

: LUNA 5U PHENYL-HEXYL : 25CMX4.6MM

Column size ID Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL27005A 12/27/2004 14:47

CONC UNIT

	RT	RT W	MOOM	TRUE	AVERAGE	RESU	JLT		Ī	%D
COMPOUND	MINUTES	FROM	TO	CONC	CF	AREA	CONC	%D	QL	LIMITS
		======	======	======	========	=======	=======	=====	==	=====
HMX	6.275	6.195	6.355	400.0	245.000	91068	371.73	-7	İ	15
RDX	8.058	7.954	8.162	400.0	268.600	100246	373.15	-7	1	15
Nitrobenzene	10.783	10.679	10.887	400.0	338.000	128489	380.15	-5	ĺ	15
1,3-DNB	15.500	15.139	15.861	400.0	515.000	199881	388.10	-3	ĺ	15
2-Nitrotoluene	15.900	15.640	16.160	400.0	273.500	108011	394.98	-1	l	15
4-Nitrotoluene	16.492	16.202	16.782	400.0	284.900	112972	396.58	-1	l	15
4-AM-2,6-DNT	17.575	17.012	18.138	400.0	261.800	94475	360.89	-10	l	15
3-Nitrotoluene	17.942	17.575	18.309	400.0	352.500	136658	387.66	-3	1	15
2-AM-4,6-DNT	19.775	19.017	20.533	400.0	421.400	152274	361.37	-10	İ	15
1,3,5-TNB	20.475	19.862	21.088	400.0	355.300	132940	374.16	-6		15
2,6-DNT	21.917	21.193	22.641	400.0	255.700	97703	382.15	-4	1	15
2,4-DNT	23.292	22.495	24.089	400.0	498.400	198391	398.03	-0		15
Tetryl	32.775	31.125	34.425	400.0	524.000	201490	384.49	-4	1	15
2,4,6-TNT	33.817	32.474	35.160	400.0	517.700	216732	418.66	5		15
SURROGATE	MINUTES	FROM	TO	TRUECON	CF	AREA	CONC	%D	1	LIMITS
		======	======	======		======		=====	==	=====
3,4-DNT	18.950	18.417	19.483	400.0	256.000	95187	371.76	-7		15
:	<u> </u>	I 	I	<u> </u>	<u></u>			 		<u> </u>

Lab Name

: EMAX

Instrument ID GC Column

: HPLC1 LCT001(T017) : LUNA 5U PHENYL-HEXYL

Column size ID

: 25CMX4.6MM

Mid Conc Init LFID & Datetime: PH17005A 08/17/2004 14:58

Conc Cont LFID & Datetime: PL27011A 12/27/2004 18:56 CONC UNIT

	RT	RT W	NDOW	TRUE	AVERAGE	RESU	JLT			%D
COMPOUND	MINUTES	FROM	то	CONC	CF	AREA	CONC	%D	QL	LIMITS
	== ======	======	======	======					==	=====
HMX	6.275	6.195	6.355	400.0	245.000	94700	386.55	-3		15
RDX	8.058	7.954	8.162	400.0	268.600	96936	360.83	-10		15
Nitrobenzene	10.792	10.688	10.896	400.0	338.000	128609	380.51	-5	i	15
1,3-DNB	15.492	15.131	15.853	400.0	515.000	201715	391.66	-2	l	15
2-Nitrotoluene	15.917	15.657	16.177	400.0	273.500	110711	404.85	1	i	15
4-Nitrotoluene	16.492	16.202	16.782	400.0	284.900	113923	399.92	-0	i	15
4-AM-2,6-DNT	17.567	17.004	18.130	400.0	261.800	91957	351.28	-12		15
3-Nitrotoluene	17.942	17.575	18.309	400.0	352.500	143786	407.88	2		15
2-AM-4,6-DNT	19.767	19.009	20.525	400.0	421.400	151933	360.56	-10	1	15
1,3,5-TNB	20.483	19.870	21.096	400.0	355.300	128895	362.78	-9		15
2,6-DNT	21.933	21.209	22.657	400.0	255.700	94871	371.07	-7		15
2,4-DNT	23.292	22,495	24.089	400.0	498,400	200622	402.50	1	l	15
Tetryl	32.800	31.150	34.450	400.0	524.000	201341	384.21	-4	İ	15
2,4,6-TNT	33.842	32.499	35.185	400.0	517,700	215930	417.11	4		15
SURROGATE	MINUTES	FROM	то	TRUECON	CF	AREA	CONC	%D	QL	LIMITS
	== ======	======	======	======					==	=====
3,4-DNT	18.950	18.417	19.483	400.0	256.000	97050	379.04	-5		15
<u> </u>		l	<u> </u>							

ANALYTICAL LOGS

SOP D EMAX-8330 Rev. No: 2 D EMAX-8310 Rev. No: 4 D EMAX-8332 Rev. No: 0 D

Book # A81-02-005

Startin	g Date: 10 /19	loy	Time	70 101101 16115 11	:27		Endin	g Date: 10/19/04	Time: 20	:05	JB. W 7301-02-003
	Preparation Batch	Data File Name	Lab Samp	le ID	DF	Ma (W)	trix (S)	Notes	1	nstrument Number	81
		XJ19.001	TEST						INIT	TAL CALIBRATION REFER	RENCE
		2			-					T	
		3							Date	10/19/04	
		5							Method	EX81719	1
		6		· · · · · · · · · · · · · · · · · · ·	-				Mid Point	XT19014A (4/5)	management of the state of the
4		7			1				ICAL ID	SH18-03-40-3	
X		8		a ya ya ka ka ka ka ka ka ka ka ka ka ka ka ka					ICV ID	SHIB-03-36-2	(10ppm)
		9		- Andrews				-	DCC ID		
ICA	And the second s	10	IB81 T614	· · · · · · · · · · · · · · · · · · ·							
ANALYTICAL BATCH	AIA	U	EX8171901	20) Alot evaluated			
ATC		12	02	100				RF shifted			
H		13	03	200				<u> </u>		Solvents ID	
		14	04	400				8330 Ical	Acetonitrile		
		15	05	8 <i>0</i> 0				(Primary col.)	Methanol	43206332	
		16	01	20					Water	43189	
		17	W v	100						<u></u>	
	<u> </u>	1 18	IEXBIJ1901	400				<u> </u>		Electronic Data Archival	
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	1								0		
									Comments:	Samples disposed of	7 10/20/04
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									Analyzed By:	KP.	
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JANAX LABORATONES, INC. 1835 W. 205* St. Tourston, CA 90501

0004



EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 |

Book # A17-010

						A-0310 Key. No	'-1 L					mre	-ra)	
Starti	ng Date	e: 8/17/0			Time:	12:11		Endin			117/04	Time: 23!5		
	Pr	reparation Batch		Data File Name		Lab Sample ID		DF	Ma S	trix W	Notes	In	strument Number	17
			P	H17.001	IBI-	7H658							Initial Calibration	
				1 2		H17C-01	20				Moberalueted	Date	08/17/04	
				3	•	02	100)	met.	EXITHITC	
				4		63	200				8330 C Teal	m.p	PH17005A	
				5		σγ	400				Phenyl-heryl			
			1	6		05	800				eclumn		Standards	
				7		v 01	w					Name	ID	Conc. (µg/L)
ΑN				8	IEX	17 HITE -01	400				<u>J</u>	DCC ID	SHIC -03-47-2 ************************************	400
AL.	€	XHOU1S		9		156-18T		5				Ical Stock		1600
ANALYTICAL BATCH				lo		1807		5				IeV	5HIC-03-53-1	400
3				1)		18		1						
LB,				12	J	180		1						
177	ě	EXHOOZW		13	०५७	745-24T		10					Solvent ID	
Ħ				iψ		2405		1				Methanol	43206332	
				15		24		<u> </u>				Water	U3189	
E E		1		16		Cho L		4				Acetonitrile		
70				17	IB	:							Electronic Data Archival	
PH17 508 A				18	ŒYI	7H17C658		ļ					Location	Date
7								-	<u></u>					1 1
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MAX ABORATORIES, INC. 1835 W. 20* St. Touranns, Cd 90501

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00091499

Book # A81-02-005 EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 | | 12/20/04 Time: 23144 **Ending Date:** 17100 12/20/04 Time: **Starting Date:** Matrix 81 Instrument Number Preparation Data Notes DF Lab Sample ID File Name (W) (S) Batch TEST INITIAL CALIBRATION REFERENCE XE XL20.001 PB812664 10/19/04 800 Date 3 CEX81J19664 EXCIJ19 Method EXLOOYWB EXLOURN XJ19014A (4/5) Mid Point 5 ICAL ID E ICV ID ANALYTICAL OUL128-11 SHIC-03-54-2 DCC ID 12 046/11/2-07 E Sat. lo 04145-01 Ringe Ħ BATCH 12 gat. 04L145-02 EXLORGE Solvents ID 13 Ringe Acetonitrile 14 43206339 X12800 Methanol 800 CEX81719665 44168 Water Electronic Data Archival 34 Date Location **EZC 5 HPLC** XP 12/20/54 Comments: gamples disposed off Analyzed By: This page is checked during the data review process.

SOP 5 EMAX-8330 Rev. No: 2 D EMAX-8310 Rev. No: 4 D EMAX-8332 Rev. No: 0 D

Book # A81-02-005

Startin	g Date:		12/2			Time:	11:48				g Date:	12/21/04	Time: Oli	44	
		aration atch		Data ile Name		Lab Sample ID		DF	Ma (W)	trix (S)		Notes	1	nstrument Number	81
			XL2	1.001	IB 81 L	-666							INIT	IAL CALIBRATION REFER	ENCE
				2	eex81	J19666					800			<u></u>	
	EXL	ovyw		3	ouliz	8-11I		50	V				Date	16/19/04	
	,			4	1	HT	a latinama il magnagation	5					Method	EXBIJ19	
	L			5	ouliu	5-OIT		500					Mid Point	XJ19014 A (4/8	1
				6		OIT		20				and the second s	ICAL ID		
ANALYTICAL				7		025		500					ICV ID		
AL I				- 8	1	02 T		20					DCC ID	5HIC-03-54-Z	····
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×		-		14	4		<u> </u>						Acetonitrile		
Ĉ				15	OUL12								Methanol	43206332	
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MAXI ABORATORIES, INC. 1835 W. 205th St. Totrande, CA 91501

000915042

This page is checked during the data review process.

Book # A81-02-005 12/23/04 Time: 10:2-3 Ending Date: 12/24/64 Time: 10:10 Starting Date: Preparation Matrix Data Lab Sample ID DF Notes **Instrument Number** 81 Batch File Name (W) (S) XL23.001 TB 81 L 672 INITIAL CALIBRATION REFERENCE CEX 81 I 19672 4002PB 5413-03-44-2 002 8330 Sur - Citic * 003 Date 10/19/04 EX \$006 SB EXLOUES EX81 J19 .004 Method .005 X J19014A (4/5 Mid Point 04 6145-03 ICAL ID .006 ANALYTICAL BATCH · 04 45612/2017 007 ICV ID COZ -04 M 3HIC-03-54-2 DCC ID 009 -045 010 - 05 \mathbf{v} u - 06 Me pearite commer. 012 - 07 013 - 03 Solvents ID 014 IB81 673 Acetonitrile × _ OK Methanol 43206332 N CEX 81 J19 673 44168 400 016 Water () EXLOGGE 04 L 154 - 03 I 1000 O 017 0 LOUI Electronic Data Archival OLX 1000 Z - D3T Location Date 019 10 RS -04T EZC 5 HPLC 12/27/04 020 10 021 046154-03 Comments: * SHIB - 03 - 44-2 022 BLNK Sampus disposed off 12/27 lox lo 2 m JKS 023 046154-04 024 BLNK 025 IB IB81674 026 CEX 81 J 19674 027 400 PXL007W ٧ EXLOUT WB 028 Analyzed By: مدن ŧ C

030

00091502

ANALYSIS RUN LOG FOR HPLC SOP EMAX-8330 Rev. No: 2

EMAX-8310 Rev. No: 4

EMAX-8332 Rev. No: 0 Book # A81-02-005 Starting Date: 12 2 15 Time: 00 ; 49 Ending Date: 12/24 Time: 04:1/ Preparation Data Matrix Lab Sample ID DF Notes Instrument Number 81 Batch File Name (W) (S) EXLCO7W XL 23, 031 046134-01 INITIAL CALIBRATION REFERENCE -02 ·032 IB 10/19/04 .033 Date EXL 5065 041145.070 EX81519 いかん V Method (044145 065 X J19014 A 030 Mid Point iB .036 ICAL ID ANALYTICAL BATCH IB81675 .037 ICV ID CEX 81519675 .038 3HIC-03-54-2 400 DCC ID Solvents ID Acetonitrile × 4320 6332 Methanol دم 44168 Water Ç 27 00 X Electronic Data Archival Location Date ₽EZC 5 HPLC 12/276x No 12/27/04 Comments: myrus dispused off, 12/27 lox Analyzed By:

MAXLaboratories, INC, 1835 W, 20 $^{\circ}$ St. Tombres, CA9130

6050

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ANALYSIS RUN LOG FOR HPLC

MAX-8330 Rev. No: 2 □ EMAX-8310 Rev. No: 4 □ EMAX-8332 Rev. No: 0 □

Book # A17-010

Starting		the grant that the same to be a second to the same	Time: 13:47				2/21/04	Time: 27 !	56	DUUR WALL-VIO
- Jun call	Preparation Bate	Data File	Lab Sample ID	DF		atrix	Notes		Instrument Number	17
	Preparation Bate	Name		Dr	S	W	140165			
		P L 21.001	IB171694		<u> </u>	ļ			Initial Calibration	
		2	CEXITHI7C694		ļ		300.	Date	08/17/04	
	EXLOUYE	3	04L128-11T	5		V	hup. RR	met.	EX17H17C	
	<u> </u>	14	+ 117	<u> </u>				m.p	PH17005A	(4/5)
		5	1/2	1						
		6	04L145-01T	20					Standards	•
		7	01					Name	ID	Conc. (µg/L)
A		8	ORT	20				DCC ID	841C-03-54-Z	80 400
K		9	+ 01	1	<u> </u>					
77		10	04L142-07T	i0			1			
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ANALYTICAL BATCH	exlosss	12	041128-01 ************************************	1	V					
TC.		13	EXTENCEXITHITC69	5			800		Solvent ID	
H	1							Methanol	432063372	purs
							<u> </u>	Water	44168	4
PL21002A								Acetonitrile		
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MAXLABORATORIES, INC. 1835 W. 20° St. Torraine, CA 91301

Page 64

ANALYSIS RUN LOG FOR HPLC

SOP __ EMAX-8330 Rev. No: 2 | EMAX-8310 Rev. No: 4 | EMAX-8332 Rev. No: 0 | |

Book # A17-010

			EMAX-8310 Rev. No: 4							Book # A17
Starti	ing Date: 12 27 16		Time: : >\frac{14}{2}	Endir	ig Date	e: (7	12764	Time: 23	: 01	
	Preparation Batch	Data File Name	Lab Sample ID	DF	Ma S	atrix W	Notes	I	nstrument Number	17
		PL27.00/	TEST						Initial Calibration	
		1002						Date	08/17/04	
		-003	IB 17 L 703					met.	שרו H רו אט	
		, no.h	TEST					m.p	PHITOMIA	
		ं जार्	CE X17417 C703				५००७ व्यव			
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X		.088	-03				1	DCC ID	3H 1C-03 56-2	KOO
. .		.004	-01							
STE	9	.010	J - 076	b						
ANALYTICAL RATCH		-04	CEX 17 H17 C704				400 pp			
B	BXLCOTW	012	046114-61	ı		v				
È	1	013	1 -02			<u>, </u>			Solvent ID	
T T	EXL0063	.014	-03					Methanol	43306332	guna
-4.P	<u>,</u>	210	J 04					Water	44168	1
رم د		016	IB					Acetonitrile		
2		3.017	CEXITHIT CTOS				400 pps		Electronic Data Archival	
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 ${\cal L}_{MAX}$ Laboratories, IMC, 1835 W/ 23° St Tourne, CA 91501

EXTRACTION LOGS

EXTRACTION LOG FOR EXPLOSIVES

#******* JV 12/20/4 Book # EEX-010 000 0.0 Ī SP/B- 35 MILES 01-267 0d091506 STU14- 02-1478 Extract Location Lot#/ID 36 v£3080 12/20/04 -E0-8/#S 08:51 77 (#B M JF. 12/201K -81#5 Stox Time: Extract Received By: Standard Added By: Checked By: Comments: Disposal Date: Prepared By: Standards Reagent *9QS 12/20/04 Acetonitrile Silica Sand Surrogate LCS/MS CaCl NaC End Date: Notes 13:00 Volume 1 4 4 * 7 7 7 7 Time: 12/20/04 Amount (g | ml) Sample 200% 200 200 200 200 200 200 200 20/04 Start Date: WC 12 .tVB Z 77 O K ó 103 X EMAX-8330 Rev.No.: 3 Sample ID 4001XI 145 821740 100 700 WATER Sample Prep U *01 *02 *03 *04 90* *10 *05 *07 *08 **\$**0 *12 *13 *14 *15 *16 *18 *19 *17 *20 *22 *23 *24 *25 *26 *21 Matrix: SOP: PREPARATION BATCH: EXLOO4-W

EXTRACTION LOG FOR EXPLOSIVES

Book # EEX-010 Amount Added O. Ā Ē 9.4 00091507 SP18-01-267 Extract Location 4.2289249 23 (0) Lot#/ID SH1B-03-36-43080 34118-03-36 88 <u>で</u> を St.04.# Z 72 20.77 Standard Added By: Extract Received By: Disposal Date: Prepared By: 12/23/64 Time: Checked By: Comments: Standards Reagent # 9QS Acetonitrile Silica Sand Surrogate LCS/MS Co NaC End Date: Notes Time: 19:00 Volume Extract 1 S 30 8 Ş જ B Amount (g | ml) Sample 2.04 2.03 x, 033 ઇ Start Date: /2/22/64/ 10 X 2.01 2.02 2.63 2.00 2.01 ck. 2.0 122/04 ςį Jr 12/ -04M 1040 SL 105 - SB 8 2 201 60-00 9 B K EMAX-8330 Rev.No.: 3 □ ì Sample ID 5007XY 57/7 75/740 7:0 7/08 Sample *26 Prep ID *16 *18 *19 *20 *24 *25 *10 *15 *23 *01 *02 *03 \$0 *05 90* *07 *08 60 * **II*** *12 *13 *14 *17 *21 *22 Matrix: SOP: PREPARATION BATCH: EXLCO6 - S

LABORATORY REPORT FOR

SHAW E&I

LONG HORN ARMY AMMUNITION PLANT

EPA METHOD 8330 EXPLOSIVES

SDG#: 04L154

CASE NARRATIVE

CLIENT:

SHAW E & I

PROJECT:

LONG HORN ARMY AMMUNITION PLANT

EMAX SDG:

04L154

EPA METHOD 8330 EXPLOSIVES

Two (2) water and two (2) soil samples were received on 12/21/04 for Explosives analysis by EPA Method 8330 in accordance with USEPA-SW846 3rd edition, and EMAX-8330.

1. Holding Time

Analytical holding time was met. Extraction for water samples was started and completed on 12/23/04. Extraction for soil samples was started on 12/22/04 and completed on 12/23/04.

2. Calibration

Initial calibration was 5 point. %RSDs were within 20%. All continuing calibrations of the primary column were carried out at 12-hour intervals and the recoveries were within 85-115%.

3. Method Blank

Method blanks were free of contamination at the Reporting Limit.

4. Surrogate recovery

All surrogate recoveries were within QC limits.

5. Lab Control Sample / Lab Control Duplicate

All recoveries were within QC limits.

6. Matrix Spike/Matrix Spike Duplicate

No sample was spiked.

7. Sample Analysis

Sample analyses were within QC requirements. Quantitation is from the primary column. All positive results above RL were confirmed by LC-CN column and the confirmation is presumptive because it was based on retention time window.

Samples were air-dried prior to extraction; hence, no moisture correction was applied to RL, MDL and results.

LAB CHRONICLE EXPLOSIVES

		CONGRESS AND AND LICE TERM							Instrument ID : TOB1
					SOIL				
Client	Laboratory	Dilution	%	Analysis	Extraction	Sample	Calibration Prep.	n Prep.	
Sample ID	Sample ID	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	1				1		
MRIKTS	EXL006SB	-	AN	12/23/0411:51	12/22/0417:00	XL23004A	XL23002A	EXIL006S	Method Blank
I CS1S	EXL006SL	•	X.	12/23/0412:20	12/22/0417:00	XL23005A	XL23002A	EXL006S	Lab Control Sample (LCS)
77US62	1154-03	_	Z	12/23/0420:01	12/22/0417:00	XL23021A	XL23016A	EXL006S	Field Sample
29SD45	L154-04	-	A.	12/23/0420:59	12/22/0417:00	XL23023A	XL23016A	EXL 006S	Field Sample
					WATER				
Client	Laboratory	Dilution	34	Analysis	Extraction	Sample	Calibration Prep.	n Prep.	
Sample ID	Sample 1D	Factor	Moist	DateTime	DateTime	Data FN	Data FN	Batch	Notes
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1		1 1 1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1	1 1 1 1	
MRI K1U	EXL007WB	•	X X	12/23/0423:23	12/23/0411:00	XL23028A	XL23027A	EXL007W	Method Blank
1 CS1W	EXL0074L	. 	Ā	12/23/0423:52	12/23/0411:00	XL23029A	XL23027A	EXL007W	Lab Control Sample (LCS)
1.69.1	EXL0074C	-	¥	12/24/0400:20	12/23/0411:00	XL23030A	XL23027A	EXL007W	LCS Duplicate
595W44	L154-01	-	¥.	12/24/0400:49	12/23/0411:00	XL23031A	XL23027A	EXL007W	Field Sample
	1	•	•	0,0000000000000000000000000000000000000	00-11/0/ 50/04	***************************************	*CC080 175	1000	Comment of the Contract of the

FN - Filename % Moist - Percent Moisture

Client : SHAW E&I	Date Collected: 12/19/04
Project : LONGHORN ARMY AMMUNITION PLANT	Date Received: 12/21/04
Batch No. : 04L154	Date Extracted: 12/23/04 11:00
Sample ID: 29SW44	Date Analyzed: 12/24/04 00:49
Lab Samp ID: L154-01	Dilution Factor: 1
Lab File ID: XL23031A	Matrix : WATER
Ext Btch ID: EXLOO7W	% Moisture : NA
Calib. Ref.: XL23027A	Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)

ĤMX	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	.4.1	1	.2
4-AM-2,6-DNT	2	1	.2
2-AM-4,6-DNT	.56J	1	.2
2,6-DNT	ND	-1	.2
2,4-DNT	ND	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	1	.2
4-NITROTOLUENE	ND	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	

99

63-143

Note: All positive results are confirmed by CN column

3,4-DINITROTOLUENE

Client : SHAW E&I Date Collected: 12/19/04
Project : LONGHORN ARMY AMMUNITION PLANT
Batch No. : 04L154
Batch No. : 04L154
Date Extracted: 12/23/04 11:00
Date Analyzed: 12/24/04 01:18
Lab Samp ID: L154-02
Dilution Factor: 1
Lab File ID: XL23032A
Ext Btch ID: EXL007W
Moisture : NA
Calib. Ref.: XL23027A

Date Analyzed: 12/24/04 01:18
Matrix : WATER
Instrument ID : T-081

	RESULTS	RL	MDL
PARAMETERS	(ug/L)	(ug/L)	(ug/L)
HMX	ND	1	.2
RDX	ND	1	.2
1,3,5-TNB	ND	1	.2
1,3-DNB	ND	1	.2
TETRYL	ND	.1	.2
NITROBENZENE	ND	1	.2
2,4,6-TNT	.39J	1	.2
4-AM-2,6-DNT	1.9	1	.2
2-AM-4,6-DNT	.53J	1	.2
2,6-DNT	ND	1	.2
2,4-DNT	,ND	1	.2
2-NITROTOLUENE	ND	1	.2
3-NITROTOLUENE	ND	1	.2
4-NITROTOLUENE	ND	1	.2
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	90	63-143	

Client : SHAW E&I Date Collected: 12/20/04 Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L154 Date Received: 12/21/04 Date Extracted: 12/22/04 17:00 Sample ID: 29SD44 Lab Samp ID: L154-03 Date Analyzed: 12/23/04 20:01 Dilution Factor: 1 Lab File ID: XL23021A Matrix : SOIL Ext Btch ID: EXLOG6S % Moisture Instrument ID : T-081 Calib. Ref.: XL23016A _____

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
****	alan yan bara daki daki daki daki daki daki		
3,4-DINITROTOLUENE	110	63-143	

Date Collected: 12/20/04 Client : SHAW E&I Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L154 Date Received: 12/21/04

Date Extracted: 12/22/04 17:00 Sample ID: 29SD45 Date Analyzed: 12/23/04 20:59

Lab Samp ID: L154-04 Dilution Factor: 1 Lab File ID: XL23023A : SOIL Matrix Ext Btch ID: EXLO06S % Moisture : NA Instrument ID : T-081 Calib. Ref.: XL23016A

	RESULTS	RL	MDL
PARAMETERS	(ug/kg)	(ug/kg)	(ug/kg)
			:
нмх	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	410	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	ND	400	200
2,6-DNT	ND	400	200
2,4-DNT	ND	400	200
2-NITROTOLUENE	ND	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	116	63-143	

Client : SHAW E&I Date Collected: NA Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L154 Date Received: 12/23/04 Date Extracted: 12/23/04 11:00 Sample ID: MBLK1W Date Analyzed: 12/23/04 23:23 Dilution Factor: 1 Lab Samp ID: EXLOO7WB Matrix : WATER % Moisture : NA Instrument ID : T-081 Lab File ID: XL23028A Ext Btch ID: EXLO07W

Calib. Ref.: XL23027A

essessessessessessessessessessessessess	1 NS CI ⁻ C	Instrument ID : 1-001					
PARAMETERS	RESULTS (ug/L)	RL (ug/L)	MDL (ug/L)				
HMX	ND	4	.2				
		1	.2				
RDX	ND	1					
1,3,5-TNB	ND	!	.2				
1,3-DNB	ND	1	.2				
TETRYL	ND	1	.2				
NITROBENZENE	ND	1	.2				
2,4,6-TNT	'ND	1	.2				
4-AM-2,6-DNT	ND	1	.2				
2-AM-4,6-DNT	ND	1	.2				
2,6-DNT	ND	1	.2				
2,4-DNT	ND	1	.2				
2-NITROTOLUENE	ND	1	.2				
3-NITROTOLUENE	ND	1	.2				
4-NITROTOLUENE	ND	1	.2				
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT					

91

63-143

Note: All positive results are confirmed by CN column

3,4-DINITROTOLUENE

EMAX QUALITY CONTROL DATA LCS/LCD ANALYSIS

CLIENT:

SHAW E&I

PROJECT:

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.: METHOD:

04L154 EPA 8330

MATRIX: DILUTION FACTOR: 1

WATER

% MOISTURE:

NA

SAMPLE ID: LAB SAMP ID:

LAB FILE ID:

MBLK1W

1

1

EXL007WC

EXL007WB XL23028A

XL23029A

EXL007WL

XL23030A

DATE ANALYZED: 12/23/0423:23 12/23/0423:52 12/24/0400:20 DATE RECEIVED: 12/23/04

DATE EXTRACTED: 12/23/0411:00 12/23/0411:00 12/23/0411:00 DATE COLLECTED: NA

PREP. BATCH: EXLOO7W CALIB. REF:

XL23027A

EXL007W XL23027A

EXL007W XL23027A

ACCESSION:

PARAMETER	BLNK RSLT (ug/L)	SPIKE AMT (ug/L)	BS RSLT (ug/L)	BS % REC	SPIKE AMT	BSD RSLT (ug/L)	BSD % REC	RPD (%)	QC LIMIT	MAX RPD
HMX	ND	4	3.94	98	4	4.07	102	3	70-130	30
RDX	ND ND	4	3.13	78	4	3.23	81	3	60-130	30
1,3,5-TNB	ND	4	3.65	91	4	3.81	95	4	70-130	30
1,3-DNB	NĎ	4	3.45	86	4	3.63	91	5	70-130	30
Tetryl	ND	4	3.55	89	4	3.81	95	7	50-140	30
Nitrobenzene	ND	4	3.28	82	4	3.47	87	6	60-130	30
2,4,6-TNT	ND	4	3.96	99	4	4.14	104	5	70-140	30
4-AM-2,6-DNT	ND	.4	3.47	87	4	3.68	92	6	70-130	30
2-AM-4,6-DNT	ND	4	3.59	90	4	3.82	95	6	70-130	30
2,6-DNT	ND	4	3.61	90	4	3.9	97	8	70-130	30
2,4-DNT	ND	4	3.67	92	4	3.91	98	6	70-130	30
2-Nitrotoluene	ND	4	3.43	86	4	3.55	89	3	70-130	30
3-Nitrotoluene	ND	4	3.48	87	4	3.68	92	6	70-130	30
4-Nitrotoluene	ND	4	3.6	90	4	3.77	94	5	70-130	30

SURROGATE PARAMETER	SPIKE AMT (ug/L)	BS RSLT (ug/L)	BS % REC	SPIKE AMT (ug/L)	BSD RSLT (ug/L)	BSD % REC	QC LIMIT	
3.4-Dinitrotoluene	4	3.72	93	4	4.05	101	70-130	

Client : SHAW E&I Date Collected: NA Project : LONGHORN ARMY AMMUNITION PLANT Batch No. : 04L154 Date Received: 12/22/04 Date Extracted: 12/22/04 17:00 Date Analyzed: 12/23/04 11:51 Sample ID: MBLK1S Lab Samp ID: EXLOGSB Dilution Factor: 1 : SOIL Lab File ID: XL23004A Matrix % Moisture : NA Instrument ID : T-081 Ext Btch ID: EXLO06S Calib. Ref.: XL23002A

PARAMETERS	RESULTS (ug/kg)	RL (ug/kg)	MDL (ug/kg)
		400	200
HMX	ND	400	200
RDX	ND	400	200
1,3,5-TNB	ND	400	200
1,3-DNB	ND	400	200
TETRYL	ND	400	200
NITROBENZENE	ND	400	200
2,4,6-TNT	ND	400	200
4-AM-2,6-DNT	ND	400	200
2-AM-4,6-DNT	NĎ	400	200
2,6-DNT	NĎ	400	200
2,4-DNT	NĎ	400	200
2-NITROTOLUENE	NĎ	400	200
3-NITROTOLUENE	ND	400	200
4-NITROTOLUENE	ND	400	200
SURROGATE PARAMETERS	% RECOVERY	QC LIMIT	
3,4-DINITROTOLUENE	106	63-143	

EMAX QUALITY CONTROL DATA LCS ANALYSIS

CLIENT: PROJECT: SHAW E&I

LONGHORN ARMY AMMUNITION PLANT

BATCH NO.: METHOD:

04L154 EPA 8330

MATRIX: SOIL DILUTION FACTOR: 1

% MOISTURE:

NA

SAMPLE ID:

MBLK1S

LAB SAMP ID:

EXL006SB

EXL006SL

LAB FILE ID:

XL23004A DATE EXTRACTED: 12/22/0417:00 12/22/0417:00

XL23005A

DATE ANALYZED:

12/23/0411:51 12/23/0412:20

DATE COLLECTED: NA DATE RECEIVED: 12/22/04

PREP. BATCH:

EXL006S

EXL006S

CALIB. REF:

XL23002A

XL23002A

ACCESSION:

BLNK RSLT (ug/kg)	SPIKE AMT (ug/kg)	BS RSLT (ug/kg)	BS % REC	QC LIMIT
ND	2000	2050	102	70-140
ND	2000	2000	100	70-140
ND	2000	2160	108	70-130
ND	2000	2210	111	70-130
ND	2000	1970	98	60-140
ND	2000	2190	110	70 - 130
ND	2000	2140	107	70-140
ND	2000	2090	104	70-130
ND	2000	2120	106	70 - 130
ND	2000	2140	107	70-140
ND	2000	2150	108	70-130
ND	2000	2030	102	70-130
ND	2000	2060	103	70-130
ND	2000	2210	111	70-130
	(ug/kg) ND ND ND ND	(ug/kg) (ug/kg) ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000 ND 2000	(ug/kg) (ug/kg) (ug/kg) ND 2000 2050 ND 2000 2000 ND 2000 2160 ND 2000 2210 ND 2000 1970 ND 2000 2190 ND 2000 2140 ND 2000 2090 ND 2000 2120 ND 2000 2140 ND 2000 2150 ND 2000 2030 ND 2000 2030 ND 2000 2030 ND 2000 2030	(ug/kg) (ug/kg) (ug/kg) % REC ND 2000 2050 102 ND 2000 2000 100 ND 2000 2160 108 ND 2000 2210 111 ND 2000 1970 98 ND 2000 2190 110 ND 2000 2140 107 ND 2000 2090 104 ND 2000 2120 106 ND 2000 2140 107 ND 2000 2150 108 ND 2000 2030 102 ND 2000 2030 102 ND 2000 2030 102 ND 2000 2060 103

SURROGATE PARAMETER	SPIKE AMT (ug/kg)	BS RSLT (ug/kg)		QC LIMIT
SORROGATE TARABLETER		(49/79/		
3 4-Dinitrotoluene	2000	2140	107	70-130



156 Starlite Drive, Marietta, OH 45750 • TEL 740-373-4071 • FAX 740-373-4835 • http://www.kemron.com

Laboratory Report Number: L0502503 - Revised

Please find enclosed the analytical results for the samples you submitted to KEMRON Environmental Services.

Review and compilation of your report was completed by KEMRON's Sales and Service Team. If you have questions, comments or require further assistance regarding this report, please contact our team member noted in the Reviewed box below at 800-373-4071. Team member e-mail addresses also appear here for your convenience.

Debra Elliott - Team Leader delliott@kemron-lab.com

Cheryl Koelsch - Team Chemist/Data Specialist ckoelsch@kemron-lab.com

 $\begin{tabular}{ll} \bf Stephanie \ Mossburg - Team \ Chemist/Data \ Specialist \\ smossburg@kemron-lab.com \end{tabular}$

Kathy Albertson - Team Chemist/Data Specialist kalbertson@kemron-lab.com

 $\begin{tabular}{ll} \bf Micalyn \ Harris - Team \ Chemist/Data \ Specialist \\ \hline \bf mharris@kemron-lab.com \\ \end{tabular}$

This report was reviewed on March 17, 2005:

-Stephanie Mossburg Amanda Fickiesen - Client Services Specialist afickiesen@kemron-lab.com

Nina Scott - Client Services Specialist ascott@kemron-lab.com

Vicki Lauer - Client Services Specialist vlauer@kemron-lab.com

I certify that all test results meet all of the requirments of the NELAP standards and other applicable contract terms and conditions. All results for soil samples are reported on a 'dry-weight' basis unless specified otherwise. Analytical results for water and wastes are reported on an 'as received' basis unless specified otherwise. A statement of uncertainty for each analysis is available upon request. This laboratory report shall not be reproduced, except in full, without the written approval of KEMRON Environmental Services.

This report was certified on March 17, 2005:

Din & Vande berg

FL DOH NELAP ID: E87551

This report contains a total of <u>49</u> pages.

Protecting Our Environmental Future

LABORATORY REPORT

L0502503

03/14/05 08:44

00091520

Submitted By

KEMRON Environmental Services 156 Starlite Drive Marietta, OH 45750 (740)373-4071

For

Account Name: Shaw E & I. Inc.
ABB Lummus Biulding

3010 Briarpark Houston, TX 77042

Attention: Diane Mever

Account Number: 307-ALLIANCE-798

Work ID: CHAAP-29 MANHOLES

P.O. Number: 69840

Sample Summary

Client ID	Lab ID	Date Collected	Date Received
29WL34-MH03-02	L0502503-01	24-FEB-05	25-FEB-05
29WL36-MH05-02	L0502503-02	24-FEB-05	25-FEB-05
29WL37-MH06-02	L0502503-03	24-FEB-05	25-FEB-05
29WL38-MH07-02	L0502503-04	23-FEB-05	25-FEB-05
29WL39-MH08-02	L0502503-05	23-FEB-05	25-FEB-05
29WL40-MH09-02	L0502503-06	23-FEB-05	25-FEB-05
29WL40-MH09-52	L0502503-07	23-FEB-05	25-FEB-05
29WL41-MH10-02	L0502503-08	23-FEB-05	25-FEB-05
29WL42-MH11-02	L0502503-09	23-FEB-05	25-FEB-05
29WL43-MH12-02	L0502503-10	23-FEB-05	25-FEB-05

KEMRON FORMS - Modified 11/05/2004 Version 1.5 PDF File ID: 201367 Report generated 03/14/2005 08:44

1 OF 1

ID: 16386

00091521

KEMRON ENVIRONMENTAL SERVICES REPORT NARRATIVE

KEMRON Login No.: L0502503

CHAIN OF CUSTODY: The chain of custody number was 01-KEMM-FEB05.

SHIPMENT CONDITIONS: The chain of custody forms were received sealed in a cooler. The cooler

temperatures were 2, 3, and 4 degrees C.

SAMPLE MANAGEMENT: All samples received were intact.

I certify that this data package is in compliance with the terms and conditions agreed to by the client and KEMRON Environmental Services, both technically and for completeness, except for the conditions noted above. Release of the data contained in this hardcopy data package has been authorized by the Laboratory Manager or designated person, as verified by the following signature.

Approved: 01-MAR-05

Sitephanic Mossburg

00091522

KEMRON ENVIRONMENTAL SERVICES HPLC-EXPLOSIVE RESIDUES

KEMRON Login No.: L0502503

METHOD

Analysis: SW-846 8330

HOLDING TIMES

Sample Preparation: All holding times were met.

Sample Analysis: All holding times were met.

PREPARATION

Sample preparation proceeded normally.

CALIBRATION

Initial Calibration: For all compounds linear equations were applied. All acceptance criteria were met.

Alternate Source Standards: All acceptance criteria were met.

Continuing Calibration: All acceptance criteria were met.

BATCH QA/QC

Method Blank: All acceptance criteria were met.

Laboratory Control Sample: All acceptance criteria were met.

Matrix Spikes: The MS/MSD results were not associated with this sample delivery group.

SAMPLES

Surrogates: Sample fractions 01 through 03 yielded a percent recovery for the surrogate that was below the advisory limit. For fractions 02 and 03 the surrogate co-eluted with the high 2,4,6-trinitrotoluene peak. For fraction 01 the surrogate was poorly resolved from the 2,4,6-trinitrotoluene peak.

Samples: Sample fractions 01 through 03 and 06 through 10 were re-analyzed at a dilution in order to maintain the analysis within the range of calibration. All acceptance criteria were met.

Manual Integration Reason Codes

KEMRON laboratory management has identified four general cases with valid reasons supporting the use of manual integration techniques.

Reason #1: Data System Fails to Select Correct Peak

In some cases the chromatography system selects and integrates the "wrong peak". In this case the analyst must correct the selection and force the system to integrate the proper peak. Other times the system may miss the peak completely.

'Reason #2: Data System Splits the Peak Incorrectly or Integrates a False Peak as a Rider Peak 00091523

This phenomena is common at low concentrations where the signal:noise ratio is low. A single compound (peak) is incorrectly split into multiple peaks or integrated as a main peak with one or more rider peaks resulting in low area counts for the target compound.

Reason #3: Improperly Integrated Isomers and/or coeluting compounds.

This system often fails to distinguish coeluting compounds and or isomers. The integration areas and concentrations are wrong, and they must be corrected by manual integration. Prime examples are benzo(k)fluoranthene and benzo(b)fluoranthene which are often unresolved and integrated improperly when both are present at low concentrations in standards or samples.

Reason #4: System Establishes Incorrect Baseline

There are numerous situations in chromatography where the system establishes the baseline incorrectly. Some baseline errors will be obvious to the analyst and should be corrected via manual procedures.

Reason #5: Miscellaneous

Other situations involving integration errors may require in-depth review and technical judgment. These cases should be brought to the attention of the laboratory management. If the form of manual integration is not clearly covered by these four cases, then review and approval by the Laboratory Director or the QA/QC Supervisor will be required.

I certify that this data package is in compliance with the terms and conditions agreed to by the client and KEMRON Environmental Services, both technically and for completeness, except for the conditions noted above. Release of the data contained in this hardcopy data package has been authorized by the Laboratory Manager or designated person, as verified by the following signature.

Analyst: RDC

Approved: 11-MAR-05

KEMRON ENVIRONMENTAL SERVICES

Report Number: L0502503

Sample Tag: 01

Report Date : March 14, 2005

00091524

 Sample Number: L0502503-01
 Prep Method: 3535
 Instrument: HPLC4

 Client ID: 29WL34-MH03-02
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

 Matrix: Water
 Analyst: ECL
 Cal Date: 03/02/2005 16:53

 Workgroup Number: WG184109
 Dilution: 1
 Run Date: 03/02/2005 19:59

 Collect Date: 24-FEB-05
 Units: ug/L
 File ID: 4L007772.F

Analyte	CAS. Numb	per	Re	esult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	1			υ		1.05	0.263
1,3-Dinitrobenzene	99-65-0)			υ		1.05	0.263
2,4,6-Trinitrotoluene	118-96-	7	2	23.5	I		1.05	0.263
2,4-Dinitrotoluene	121-14-	2			υ		1.05	0.263
2,6-Dinitrotoluene	606-20-	2			U		1.05	0.263
2-Amino-4,6-dinitrotoluene	35572-78	-2	1	L.19			1.05	0.263
2-Nitrotoluene	88-72-2	2			υ		1.05	0.263
3-Nitrotoluene	99-08-1	-			υ		1.05	0.263
4-Nitrotoluene	99-99-0)			U		1.05	0.263
4-Amino-2,6-dinitrotoluene	19406-51	-0	2	2.13			1.05	0.263
нмх	2691-41-	-0			υ		1.05	0.263
Nitrobenzene	98-95-3	3			υ		1.05	0.263
RDX	121-82-	121-82-4			U		1.05	0.263
Tetryl	479-45-	479-45-8			υ		1.05	0.263
Surrogate	% Recovery	Lowe	er	Uppe	r	Qual		•
3,4-Dinitrotoluene	42.9	50		150		SMI		

I Semiquantitative result (out of instrument calibration range)

SMI Sample matrix interference on surrogate

U Not detected at or above the method detection limit

Sample Number:L0502503-01	Prep Method: 3535	Instrument: HPLC4
Client ID: 29WL34-MH03-02	Analytical Method: 8330	Prep Date: 03/02/2005 08:00
Matrix: Water	Analyst: ECL	Cal Date: 03/02/2005 16:53
Workgroup Number: WG184109	Dilution: 5	Run Date: 03/03/2005 18:31
Collect Date: 24-FEB-05	Units:ug/L	File ID:4L007786.F
Sample Tag:DL01		

Analyte	CAS. Numbe	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	99-35-4		U		5.26	1.32
1,3-Dinitrobenzene	99-65-0			U		5.26	1.32
2,4,6-Trinitrotoluene	118-96-7	'	23.0			5.26	1.32
2,4-Dinitrotoluene	121-14-2	1		Ū		5.26	1.32
2,6-Dinitrotoluene	606-20-2	1		U		5.26	1.32
2-Amino-4,6-dinitrotoluene	35572-78-	35572-78-2		Ū		5.26	1.32
2-Nitrotoluene	88-72-2	88-72-2		U		5.26	1.32
3-Nitrotoluene	99-08-1			Ū	U 5.26		1.32
4-Nitrotoluene	99-99-0			υ		5.26	1.32
4-Amino-2,6-dinitrotoluene	19406-51-	0	2.20	J		5.26	1.32
нмх	2691-41-	0		U		5.26	1.32
Nitrobenzene	98-95-3			Ū	5.26		1.32
RDX	121-82-4			U		5.26	1.32
Tetryl	479-45-8	1		υ		5.26	1.32
Surrogate	% Recovery	Lower	Upp	er	Qual		•
3,4-Dinitrotoluene	42.7	50	15	50	SMI		

 $^{{\}tt J}$ The analyte was positively identified, but the quantitation was below the RL SMI Sample matrix interference on surrogate

1 of 9

 $^{{\}tt U}\,\,$ Not detected at or above the method detection limit

KEMRON ENVIRONMENTAL SERVICES

Report Number: L0502503

Report Date : March 14, 2005

00091525

 Sample Number: L0502503-02
 Prep Method: 3535
 Instrument: HPLC4

 Client ID: 29WL36-MH05-02
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

 Matrix: Water
 Analyst: ECL
 Cal Date: 03/02/2005 16:53

 Workgroup Number: WG184109
 Dilution: 1
 Run Date: 03/02/2005 20:36

Collect Date: 24-FEB-05 Units: ug/L File ID: 4L007773.F Sample Tag: 01

Analyte	CAS. Numb	per	Re	esult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	!			υ		1.04	0.260
1,3-Dinitrobenzene	99-65-0)			υ		1.04	0.260
2,4,6-Trinitrotoluene	118-96-	7	ε	38.3	I		1.04	0.260
2,4-Dinitrotoluene	121-14-	2			υ		1.04	0.260
2,6-Dinitrotoluene	606-20-	2			Ū		1.04	0.260
2-Amino-4,6-dinitrotoluene	35572-78	-2	1	L.82			1.04	0.260
2-Nitrotoluene	88-72-2	2			Ū		1.04	0.260
3-Nitrotoluene	99-08-1	_			υ		1.04	0.260
4-Nitrotoluene	99-99-0)			Ū		1.04	0.260
4-Amino-2,6-dinitrotoluene	19406-51	-0	2	2.74			1.04	0.260
нмх	2691-41-	-0			Ū		1.04	0.260
Nitrobenzene	98-95-3	3			υ		1.04	0.260
RDX	121-82-	4			υ		1.04	0.260
Tetryl	479-45-	8			Ū		1.04	0.260
Surrogate	% Recovery	Lowe	er	Uppe	r	Qual		•
3,4-Dinitrotoluene		50		150		SMI		

I Semiquantitative result (out of instrument calibration range)

SMI Sample matrix interference on surrogate

U Not detected at or above the method detection limit

Sample Number: L0502503-02	Prep Method: 3535	Instrument: HPLC4
Client ID: 29WL36-MH05-02	Analytical Method: 8330	Prep Date: 03/02/2005 08:00
Matrix: Water	Analyst: ECL	Cal Date: 03/02/2005 16:53
Workgroup Number: WG184109	Dilution: 10	Run Date: 03/03/2005 19:09
Collect Date: 24-FEB-05	Units: ug/L	File ID:4L007787.F
Sample Tag:DL01		

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	99-35-4		U		10.4	2.60
1,3-Dinitrobenzene	99-65-0			Ū		10.4	2.60
2,4,6-Trinitrotoluene	118-96-7	7	84.3			10.4	2.60
2,4-Dinitrotoluene	121-14-2	2		U		10.4	2.60
2,6-Dinitrotoluene	606-20-2	2		υ		10.4	2.60
2-Amino-4,6-dinitrotoluene	35572-78-	-2		U		10.4	2.60
2-Nitrotoluene	88-72-2			υ		10.4	2.60
3-Nitrotoluene	99-08-1			Ū		10.4	2.60
4-Nitrotoluene	99-99-0			U		10.4	2.60
4-Amino-2,6-dinitrotoluene	19406-51-	-0	2.88	J		10.4	2.60
HMX	2691-41-	0		U		10.4	2.60
Nitrobenzene	98-95-3			Ū		10.4	2.60
RDX	121-82-4	4		U		10.4	2.60
Tetryl	479-45-8	3		υ		10.4	2.60
Surrogate	% Recovery	Lower	Upp	er	Qual		•
3,4-Dinitrotoluene		50	15	50	DL		

DL Surrogate or spike compound was diluted out

2 of 9

 $^{{\}tt J}$ The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

KEMRON ENVIRONMENTAL SERVICES

Report Number: L0502503

Report Date : March 14, 2005

00091526

Collect Date: 24-FEB-05 Units: ug/L File ID: 4L007774.F
Sample Tag: 01

Analyte	CAS. Numb	per	Re	esult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	99-35-4 1.34				1.04	0.260	
1,3-Dinitrobenzene	99-65-0)			U		1.04	0.260
2,4,6-Trinitrotoluene	118-96-	7		452	I		1.04	0.260
2,4-Dinitrotoluene	121-14-	2			U		1.04	0.260
2,6-Dinitrotoluene	606-20-	2			U		1.04	0.260
2-Amino-4,6-dinitrotoluene	35572-78	-2	ϵ	5.27			1.04	0.260
2-Nitrotoluene	88-72-2	2			U		1.04	0.260
3-Nitrotoluene	99-08-1	L			U		1.04	0.260
4-Nitrotoluene	99-99-0)			U		1.04	0.260
4-Amino-2,6-dinitrotoluene	19406-51	-0	ε	3.15			1.04	0.260
нмх	2691-41-	-0			U		1.04	0.260
Nitrobenzene	98-95-3	3			U		1.04	0.260
RDX	121-82-	.21-82-4 0.494		.494	J	1.04		0.260
Tetryl	479-45-	8			U		1.04	0.260
Surrogate	% Recovery	Lowe	er	Uppe	r	Qual		•
3,4-Dinitrotoluene		50		150)	SMI		

I Semiquantitative result (out of instrument calibration range)

SMI Sample matrix interference on surrogate

U Not detected at or above the method detection limit

Sample Number: L0502503-03	Prep Method: 3535	Instrument:HPLC4
Client ID: 29WL37-MH06-02	Analytical Method: 8330	Prep Date: 03/02/2005 08:00
Matrix: Water	Analyst: ECL	Cal Date: 03/02/2005 16:53
Workgroup Number: WG184109	Dilution: 100	Run Date: 03/03/2005 19:46
Collect Date: 24-FEB-05	Units: ug/L	File ID:4L007788.F
Sample Tag:DL01		

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	99-35-4		υ		104	26.0
1,3-Dinitrobenzene	99-65-0			υ		104	26.0
2,4,6-Trinitrotoluene	118-96-7	,	430			104	26.0
2,4-Dinitrotoluene	121-14-2	2		Ū		104	26.0
2,6-Dinitrotoluene	606-20-2	2		U		104	26.0
2-Amino-4,6-dinitrotoluene	35572-78-	-2		U		104	26.0
2-Nitrotoluene	88-72-2	88-72-2		U		104	26.0
3-Nitrotoluene	99-08-1			υ		104	26.0
4-Nitrotoluene	99-99-0			υ		104	26.0
4-Amino-2,6-dinitrotoluene	19406-51-	19406-51-0		υ		104	26.0
HMX	2691-41-	0		U		104	26.0
Nitrobenzene	98-95-3			Ū		104	26.0
RDX	121-82-4	Ł		υ		104	26.0
Tetryl	479-45-8	В		Ū		104	26.0
Surrogate	% Recovery	Lower	Upp	er	Qual		1
3,4-Dinitrotoluene		50	15	0	DL		

DL Surrogate or spike compound was diluted out

3 of 9

J The analyte was positively identified, but the quantitation was below the RL

 $^{{\}tt U}\,\,$ Not detected at or above the method detection limit

Report Number: L0502503

Report Date : March 14, 2005

00091527

___ Instrument:<u>HPLC4</u> Sample Number: L0502503-04 Prep Method: 3535

Prep Date: 03/02/2005 08:00 Client ID: 29WL38-MH07-02 Analytical Method: 8330 Matrix: Water Analyst:**ECL** Cal Date: 03/02/2005 16:53 Workgroup Number: WG184109 Dilution: 1 Run Date: 03/02/2005 22:28 Collect Date: 23-FEB-05

File ID: 4L007776.F Units:ug/L Sample Tag: 01

Analyte	CAS. Numb	per	Re	sult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	<u> </u>			υ		1.04	0.260
1,3-Dinitrobenzene	99-65-0)			υ		1.04	0.260
2,4,6-Trinitrotoluene	118-96-	7	0	.955	J		1.04	0.260
2,4-Dinitrotoluene	121-14-	2			υ		1.04	0.260
2,6-Dinitrotoluene	606-20-	2			υ		1.04	0.260
2-Amino-4,6-dinitrotoluene	35572-78	-2	0	.428	J		1.04	0.260
2-Nitrotoluene	88-72-2	2			υ		1.04	0.260
3-Nitrotoluene	99-08-1	L			υ		1.04	0.260
4-Nitrotoluene	99-99-0)			υ		1.04	0.260
4-Amino-2,6-dinitrotoluene	19406-51	-0	0	.364	J		1.04	0.260
нмх	2691-41-	-0			υ		1.04	0.260
Nitrobenzene	98-95-3	3			υ		1.04	0.260
RDX	121-82-	4			U		1.04	0.260
Tetryl	479-45-	8			υ		1.04	0.260
Surrogate	% Recovery	Lowe	er	Uppe	er	Qual		•
3,4-Dinitrotoluene	74.5	50		150)			
							-	

J The analyte was positively identified, but the quantitation was below the RL

Not detected at or above the method detection limit

____ Instrument: HPLC4 Sample Number: L0502503-05 Prep Method: 3535 Prep Date: 03/02/2005 08:00 Client ID: 29WL39-MH08-02 Analytical Method: 8330 Matrix: Water Analyst: ECL Cal Date: 03/02/2005 16:53 Workgroup Number: WG184109 Run Date: 03/02/2005 23:05 Dilution:1

Collect Date: 23-FEB-05 File ID: 4L007777.F Units:ug/L Sample Tag: 01

Analyte	CAS. Numb	er	Result	Qual	RL	MDL
1,3,5-Trinitrobenzene	99-35-4			U	1.03	0.258
1,3-Dinitrobenzene	99-65-0			U	1.03	0.258
2,4,6-Trinitrotoluene	118-96-7	7	6.36		1.03	0.258
2,4-Dinitrotoluene	121-14-2	2		Ū	1.03	0.258
2,6-Dinitrotoluene	606-20-2	2		U	1.03	0.258
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.29		1.03	0.258
2-Nitrotoluene	88-72-2			U	1.03	0.258
3-Nitrotoluene	99-08-1			U	1.03	0.258
4-Nitrotoluene	99-99-0			U	1.03	0.258
4-Amino-2,6-dinitrotoluene	19406-51-	-0	1.70		1.03	0.258
HMX	2691-41-	0		U	1.03	0.258
Nitrobenzene	98-95-3			υ	1.03	0.258
RDX	121-82-4	l		U	1.03	0.258
Tetryl	479-45-8	3		υ	1.03	0.258
Surrogate	% Recovery	Lower	Upp	er	Qual	
3,4-Dinitrotoluene	61.7	50	15	0		

U Not detected at or above the method detection limit

οf 9

Report Number: L0502503

Report Date : March 14, 2005

00091528

Sample Number: L0502503-06 Prep Method: 3535 Instrument: HPLC4

Client ID: 29WL40-MH09-02 Analytical Method: 8330 Prep Date: 03/02/2005 08:00
Matrix: Water Analyst: ECL Cal Date: 03/02/2005 16:53
Workgroup Number: WG184109 Dilution: 1 Run Date: 03/02/2005 23:43

Collect Date: 23-FEB-05 Units: ug/L File ID: 4L007778.F Sample Tag: 01

Analyte	CAS. Numb	er	Resul	t Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	1		υ		1.06	0.266
1,3-Dinitrobenzene	99-65-0)		υ		1.06	0.266
2,4,6-Trinitrotoluene	118-96-	7	20.4	I		1.06	0.266
2,4-Dinitrotoluene	121-14-	2	1.13			1.06	0.266
2,6-Dinitrotoluene	606-20-	2	1.27			1.06	0.266
2-Amino-4,6-dinitrotoluene	35572-78	-2	1.68			1.06	0.266
2-Nitrotoluene	88-72-2	2		Ū		1.06	0.266
3-Nitrotoluene	99-08-1			υ		1.06	0.266
4-Nitrotoluene	99-99-0)		Ū		1.06	0.266
4-Amino-2,6-dinitrotoluene	19406-51	-0	2.42			1.06	0.266
HMX	2691-41-	0		Ū		1.06	0.266
Nitrobenzene	98-95-3	3		υ		1.06	0.266
RDX	121-82-	4		υ		1.06	0.266
Tetryl	479-45-	8		Ū		1.06	0.266
Surrogate	% Recovery	Lowe	er	Upper	Qual		•
3,4-Dinitrotoluene	67.4	50		150			

I Semiquantitative result (out of instrument calibration range)

Sample Number: L0502503-06 Prep Method: 3535 _ Instrument: HPLC4 Client ID: 29WL40-MH09-02 Analytical Method:8330 Prep Date: 03/02/2005 08:00 Analyst:**ECL** Cal Date: 03/02/2005 16:53 Matrix: Water Workgroup Number: WG184109 Dilution: 5 Run Date: 03/03/2005 20:23 Collect Date: 23-FEB-05 Units:ug/L File ID: 4L007789.F Sample Tag: DL01

Analyte	CAS. Numbe	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4			U		5.32	1.33
1,3-Dinitrobenzene	99-65-0			U		5.32	1.33
2,4,6-Trinitrotoluene	118-96-7	,	20.0		į	5.32	1.33
2,4-Dinitrotoluene	121-14-2	2		U		5.32	1.33
2,6-Dinitrotoluene	606-20-2	2		U	į	5.32	1.33
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.63	J		5.32	1.33
2-Nitrotoluene	88-72-2			U	į	5.32	1.33
3-Nitrotoluene	99-08-1			U		5.32	1.33
4-Nitrotoluene	99-99-0			U	į	5.32	1.33
4-Amino-2,6-dinitrotoluene	19406-51-	0	2.35	J		5.32	1.33
HMX	2691-41-	0		U	į	5.32	1.33
Nitrobenzene	98-95-3			U		5.32	1.33
RDX	121-82-4	<u> </u>		U	į	5.32	1.33
Tetryl	479-45-8	3		υ		5.32	1.33
Surrogate	% Recovery	Lower	Upp	er	Qual		•
3,4-Dinitrotoluene	56.1	50	15	0			

J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

U Not detected at or above the method detection limit

Report Number: L0502503

Report Date : March 14, 2005

00091529

Sample Number: L0502503-07 Prep Method: 3535 Instrument: HPLC4

 Client ID: 29WL40-MH09-52
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

 Matrix: Water
 Analyst: ECL
 Cal Date: 03/02/2005 16:53

 Workgroup Number: WG184109
 Dilution: 1
 Run Date: 03/03/2005 00:20

Collect Date: 23-FEB-05 Units: ug/L File ID: 4L007779.F Sample Tag: 01

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4			υ	1	.03	0.258
1,3-Dinitrobenzene	99-65-0			U	1	03	0.258
2,4,6-Trinitrotoluene	118-96-7	7	24.8	I	1	.03	0.258
2,4-Dinitrotoluene	121-14-2	2	1.09		1	03	0.258
2,6-Dinitrotoluene	606-20-2	2	1.24		1	.03	0.258
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.63		1	03	0.258
2-Nitrotoluene	88-72-2			U	1	.03	0.258
3-Nitrotoluene	99-08-1			U	1	03	0.258
4-Nitrotoluene	99-99-0			U	1	.03	0.258
4-Amino-2,6-dinitrotoluene	19406-51-	-0	2.36		1	.03	0.258
HMX	2691-41-	0		U	1	.03	0.258
Nitrobenzene	98-95-3			U	1	03	0.258
RDX	121-82-4	1		U	1	.03	0.258
Tetryl	479-45-8	3		υ	1	.03	0.258
Surrogate	% Recovery	Lower	Upı	er	Qual		•
3,4-Dinitrotoluene	74.8	50	15	50			

I Semiquantitative result (out of instrument calibration range)

Sample Number: L0502503-07 Prep Method: 3535 _ Instrument: HPLC4 Client ID: 29WL40-MH09-52 Analytical Method:8330 Prep Date: 03/02/2005 08:00 Analyst:**ECL** Cal Date: 03/02/2005 16:53 Matrix: Water Workgroup Number: WG184109 Dilution: 5 Run Date: 03/03/2005 21:00 Collect Date: 23-FEB-05 Units:ug/L File ID: 4L007790.F Sample Tag: DL01

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	:		U		5.15	1.29
1,3-Dinitrobenzene	99-65-0	1		U		5.15	1.29
2,4,6-Trinitrotoluene	118-96-	7	24.0			5.15	1.29
2,4-Dinitrotoluene	121-14-	2		U		5.15	1.29
2,6-Dinitrotoluene	606-20-2	2		U		5.15	1.29
2-Amino-4,6-dinitrotoluene	35572-78	-2	1.61	J		5.15	1.29
2-Nitrotoluene	88-72-2			U		5.15	1.29
3-Nitrotoluene	99-08-1			U		5.15	1.29
4-Nitrotoluene	99-99-0	1		U		5.15	1.29
4-Amino-2,6-dinitrotoluene	19406-51	-0	2.41	J		5.15	1.29
нмх	2691-41-	0		U		5.15	1.29
Nitrobenzene	98-95-3			U		5.15	1.29
RDX	121-82-	4		U		5.15	1.29
Tetryl	479-45-8	8		U		5.15	1.29
Surrogate	% Recovery	Lowe	r t	Jpper	Qual		•
3,4-Dinitrotoluene	68.3	50		150			

J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

U Not detected at or above the method detection limit

Report Number: L0502503

Report Date : March 14, 2005

00091530

Sample Number: L0502503-08 Prep Method: 3535 Instrument: HPLC4

 Client ID: 29WL41-MH10-02
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

 Matrix: Water
 Analyst: ECL
 Cal Date: 03/02/2005 16:53

 Workgroup Number: WG184109
 Dilution: 1
 Run Date: 03/03/2005 00:57

Collect Date: 23-FEB-05 Units: ug/L File ID: 4L007780.F
Sample Tag: 01

Analyte	CAS. Numb	per	Res	ult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	1			U		1.03	0.258
1,3-Dinitrobenzene	99-65-0)			U		1.03	0.258
2,4,6-Trinitrotoluene	118-96-	7	15	.4	I		1.03	0.258
2,4-Dinitrotoluene	121-14-	2	1.0	05			1.03	0.258
2,6-Dinitrotoluene	606-20-	2	1.	35			1.03	0.258
2-Amino-4,6-dinitrotoluene	35572-78	-2	2.	01			1.03	0.258
2-Nitrotoluene	88-72-2	2			U		1.03	0.258
3-Nitrotoluene	99-08-1	L			U		1.03	0.258
4-Nitrotoluene	99-99-0)			U		1.03	0.258
4-Amino-2,6-dinitrotoluene	19406-51	-0	2.	58			1.03	0.258
нмх	2691-41-	-0			U		1.03	0.258
Nitrobenzene	98-95-3	3			υ		1.03	0.258
RDX	121-82-	4			U		1.03	0.258
Tetryl	479-45-	8			U		1.03	0.258
Surrogate	% Recovery	Lowe	r	Upper		Qual		•
3,4-Dinitrotoluene	87.7	50		150				

I Semiquantitative result (out of instrument calibration range)

Sample Number: L0502503-08 Prep Method: 3535 _ Instrument: HPLC4 Client ID: 29WL41-MH10-02 Analytical Method:8330 Prep Date: 03/02/2005 08:00 Analyst: ECL Cal Date: 03/02/2005 16:53 Matrix: Water Workgroup Number: WG184109 Dilution: 4 Run Date: 03/03/2005 21:38 Collect Date: 23-FEB-05 Units:ug/L File ID:4L007791.F Sample Tag: DL01

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4			υ		4.12	1.03
1,3-Dinitrobenzene	99-65-0			Ū		4.12	1.03
2,4,6-Trinitrotoluene	118-96-7	7	15.0			4.12	1.03
2,4-Dinitrotoluene	121-14-2	2	1.07	J		4.12	1.03
2,6-Dinitrotoluene	606-20-2	2	1.30	J		4.12	1.03
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.98	J		4.12	1.03
2-Nitrotoluene	88-72-2			U		4.12	1.03
3-Nitrotoluene	99-08-1			Ū		4.12	1.03
4-Nitrotoluene	99-99-0			U		4.12	1.03
4-Amino-2,6-dinitrotoluene	19406-51-	-0	2.54	J		4.12	1.03
HMX	2691-41-	0		U		4.12	1.03
Nitrobenzene	98-95-3			U		4.12	1.03
RDX	121-82-4	l		U		4.12	1.03
Tetryl	479-45-8	3		U		4.12	1.03
Surrogate	% Recovery	Lower	· Uj	pper	Qual		•
3,4-Dinitrotoluene	83.7	50		150			

J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

U Not detected at or above the method detection limit

Report Number: L0502503

Report Date : March 14, 2005

00091531

 Sample Number: L0502503-09
 Prep Method: 3535
 Instrument: HPLC4

 Client ID: 29WL42-MH11-02
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

 Matrix: Water
 Analyst: ECL
 Cal Date: 03/02/2005 16:53

 Workgroup Number: WG184109
 Dilution: 1
 Run Date: 03/03/2005 01:34

Collect Date: 23-FEB-05 Units: ug/L File ID: 4L007781.F

Analyte	CAS. Numb	er	Re	esult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4	1			U		1.03	0.258
1,3-Dinitrobenzene	99-65-0)			Ū		1.03	0.258
2,4,6-Trinitrotoluene	118-96-	7	1	.8.5	I		1.03	0.258
2,4-Dinitrotoluene	121-14-	2	0	.922	J		1.03	0.258
2,6-Dinitrotoluene	606-20-	2	1	15			1.03	0.258
2-Amino-4,6-dinitrotoluene	35572-78	-2	1	. 29			1.03	0.258
2-Nitrotoluene	88-72-2	2			U		1.03	0.258
3-Nitrotoluene	99-08-1				Ū		1.03	0.258
4-Nitrotoluene	99-99-0)			Ū		1.03	0.258
4-Amino-2,6-dinitrotoluene	19406-51	-0	1	.96			1.03	0.258
HMX	2691-41-	0			U		1.03	0.258
Nitrobenzene	98-95-3	3			Ū		1.03	0.258
RDX	121-82-	4			U		1.03	0.258
Tetryl	479-45-	8			Ū		1.03	0.258
Surrogate	% Recovery	Lowe	er	Upper	r	Qual		•
3,4-Dinitrotoluene	66.5	50		150				

I Semiquantitative result (out of instrument calibration range)

__Instrument: HPLC4 Sample Number: L0502503-09 Prep Method: 3535 Analytical Method: 8330 Prep Date: 03/02/2005 08:00 Client ID: 29WL42-MH11-02 Matrix:**Water** Analyst:**ECL** Cal Date: 03/02/2005 16:53 Workgroup Number: WG184109 Dilution: 5 Run Date: 03/03/2005 22:15 Collect Date: 23-FEB-05 File ID: 4L007792.F Units:ug/L Sample Tag:DL01

Analyte	CAS. Numb	er	Result	Qual	.	RL	MDL
1,3,5-Trinitrobenzene	99-35-4			U		5.15	1.29
1,3-Dinitrobenzene	99-65-0			U		5.15	1.29
2,4,6-Trinitrotoluene	118-96-7	7	18.0			5.15	1.29
2,4-Dinitrotoluene	121-14-2	2		U		5.15	1.29
2,6-Dinitrotoluene	606-20-2	2		U		5.15	1.29
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.32	J		5.15	1.29
2-Nitrotoluene	88-72-2			U		5.15	1.29
3-Nitrotoluene	99-08-1			U		5.15	1.29
4-Nitrotoluene	99-99-0			U		5.15	1.29
4-Amino-2,6-dinitrotoluene	19406-51-	-0	1.92	J		5.15	1.29
HMX	2691-41-	0		U		5.15	1.29
Nitrobenzene	98-95-3			U		5.15	1.29
RDX	121-82-4	4		U		5.15	1.29
Tetryl	479-45-8	В		U		5.15	1.29
Surrogate	% Recovery	Lower	Tp)	per	Qual		•
3,4-Dinitrotoluene	66.5	50	1.	50			

J The analyte was positively identified, but the quantitation was below the RL

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J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

U Not detected at or above the method detection limit

Report Number: L0502503

Report Date : March 14, 2005

00091532

 Sample Number: L0502503-10
 Prep Method: 3535
 Instrument: HPLC4

 Client ID: 29WL43-MH12-02
 Analytical Method: 8330
 Prep Date: 03/02/2005 08:00

Matrix: Water Analyst: ECL Cal Date: 03/02/2005 08:00

Workgroup Number: WG184109 Dilution: 1 Run Date: 03/03/2005 02:12

Collect Date: 23-FEB-05 Units: ug/L File ID: 4L007782.F
Sample Tag: 01

Analyte	CAS. Numb	per	Re	sult	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4				U		1.10	0.275
1,3-Dinitrobenzene	99-65-0)			U		1.10	0.275
2,4,6-Trinitrotoluene	118-96-	7	2	5.5	I		1.10	0.275
2,4-Dinitrotoluene	121-14-	2	0	.934	J		1.10	0.275
2,6-Dinitrotoluene	606-20-	2	1	.31			1.10	0.275
2-Amino-4,6-dinitrotoluene	35572-78	-2	1	75			1.10	0.275
2-Nitrotoluene	88-72-2	2			U		1.10	0.275
3-Nitrotoluene	99-08-1	-			U		1.10	0.275
4-Nitrotoluene	99-99-0)			U		1.10	0.275
4-Amino-2,6-dinitrotoluene	19406-51	-0	2	.67			1.10	0.275
нмх	2691-41-	-0			U		1.10	0.275
Nitrobenzene	98-95-3	3			U		1.10	0.275
RDX	121-82-	4			U		1.10	0.275
Tetryl	479-45-	8			U		1.10	0.275
Surrogate	% Recovery	Lowe	er	Uppe	r	Qual		•
3,4-Dinitrotoluene	68.4	50		150)			

I Semiquantitative result (out of instrument calibration range)

__ Instrument: HPLC4 Sample Number: L0502503-10 Prep Method: 3535 Analytical Method: 8330 Prep Date: 03/02/2005 08:00 Client ID: 29WL43-MH12-02 Matrix:**Water** Analyst:**ECL** Cal Date: 03/02/2005 16:53 Workgroup Number: WG184109 Dilution: 5 Run Date: 03/03/2005 22:52 File ID: 4L007793.F Collect Date: 23-FEB-05 Units:ug/L Sample Tag:DL01

Analyte	CAS. Numb	er	Result	Qual		RL	MDL
1,3,5-Trinitrobenzene	99-35-4			U		5.49	1.37
1,3-Dinitrobenzene	99-65-0			Ū		5.49	1.37
2,4,6-Trinitrotoluene	118-96-7	7	25.0			5.49	1.37
2,4-Dinitrotoluene	121-14-2	2		U		5.49	1.37
2,6-Dinitrotoluene	606-20-2	2		U		5.49	1.37
2-Amino-4,6-dinitrotoluene	35572-78-	-2	1.69	J		5.49	1.37
2-Nitrotoluene	88-72-2			U		5.49	1.37
3-Nitrotoluene	99-08-1			Ū		5.49	1.37
4-Nitrotoluene	99-99-0			U		5.49	1.37
4-Amino-2,6-dinitrotoluene	19406-51-	-0	2.56	J		5.49	1.37
нмх	2691-41-	0		U		5.49	1.37
Nitrobenzene	98-95-3			U		5.49	1.37
RDX	121-82-4	4		U		5.49	1.37
Tetryl	479-45-8	3		Ū		5.49	1.37
Surrogate	% Recovery	Lower	Upp	er	Qual		•
3,4-Dinitrotoluene	60.7	50	15	0			

J The analyte was positively identified, but the quantitation was below the RL

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J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above the method detection limit

U Not detected at or above the method detection limit

WORKGROUP SUMMARY BY METHOD

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WORKGROUP SUMMARY BY METHOD

00091534

Analysis:Explosives

Extraction Method: 3535
Workgroup: WG184026

Lab ID	Client ID	Tclp Date	Prep Date	Analysis Date	Tag	Inst Id	Analyst
L0502503-01	29WL34-MH03-02		03/02/05 08:00			SPE	CSH
L0502503-02	29WL36-MH05-02		03/02/05 08:00			SPE	CSH
L0502503-03	29WL37-MH06-02		03/02/05 08:00			SPE	CSH
L0502503-04	29WL38-MH07-02		03/02/05 08:00			SPE	CSH
L0502503-05	29WL39-MH08-02		03/02/05 08:00			SPE	CSH
L0502503-06	29WL40-MH09-02		03/02/05 08:00			SPE	CSH
L0502503-07	29WL40-MH09-52		03/02/05 08:00			SPE	CSH
L0502503-08	29WL41-MH10-02		03/02/05 08:00			SPE	CSH
L0502503-09	29WL42-MH11-02		03/02/05 08:00			SPE	CSH
L0502503-10	29WL43-MH12-02		03/02/05 08:00			SPE	CSH

Analysis:Explosives

Analytical Method:8330
Workgroup:WG184109

Lab ID	Client ID	Tclp Date	Prep Date	Analysis Date	Tag	Inst Id	Analyst
L0502503-01	29WL34-MH03-02		03/02/05 08:00	03/02/05 19:59	01	HPLC4	ECL
L0502503-01	29WL34-MH03-02		03/02/05 08:00	03/03/05 18:31	DL01	HPLC4	ECL
L0502503-02	29WL36-MH05-02		03/02/05 08:00	03/02/05 20:36	01	HPLC4	ECL
L0502503-02	29WL36-MH05-02		03/02/05 08:00	03/03/05 19:09	DL01	HPLC4	ECL
L0502503-03	29WL37-MH06-02		03/02/05 08:00	03/02/05 21:14	01	HPLC4	ECL
L0502503-03	29WL37-MH06-02		03/02/05 08:00	03/03/05 19:46	DL01	HPLC4	ECL
L0502503-04	29WL38-MH07-02		03/02/05 08:00	03/02/05 22:28	01	HPLC4	ECL
L0502503-05	29WL39-MH08-02		03/02/05 08:00	03/02/05 23:05	01	HPLC4	ECL
L0502503-06	29WL40-MH09-02		03/02/05 08:00	03/02/05 23:43	01	HPLC4	ECL
L0502503-06	29WL40-MH09-02		03/02/05 08:00	03/03/05 20:23	DL01	HPLC4	ECL
L0502503-07	29WL40-MH09-52		03/02/05 08:00	03/03/05 00:20	01	HPLC4	ECL
L0502503-07	29WL40-MH09-52		03/02/05 08:00	03/03/05 21:00	DL01	HPLC4	ECL
L0502503-08	29WL41-MH10-02		03/02/05 08:00	03/03/05 00:57	01	HPLC4	ECL
L0502503-08	29WL41-MH10-02		03/02/05 08:00	03/03/05 21:38	DL01	HPLC4	ECL
L0502503-09	29WL42-MH11-02		03/02/05 08:00	03/03/05 01:34	01	HPLC4	ECL
L0502503-09	29WL42-MH11-02		03/02/05 08:00	03/03/05 22:15	DL01	HPLC4	ECL
L0502503-10	29WL43-MH12-02		03/02/05 08:00	03/03/05 02:12	01	HPLC4	ECL
L0502503-10	29WL43-MH12-02		03/02/05 08:00	03/03/05 22:52	DL01	HPLC4	ECL

AJF - AMANDA J. FICKIESEN	ALB - ANNIE L. BOCK	ALT - ANN L. THAYER
BRG - BRENDA R. GREGORY	CAF - CHERYL A. FLOWERS	CAK - CHERYL A. KOELSCH
CEB - CHAD E. BARNES	CLC - CHRYS L. CRAWFORD	CLK - CARL L. KING
CLS - CARA L. STRICKLER	CLW - CHARISSA L. WINTERS	CM - CHARLIE MARTIN
CMS - CRYSTAL M. STEPHENS	CPD - CHAD P. DAVIS	CRC - CARLA R. COCHRAN
CSH - CHRIS S. HILL	DAS - DALLAS A. SULLIVAN	DD - DIANE M. DENNIS
DDE - DEBRA D. ELLIOTT	DEL - DON E. LIGHTFRITZ	DEV - DAVID E. VANDENBERG
DGB - DOUGLAS G. BUTCHER	DIH - DEANNA I. HESSON	DLB - DAVID L. BUMGARNER
DLP - DOROTHY L. PAYNE	DLR - DIANNA L. RAUCH	DP - DEANNA L. PIERSON
DR - DEANNA ROBERTS	DRB - DOUG R. BARNETT	DSM - DAVID S. MOSSOR
DST - DENNIS S. TEPE	ECL - ERIC C. LAWSON	EED - EMILY E. DECKER
HAV - HEMA VILASAGAR	JAL - JOHN A. LENT	JJG - JOHN J. GREUEY
JKT - JANE K. THOMPSON	JLS - JANICE L. SCHIMMEL	JWR - JOHN W. RICHARDS
JWS - JACK W. SHEAVES	JYH - JI Y. HU	KEB - KATHRYN E. BARNES
KHR - KIM H. RHODES	KRA - KATHY R. ALBERTSON	LKN - LINDA K. NEDEFF
LSA - LUCINDA S. ARNOLD	LSB - LESLIE S. BUCINA	MAH - MICALYN A. HARRIS
MDA - MICHAEL D. ALBERTSON	MDC - MICHAEL D. COCHRAN	MES - MARY E. SCHILLING
MKZ - MARILYN K. ZUMBRO	MLR - MARY L. ROCHOTTE	MLS - MICHAEL L. SCHIMMEL
MMB - MAREN M. BEERY	MSW - MATT S. WILSON	NJB - NATALIE J. BOOTH
OGT - OKEY G. TUCKER	PAS - PATRICK A. STREET	RB - ROBERT BUCHANAN
RDC - REBECCA D. CUTLIP	REK - ROBERT E. KYER	RWC - RODNEY W. CAMPBELL
SCM - SUSAN C. MOELLENDICK	SK - SANDRA KEENER	SLM - STEPHANIE L. MOSSBURG
SLP - SHERI L. PFALZGRAF	SMH - SHAUNA M. HYDE	TD - TIMOTHY DYSERT
TMM - TAMMY M. MORRIS	VC - VICKI COLLIER	VKL - VICKY K. LAUER

KEMRON Environmental Services, Inc. List of Valid Qualifiers March 14, 2005

These are KEMRON's standard report qualifiers:

В	Present in the method blank	NS	Not spiked
C	Confirmed by GC/MS	P	Concentration >40% difference between
CG	Confluent growth		the two GC columns
D	The analyte was quantified as a secondary	QNS	Quantity not sufficient to perform analysis
	dilution factor	RA	Reanalysis confirms reported results
DL	Surrogate or spike was diluted out	RE	Reanalysis confirms sample matrix
			interference
E	Estimated concentration due to sample	S	Analyzed by method of standard addition
	matrix interference	SMI	Sample matrix interference on surrogate
FL	Free liquid	SP	Reported results are for spike compounds
I	Semi-quantitative result, out of instrument		only
	calibration range	TNTC	Too numerous to count
J	Present below normal reporting limit	U	Analyzed for but not detected
L	Sample reporting limits elevated due to	W	Post-digestion spike for furnace AA out
	matrix interference		out of control limits
N	Tentatively Identified Compound (TIC)	X	Exceeds regulatory limit
NA	Not applicable	Z	Can not be resolved from isomer.***
ND	Not detected at or above the reporting limit (RL)	+	Correlation coefficient for the MSA is less
NF	Not found		than 0.995
NFL	No free liquid	<	Less than
NI	Non-ignitable	>	Greater than
	-	*	Surrogate or spike compound out of range

***Special Notes for Organic Analytes

- 1. Acrolein and acrylonitrile by method 624 are semi-quantitative screens only.
- 2. 1,2-Diphenylhydrazine is unstable and is reported as azobenzene.
- 3. N-nitrosodiphenylamine cannot be separated from diphenylamine.
- 4. 3-Methyphenol and 4-Methylphenol are unresolvable compounds.
- 5. m-Xylene and p-Xylene are unresolvable compounds.
- The reporting limits for Appendix II/IX compounds by method 8270 are based on EPA estimated PQLs
 referenced in 40 CFR Part 264, Appendix IX. They are not always achievable for every compound and are
 matrix dependent.

AFCEE Qualifiers

These are KEMRON's AFCEE Report Qualifiers

- **J** The analyte was positively identified, the quantitiation is an estimation.
- U The analyte was analyzed for, but not detected. The associated numerical value is at or below the MDL
- F The anlyte was positively identified by the associated numerical value is below the RL
- **R** The data is unusable due to deficiencies in the ability to analyze the sample and meet QC criteria
- **B** The analyte was found in an associated blank, as well as in the sample
- M The matrix effect was present
- S To be applied to all field screening data
- T Tentatively identified compound (using GC/MS)

Organic Instrument Data

Run Date: 3-2-05				Login no.	Due Date	Priority
Analyst: ECL / RPC Instrument: HPLC 4				02-503	3/4	PΙ
1101 C 4						
						HARLU
Method: 8330						
	1	Analyst	Peer			
System Performance Check:	Endrin/DDT Breakdown	7				
Initial Calibration:	ICAL summary		V			
	Linear or quadriatic regression	V	V		· ·	
	Alt Source Check	V	V			
Continuing Calibration:	Continuing Calibration		U			
	Ending standards		1			
	Client Specific Requirements					
	Special Standards			Comments	:	
Blanks:	Quant Report/Chromatogram		V			
	Surrogates	V.	V	All sample	y except.	
LCS/LCS DUP:	Quant Report/Chromatogram	V	V			
	Surrogates	V.	1	in ee d	dilutions	
	Spike Compounds	√	1			
	MS/MSD					
Samples:	Quant Reports/Chromatograms		1			
	Mass spectra					
	Surrogates					
	Dilution runs					
	Confirmations	V ,	/			
	Correct Factors	V ,	U			
	Manual integrations		V			
Data Package:	Run logs		0			
	Bench sheets	V.	V			
	Upload results	V/				
	QC forms	$\sqrt{}$	V			
	Seedpak workgroups	✓	1			
Client Data	Data scanned					
	Integrations digitally signed	V				
	Level 2 pdf files					
	Level 3/Level x					
	Level 4 copies					
	Case narratives					
		Supervisor				
Integrations digitally cosigned		V				
Corrective Action						
Results Reporting/Data Qualifier	rs	\ \\				
Client Data/digital signatures						
Check for Completeness		V	1			
Check for compliance with meth	od and project requirements	U	1			
Check the reasonableness of re-	sults	U	1			
	٧	= Checked & OK				
	, NA	= Not Applicable	!			
	c - 1 1					
Primary Reviewer:	CC 3/4/05					
Secondary Reviewer:	ECZ 3/4/05 mliz/4/5					

Semi-Volatile HPLC Checklist

00091539

				Login no.	Due Date	Priority
Run Date: 03-MAR-2005				02-503	04-Mar-05	P1
Analyst: ECL/ RDC	·			_		
Instrument: HPLC4						
Method: 8330						
		Analyst	Peer			
Initial Calibration:	ICAL summary					
Continuing Calibration:		√				
		1				
		1				
		· · · · · · · · · · · · · · · · · · ·		Comments:		
Blanke:		†				
Diame.		†	+			
I CS/I CS DI IB:			-1		<u></u>	
LCG/LCG BOP.		 				
		-	-			
			+-			
Samulas		-1				
Samples:						
·						
		1 V	+			
		<u> </u>	+			
		1				
						
Data Package:			1 , 11			
			 			
		٧	السنيا			
Client Data						
	Level 3/Level x					
·						
	Integrations digitally signed	√				
Analyst:ECL/_RDC						
Corrective Action:		-				
Results Reporting/Data Qualifiers:	·	V				
Client Data/digital signatures						
Check for Completeness:		1				
		/				
Check the reasonableness of resul	ts:]			
	√ = C	hecked & OK	-			
		••		•		
Primary Reviewer:	RDC 3/7/05			· · · · · · · · · · · · · · · · · · ·		
•	. ///	-		•		
Secondary Reviewer:	nde 3/ des					
•	V	-				

1.0 Calculating the Calibration Factor (RF) from the initial calibration (ICAL) data:

$$CF = \frac{C_s}{A_s}$$

where: Example: $A_s = \text{Area of the compound being measured in the standard} \qquad 10000$ $C_s = \text{Concentration of the compound being measured } (nug/mL) \qquad 100$ CF = 0.01

$\textbf{2.0 Calculating the concentration } \textbf{(C) of a compuond in water using data from prep \ log \ and \ quantitation \ report:*$

$$C = \frac{(A_x)(CF)(V_f)(D)}{V_i}$$

3.0 Calculating the concentration (C) of a compound in soil using data from prep log and quantitation report:*

$$C = \frac{(A_x)(CF)(V_f)(D)}{W_i}$$

where: Example: $A_x = \text{Area of the compound being measured} \qquad 10000$ $V_f = \text{Final volume of sample extract (mL) (prep log)} \qquad 1$ $D = \text{Dilution factor for sample as a multiplier (10X = 10)} \qquad 1$ $CF = \text{Calibration factor from ICAL calculated above} \qquad 0.01$ $W_i = \text{Initial weight of sample (g) (prep log)} \qquad 30$ $\text{C } (\mu g/kg) = 3.333333$

^{*} Concentrations appearing on instrument quantitation reports are on-column results and do not take into account initial volume, final volume and dilution factor.



 $^{23}_{3}$

Document Control No.: EE0005 rage: 28 of 50

Sample Extraction Log Sheet – Method 8330 / Explosives

Analyst: CSH Date: 3-2-5 (20800 SOP#: EXTINTOL PEV. 6 Witness: Spike Analyst: CSH Sample Matrix: Lot#: A42820 Ext Solvent: CH2N Ext Solvent: MEOH Lot#: A38E20 Lot#: 760098 Ext Disk: 50B-F15 Lot#: A29807 Other:

Extract Relinquished By: Extract Received By: Date Extract Received:

Matrix Spike # / Conc: <u>F550050-34</u> 01.0 pp. Surrogate Spike # / Conc: <u>F550050-27</u> 01.0 pp.

Extraction Work Group: _W6184026

Analytical Work Group:

Sonic Bath On – Date: Time (1) Bath Time (2) Pemp (2) Ctrol Bath Sonic Bath Off – Date: Time (3) Temp (3) Ctrl Bath

	Project ID	Sample ID	Sample Wt (g) / Vol (mL)	Surrogate Amount (uL)	Matrix Spike Amount (uL)	Extract F. Volume (mL)	Comments
1		BY	1000mL	1000		10 mL	WG 184026-01
2		(05		i	1000		-02
3		ics oup	4		<u></u> 上		03
4		02-503-01	950 mL		-		
5		-02	960mL				
6		703	1				
7		-04	<u> </u>				
8		-05	970 mC				
9		_0b	940 ML				
10		40-	970 mL				
11		-03					
12		-09	<u> </u>				
13		~10	910mL				
14							
15 16							
17							
18					y 3-2-5		
19				C	# 3-2		
20			ę.				
21							
22							
23							
24							

All soil samples are air dried to a constant weight prior to extraction All extracts are filtered through a 0.45 um teflon ACRODISC prior to analysis Reviewed by:

Sel	Run	Location	Method	Datafile	SeqTable	Calib:RF:RT	Sample Name	
								00091542
No	1	Vial 1	8330	4L007761	01:01		BLANK SOLVEN	1T
No	2	Vial 2	8330	4L007762	02:01	V	WG184085-01	STD6 - SOU73-18
No	3	Vial 3	8330	4L007763	03:01	I	WG184085-02	STD5
No	4	Vial 4	8330	4L007764	04:01		WG184085-03	STD4
No	5	Vial 5	8330	4L007765	05:01		WG184085-04	STD3
No	6	Vial 6	8330	4L007766	06:01		WG184085-05	STD2
No	7	Vial 7	8330	4L007767	07:01	7	WG184085-06	
No	8	Vial 8	8330	4L007768	08:01	Y	WG184085-07	ALT - 50573-13
No	9	Vial 9	8330	4L007769	09:01		WG184026-01	BLK
No	10	Vial 10	8330	4L007770	10:01		WG184026-02	
No	11	Vial 11	8330	4L007771	11:01		WG184026-03	
No	12	Vial 12	8330	4L007772	12:01		L0502503-01	833W-RR5X-X
No	13	Vial 13	8330	4L007773	13:01		L0502503-02	833W-RR10X-X
No	14	Vial 14	8330	4L007774	14:01	3	L0502503-03	833W-RRIVOX-X
No	15	Vial 5	8330	4L007775	15:01	V		CCV - 505 73-18
No	16	Vial 15	8330	4L007776	16:01	Ì	L0502503-04	
No	17	Vial 16	8330	4L007777	17:01)	L0502503-05	
No	18	Vial 17	8330	4L007778	18:01	j	L0502503-06	
No	19	Vial 18	8330	4L007779	19:01		L0502503-07	
No	20	Vial 19	8330	4L007780	20:01	I	L0502503-08	833W - RR 4X
No	21	Vial 20	8330	4L007781	21:01		L0502503-09	
No	22	Vial 21	8330	4L007782	22:01	Į.	L0502503-10	
No	23	Vial 5	8330	4L007783	23:01	J.	WG184085-09	CCV - Ses 73-18

ECZ 3/4/05
RDC 3/4/05

00091543

KEMRON ENVIRONMENTAL SERVICES Semivolatile Laboratory HPLC Routine Maintenance/Runlog

Analysis Date: 3-2-05 Analyst: Roc EcL Instrument ID: HPLC'4 Column ID: Ultra Carb 5-005 Data subdirectory: 030205	Routine maintenance (marufacturer recommendation in parenthesis) Check eluent volume Check eluent waste container System pressure 280 km
Method/SOP:8310 Rev.5 8330 Rev. 5 830-MBA Rev. 0	
8315a formaldehyde Rev. 0 Comments	
X - Surrogate failed low due t	-o SMI
	Reviewed by: 70(3/4/05

Sel	Run	Location	Method	Datafile S	eqTable Calib:RF:RT	Sample Name00091544
No	1	Vial 1	8330	4L007784	01:01	BLANK SOLVENT
No	2	Vial 2	8330	4L007785	01:01 02:01 Sos 73-18	WG184223-01 CCV
No	3	Vial 3	8330	4L007786	03:01	L0502503-01 5X
No	4	Vial 4	8330	4L007787	04:01	L0502503-02 10X
No	5	Vial 5	8330	4L007788	05:01	L0502503-03 100X
No	6	Vial 6	8330	4L007789	06:01/	L0502503-06 5X
No	7	Vial 7	8330	4L007790	07:01/	L0502503-07 5X
No	8	Vial 8	8330	4L007791	08:01/	L0502503-08 4X
No	9	Vial 9	8330	4L007792	09:01	L0502503-09 5X
No	10	Vial 10	8330	4L007793	10:01	L0502503-10 5X
No	11	Vial 2	8330	4L007794	11:01 V SDS 73-18	WG184223-02 CCV

Rf C 3/7/05 rde 3/1/05

00091545

KEMRON ENVIRONMENTAL SERVICES Semivolatile Laboratory HPLC Routine Maintenance/Runlog

Analysis Date: 3/03/05 Analyst: £CL RDC Instrument ID: HPLCY Column ID: Ultracarb 5 005	Routine maintenance (manufacturer recommendation in parenthesis) Check eluent volume Check eluent waste container
Data subdirectory: 0 30 30 5	System pressure 390 bar
Method/SOP:8310 Rev.58330 Rev. 5830-MBA Rev. 08315a formaldehyde Rev. 0 Comments	
L0502503-01 SUN. Recove SMI due to 2,4,6.	ry 2 Adv. /imit -
L0502503-02,03 - Sum. De	
	Paviowed by: 42/2/2

KEMRON Environmental Services HOLDING TIMES EQUIVALENT TO AFCEE FORM 9

00091546

AAB#: WG184109

Analytical Method: 8330

Login Number: L0502503

	Date	Date	Date	Max Hold	Time Held	Date	Max Hold	Time Held	
Client ID	Collected	Received	Extracted	Time Ext.	Ext.	Analyzed	Time Anal	Anal.	Q
29WL34-MH03-02	02/24/05	02/25/05	03/02/05	7	5.75	03/02/05	40	0.500	
29WL34-MH03-02	02/24/05	02/25/05	03/02/05	7	5.75	03/03/05	40	1.44	
29WL36-MH05-02	02/24/05	02/25/05	03/02/05	7	5.74	03/02/05	40	0.526	
29WL36-MH05-02	02/24/05	02/25/05	03/02/05	7	5.74	03/03/05	40	1.46	
29WL37-MH06-02	02/24/05	02/25/05	03/02/05	7	5.73	03/02/05	40	0.552	
29WL37-MH06-02	02/24/05	02/25/05	03/02/05	7	5.73	03/03/05	40	1.49	
29WL38-MH07-02	02/23/05	02/25/05	03/02/05	7	6.66	03/02/05	40	0.603	
29WL39-MH08-02	02/23/05	02/25/05	03/02/05	7	6.70	03/02/05	40	0.629	
29WL40-MH09-02	02/23/05	02/25/05	03/02/05	7	6.74	03/02/05	40	0.655	
29WL40-MH09-02	02/23/05	02/25/05	03/02/05	7	6.74	03/03/05	40	1.52	
29WL40-MH09-52	02/23/05	02/25/05	03/02/05	7	6.74	03/03/05	40	0.681	
29WL40-MH09-52	02/23/05	02/25/05	03/02/05	7	6.74	03/03/05	40	1.54	
29WL41-MH10-02	02/23/05	02/25/05	03/02/05	7	6.73	03/03/05	40	0.707	
29WL41-MH10-02	02/23/05	02/25/05	03/02/05	7	6.73	03/03/05	40	1.57	
29WL42-MH11-02	02/23/05	02/25/05	03/02/05	7	6.76	03/03/05	40	0.732	
29WL42-MH11-02	02/23/05	02/25/05	03/02/05	7	6.76	03/03/05	40	1.59	
29WL43-MH12-02	02/23/05	02/25/05	03/02/05	7	6.78	03/03/05	40	0.758	
29WL43-MH12-02	02/23/05	02/25/05	03/02/05	7	6.78	03/03/05	40	1.62	

^{*} EXT = SEE PROJECT QAPP REQUIREMENTS

^{*}ANAL = SEE PROJECT QAPP REQUIREMENTS

KEMRON Environmental Services

SURROGATE STANDARDS

00091547

Login Number:L0502503
Instrument Id:HPLC4
Workgroup (AAB#):WG184109

Method:8330	
CAL ID: HPLC4-02-MAR-05	
Matriv•WATED	

Sample Number	Dilution	Tag	1
L0502503-01	1.00	01	<u>42.9</u>
L0502503-01	5.00	DL01	42.7
L0502503-02	1.00	01	ND
L0502503-02	10.0	DL01	DL
L0502503-03	1.00	01	ND
L0502503-03	100	DL01	DL
L0502503-04	1.00	01	74.5
L0502503-05	1.00	01	61.7
L0502503-06	1.00	01	67.4
L0502503-06	5.00	DL01	56.1
L0502503-07	1.00	01	74.8
L0502503-07	5.00	DL01	68.3
L0502503-08	1.00	01	87.7
L0502503-08	4.00	DL01	83.7
L0502503-09	1.00	01	66.5
L0502503-09	5.00	DL01	66.5
L0502503-10	1.00	01	68.4
L0502503-10	5.00	DL01	60.7
WG184026-01	1.00	01	92.4
WG184026-02	1.00	01	101
WG184026-03	1.00	01	94.5

Surrogates

1 - 3,4-Dinitrotoluene

Surrogate Limits

50 - 150

Underline = Result out of surrogate limits

DL = surrogate diluted out
ND = surrogate not detected

KEMRON FORMS - Modified 11/15/2004 Version 1.5 PDF File ID: 200930 Report generated 03/10/2005 16:19

KEMRON Environmental Services METHOD BLANK SUMMARY

00091548

Login Number:L0502503 Work Group:WG184109

Blank File ID:4L007769.F Blank Sample ID:WG184026-01

Date Analyzed:03/02/05 Instrument ID:HPLC4

Time Analyzed:18:08 Method:8330

Analyst:ECL

This Method Blank Applies To The Following Samples:

Client ID	Lab Sample ID	Lab File ID	Time Analyzed	TAG
LCS	WG184026-02	4L007770.F	03/02/05 18:45	01
LCS2	WG184026-03	4L007771.F	03/02/05 19:22	01
29WL34-MH03-02	L0502503-01	4L007772.F	03/02/05 19:59	01
29WL36-MH05-02	L0502503-02	4L007773.F	03/02/05 20:36	01
29WL37-MH06-02	L0502503-03	4L007774.F	03/02/05 21:14	01
29WL38-MH07-02	L0502503-04	4L007776.F	03/02/05 22:28	01
29WL39-MH08-02	L0502503-05	4L007777.F	03/02/05 23:05	01
29WL40-MH09-02	L0502503-06	4L007778.F	03/02/05 23:43	01
29WL40-MH09-52	L0502503-07	4L007779.F	03/03/05 00:20	01
29WL41-MH10-02	L0502503-08	4L007780.F	03/03/05 00:57	01
29WL42-MH11-02	L0502503-09	4L007781.F	03/03/05 01:34	01
29WL43-MH12-02	L0502503-10	4L007782.F	03/03/05 02:12	01
29WL34-MH03-02	L0502503-01	4L007786.F	03/03/05 18:31	DL01
29WL36-MH05-02	L0502503-02	4L007787.F	03/03/05 19:09	DL01
29WL37-MH06-02	L0502503-03	4L007788.F	03/03/05 19:46	DL01
29WL40-MH09-02	L0502503-06	4L007789.F	03/03/05 20:23	DL01
29WL40-MH09-52	L0502503-07	4L007790.F	03/03/05 21:00	DL01
29WL41-MH10-02	L0502503-08	4L007791.F	03/03/05 21:38	DL01
29WL42-MH11-02	L0502503-09	4L007792.F	03/03/05 22:15	DL01
29WL43-MH12-02	L0502503-10	4L007793.F	03/03/05 22:52	DL01

KEMRON FORMS - Modified 02/18/2005 Version 1.5 PDF File ID: 200925 Report generated 03/10/2005 16:18

KEMRON Environmental Services

METHOD BLANK REPORT

00091549

Login Number:L0502503	Run Date: 03/02/2005	Sample ID: WG184026-01
Instrument ID: HPLC4	Run Time:18:08	Prep Method: 3535
File ID:4L007769.F	Analyst:ECL	Method: 8330
Workgroup (AAB#):WG184109	Matrix: Water	Units:ug/L
Contract #:DACA56-94-D-0020	Cal ID: HPL	C4 - 02-MAR-05

Analytes	MDL	RDL	Concentration	Dilution	Qualifier
1,3,5-Trinitrobenzene	0.250	1.00	0.250	1	υ
1,3-Dinitrobenzene	0.250	1.00	0.250	1	υ
2,4,6-Trinitrotoluene	0.250	1.00	0.250	1	υ
2,4-Dinitrotoluene	0.250	1.00	0.250	1	υ
2,6-Dinitrotoluene	0.250	1.00	0.250	1	υ
2-Amino-4,6-dinitrotoluene	0.250	1.00	0.250	1	U
2-Nitrotoluene	0.250	1.00	0.250	1	υ
3-Nitrotoluene	0.250	1.00	0.250	1	υ
4-Nitrotoluene	0.250	1.00	0.250	1	υ
4-Amino-2,6-dinitrotoluene	0.250	1.00	0.250	1	U
нмх	0.250	1.00	0.250	1	υ
Nitrobenzene	0.250	1.00	0.250	1	υ
RDX	0.250	1.00	0.250	1	υ
Tetryl	0.250	1.00	0.250	1	υ

Surrogates	% Recovery	Surro	gate I	Limits	Qualifier
3,4-Dinitrotoluene	92.4	50	-	150	PASS

^{*} Analyte detected above RDL

KEMRON FORMS - Modified 11/05/2004 Version 1.5 PDF File ID: 200926 Report generated 03/10/2005 16:19

ND Analyte Not detected at or above reporting limit

KEMRON Environmental Services

LABORATORY CONTROL SAMPLES

Login Number:L0502503 Analyst:ECL Prep Method:3535 00091550
Instrument ID:HPLC4 Matrix:Water Method:8330

Units:ug/L

Sample ID:WG184026-02 LCS File ID:4L007770.F Run Date:03/02/2005 18:45
Sample ID:WG184026-03 LCS2 File ID:4L007771.F Run Date:03/02/2005 19:22

		LCS			LCS2			%Rec	RPD	
Analytes	Known	Found	% REC	Known	Found	% REC	%RPD	Limits	Lmt	Ç
1,3,5-Trinitrobenzene	1.00	0.879	87.9	1.00	0.928	92.8	5.41	58 - 120	40	T
1,3-Dinitrobenzene	1.00	0.996	99.6	1.00	1.02	102	2.26	68 - 135	40	t
2,4,6-Trinitrotoluene	1.00	0.934	93.4	1.00	0.934	93.4	0.0125	27 - 137	40	Ť
2,4-Dinitrotoluene	1.00	0.979	97.9	1.00	1.01	101	3.51	69 - 109	40	Ť
2,6-Dinitrotoluene	1.00	0.994	99.4	1.00	1.00	100	1.05	55 - 121	40	Ť
2-Amino-4,6-dinitrotoluene	1.00	0.934	93.4	1.00	0.911	91.1	2.53	72 - 112	40	T
2-Nitrotoluene	1.00	0.958	95.8	1.00	1.00	100	4.41	67 - 121	40	Ť
3-Nitrotoluene	1.00	0.945	94.5	1.00	0.977	97.7	3.34	66 - 110	40	Ť
4-Nitrotoluene	1.00	0.988	98.8	1.00	1.03	103	4.63	68 - 110	40	Ť
4-Amino-2,6-dinitrotoluene	1.00	1.06	106	1.00	1.02	102	3.31	74 - 116	40	T
нмх	1.00	0.847	84.7	1.00	0.849	84.9	0.203	54 - 99	40	T
Nitrobenzene	1.00	1.08	108	1.00	1.01	101	7.24	70 - 131	40	T
RDX	1.00	0.821	82.1	1.00	0.860	86.0	4.64	60 - 116	40	t
Tetryl	1.00	0.832	83.2	1.00	0.828	82.8	0.477	10 - 147	40	T

	LCS	LCS2			
Surogates	% Recovery % Re		Surrogate Limits	Qualifier	
3,4-Dinitrotoluene	101	94.5	50 - 150	PASS	

^{*} FAILS %REC LIMIT

Workgroup (AAB#):WG184109

KEMRON FORMS - Modified 01/03/2005 Version 1.5 PDF File ID: 200927 Report generated 03/10/2005 16:19

[#] FAILS RPD LIMIT

Calibration Table ______

00091551

ICAL WG184085 8330 HPLC4

3/3/2005 2:15:02 PM Calib. Data Modified :

 External Standard Peak Area Calculate

Based on

Rel. Reference Window: 0.000 % Abs. Reference Window: 0.000 min Rel. Non-ref. Window: 0.000 % Abs. Non-ref. Window: 0.000 % Use Multiplier & Dilution Factor with ISTDs

Uncalibrated Peaks : using compound Nitrobenzene #6
Partial Calibration : Yes, identified peaks are recalibrated
Correct All Ret. Times: Yes, even for non-identified peaks

Linear Ignored Curve Type Origin Weight Equal

Recalibration Settings:

Average all calibrations Floating Average New 75% Average Response : Average Retention Time: Floating Average New 75%

Calibration Report Options :

Printout of recalibrations within a sequence: Calibration Table after Recalibration Normal Report after Recalibration If the sequence is done with bracketing: Results of first cycle (ending previous bracket)

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

RetTime [min] S		vl	Amount [ug/L]	Area	Amt/Area	Ref	Grp	Name
							1	
4.622	1	1	10.00000	1.44657	6.91290			HMX #1
		2	25.00000	3.85678	6.48210			
		3	50.00000	7.55162	6.62109			
		4	100.00000	16.09624	6.21263			
		5	500.00000	83.06084	6.01968			
		6	1000.00000	168.22462	5.94443			
7.156	1	1	10.00000	1.52740	6.54706			RDX #2
		2	25.00000	4.26468	5.86210			
		3	50.00000	9.00214	5.55424			
		4	100.00000	18.89868	5.29137			
		5	500.00000	97.60657	5.12261			
		6	1000.00000	198.12622	5.04729			
9.726	1	1	10.00000	4.22828	2.36503			1,3,5-Trinitrobenzene #3
		2	25.00000	10.70963	2.33435			
		3	50.00000	21.61587	2.31312			
		4	100.00000	44.45069	2.24968			
		5	500.00000	224.03819	2.23176			
		6	1000.00000	450.35959	2.22045			
11.905	1	1	10.00000	6.79459	1.47176			1,3-Dinitrobenzene #4
		2	25.00000	15.32882	1.63091			~
		3	50.00000	30.33624	1.64819			
		4	100.00000	61.96233	1.61388			
		5	500.00000	303.22598	1.64894			
		. 6	1000.00000	610.60284	1.63773			
12.595	1	1	10.00000	4.10279	2.43737			Tetryl #5
		2	25.00000	8.12486	3.07698			
		3	50.00000	16.29603	3.06823			

RetTime [min] S	iq	vl 	Amount [ug/L] 	Area	Amt/Area	_		00091552
'	1	4	100.00000	31.50425	3.17417			
		5	500.00000	160.81532	3.10916			
			1000.00000	322.53574	3.10043			
13.516	1	1	10.00000	4.31157	2.31934		Nitrobe	enzene #6
		2	25.00000	9.97288	2.50680			
		3	50.00000	19.14519	2.61162			
		4	100.00000	39.26730	2.54665			
		5	500.00000	192.74368	2.59412			
		6	1000.00000	385.12140	2.59658			
14.456	1	1	10.00000	2.55430	3.91497		3,4-Din	nitrotoluene #7 *
		2	25.00000	6.41116	3.89945			
		3	50.00000	11.13751	4.48934			
		4 5	100.00000	22.86400	4.37369			
		6	500.00000	115.69042 231.68690	4.32188 4.31617			
15.291	1	1	10.00000	4.17256	2.39661		2 4 6-Т	Trinitrotoluene #8
10.201	_	2	25.00000	11.51173	2.17170		2,4,0 1	
		3	50.00000	20.14398	2.48213			
		4	100.00000	41.79925	2.39239			
		5	500.00000	209.21013	2.38994			
		6	1000.00000	420.06686	2.38057			
15.974	1	1	10.00000	2.30618	4.33618		4-Amino	o-2,6-Dinitrotoluene #9
		2	25.00000	7.22222	3.46154			
		3	50.00000	11.95746	4.18149			
		4	100.00000	25.35186	3.94448			
		5	500.00000	126.42713	3.95485			
		6	1000.00000	253.37405	3.94673			
16.875	1	1	10.00000	3.28896	3.04047		2-Amino	o-4,6-Dinitrotoluene #10
		2	25.00000	9.56106	2.61477			
		3	50.00000	17.44535	2.86609			
		4	100.00000	35.89659	2.78578			
		5 6	500.00000	180.40312 362.57553	2.77157 2.75805			
17.835	1	1	10.00000	2.70280	3.69986		2 6_Dir	nitrotoluene #11
17.033		2	25.00000	7.63130	3.27598		2,00011	ittlocordene #11
		3	50.00000	14.78704	3.38134			
		4	100.00000	28.97582	3.45115			
		5	500.00000	145.51337	3.43611			
		6	1000.00000	293.94946	3.40195			
18.501	1	1	10.00000	4.96485	2.01416		2,4-Dir	nitrotoluene #12
		2	25.00000	12.89109	1.93932			
		3	50.00000	26.29363	1.90160			
		4	100.00000	51.16483	1.95447			
		5	500.00000	256.94580	1.94594			
01 707	-	6	1000.00000	518.46100	1.92879		0	
21.707	1	1	10.00000	1.89515	5.27663		2-Nitro	otoluene #13
		3	25.00000	5.06007	4.94064			
		3 4	50.00000	9.95469 21.44048	5.02276 4.66407			
		5	500.00000	108.98688	4.58771			
		6	1000.00000	221.48364	4.51501			
23.241	1	1	10.00000	1.52266	6.56746		4-Nitro	otoluene #14
20.211	_	2	25.00000	4.00727	6.23865		1 1/1010	
		3	50.00000	7.87646	6.34803			
		4	100.00000	17.27542	5.78857			
		5	500.00000	91.24621	5.47968			
		6	1000.00000	178.99739	5.58667			
25.075	1	1	10.00000	2.84725	3.51216		3-Nitro	otoluene #15
		2	25.00000	5.41142	4.61986			
		3	50.00000	11.93896	4.18797			
		4	100.00000	23.79573	4.20243			
		5	500.00000	124.08713	4.02943			
=======		6 	1000.00000	245.04230	4.08093 			

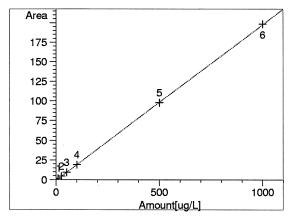
00091553

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***No Entries in table***
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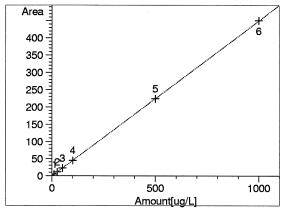
Calibration Curves

_____ Area 7 160 140 -120 100 80 60 40 -20 1000 500 Amount[ug/L]

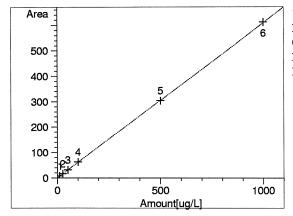
HMX #1 at exp. RT: 4.622 DAD1 B, Sig=254,16 Ref=360,100 Correlation: 0.99998 Residual Std. Dev.: 0.42968 Formula: y = mx + bm: 1.68544e-1 b: -6.26684e-1 x: Amount[ug/L] y: Area



RDX #2 at exp. RT: 7.156 DAD1 B, Sig=254,16 Ref=360,100 Correlation: 0.99998 Residual Std. Dev.: 0.51094 Formula: y = mx + bm: 1.98574e-1 b: -8.61938e-1 x: Amount[ug/L] y: Area



1,3,5-Trinitrobenzene #3 at exp. RT: 9.726 DAD1 B, Sig=254,16 Ref=360,100 Correlation: 1.00000 Residual Std. Dev.: 0.43322 Formula: y = mx + b4.50713e-1 -6.74780e-1 x: Amount[ug/L] y: Area

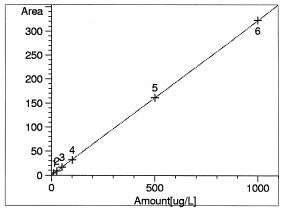


```
1,3-Dinitrobenzene #4 at exp. RT: 11.905 DAD1 B, Sig=254,16 Ref=360,100 Correlation: 0.99999 00091554
```

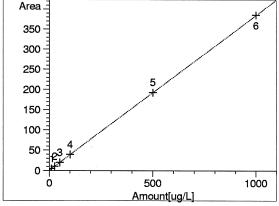
Residual Std. Dev.: 1.09677 Formula: y = mx + b

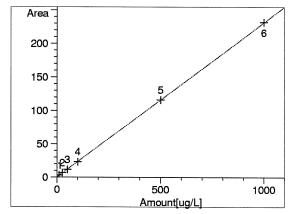
m: 6.09621e-1 b: 1.73360e-1 x: Amount[ug/L]

y: Area



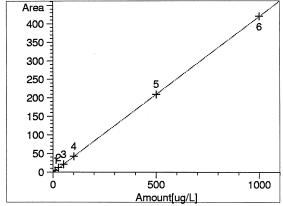
b: 7.54201e-2 x: Amount[ug/L] y: Area



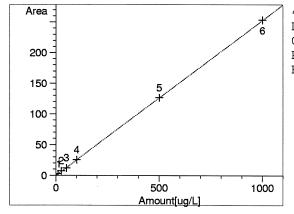


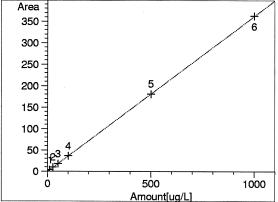
m: 2.31563e-1 b: 2.67966e-2 x: Amount[ug/L]

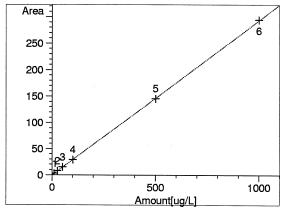
y: Area

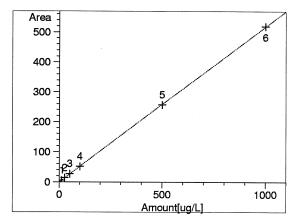


```
2,4,6-Trinitrotoluene #8 at exp. RT: 15.291
DAD1 B, Sig=254,16 Ref=360,100
Correlation: 0.99999
Residual Std. Dev.: 0.75740
Formula: y = mx + b
m: 4.19820e-1
b: -8.19160e-2
x: Amount[ug/L]
y: Area
```



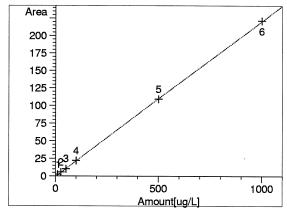


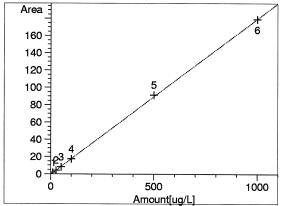


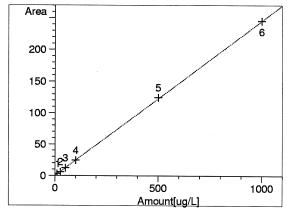


```
2,4-Dinitrotoluene #12 at exp. RT: 1800091556 DAD1 B, Sig=254,16 Ref=360,100 Correlation: 0.99999 Residual Std. Dev.: 1.03666 Formula: y = mx + b
```

ula: y = mx + b m: 5.17973e-1 b: -3.43882e-1 x: Amount[ug/L] y: Area







Data File C:\HPCHEM\1\DATA\030205\4L007768.D Sample Name: WG184085-07 ALT HPLC4 3/3/2005 2:17:06 PM ECL/RDC

1,1 SOS73-13 50 ppb

Injection Date : 3/2/2005 5:30:47 PM

Seq. Line: 8

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

Compound	RT	Known Conc.	Cal. Conc.	%D
HMX #1	4.620	50.0	48.113	-3.8
RDX #2	7.148	50.0	50.374	0.7
1,3,5-Trinitrobenzene #3	9.724	50.0	50.579	1.2
1,3-Dinitrobenzene #4	11.903	50.0	48.623	-2.8
Tetryl #5	12.601	50.0	49.985	0.0
Nitrobenzene #6	13.517	50.0	47.963	-4.1
3,4-Dinitrotoluene #7 *	14.438	50.0	48.787	-2.4
2,4,6-Trinitrotoluene #8	15.278	50.0	50.883	1.8
4-Amino-2,6-Dinitrotolue	15.965	50.0	51.879	3.8
2-Amino-4,6-Dinitrotolue	16.863	50.0	51.788	3.6
2,6-Dinitrotoluene #11	17.827	50.0	49.902	-0.2
2,4-Dinitrotoluene #12	18.482	50.0	52.380	4.8
2-Nitrotoluene #13	21.722	50.0	49.950	-0.1
4-Nitrotoluene #14	23.220	50.0	46.576	-6.8
3-Nitrotoluene #15	25.029	50.0	49.554	-0.9

^{# =} Failed 15.0% Criteria

Data File C:\HPCHEM\1\DATA\030205\4L007775.D Sample Name: WG184085-08 CCV HPLC4 3/3/2005 2:18:49 PM ECL/RDC

1,1 SOS73-18 50 ppb

Injection Date : 3/2/2005 9:51:24 PM Seq. Line : 15

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

Compound	RT	Known Conc.	Cal. Conc.	%D
HMX #1	4.624	50.0	48.591	-2.8
RDX #2	7.156	50.0	49.943	-0.1
1,3,5-Trinitrobenzene #3	9.723	50.0	49.405	-1.2
1,3-Dinitrobenzene #4	11.900	50.0	49.319	-1.4
Tetryl #5	12.605	50.0	47.438	-5.1
Nitrobenzene #6	13.517	50.0	52.843	5.7
3,4-Dinitrotoluene #7 *	14.441	50.0	50.544	1.1
2,4,6-Trinitrotoluene #8	15.283	50.0	49.457	-1.1
4-Amino-2,6-Dinitrotolue	16.014	50.0	47.981	-4.0
2-Amino-4,6-Dinitrotolue	16.900	50.0	49.528	-0.9
2,6-Dinitrotoluene #11	17.849	50.0	48.725	-2.6
2,4-Dinitrotoluene #12	18.497	50.0	49.095	-1.8
2-Nitrotoluene #13	21.742	50.0	53.201	6.4
4-Nitrotoluene #14	23.248	50.0	50.461	0.9
3-Nitrotoluene #15	25.043	50.0	45.942	-8.1

^{# =} Failed 15.0% Criteria

Data File C:\HPCHEM\1\DATA\030205\4L007783.D Sample Name: WG184085-09 CCV HPLC4 3/3/2005 2:19:44 PM ECL/RDC

1,1 SOS73-18 50 ppb

Injection Date : 3/3/2005 2:49:16 AM

Seq. Line: 23

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

Compound	RT	Known Conc.	Cal. Conc.	%D		
						
HMX #1	4.618	50.0	48.171	-3.7		
RDX #2	7.150	50.0	49.393	-1.2		
1,3,5-Trinitrobenzene #3	9.687	50.0	49.696	-0.6		
1,3-Dinitrobenzene #4	11.865	50.0	48.944	-2.1		
Tetryl #5	12.570	50.0	44.310	-11.4		
Nitrobenzene #6	13.465	50.0	50.960	1.9		
3,4-Dinitrotoluene #7 *	14.389	50.0	53.384	6.8		
2,4,6-Trinitrotoluene #8	15.211	50.0	50.149	0.3		
4-Amino-2,6-Dinitrotolue	16.017	50.0	50.489	1.0		
2-Amino-4,6-Dinitrotolue	16.899	50.0	49.209	-1.6		
2,6-Dinitrotoluene #11	17.771	50.0	48.344	-3.3		
2,4-Dinitrotoluene #12	18.420	50.0	48.466	-3.1		
2-Nitrotoluene #13	21.638	50.0	50.611	1.2		
4-Nitrotoluene #14	23.106	50.0	45.902	-8.2		
3-Nitrotoluene #15	24.901	50.0	48.745	-2.5		

^{# =} Failed 15.0% Criteria

Data File C:\HPCHEM\1\DATA\030305\4L007785.D Sample Name: WG184223-01 CCV HPLC4 3/7/2005 12:11:29 PM ECL/RDC

1,1 SOS73-18 50 ppb

Injection Date : 3/3/2005 5:54:36 PM Seq. Line : 2

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

Compound	RT	Known Conc.	Cal. Conc.	%D
HMX #1	4.616	50.0	50.475	0.9
RDX #2	7.135	50.0	50.891	1.8
1,3,5-Trinitrobenzene #3	9.714	50.0	50.973	1.9
1,3-Dinitrobenzene #4	11.886	50.0	49.913	-0.2
Tetryl #5	12.576	50.0	46.216	-7.6
Nitrobenzene #6	13.509	50.0	46.577	-6.8
3,4-Dinitrotoluene #7 *	14.419	50.0	44.332	-11.3
2,4,6-Trinitrotoluene #8	15.265	50.0	47.545	-4.9
4-Amino-2,6-Dinitrotolue	15.943	50.0	47.111	-5.8
2-Amino-4,6-Dinitrotolue	16.843	50.0	48.110	-3.8
2,6-Dinitrotoluene #11	17.823	50.0	48.991	-2.0
2,4-Dinitrotoluene #12	18.478	50.0	50.014	0.0
2-Nitrotoluene #13	21.714	50.0	51.606	3.2
4-Nitrotoluene #14	23.211	50.0	45.742	-8.5
3-Nitrotoluene #15	25.038	50.0	45.768	-8.5

^{# =} Failed 15.0% Criteria

Data File C:\HPCHEM\1\DATA\030305\4L007794.D Sample Name: WG184223-01 CCV HPLC4 3/7/2005 12:17:44 PM ECL/RDC

1,1 SOS73-18 50 ppb

Injection Date : 3/3/2005 11:29:50 PM Seq. Line : 11

Signal 1: DAD1 B, Sig=254,16 Ref=360,100

Compound	RT	Known Conc.	Cal. Conc.	%D
HMX #1	4.608	50.0	49.755	-0.5
RDX #2	7.123	50.0	50.087	0.2
1,3,5-Trinitrobenzene #3	9.682	50.0	50.782	1.6
1,3-Dinitrobenzene #4	11.848	50.0	50.643	1.3
Tetryl #5	12.525	50.0	49.931	-0.1
Nitrobenzene #6	13.451	50.0	49.478	-1.0
3,4-Dinitrotoluene #7 *	14.357	50.0	50.408	0.8
2,4,6-Trinitrotoluene #8	15.201	50.0	51.020	2.0
4-Amino-2,6-Dinitrotolue	15.902	50.0	49.917	-0.2
2-Amino-4,6-Dinitrotolue	16.804	50.0	50.791	1.6
2,6-Dinitrotoluene #11	17.749	50.0	51.070	2.1
2,4-Dinitrotoluene #12	18.403	50.0	50.068	0.1
2-Nitrotoluene #13	21.630	50.0	51.261	2.5
4-Nitrotoluene #14	23.138	50.0	48.898	-2.2
3-Nitrotoluene #15	24.900	50.0	48.320	-3.4

^{# =} Failed 15.0% Criteria



Environmental & Infrastructure, Inc.

1430 Enclave Parkway Houston, TX 77077 (281) 368-4000

CHAIN-OF-CUSTODY

No. 01-KEMM-FEB05

Laboratory Name: Kemron Ad					Add	dress:	109 Starlite Park Marietta, OH 45750		Conta	ct: 74	0 373	-4071				
Project Lo Project Name Longhorn AAP Manhol				h L (AR)		Analysis and Method Desired (Indicate separate containers)								Remarks		
Projec			Project (Project Telephone No.			0							
'''			1				281-368-4408	S S	and 8330							
LICAC	845714		<u> </u>	Diane Meyer			Manager/Supervisor	tai	cs a							
USACE Point of contact: Cliff Murray				Troject Marage, Oupervisor		Number of Containers	natic nes b									
USAC	E Telephone No.					Praveen Srivastav			일필							
Item No.	Sample Number	Date	Time	Comp	Grab	Matrix	Sample Description, Location	Num	Nitroaromatics a							
1	29WL34-MH03-02	2/21/05	14:05			WATER	29WL34-MH03	2	х							
2	29WL35-MH04-02MAD	2/24/05				WATER	29WL359MH04 A	2	X	_						No Sample
3	29WL36-MH05-02	2/24/05	14:13			WATER	29WL36-MH05	2	х							
4	29WL37-MH06-02	2/24/05				WATER	29WL37-MH06	2	х							
5	29WL38-MH07-02	2/33/05	16:15			WATER	29WL38-MH07	2	Х							
6	29WL39-MH08-02	2/23/05	15:17			WATER	29WL39-MH08	2	х							
7	29WL40-MH09-02	2/23/05	14:18			WATER	29WL40-MH09	2	Х			<u></u>				
8	29WL40-MH09-52	723/03				WATER	29WL40-MH09	2	Х							
9	29WL41-MH10-02	e 23/05	14:34			WATER	29WL41-MH10	2	х							
10	29WL42-MH11-02	2/2/15	1 12			WATER	29WL42-MH11	2	X				ļ			
11	29WL43-MH12-02	2/2965				WATER	29WL43-MH12	2	<u> </u>							
Transfers Relinquished By (Signature) Date/Time				Tra	Transfers Accepted By (Signature)		Date/Time Special Instructions					tant				
M. fll (1 424/05		5					special Instructions COC Dealed, DXD untact CYD									
							Of the state of th									
		· · · · · ·					FedEx Airbill No.:									
						Laborato	aboratory Struckler 725/05 9:40 Sampler's Signature U. Ill Co					1				
	TAT: 1 dec Standard Rush Due: Seals Intact? VY N Received Good Condition VY N Cold 2, 3°, 4° OHO									N	c	old 2	,3°,1	10 (JAPO	

Internal Chain of Custody Report

Login: L0502503

Account: SHAW-ALLIANCE-798

Project: 798-LONGHORN

Samples: 10

Due Date: 04-MAR-2005

<u>Samplenum</u> <u>Container ID</u> <u>Products</u>

L0502503-01 117553 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:21	BRG	DEL

00091563

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

<u>Samplenum</u> <u>Container ID</u> <u>Products</u>

L0502503-02 117554 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:17	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:21	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

<u>Samplenum</u> <u>Container ID</u> <u>Products</u>

L0502503-03 117555 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:17	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

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Internal Chain of Custody Report

Login: L0502503

Account: SHAW-ALLIANCE-798

Project: 798-LONGHORN

Samples: 10

Due Date: 04-MAR-2005

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0502503-04</u> 117556 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:17	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

00091564

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

 Samplenum
 Container ID
 Products

 L0502503-05
 117557
 8330

Bottle: 1

	· -					
Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0502503-06</u> 117558 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

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Internal Chain of Custody Report

Login: L0502503

Account: SHAW-ALLIANCE-798

Project: 798-LONGHORN

Samples: 10

Due Date: 04-MAR-2005

 Samplenum
 Container ID
 Products

 L0502503-07
 117559
 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

00091565

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0502503-08</u> 117560 8330

Bottle: 1

Seq.	Purpose From To Date/Time		Accept	Relinquish		
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN 25-FEB-2005 11:14		CLS			
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0502503-09</u> 117561 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:16	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:22	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

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Internal Chain of Custody Report

Login: L0502503

Account: SHAW-ALLIANCE-798

Project: 798-LONGHORN

Samples: 10

Due Date: 04-MAR-2005

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0502503-10</u> 117562 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	PREP	W1	EXT	02-MAR-2005 08:17	CSH	CLS
3	DISP	EXT	DISP	02-MAR-2005 15:21	BRG	DEL

Bottle: 2

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			25-FEB-2005 11:14	CLS	
2	STORE	W1	A1	03-MAR-2005 08:46	CEB	CEB

00091566

SAMPLE RECEIPT FORM

00091567

Revised 8/22/03

Date: 2/25/05 Client: Shaw- Houston Shipped By: () Fed-Ex (YUPS ()DHL () KEMRON () Client () Other Opened By: US	9:40	156 STARLITE DRIVE MARIETTA, OH 45750 (740) 373-4071
Logged By: US Login # L05 2 508		

COOLER INFORMATION

Comments:

Number	Cooler ID	Temp ° C	- Airbill#	COC#	Other "
1	KL910	Q	12667725019083402		
2	LaGroon	1 1	12667725019203 3410		·
3	KL832		126677250194207407		
4					
5					
6					

		 						 		F
6	<u> </u>								.	
Were all	coolers seale	ad2			<u> </u>	N	N/A	 -		
	stody seals u		coolers?	>	Κ.	N	N/A N/A			
	stody seals in				$\stackrel{\ \ }{\ \ }$	N	N/A			
	ble ice prese		•	7	$\stackrel{\checkmark}{\sim}$	N	N/A			
	•		ture range of 2-6C? (>6C*)	\sim	$\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $	N	N/A			
	samples fro	•	,	V	Y	(N)	N/A			
	DC papers pro			($\overline{\hat{\gamma}}$	N	N/A			
	sample conta		ct?*	٦	$\stackrel{\triangleright}{\sim}$	N	N/A			
Were all	sample label	s intact?	<u>L</u>	7	₹\	N	N/A			
Were all	sample label	s legible?	•	7	$\widetilde{\gamma}$	N	N/A	1		
Did all sa	ample labels i	match the	COC?*		Ÿ)	N	N/A			
Was the	label informa	tion comp	lete?*	7	\overline{V}	N	N/A			
Were the	correct cont	ainers use	ed?*	Č	8)	N	N/A			
Were the	correct pres	ervatives	added to water samples?*	,	Y	N	(N/A)			
Was the	pH tested on	preserve	d water samples?	•	Y	N	(N/A)			
Were pH	ranges acce	ptable?*		•	Y	N	(N/A)			
Was suff	icient amount	of sample	e provided?*	($\mathbf{\hat{Y}}$	N	N/A			
Were bul	bbles present	in VOA s	amples?*	•	Y	N	(N/A)			
Were CC	C's signed a	nd dated?		(\widehat{Y}	Ν	N/A			
Did samp	oles arrive be	fore hold t	time expired?*	Č	\tilde{Y}	N	N/A			
	epancy forms s a discrepar		?	``	Y	Ν	(N/A			
	· • .	-							CI	RF #1

Appendix B

Additional Investigation Data Summary Report (2006 and 2008)

APPENDIX B ADDITIONAL INVESTIGATION DATA SUMMARY REPORT

FINAL FEASIBILITY STUDY LHAAP-29, FORMER TNT PRODUCTION AREA, GROUP 2 LONGHORN ARMY AMMUNITION PLANT KARNACK, TEXAS



Prepared for
U.S. Army Corps of Engineers
Tulsa District
1645 South 101st Avenue
Tulsa, Oklahoma

Prepared by Shaw Environmental, Inc. 1401 Enclave Parkway, Suite 250 Houston, Texas 77077

Contract Number W912QR-04-D-0027 **Task Order No. DS02**

April 2010

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Attachment 1 Monitoring Well Drilling Logs

Attachment 2 Monitoring Well Development Records

Attachment 3 Activated Persulfate Oxidation Treatability Study Report

Attachment 4 Groundwater Sampling Forms

Attachment 5 Laboratory Reports (on Compact Disc)

Acronyms and Abbreviations

μg/L micrograms per liter
bgs below ground surface

DCA dichloroethane

DCE dichloroethene

DNB dinitrobenzene

DNT dinitrotoluene

DPE dichloropropene

FID flame-ionization detector

HMX octohydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine

LHAAP Longhorn Army Ammunition Plant

MCL maximum contaminant level

mg/kg milligrams per kilogram
PID photo-ionization detector

PVC polyvinyl chloride

RDX cyclotrimethylenetrinitramine

Shaw Environmental, Inc.

TCE trichloroethene
TNB trinitrobenzene
TNT trinitrotoluene

USACE U.S. Army Corps of Engineers

USEPA U.S. Environmental Protection Agency

VOC volatile organic compound

1.0 Introduction

Shaw Environmental, Inc. (Shaw) performed several field investigation activities at LHAAP-29 between September 2006 and February 2008. The purpose of the sampling events was to identify the extent of contamination within a former transite wastewater line and to further delineate sediment and groundwater in the shallow and intermediate groundwater zones at LHAAP-29.

1.1 TNT Wastewater Line Sampling

Four grab samples (32WL05, 29WL12, 29WL13, and 29WL14) of wastewater line contents were collected from the TNT wastewater transite pipe line. Samples were collected at two points along the gravity portion of the line that runs from the southern portion of the site to the former pump house location at the northern portion of the site. Samples were also collected at two points along the pressurized portion of the line that extends from the former pump house location to LHAAP-32, located north of LHAAP-29. The wastewater line content samples were analyzed for explosives to characterize any contents remaining in the wastewater line. A summary of the TNT wastewater line samples collected and analyses performed is presented in **Table B-1** and sample locations are provided in **Figure B-1**.

1.2 Sediment Sampling

Four sediment grab samples, including one duplicate, were collected from three locations (29SD47, 29SD48, and 29SD49) at 0 to 0.5 feet below ground surface (bgs) along the cooling water outfall ditch located at the northeastern portion of LHAAP-29. These samples were situated hydraulically downgradient from the location of previous sediment sample 29SD46, which exhibited elevated concentrations of the explosives compounds TNT and dinitrotoluene (DNT). These sediment samples were analyzed for explosives. A summary of the sediment samples collected and analyses performed are presented in **Table B-1**, and sample locations are provided in **Figure B-1**.

1.3 Groundwater Sampling

Between September 2006 and February 2008, a total of 23 groundwater samples, including three duplicate samples, were collected from nine monitoring wells at LHAAP-29. Shaw installed two monitoring wells (29WW36 and 29WW38) into the shallow groundwater zone (37 and 45 feet, respectively), three monitoring wells (29WW35, 29WW37, and 29WW39) into the intermediate groundwater zone (98, 95, and 92 feet, respectively), and one monitoring well (29WW40) into the deep groundwater zone (159 feet).

For this additional investigation, groundwater samples were first collected from all the newly installed wells during two sampling events in September and November 2006. Also, one groundwater sample was collected from existing intermediate monitoring well 29WW16 during the September 2006 sampling event. Groundwater sampling for natural attenuation evaluation at LHAAP-29 was conducted in February 2007. As part of the evaluation, groundwater samples were collected from three of the newly installed wells (29WW35, 29WW36, and 29WW38) as well as from two previously installed wells (29WW06 and 29WW15) in the shallow zone. In February 2008, two more groundwater samples were collected from wells 29WW37 and 29WW39 to further define the area of the methylene chloride plume in the intermediate zone.

The wells installed by Shaw were established at the various depths and locations at LHAAP-29 to better delineate the extent of methylene chloride in the shallow, intermediate and deep groundwater zones and perchlorate in the shallow groundwater zone. All groundwater samples were analyzed for volatile organic compounds (VOCs). The groundwater samples collected from the shallow zone in September and November 2006 were also analyzed for perchlorate. The groundwater samples collected in February 2007 for the evaluation of natural attenuation were analyzed for various analytes; however, only the data results for VOCs and perchlorate from this sampling event are presented here. The other analytes, bacteria, decomposition products, and general water chemistry are all presented in the Natural Attenuation Evaluation. A summary of the groundwater samples collected, which includes monitoring well locations, groundwater zones depths and analyses performed, is presented in **Table B-2**. The monitoring well locations are provided in **Figure B-2**.

2.0 Monitoring Well Installation

Monitoring wells were drilled and installed using a high-torque hollow stem auger or mud rotary drill rig. Each well was constructed with 4-inch diameter, flush-joint threaded, schedule 40, polyvinyl chloride (PVC). Soil was collected continuously using a 5-foot long, 2-inch diameter, split barrel core sampler advanced with the drill bit. The soil in the samplers was field screened using a photo-ionization detector (PID) or flame-ionization detector (FID). Soil stratigraphy was described according to ASTM D2488-00, *Standard Practice for Description and Identification of Soils (Visual-Manual Procedure)* (ASTM International, 2003), and logged on U.S. Army Corps of Engineers (USACE) Engineering Form 1836 (Drilling Log) or equivalent. The monitoring wells were installed in accordance with Appendix D, Field Procedures, of the *Final Installation-Wide Work Plan* (Shaw, 2006a).

The 4-inch diameter monitoring wells were installed in the annulus of hollow-stem augers. The PVC well screen installed for each well was of 0.01-inch slotted and 10 feet in length. A threaded PVC bottom cap was secured to the bottom of the screen interval. Solid PVC casing was installed from the top of the screen interval to approximately 3 feet above surface grade.

A filter pack consisting of clean silica sand (20-40 size) was placed in the auger-well annulus from approximately 0.5 feet below the well bottom to approximately 2 feet above the screen interval. A 3-foot thick bentonite seal (pellets or chips) was placed above the sand filter pack and hydrated with potable water. The annular space from the top of the bentonite seal to the surface was filled with a bentonite-cement grout.

Procedures were followed to ensure that contamination in each of the groundwater zones remain isolated and does not have the potential to migrate to the other zones. For the wells installed in the intermediate groundwater zone, the shallow groundwater zone was isolated using 12-inch diameter steel casing. The casing was installed from near surface grade to the top of the first confining layer. Upon grouting and setting of the isolation casing, drilling proceeded into the intermediate zone. For the well installed in the deep groundwater zone, the shallow and intermediate groundwater zones were isolated using 16-inch diameter steel casing and 12-inch diameter steel casing, respectively.

The drilling equipment was decontaminated prior to arrival at the site and between well installations. Additional information on decontamination procedures can be found in Appendix D, Attachment 9, of the *Final Installation-Wide Work Plan* (Shaw, 2006a). Core samplers were washed between sampling intervals in a detergent/water solution and double rinsed with potable tap water in clean buckets. The decontamination wastewater and the drill

cuttings were containerized separately and transported to an assigned staging area for proper handling as discussed in Appendix D of the *Final Installation-Wide Work Plan* (Shaw, 2006a).

Aboveground surface completions were constructed for each new monitoring well as described in Appendix D of the *Final Installation-Wide Work Plan* (Shaw, 2006a). The surface completions consist of a 6-inch-square protective steel casing, 5-feet long with a hinged, lockable lid set a minimum of 2 feet into a 4-foot-square by 6-inch-thick concrete pad. Concrete-filled steel bollards were installed just outside the corners of the concrete pad.

The monitoring wells and surface completions were installed in general accordance with USACE and State of Texas requirements by a drilling subcontractor licensed in the State of Texas. Following the completion of the field work for monitoring well installation, a State of Texas Well Report was submitted to the Texas Department of Licensing and Regulations for construction of each well. Drilling logs for the monitoring wells installed during this sample event are included in **Attachment 1**.

2.1 Well Development

The newly installed monitoring wells were developed to remove drilling fines and enhance hydraulic communication between the well and the groundwater zone. The wells were developed no sooner than 48 hours and no later than 7 days after installation. Well development was performed by pumping and gentle surging of the screened interval using a rubber-lined surge block. A minimum of three well borehole volumes of water (including the diameter of the well borehole and assumed 30-percent filter pack porosity) was pumped from each well. The volume of groundwater removed from each well was calculated based on the static water level as measured from the top-of-casing. An electronic interface probe was used to measure the water levels. General water quality parameters (temperature, pH, conductivity, and turbidity) were measured using field instruments and recorded in the field logbook. Development was performed until the water quality parameters were stabilized to within 10 percent and the water was visually clear. Monitoring Well 29WW38 had stable water quality parameters, but did not reach visual clarity during well development. Well development procedures were performed in accordance with the guidance provided in Appendix D, Attachment 3, of the Final Installation-Wide Work Plan (Shaw, 2006a). Development records for the newly installed monitoring wells are included in **Attachment 2**.

A Shaw hydrogeologist supervised well development and documented the development process and measurements in a Well Development Record specific to each well. Downhole development equipment was decontaminated prior to and following use at each well location by cleaning in a detergent/water solution and double rinsing with tap water in clean buckets. The development and decontamination wastewater was placed in 55-gallon drums and handled in accordance with Appendix D of the *Final Installation-Wide Work Plan* (Shaw, 2006a).

2.2 Survey of Monitoring Well Locations

A State of Texas-licensed professional land surveyor surveyed the locations and elevations of the newly installed monitoring wells. The horizontal coordinates (northings and eastings) of the wells were surveyed to the nearest foot based on the North American Datum of 1983. The vertical elevations of the tops of the wells (top-of-casing) were surveyed to nearest 0.01 feet. The ground surface elevation at each well location was surveyed to the nearest 0.1 feet. The survey information is included on the drilling logs in **Attachment 1**.

3.0 Bench Scale Chemical Oxidation Testing

Due to the elevated levels of methylene chloride contamination in the intermediate zone, soil and groundwater samples were collected during the installation of the monitoring wells for bench scale testing of activated persulfate formulations. Approximately 5 kilograms of soil and 10 liters of groundwater were collected for the bench-scale testing. The soil was collected from the intermediate zone sands during well installation from an area representative of the contaminated zone. The groundwater was collected from 29WW16, which represents the methylene chloride plume hot spot in the intermediate zone.

Upon sample receipt at Shaw's Technology Development Laboratory in Knoxville, Tennessee, batch experiments were established to evaluate the following activation methods for persulfate oxidation of methylene chloride: chelated ferrous iron, heat, and caustic pH adjustment. The objective of the bench-scale testing was to identify the necessary activation methods and concentrations of persulfate that would be required to oxidize the levels of methylene chloride present in the intermediate groundwater should treatment be deemed necessary. The results of the bench-scale testing concluded that combined heat and an alkaline activated persulfate oxidation would be the best treatment, if necessary. *The Activated Persulfate Oxidation Treatability Study Report* is included in **Attachment 3**.

4.0 Sampling and Analysis

This section describes the sampling and analysis procedures applicable to groundwater, sediment and soil samples collected at LHAAP-29. Samples were collected and handled in accordance with the Chemical Data Acquisition Plan, Appendix C of the *Final Installation-Wide Work Plan* (Shaw, 2006a). Health and safety procedures, including screening methods, are presented in the Health and Safety Plan, Appendix A of the *Final Installation-Wide Work Plan* (Shaw, 2006a).

4.1 TNT Wastewater Line Sampling

Residual contents from the former transite TNT wastewater line were collected at the locations identified in **Figure B-1**. At each of the sample locations, trenches were excavated down to the depth of the former wastewater line, or approximately 3 feet bgs. A sample of the contents of the wastewater line sample was collected from each proposed location as discussed in Addendum 6, *Additional Investigation at LHAAP-29* (Shaw, 2006b). At each location, a grab sample was collected from the wastewater line and placed directly into a 4-ounce glass sample jar with a Teflon-lined cap. Each sample container was labeled as described in Section 4.6.3 of Appendix C of the *Final Installation-Wide Work Plan* (Shaw, 2006a), enclosed in a sealable plastic bag, and placed in a cooler containing ice to preserve the samples at 4 degrees Celsius or less. Following collection of the samples, the location and sample depth and/or field measurements were recorded in the field logbook and chain-of-custody documentation was completed. The samples were delivered to the analytical laboratory for analysis using U.S. Environmental Protection Agency (USEPA) Method SW 8330 for explosives.

4.2 Sediment Sampling

Sediment samples were collected along the former cooling water outfall ditch at the locations identified in **Figure B-1**. The sediment sampling interval at each of the locations was 0 to 0.5 feet bgs. At each location, a grab sediment sample was collected and placed directly into a 4-ounce glass sample jar with a Teflon-lined cap. Each sample container was labeled as described in Section 4.6.3 of Appendix C of the *Final Installation-Wide Work Plan* (Shaw, 2006a), enclosed in a sealable plastic bag, and placed in a cooler containing ice to preserve the samples at 4 degrees Celsius or less. Following collection of the samples, the location and sample depth and/or field measurements were recorded in the field logbook and chain-of-custody documentation was completed. The samples were delivered to the analytical laboratory for analysis using USEPA Method SW 8330 for explosives.

A field duplicate (quality control sample) was collected and analyzed to assess the precision of the field sampling and laboratory analytical process. The field duplicate was collected by filling a second sample container in rapid succession after collecting the primary sediment sample. The duplicate was collected for sediment sample 29SD49.

4.3 Groundwater Sampling

Groundwater samples were collected from monitoring wells identified in **Figure B-2**. The groundwater samples were collected as discussed in Addendum 6, *Additional Investigation at LHAAP-29* (Shaw, 2006b). Groundwater samples were collected using the low-flow sampling methodology in accordance with Appendix C of the *Final Installation-Wide Work Plan* (Shaw, 2006a). General water quality parameters (temperature, pH, conductivity, and turbidity) were measured throughout the sampling process at each well location using field instruments. This information was recorded in the field logbook. Each sample bottle was labeled as described in Section 4.6.3 of Appendix C of the *Final Installation-Wide Work Plan* (Shaw, 2006a), enclosed in a sealable plastic bag, and placed in a cooler containing ice to preserve the samples at 4 degrees Celsius or less. Following collection of the samples, the location and field measurements were recorded on groundwater sampling forms (**Attachment 4**) and a chain-of-custody documentation was completed. The analytical parameters for which the groundwater samples were submitted for laboratory analysis are presented in **Table B-2**.

A field duplicate (quality control sample) was collected during each sampling event. The field duplicates were collected by filling a second sample container in rapid succession after collecting the primary groundwater sample. The duplicate samples collected for each of the sample events are presented in **Table B-2**.

5.0 Results

This section discusses the results of the wastewater line contents, sediment and groundwater samples collected as part of the additional investigation sampling event. The results are presented in **Tables B-3**, **B-4** and **B-5**, respectively. The associated laboratory data reports are included as **Attachment 5** of this document.

5.1 TNT Wastewater Line

Various explosives in the TNT wastewater line, 1,3,5-trinitrobenzene (TNB), 1,3-dinitrobenzene (DNB), TNT, 2,4-DNT, 2-amino-4,6-DNT, 4-amino-2,6-DNT, octohydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine (HMX) and cyclotrimethylenetrinitramine (RDX), were detected at the four sample locations. The highest concentrations of explosives (TNT at 526 milligrams per kilogram [mg/kg], 1,3,5-TNB at 53.4 mg/kg, 1,3-DNB at 1.08 mg/kg and 2,4-DNT at 89 mg/kg) were in sample 29WL13, which was collected from the southern (gravity) segment of the wastewater line. Results are summarized in **Table B-3**, and sample locations are shown on **Figure B-1**.

5.2 Sediment

Low concentrations of HMX were detected at two sediment sample locations, 29SD48 and the 29SD49 field duplicate, at estimated concentrations of 2.1J mg/kg and 0.88J mg/kg, respectively. A concentration of p-nitrotoluene was also detected at 29SD48 at 4.88 mg/kg. Results are summarized in **Table B-4**, and sample locations are shown in **Figure B-1**.

5.3 Groundwater

In the September 2006 sample event, newly installed intermediate zone wells (29WW35, 29WW37, and 29WW39) had detected concentrations of methylene chloride greater than the Maximum Contaminant Level (MCL) of 5 μ g/L, the cleanup goal for methylene chloride. The highest concentration (7,110,000 μ g/L) was at existing well 29WW16.

In the November 2006 sample event, methylene chloride concentrations in the intermediate wells around 29WW16 were less than before, with the exception of 29WW37 which maintained a relatively steady concentration as compared to the initial sample round.

In the February 2007 sample event, one intermediate well, 29WW35, had a detected methylene chloride concentration of 237 μ g/L, which was a decrease of nearly 98% from the September 2006 concentration of 8,770 μ g/L at that same well. In February 2008, subsequent sampling at the well locations assumed to be at the outer edge of the methylene chloride plume in the intermediate zone, 29WW37 and 29WW39, indicated that methylene chloride concentrations were below the MCL.

Based on the four intermediate zone monitoring wells (29WW16, 29WW35, 29WW37, and 29WW39) and results of the groundwater sample events conducted between September 2006 and February 2008, the methylene chloride plume in the intermediate groundwater zone has been adequately defined. Groundwater measurements suggest groundwater in the intermediate zone to be flowing towards to the northeast. This is further evidenced by the two wells with the highest methylene chloride concentrations, 29WW16 and 29WW35 (7,110,000 and 237 μ g/L respectively) which indicate a decrease in concentrations in northeast direction.

An elevated methylene chloride concentration of 92.8 μ g/L was detected in the deep well 29WW40 during the initial sample round in September 2006. Results were much lower in the subsequent November and December 2006 sample events at this well location. In the December 2006 sample round, the methylene chloride result was below the detection limit of 0.25 μ g/L.

Other VOCs detected in the groundwater samples above the MCLs included trichloroethene (TCE), 1,2-dichloroethane (DCA), 1,1-dichloroethene (DCE), 1,1-dichloropropene (DPE) and vinyl chloride. The maximum concentrations for TCE and vinyl chloride as well as the only detect above the MCL for 1,1-DPE were at intermediate zone well 29WW16. TCE was detected in the intermediate groundwater zone at one other well location, 29WW35. The decrease in TCE concentrations between wells 29WW16 and 29WW35 (4,340 and 25.6 µg/L, respectively) and the east-northeasterly groundwater flow direction suggests that the TCE plume in the intermediate zone is predominantly isolated between the two well locations.

The maximum concentration of 1,2-DCA (5,520 μ g/L) was detected at shallow zone well 29WW15 that is co-located with well 29WW16. Concentrations of TCE (344 μ g/L) and 1,1-DCE (7.5 μ g/L) were also identified at 29WW15 and is the only shallow well where these VOCs have been detected. The presence of TCE and 1,1-DCE solely at well 29WW15 and 1,2-DCA at co-located wells 29WW15 and 29WW16 indicates that these contaminants are isolated at this location. It appears that the 1,2-DCA plume is slowly migrating towards the intermediate zone; however, the maximum concentration detected in well 29WW16 (14.3 μ g/L) is still nearly 400 times less than the shallow zone concentration.

Results are summarized in **Table B-5**. Methylene chloride results are shown on **Figure B-2** and other VOC Results are shown on **Figure B-3**.

6.0 References

ASTM International, 2003, ASTM D2488-00, Standard Practice for Description and Identification of Soils (Visual-Manual Procedure).

Shaw, 2006a, Final Installation-Wide Work Plan, Longhorn Army Ammunition Plant, Karnack, Texas, Final, Houston, Texas, January.

Shaw, 2006b, Addendum 6, Additional Investigation at LHAAP-29 Former TNT Production Area, Longhorn Army Ammunition Plant, Karnack, Texas, Final, Houston, Texas, April.

Tables

Table B-1
TNT Wastewater Line and Sediment Sampling Analysis
LHAAP-29

Media	Sample Locations	Primary Samples	Field Duplicates	Analytical Suite	Results Table
TNT Wastewater Line					
Contents of north segment of transite wastewater line that extends from former pump house location to LHAAP-32.	32WL05	1	0	Explosives	B-3
Contents of south segment of transite wastewater line (gravity portion) near center of LHAAP-29.	29WL13	1	0	Explosives	B-3
Contents of north segment of transite wastewater line (pressure portion) at former pump house location.	29WL12	1	0	Explosives	B-3
Contents of south end of transite wastewater line (gravity portion) at south end of LHAAP-29.	29WL14	1	0	Explosives	B-3
Sediment					
Intermediate locations between the cooling water outfall ditch and the northeast property boundary.	29SD47, 29SD48, 29SD49	3	1	Explosives	B-4

Table B-2 Groundwater Sampling and Analysis LHAAP-29

Well Location	Well Depth (ft BTOC)	Groundwater Zone	September 2006	November 2006	December 2006	February 2007	February 2008	Field Duplicate	Analytical Suite	Results Table
29WW06	35	Shallow				1			VOCs, Perchlorate	
29WW15	33	Shallow				1			VOCs	
29WW16	90	Intermediate	1						VOCs	
29WW35	98	Intermediate	1	1		1		1 (Feb 2007)	VOCs, Perchlorate ^a	
29WW36	37	Shallow	1	1		1			VOCs, Perchlorate	B-5
29WW37	95	Intermediate	1	1			1		VOCs	
29WW38	45	Shallow	1	1		1		1 (Sept 2006)	VOCs, Perchlorate	
29WW39	92	Intermediate	1				1		VOCs	
29WW40	159	Deep	1	1	1			1 (Nov 2006)	VOCs	

Notes and Abbreviations

^a analyzed for perchlorate during the February 2007 sample event only.

ft BTOC feet below top of casing VOCs volatile organic compounds

Table B-3
Sample Results in Solids from TNT Wastewater Line
LHAAP-29

Sample D	32WL05 09/28/06 32WL05-092806 NA Reg	29WL12 09/28/06 29SB81-002 NA Reg	29WL13 09/28/06 29SB82-001 NA Reg	29WL14 09/27/06 29WL14-092706 NA Reg	
Parameter	Units				
Explosives					
1,3,5-Trinitrobenzene (1,3,5-TNB)	mg/kg	1.61 JL	< 0.249	53.4	1.61 JH
1,3-Dinitrobenzene (1,3-DNB)	mg/kg	<0.245 JL	< 0.249	1.08	< 0.246
2,4,6-Trinitrotoluene (TNT)	mg/kg	17 JL	< 0.249	526	58.4
2,4-Dintrotoluene (2,4-DNT)	mg/kg	5.15 JL	< 0.249	89	7.21
2,6-Dinitrotoluene (2,6-DNT)	mg/kg	<0.255 JL	< 0.259	< 0.251	< 0.256
2-Amino-4,6-dinitrotoluene	mg/kg	<0.255 JL	< 0.259	< 0.251	19 JH
4-Amino-2,6-dinitrotoluene	mg/kg	<0.255 JL	< 0.259	< 0.251	13.3
HMX	mg/kg	<2.16 JL	<2.19	<2.13	<2.17
m-Nitrotoluene	mg/kg	<0.245 JL	< 0.249	< 0.242	< 0.246
Nitrobenzene	mg/kg	<0.255 JL	< 0.259	<25.1	< 0.256
o-Nitrotoluene	mg/kg	<0.245 JL	< 0.249	< 0.242	< 0.246
p-Nitrotoluene	mg/kg	<0.245 JL	< 0.249	< 0.242	< 0.246
RDX	mg/kg	<0.98 JL	< 0.995	< 0.966	< 0.985
Tetryl	mg/kg	<0.637 JL	<0.647	<0.628	<0.64

Notes and Abbreviations:

result is below detection limit
 reported result was estimated
 result may be biased low

ft bgs feet below ground surface

HMX octohydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine

mg/kg milligrams per kilogram
RDX cyclotrimethylenetrinitramine

Table B-4
Sediment Sample Results
LHAAP-29

Sample D Parameter	29SD47 08/31/06 29SD47-083106 0.5 Reg	29SD48 08/31/06 29SD48-083106 0.5 Reg	29SD49 08/31/06 29SD49-083106 0.5 Reg	29SD49 08/31/06 29SD49-083106FD 0.5 FD	
Explosives	Units				
1,3,5-Trinitrobenzene (1,3,5-TNB)	mg/kg	<0.249	<0.239	<0.246	<0.242
1,3-Dinitrobenzene (1,3-DNB)	mg/kg	< 0.249	< 0.239	<0.246	<0.242
2,4,6-Trinitrotoluene (TNT)	mg/kg	< 0.249	< 0.239	< 0.246	<0.242
2,4-Dintrotoluene (2,4-DNT)	mg/kg	< 0.249	< 0.239	< 0.246	<0.242
2,6-Dinitrotoluene (2,6-DNT)	mg/kg	< 0.259	< 0.249	< 0.256	<0.251
2-Amino-4,6-dinitrotoluene	mg/kg	< 0.259	< 0.249	< 0.256	<0.251
4-Amino-2,6-dinitrotoluene	mg/kg	< 0.259	< 0.249	< 0.256	<0.251
HMX	mg/kg	<2.19	2.11 J	<2.17 J	0.88 J
m-Nitrotoluene	mg/kg	< 0.249	< 0.239	< 0.246	<0.242
Nitrobenzene	mg/kg	< 0.259	< 0.249	< 0.256	<0.251
o-Nitrotoluene	mg/kg	< 0.249	< 0.239	< 0.246	<0.242
p-Nitrotoluene	mg/kg	< 0.249	4.88	<0.246 J	<0.242 J
RDX	mg/kg	< 0.995	< 0.957	< 0.985	< 0.966
Tetryl	mg/kg	<0.647	<0.622	< 0.640	<0.628

Notes and Abbreviations:

result is below detection limit
J reported result was estimated

FD field duplicate

ft bgs feet below ground surface

HMX octohydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine

mg/kg milligrams per kilogram RDX cyclotrimethylenetrinitramine

REG regular sample

Table B-5
Groundwater Sample Results
LHAAP-29

ANALYTE	Sample Date: Sample ID: Sample Type: UNITS	29WW06 2/22/07 29WW06-FEB2007 REG	29WW15 2/24/07 29WW16-FEB2007 REG	29WW16 9/21/06 29WW16-060921 REG	29WW35 9/26/06 29WW35-060926 REG	29WW35 11/20/06 29WW35-061120 REG	29WW35 2/22/07 29WW35-FEB2007 REG
Non-Metallic Anion	UNITS						
Perchlorate	μg/L	<20	NA	NA	NA	NA	21.5 J
Volatiles	P9'L	120	1471	1471	14/1	1471	21.03
1,1,1,2-Tetrachloroethane	μg/L	NA	NA	<0.25	<0.25	<0.25	NA
1,1,1-Trichloroethane	µg/L	<0.37	<0.37	<0.25	<0.25	<0.25	< 0.37
1,1,2,2-Tetrachloroethane	µg/L	<0.46	<0.46	<0.125	<0.125	<0.125	<0.46
1,1,2-Trichloroethane	µg/L	<0.66	1.9 J	<0.25	<0.25	<0.25	<0.66
1,1-Dichloroethane	μg/L	<0.52	3.4	<0.125	0.338 JH	<0.125	<0.52
1,1-Dichloroethene	μg/L	<0.68	7.5	<0.5	<0.5	<0.5	<0.68
1,1-Dichloropropene	μg/L	NA	NA NA	26.4	<0.25	<0.25	NA
1,2,3-Trichlorobenzene	μg/L	NA	NA	<0.125	<0.125	<0.125	NA
1,2,3-Trichloropropane	μg/L	NA	NA	<0.5	<0.5	<0.5	NA
1,2,4-Trichlorobenzene	μg/L	NA	NA	<0.2	<0.2	<0.2	NA
1,2,4-Trimethylbenzene	μg/L	NA	NA	<0.25	< 0.25	<0.25	NA
1,2-Dibromo-3-chloropropane	μg/L	NA	NA	<1	<1	<1	NA
1,2-Dibromomethane	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
1,2-Dichlorobenzene	μg/L	NA	NA	0.155 J	<0.125	<2.5	NA
1,2-Dichloroethane	μg/L	< 0.53	5520	14.3	<0.25	<0.25	< 0.53
1,2-Dichloropropane	μg/L	< 0.59	<0.59	<0.2	<0.2	<0.2	<0.59
1,2-Dimethylbenzene (o-Xylen		NA	NA	< 0.25	<0.25	<0.25	NA
1,3,5-Trimethylbenzene	μg/L	NA	NA	<0.25	<0.25	< 0.25	NA
1,3-Dichlorobenzene	μg/L	NA	NA	<0.25	<0.25	< 0.25	NA
1,3-Dichloropropane	μg/L	NA	NA	0.281 J	<0.2	<0.2	NA
1,4-Dichlorobenzene	μg/L	NA	NA	0.702 J	<0.125	<0.125	NA
2,2-Dichloropropane	μg/L	NA	NA	<0.25	<0.25	<0.25	NA
2-Butanone	μg/L	<3	<3	<2.5	<2.5	<2.5	<3
2-Chloroethyl vinyl ether	μg/L	NA	NA	<2	<200	<2	NA

ANALYTE	Location Code: Sample Date: Sample ID: Sample Type: UNITS	29WW06 2/22/07 29WW06-FEB2007 Reg	29WW15 2/24/07 29WW16-FEB2007 Reg	29WW16 9/21/06 29WW16-060921 Reg	29WW35 9/26/06 29WW35-060926 Reg	29WW35 11/20/06 29WW35-061120 Reg	29WW35 2/22/07 29WW35-FEB2007 Reg
2-Chlorotoluene	μg/L	NA	NA	<0.125	<0.125	<0.125	NA
2-Hexanone	μg/L	<1.9	<1.9	<2.5	<2.5	<2.5	<1.9
4-Chlorotoluene	μg/L	NA	NA	<0.25	<0.25	<0.25	NA
Acetone	μg/L	<2.8	<2.8	<2.5	<2.5	<2.5	<2.8
Benzene	μg/L	<0.23	0.47 J	0.245 J	<0.125	<0.125	<0.23
Bromobenzene	μg/L	NA	NA	<0.125	<0.125	<0.125	NA
Bromochloromethane	μg/L	NA	NA	49.6	11 JH	<0.2	NA
Bromodichloromethane	μg/L	< 0.33	< 0.33	<0.25	<0.25	<0.25	< 0.33
Bromoform	μg/L	<0.65	<0.65	< 0.5	< 0.5	<0.5	< 0.65
Bromomethane	μg/L	<0.47	<0.47	< 0.5	< 0.5	<0.5	< 0.47
Carbon disulfide	μg/L	<0.62	<0.62	< 0.5	< 0.5	3.26	3.7
Carbon tetrachloride	μg/L	<0.52	<0.52	< 0.25	<0.25	< 0.25	< 0.52
Chlorobenzene	μg/L	<0.54	<0.54	< 0.125	<0.125	<0.125	< 0.54
Chloroethane	μg/L	<0.46	<0.46	< 0.5	< 0.5	< 0.5	< 0.46
Chloroform	μg/L	<0.66	5.3	< 0.125	<0.125	< 0.125	<0.66
Chloromethane	μg/L	<0.6	<0.6	115	1.76 JH	0.549 J	<0.6
Cis-1,2-Dichloroethene	μg/L	<0.83	1.8 J	< 0.25	2.27 JH	0.619 J	<0.83
Cis-1,3-Dichloropropene	μg/L	<0.59	<0.59	< 0.25	<0.25	< 0.25	< 0.59
Dibromochloromethane	μg/L	<0.68	<0.68	< 0.25	<0.25	< 0.25	<0.68
Dibromomethane	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
Dichlorodifluoromethane	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
Ethylbenzene	μg/L	<0.48	<0.48	< 0.25	<0.25	< 0.25	<0.48
Hexochlorobutadiene	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
Isopropylbenzene	μg/L	NA	NA	<0.25	<0.25	< 0.25	NA
m,p-xylenes	μg/L	NA	NA	<0.5	< 0.5	<0.5	NA
Methyl isobutyl ketone	μg/L	<7.3	<7.3	<2.5	<2.5	<2.5	<7.3
Methylene chloride	μg/L	<0.67	3 J	7,110,000	8,770	1,400	237
Naphthalene	μg/L	NA	NA	0.628 J	<0.2	<0.2	NA
n-Butylbenzene	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
n-Propylbenzene	μg/L	NA	NA	0.126 J	<0.125	<0.125	NA

ANALYTE	Location Code: Sample Date: Sample ID: Sample Type: UNITS	29WW06 2/22/07 29WW06-FEB2007 Reg	29WW15 2/24/07 29WW16-FEB2007 Reg	29WW16 9/21/06 29WW16-060921 Reg	29WW35 9/26/06 29WW35-060926 Reg	29WW35 11/20/06 29WW35-061120 Reg	29WW35 2/22/07 29WW35-FEB2007 Reg
p-Isopropyltoluene	μg/L	NA	NA	< 0.25	<0.25	<0.25	NA
sec-Butylbenzene	μg/L	NA	NA	< 0.25	<0.25	< 0.25	NA
Styrene	μg/L	< 0.5	<0.5	< 0.125	<0.125	<0.125	< 0.5
tert-butylbenzene	μg/L	NA	NA	< 0.25	< 0.25	<0.25	NA
Tetrachloroethene	μg/L	< 0.74	<0.74	6.47	<0.25	<0.25	<0.74
Toluene	μg/L	< 0.54	<0.54	17.3	<0.25	<0.25	< 0.54
Trans-1,2-Dichloroethene	μg/L	< 0.75	15.6	< 0.25	0.328 JH	<0.25	<0.75
Trans-1,3-Dichloropropene	μg/L	<0.61	<0.61	< 0.5	<0.5	<0.5	<0.61
Trichloroethene	μg/L	< 0.63	344	4340 J	123 JH	43.5	25.6
Trichlorofluoromethane	μg/L	NA	NA	< 0.25	< 0.25	<0.25	NA
Vinyl acetate	μg/L	NA	NA	<2.5	<2.5	<2.5	NA
Vinyl chloride	μg/L	< 0.32	<0.32	22.4	<0.25	<0.25	< 0.32
Xylenes, Total	μg/L	<1.1	<1.1	NA	NA	NA	<1.1

Sam Sample	n Code: le Date: nple ID: e Type: UNITS	29WW35 2/22/07 29WW36-FEB2007-FD FD	29WW36 9/22/06 29WW36-060922 REG	29WW36 11/17/06 29WW36-061117 REG	29WW36 2/21/07 29WW36-FEB2007 REG	29WW37 9/22/06 29WW37-060922 REG	29WW37 11/17/06 29WW37-061117 REG
Non-Metallic Anion	UNITS						
Perchlorate	μg/L	5.1 J	<5	NA	<4	NA	NA
Volatiles	μg/L	5.13	\0	IVA	\1	IVA	IVA
1,1,1,2-Tetrachloroethane	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
1		NA <0.37	<0.25 <0.25	<0.25 <0.25	NA <0.37	<0.25 <0.25	<0.25 <0.25
1,1,1-Trichloroethane	µg/L						
1,1,2,2-Tetrachloroethane	µg/L	<0.46	<0.125	<0.125	<0.46	<0.125	<0.125
1,1,2-Trichloroethane	μg/L	< 0.66	<0.25	<0.25	< 0.66	< 0.25	<0.25
1,1-Dichloroethane	μg/L	< 0.52	<0.125	<0.125	<0.52	<0.125	<0.125
1,1-Dichloroethene	μg/L	<0.68	< 0.5	< 0.5	<0.68	<0.5	< 0.5
1,1-Dichloropropene	μg/L	NA	< 0.25	<0.25	NA	<0.25	<0.25
1,2,3-Trichlorobenzene	μg/L	NA	<0.125	<0.125	NA	<0.125	<0.125
1,2,3-Trichloropropane	μg/L	NA	< 0.5	<0.5	NA	<0.5	< 0.5
1,2,4-Trichlorobenzene	μg/L	NA	< 0.2	<0.2	NA	<0.2	<0.2
1,2,4-Trimethylbenzene	μg/L	NA	< 0.25	<0.25	NA	<0.25	< 0.25
1,2-Dibromo-3-chloropropane	μg/L	NA	<1	<1	NA	<1	<1
1,2-Dibromomethane	μg/L	NA	< 0.25	<0.25	NA	< 0.25	< 0.25
1,2-Dichlorobenzene	μg/L	NA	< 0.125	<0.125	NA	<0.125	<0.125
1,2-Dichloroethane	μg/L	< 0.53	<0.25	<0.25	< 0.53	<0.25	< 0.25
1,2-Dichloropropane	μg/L	< 0.59	< 0.2	<0.2	<0.59	<0.2	<0.2
1,2-Dimethylbenzene (o-Xylene)	μg/L	NA	<0.25	<0.25	NA	<0.25	< 0.25
1,3,5-Trimethylbenzene	μg/L	NA	<0.25	<0.25	NA	<0.25	< 0.25
1,3-Dichlorobenzene	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
1,3-Dichloropropane	μg/L	NA	<0.2	<0.2	NA	<0.2	<0.2
1,4-Dichlorobenzene	μg/L	NA	0.186 J	<0.125	NA	0.41 J	<0.125
2,2-Dichloropropane	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
2-Butanone	μg/L	<3	<2.5	<2.5	<3	<2.5	<2.5
2-Chloroethyl vinyl ether	μg/L	NA	<2	<2	NA	<2	<2
2-Chlorotoluene	μg/L	NA	<0.125	<0.125	NA	<0.125	<0.125
2-Hexanone	μg/L	<1.9	<2.5	<2.5	<1.9	<2.5	<2.5

	Location Code	20/4//4/25	20/4/4/27	20/4//4/27	20/4/427	20/4/4/27	20/4//4/27
	Location Code: Sample Date:	29WW35 2/22/07	29WW36 9/22/06	29WW36 11/17/06	29WW36 2/21/07	29WW37 9/22/06	29WW37 11/17/06
	Sample ID:	29WW36-FEB2007-FD	29WW36-060922	29WW36-061117	29WW36-FEB2007	29WW37-060922	29WW37-061117
	Sample Type:	FD	REG	REG	REG	REG	REG
ANALYTE	UNITS	10	KLO	KLO	KLO	KLO	KLO
		NIA	0.25	0.25	NIA	0.25	0.25
4-Chlorotoluene	µg/L	NA	<0.25	<0.25	NA	< 0.25	<0.25
Acetone	µg/L	<2.8	3.06 J	<2.5	<2.8	5.47 J	11.2
Benzene	μg/L	<0.23	< 0.125	<0.125	<0.23	< 0.125	< 0.125
Bromobenzene	μg/L	NA	<0.125	<0.125	NA	<0.125	<0.125
Bromochloromethane	μg/L	NA	<0.2	<0.2	NA	<0.2	<0.2
Bromodichloromethane	μg/L 	< 0.33	<0.25	<0.25	< 0.33	<0.25	<0.25
Bromoform	μg/L	< 0.65	<0.5	<0.5	< 0.65	<0.5	<0.5
Bromomethane	μg/L	< 0.47	<0.5	<0.5	<0.47	<0.5	<0.5
Carbon disulfide	μg/L	2.8	<0.5	<0.5	<0.62	8.14	2.14
Carbon tetrachloride	μg/L	< 0.52	<0.25	<0.25	<0.52	<0.25	<0.25
Chlorobenzene	μg/L	< 0.54	<0.125	<0.125	<0.54	<0.125	<0.125
Chloroethane	μg/L	< 0.46	<0.5	<0.5	<0.46	<0.5	<0.5
Chloroform	μg/L	<0.66	<0.125	<0.125	<0.66	<0.125	<0.125
Chloromethane	μg/L	<0.6	<0.25	<0.25	<0.6	<0.25	<0.25
Cis-1,2-Dichloroethene	μg/L	< 0.83	<0.25	<0.25	<0.83	<0.25	<0.25
Cis-1,3-Dichloropropene	μg/L	< 0.59	<0.25	<0.25	<0.59	<0.25	<0.25
Dibromochloromethane	μg/L	<0.68	<0.25	<0.25	<0.68	<0.25	<0.25
Dibromomethane	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
Dichlorodifluoromethane	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
Ethylbenzene	μg/L	< 0.48	<0.25	<0.25	<0.48	<0.25	<0.25
Hexochlorobutadiene	μg/L	NA	<0.25	<0.25	NA	<0.25	< 0.25
Isopropylbenzene	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
m,p-xylenes	μg/L	NA	<0.5	<0.5	NA	<0.5	<0.5
Methyl isobutyl ketone	μg/L	<7.3	<2.5	<2.5	<7.3	<2.5	<2.5
Methylene chloride	μg/L	168	5.59	1.1 J	<0.67	23.2	63.4
Naphthalene	μg/L	NA	<0.2	<0.2	NA	<0.2	<0.2
n-Butylbenzene	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25
n-Propylbenzene	μg/L	NA	<0.125	<0.125	NA	<0.125	<0.125
p-Isopropyltoluene	μg/L	NA	<0.25	<0.25	NA	<0.25	<0.25

	ocation Code: Sample Date: Sample ID: Sample Type: UNITS	29WW35 2/22/07 29WW36-FEB2007-FD FD	29WW36 9/22/06 29WW36-060922 REG	29WW36 11/17/06 29WW36-061117 REG	29WW36 2/21/07 29WW36-FEB2007 REG	29WW37 9/22/06 29WW37-060922 REG	29WW37 11/17/06 29WW37-061117 REG
		NΙΛ	0.05	0.05	NΙΛ	0.05	0.05
sec-Butylbenzene	μg/L	NA	<0.25	<0.25	NA	<0.25	< 0.25
Styrene	μg/L	< 0.5	<0.125	<0.125	<0.5	<0.125	<0.125
tert-butylbenzene	μg/L	NA	<0.25	< 0.25	NA	< 0.25	< 0.25
Tetrachloroethene	μg/L	< 0.74	<0.25	<0.25	<0.74	< 0.25	< 0.25
Toluene	μg/L	< 0.54	<0.25	<0.25	<0.54	< 0.25	< 0.25
Trans-1,2-Dichloroethene	μg/L	< 0.75	<0.25	<0.25	<0.75	< 0.25	< 0.25
Trans-1,3-Dichloropropene	μg/L	<0.61	<0.5	< 0.5	<0.61	< 0.5	< 0.5
Trichloroethene	μg/L	23.4	<0.25	<0.25	<0.63	< 0.25	< 0.25
Trichlorofluoromethane	μg/L	NA	<0.25	<0.25	NA	< 0.25	< 0.25
Vinyl acetate	μg/L	NA	<2.5	<2.5 J	NA	<2.5	<2.5
Vinyl chloride	μg/L	< 0.32	<0.25	< 0.25	<0.32	< 0.25	< 0.25
Xylenes, Total	μg/L	<1.1	NA	NA	<1.1	NA	NA

ANALYTE	Sample ID: Sample Type: UNITS	29WW37 2/1/08 29WW37-020108 REG	29WW38 9/27/06 29WW38-060927 REG	29WW38 9/27/06 29WW38-060927-FD FD	29WW38 11/20/06 29WW38-061120 REG	29WW38 02/22/07 29WW38-FEB2007 REG	29WW39 9/26/06 29WW39-060926 REG
Non-Metallic Anion	ONITS						l
Perchlorate	μg/L	NA	<0.5	<0.5	NA	<4	NA
Volatiles	ру/с	107	10.0	10.0	147.1	×1	1471
1,1,1,2-Tetrachloroethane	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
1,1,1-Trichloroethane	μg/L	<0.25	<0.25 <0.25	<0.25 <0.25	<0.25 <0.25	<0.37	<0.25
1,1,2,2-Tetrachloroethane	μg/L	<0.125	<0.25 <0.125	<0.25	<0.25	<0.37 <0.46	<0.25
1,1,2-Trichloroethane	μg/L μg/L	<0.125	<0.125	<0.125	<0.125	<0.46 <0.66	<0.125
1,1-Dichloroethane	μg/L	<0.125	<0.25 <0.125	<0.25	<0.25	<0.66 <0.52	<0.25
1,1-Dichloroethene	μg/L	<0.123	<0.125	<0.125	<0.125	<0.52 <0.68	<0.125
1 '	μg/L μg/L	<0.25	<0.5 <0.25	<0.5 <0.25	<0.5	<0.68 NA	<0.5 <0.25
1,1-Dichloropropene	μg/L μg/L	<0.25	<0.25 <0.125	<0.25 <0.125	<0.25 <0.125	NA NA	<0.25 <0.125
1,2,3-Trichlorobenzene	μg/L μg/L	<0.125		<0.125 <0.5	<0.125 <0.5	NA NA	<0.125 <0.5
1,2,3-Trichloropropane		<0.2	<0.5 <0.2	<0.5 <0.2	<0.5 <0.2	NA NA	
1,2,4-Trichlorobenzene	µg/L	<0.2 <0.25	-			NA NA	<0.2
1,2,4-Trimethylbenzene	µg/L	<0.25 <1	<0.25	<0.25	<0.25	NA NA	<0.25
1,2-Dibromo-3-chloropropane		<u> </u>	<1	<1	<1	NA NA	<1
1,2-Dibromomethane	μg/L	<0.25	< 0.25	<0.25	< 0.25		< 0.25
1,2-Dichlorobenzene	μg/L	<0.125	<0.125	<0.125	<0.125	NA	<0.125
1,2-Dichloroethane	μg/L	<0.25	<0.25	<0.25	<0.25	< 0.53	< 0.25
1,2-Dichloropropane	μg/L	<0.2	<0.2	<0.2	<0.2	< 0.59	<0.2
1,2-Dimethylbenzene (o-Xyle		<0.25	<0.25	<0.25	<0.25	NA	<0.25
1,3,5-Trimethylbenzene	μg/L 	<0.25	<0.25	<0.25	<0.25	NA	<0.25
1,3-Dichlorobenzene	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
1,3-Dichloropropane	μg/L	<0.2	<0.2	<0.2	<0.2	NA	<0.2
1,4-Dichlorobenzene	μg/L	<0.125	0.252 J	0.225 J	<0.125	NA	<0.125
2,2-Dichloropropane	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
2-Butanone	μg/L	<2.5	<2.5	<2.5	<2.5	<3	<2.5
2-Chloroethyl vinyl ether	μg/L	<2	<2	<2	<2	NA	<2 J
2-Chlorotoluene	μg/L	< 0.125	<0.125	<0.125	<0.125	NA	< 0.125

	Location Code: Sample Date: Sample ID: Sample Type:	29WW37 2/1/08 29WW37-020108 REG	29WW38 9/27/06 29WW38-060927 REG	29WW38 9/27/06 29WW38-060927-FD FD	29WW38 11/20/06 29WW38-061120 REG	29WW38 02/22/07 29WW38-FEB2007 REG	29WW39 9/26/06 29WW39-060926 REG
ANALYTE	UNITS						
2-Hexanone	μg/L	<2.5	<2.5	<2.5	<2.5	<1.9	<2.5
4-Chlorotoluene	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
Acetone	μg/L	<2.5	3.62 J	<2.5	3 J	<2.8	<2.5
Benzene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.23	<0.125
Bromobenzene	μg/L	<0.125	<0.125	<0.125	<0.125	NA	<0.125
Bromochloromethane	μg/L	<0.2	<0.2	<0.2	<0.2	NA	<0.2
Bromodichloromethane	μg/L	<0.25	<0.25	<0.25	< 0.25	< 0.33	<0.25
Bromoform	μg/L	< 0.5	< 0.5	<0.5	< 0.5	<0.65	<0.5
Bromomethane	μg/L	< 0.5	< 0.5	<0.5	< 0.5	<0.47	<0.5
Carbon disulfide	μg/L	< 0.5	< 0.5	<0.5	0.72 J	<0.62	<0.5
Carbon tetrachloride	μg/L	<0.25	<0.25	<0.25	< 0.25	<0.52	<0.25
Chlorobenzene	μg/L	<0.125	<0.125	<0.125	< 0.125	< 0.54	<0.125
Chloroethane	μg/L	< 0.5	< 0.5	<0.5	< 0.5	<0.46	<0.5
Chloroform	μg/L	<0.125	0.332 J	0.312 J	0.321 J	<0.66	<0.125
Chloromethane	μg/L	<0.25	< 0.25	<0.25	< 0.25	<0.6	<0.25
Cis-1,2-Dichloroethene	μg/L	<0.25	< 0.25	<0.25	< 0.25	< 0.83	<0.25
Cis-1,3-Dichloropropene	μg/L	<0.25	< 0.25	<0.25	< 0.25	< 0.59	<0.25
Dibromochloromethane	μg/L	<0.25	< 0.25	<0.25	< 0.25	<0.68	<0.25
Dibromomethane	μg/L	< 0.25	<0.25	<0.25	<0.25	NA	<0.25
Dichlorodifluoromethane	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
Ethylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.48	<0.25
Hexochlorobutadiene	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
Isopropylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	NA	<0.25
m,p-xylenes	μg/L	<0.5	<0.5	<0.5	<0.5	NA	<0.5
Methyl acetate	μg/L	<2.5	NA	NA	NA	NA	NA
Methyl isobutyl ketone	μg/L	<2.5	<2.5	<2.5	<2.5	<7.3	<2.5
Methylene chloride	μg/L	1.03 J	12.7	12.5	0.568 J	<0.67	14.5
Naphthalene	μg/L	<0.2	<0.2	<0.2	<0.2	NA	<0.2
n-Butylbenzene	μg/L	<0.25	<0.25	<0.25	< 0.25	NA	<0.25

	Location Code: Sample Date: Sample ID: Sample Type:	29WW37 2/1/08 29WW37-020108 REG	29WW38 9/27/06 29WW38-060927 REG	29WW38 9/27/06 29WW38-060927-FD FD	29WW38 11/20/06 29WW38-061120 REG	29WW38 02/22/07 29WW38-FEB2007 REG	29WW39 9/26/06 29WW39-060926 REG
ANALYTE	UNITS						
n-Propylbenzene	μg/L	< 0.125	<0.125	<0.125	<0.125	NA	<0.125
p-Isopropyltoluene	μg/L	< 0.25	<0.25	<0.25	< 0.25	NA	<0.25
sec-Butylbenzene	μg/L	< 0.25	<0.25	< 0.25	< 0.25	NA	< 0.25
Styrene	μg/L	< 0.125	<0.125	<0.125	<0.125	< 0.5	<0.125
tert-butylbenzene	μg/L	< 0.25	< 0.25	< 0.25	< 0.25	NA	< 0.25
Tetrachloroethene	μg/L	< 0.25	< 0.25	< 0.25	< 0.25	< 0.74	< 0.25
Toluene	μg/L	< 0.25	<0.25	<0.25	<0.25	< 0.54	<0.25
Trans-1,2-Dichloroethene	μg/L	< 0.25	<0.25	<0.25	< 0.25	< 0.75	<0.25
Trans-1,3-Dichloropropene	μg/L	< 0.5	< 0.5	<0.5	<0.5	<0.61	<0.5
Trichloroethene	μg/L	< 0.25	0.354 J	0.351 J	<0.25	< 0.63	0.683 J
Trichlorofluoromethane	μg/L	< 0.25	<0.25	<0.25	< 0.25	NA	< 0.25
Vinyl acetate	μg/L	<2.5	<2.5	<2.5	<2.5 J	NA	<2.5 J
Vinyl chloride	μg/L	< 0.25	<0.25	<0.25	< 0.25	< 0.32	< 0.25
Xylenes, Total	μg/L	NA	NA	NA	NA	<1.1	NA

ANALYTE	Sample ID: Sample Type: UNITS	29WW39 11/20/06 29WW39-061120 REG	29WW39 2/1/08 29WW39-020108 REG	29WW40 9/21/06 29WW40-060921 REG	29WW40 11/21/06 29WW40-061121 REG	29WW40 11/21/06 29WW40-061121-FD FD	29WW40 12/19/06 29WW40-061219 REG
Non-Metallic Anion	00						
Perchlorate	μg/L	NA	NA	NA	NA	NA	NA
Volatiles	1 3	l		'			•
1,1,1,2-Tetrachloroethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	NA
1,1,1-Trichloroethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	< 0.25
1,1,2,2-Tetrachloroethane	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	<0.125
1,1,2-Trichloroethane	μg/L	< 0.25	< 0.25	<0.25	<0.25	<0.25	<0.25
1,1-Dichloroethane	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	<0.125
1,1-Dichloroethene	μg/L	< 0.5	< 0.5	<0.5	<0.5	<0.5	< 0.5
1,1-Dichloropropene	μg/L	<0.25	< 0.25	<0.25	<0.25	<0.25	NA
1,2,3-Trichlorobenzene	μg/L	<0.125	<0.125	<0.125	<0.125	0.164 J	NA
1,2,3-Trichloropropane	μg/L	< 0.5	< 0.5	<0.5	< 0.5	<0.5	NA
1,2,4-Trichlorobenzene	μg/L	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
1,2,4-Trimethylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	NA
1,2-Dibromo-3-chloropropane		<1	<1	<1	<1	<1	<1
1,2-Dibromomethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	< 0.25
1,2-Dichlorobenzene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	<0.125
1,2-Dichloroethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25
1,2-Dichloropropane	μg/L	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
1,2-Dimethylbenzene (o-Xyle		<0.25	<0.25	<0.25	<0.25	<0.25	NA
1,3,5-Trimethylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	NA
1,3-Dichlorobenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25
1,3-Dichloropropane	μg/L	<0.2	<0.2	<0.2	<0.2	<0.2	NA
1,4-Dichlorobenzene	μg/L	<0.125	<0.125	0.529 J	<0.125	<0.125	<0.125
2,2-Dichloropropane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	NA
2-Butanone	μg/L	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5
2-Chloroethyl vinyl ether	μg/L	<2	<2	<2	<2	<2	NA
2-Chlorotoluene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	NA

Table B-5 (*Continued*) Groundwater Sample Results LHAAP-29

	Location Code: Sample Date: Sample ID:	29WW39 11/20/06 29WW39-061120	29WW39 2/1/08 29WW39-020108	29WW40 9/21/06 29WW40-060921	29WW40 11/21/06 29WW40-061121	29WW40 11/21/06 29WW40-061121-FD	29WW40 12/19/06 29WW40-061219
	Sample Type:	REG	REG	REG	REG	FD	REG
ANALYTE	UNITS						
2-Hexanone	μg/L	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5
4-Chlorotoluene	μg/L	<0.25	<0.25	< 0.25	< 0.25	< 0.25	NA
Acetone	μg/L	5.11 J	<2.5	4.77 J	<2.5	<2.5	<2.5
Benzene	μg/L	<0.125	<0.125	< 0.125	<0.125	<0.125	< 0.125
Bromobenzene	μg/L	<0.125	<0.125	< 0.125	<0.125	<0.125	NA
Bromochloromethane	μg/L	<0.2	<0.2	0.474 J	<0.2	<0.2	NA
Bromodichloromethane	μg/L	< 0.25	<0.25	1.15	<0.25	<0.25	< 0.25
Bromoform	μg/L	< 0.5	<0.5	< 0.5	< 0.5	< 0.5	< 0.5
Bromomethane	μg/L	< 0.5	<0.5	< 0.5	< 0.5	< 0.5	< 0.5
Carbon disulfide	μg/L	< 0.5	< 0.5	< 0.5	1.54	1.89	2.34 J
Carbon tetrachloride	μg/L	< 0.25	< 0.25	< 0.25	<0.25	<0.25	< 0.25
Chlorobenzene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	<0.125
Chloroethane	μg/L	< 0.5	< 0.5	< 0.5	< 0.5	<0.5	<0.5
Chloroform	μg/L	0.179 J	<0.125	3.55	<0.125	<0.125	<0.125
Chloromethane	μg/L	< 0.25	< 0.25	<0.25	<0.25	<0.25	< 0.25
Cis-1,2-Dichloroethene	μg/L	< 0.25	< 0.25	< 0.25	<0.25	<0.25	< 0.25
Cis-1,3-Dichloropropene	μg/L	< 0.25	< 0.25	< 0.25	<0.25	< 0.25	< 0.25
Cyclohexane	μg/L	NA	NA	NA	NA	NA	< 0.25
Dibromochloromethane	μg/L	< 0.25	< 0.25	1.09	<0.25	<0.25	< 0.25
Dibromomethane	μg/L	<0.25	< 0.25	<0.25	<0.25	<0.25	NA
Dichlorodifluoromethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25 J
Ethylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	< 0.25
Freon 113	μg/L	NA	NA	NA	NA	NA	< 0.25
Hexochlorobutadiene	μg/L	<0.25	<0.25	<0.25	<0.25	0.272 J	NA
Isopropylbenzene	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25
m,p-xylenes	μg/L	<0.5	<0.5	<0.5	<0.5	<0.5	NA
Methyl acetate	μg/L	<2.5	<2.5	NA	NA	NA	<0.25
Methyl isobutyl ketone	μg/L	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5
Methyl tert-butyl ether	μg/L	NA	NA	NA	NA	NA	<0.5

Table B-5 (Continued) **Groundwater Sample Results** LHAAP-29

ANALYTE	Location Code: Sample Date: Sample ID: Sample Type: UNITS	29WW39 11/20/06 29WW39-061120 REG	29WW39 2/1/08 29WW39-020108 REG	29WW40 9/21/06 29WW40-060921 REG	29WW40 11/21/06 29WW40-061121 REG	29WW40 11/21/06 29WW40-061121-FD FD	29WW40 12/19/06 29WW40-061219 REG
Methylcyclohexane	μg/L	NA	NA	NA	NA	NA	<0.25
Methylene chloride	μg/L	1.82 J	<0.25	92.8	6.79	6.75	<0.25
Naphthalene	μg/L	< 0.2	<0.2	<0.2	<0.2	<0.2	NA
n-Butylbenzene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	NA
n-Propylbenzene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	NA
p-Isopropyltoluene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	NA
sec-Butylbenzene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	NA
Styrene	μg/L	<0.125	<0.125	<0.125	<0.125	<0.125	<0.125
tert-butylbenzene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	NA
Tetrachloroethene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Toluene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Trans-1,2-Dichloroethene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Trans-1,3-Dichloropropene	μg/L	< 0.5	<0.5	<0.5	<0.5	<0.5	< 0.5
Trichloroethene	μg/L	< 0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Trichlorofluoromethane	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Vinyl acetate	μg/L	<2.5	<2.5	<2.5	<2.5	<2.5	NA
Vinyl chloride	μg/L	<0.25	<0.25	<0.25	<0.25	<0.25	<0.25
Xylenes	μg/L	NA	NA	NA	NA	NA	<0.5

Notes:

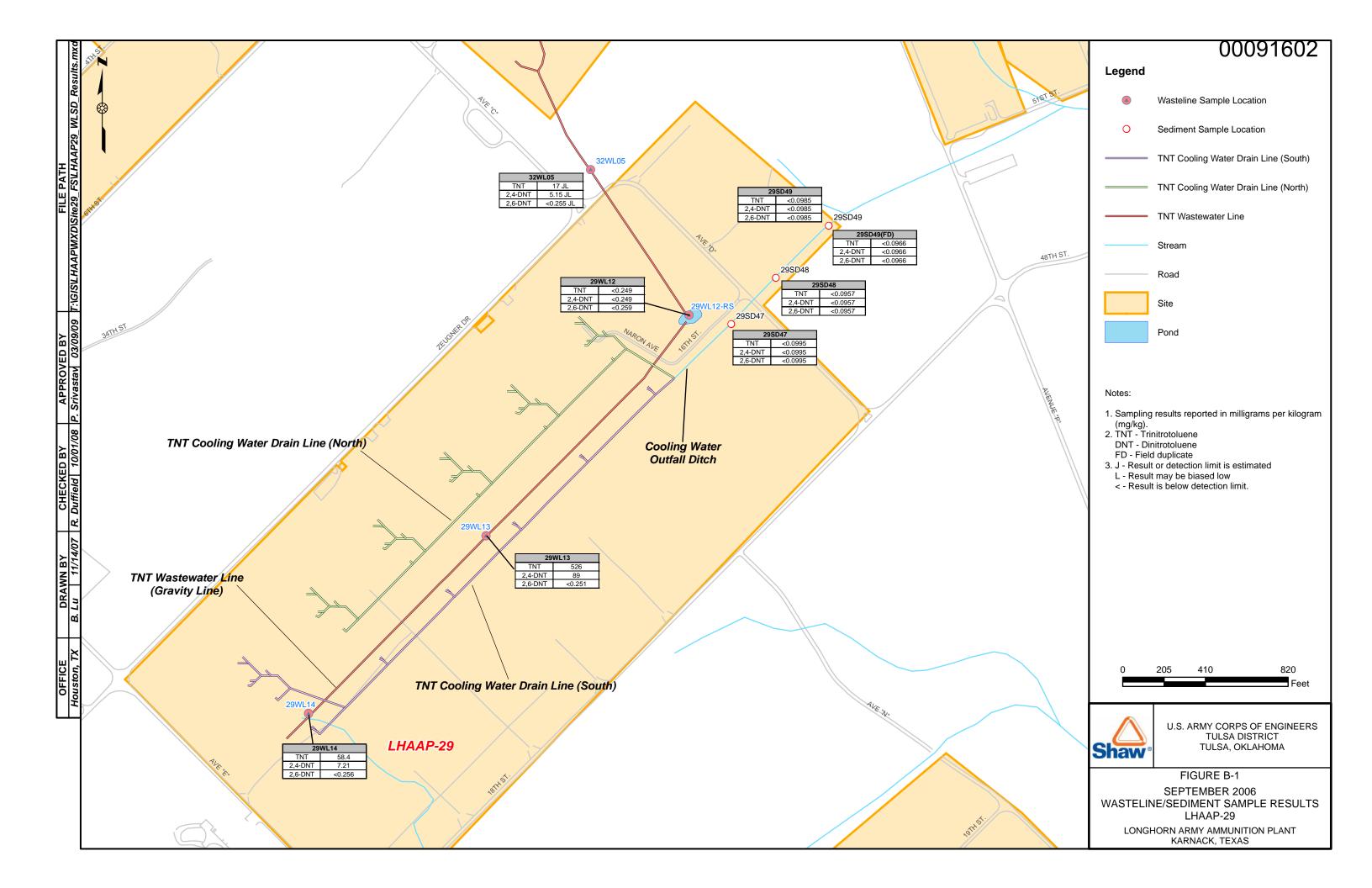
micrograms per liter result is below detection limit μg/L < field duplicate

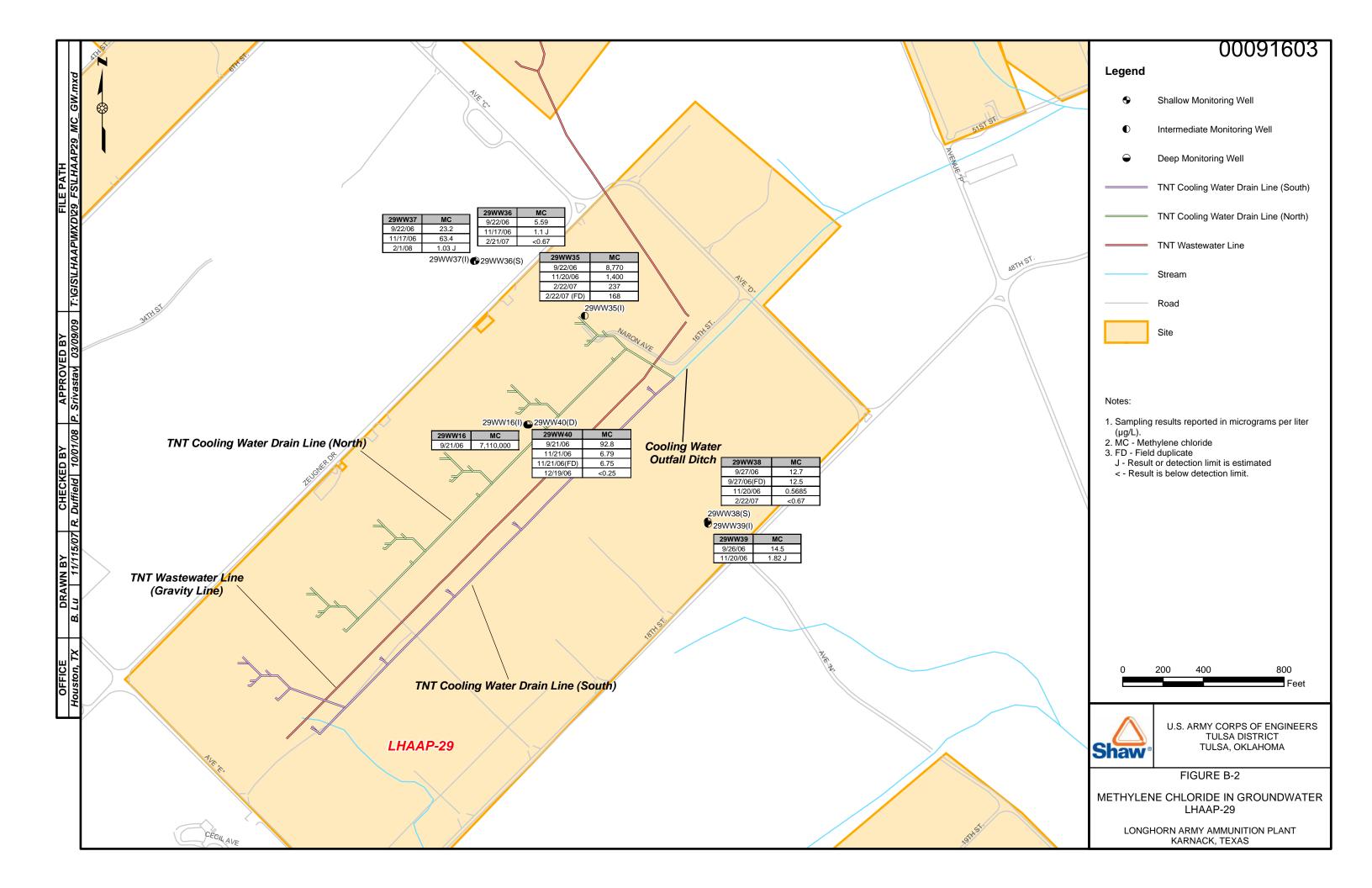
FD Н

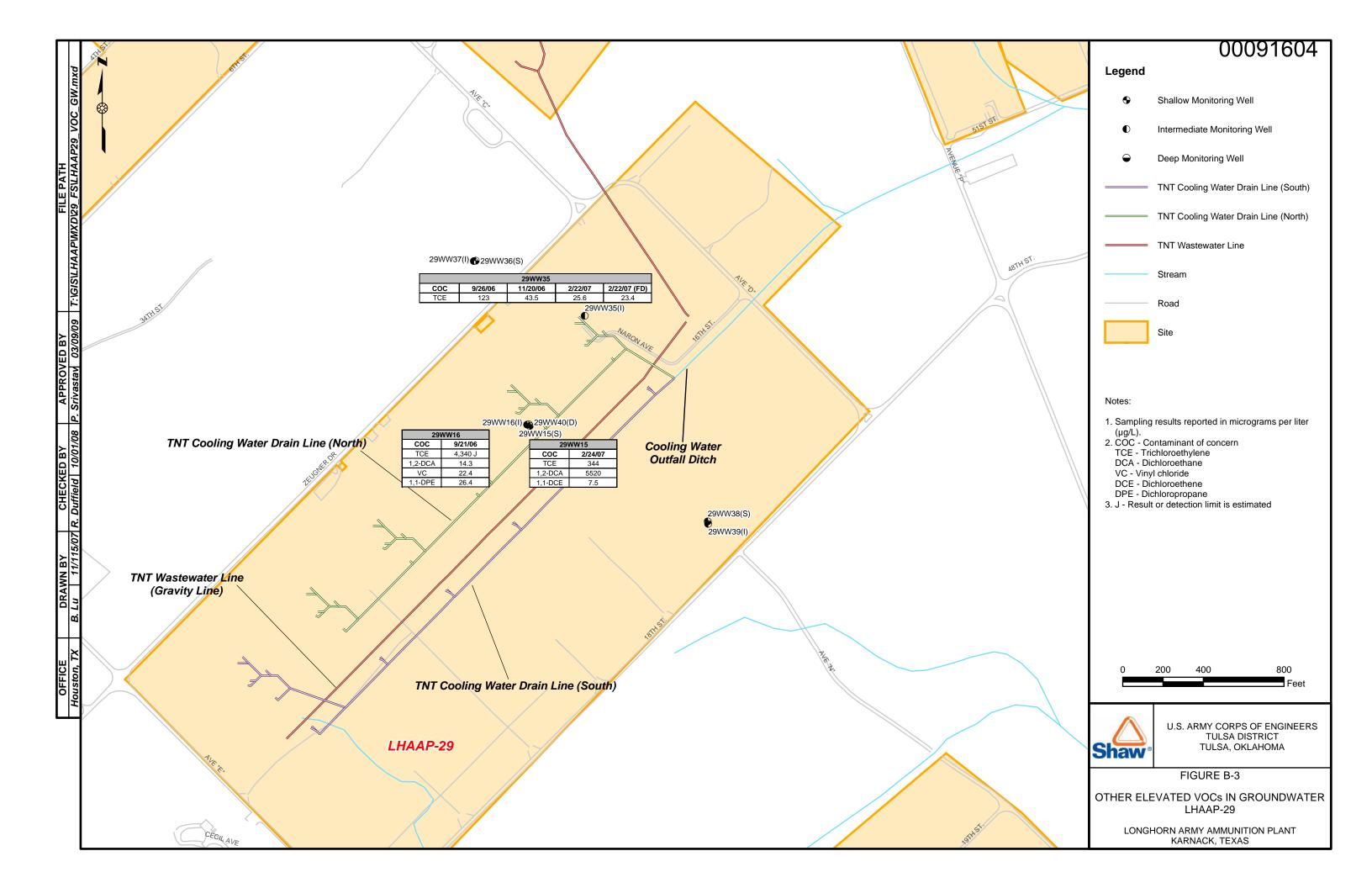
result may be biased high result or detection limit is estimated J

result may be biased low L

NA not analyzed REG regular sample **Figures**







Attachment 1 Monitoring Well Drilling Logs



Monitoring Well

00091606 29ww35

Page: 1 of 3

O 110111						rage. I of 5
Project Longhorn A		nunition Plant		. Ov		COMMENTS Hand augered 0 to 5 feet bgs.
Location Karnack,	Texas				Proj. No. <u>117591</u>	
Surface Elev. 225.	2 ft	Total Hole Depth	95.0	ft.	North 6956393.466 feast 3306421.223 ft.	Shallow Zone 12" Isolation Casing set at 49' bgs.
Top of Casing 228	.19	Water Level Initial	<u> </u>	13:05-Began drilling		
Screen: Dia 4 in.					Type/Size <u>Sch. 40 PVC/.01 in.</u>	
			~3' of r	riser)	ft. Type Sch. 40 PVC	8/24/06-Borehole was dry to 49' bgs.
					g/Core Mobil B5500	
Drill Co. ETTL						
					mant Date 9/14/06 Driller # NA	
Checked By K. Eve						
	II.		П	į.		
L Light		Sample ID % Recovery	2 ∦	Class.	Description	
Depth (ft.) Well	PID (mdd)		Log	SC	(Color, Texture, Structu	re)
S		Sar Sar	P	nscs	Geologic Descriptions are Based on	· ·
	#					
│						
- 0 	a l			SC	TOPSOIL, GRASS, ROOTING	
├	X				SAND, CLAYEY, LOOSE, MEDIUM-SOR	r, dry, no odor,
- 2 - - - - - - - - - - 	0,0			İ	RED, IRON STAINING	
				sc	-BECOMES MORE CLAYEY	
L 4 - 1831 S					-BECOMES MORE CLATET	
					CLAY, SANDY, MEDIUM TO HIGH PLAS BROWN, SLIGHTLY DAMP	FICTLY, SOFT,
F 6 -	0.0				-BECOMES MORE SILTY, ORGANIC	
					-BECOMES BROWN TO GRAY, HARD, D	NRV
- 8 - S					-BEOOMEO BROWN TO ORAT, FIARD, E	71(1
- 10 -						
	58.1				-BECOMES SANDY, MORE ORGANIC, G	GRAY IN COLOR
- 12 -	30.,			ŀ	,	
	[8]			ŀ	-BECOMES VERY SANDY, LOW PLAST!	CITY ALTERNATING
- 14 → - - - - - - - - - -					GRAY TO REDDISH-BROWN COLOR	OH I, METERIOR HINO
					-MODERATELY STIFF, LOW TO NO PLA	STICITY
L 16 - S	X					
	38.4					
10	X			CL		
├ 18 ├					-BECOMES STIFF TO HARD	
T _ 189 8	1					
├ 20 ├	X					
├ ₩ ₺	48.4					
<u>- 22 - 3 </u>	¥ 7°.7					
24 - 24						
26 –	41.2					
	Ø					
28						
	209					
<u>-</u> 30 – 30	1 200	'			Continued Next Page	
`. .	II.	11 11	11	- 1	Commune rest rage	



Monitoring Well

Continued Next Page

00091607 29WW35

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Project Longhorn Army Ammunition Plant Owner USACE Location Karnack, Texas Proj. No. <u>117591</u> Well Completion USCS Class. Description Graphic Log Depth (ft.) E (med (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 30 LIGNITE, LAYERED, ORGANIC, BLACK, BRITTLE, DRY РΤ CLAY, SILTY, HARD NO PLASTICITY, ORGANIC, DARK GRAY, 32 209 DRY, NO ODOR 34 36 36.2 38 40 6.8 42 46 19.8 48 *(ALLEN WILLMORE LOGS HOLE FROM 0 TO 49' BGS, BILL HARDMANT LOGS HOLE FROM 49' BGS TO TOTAL DEPTH)* 0.3 50 12" ISOLATION CASING SET AT 49' BGS -TRACES OF LIGNITE 52 54 56 58 DRY -IRON NODULES 0.5 60 62 64 -BECOMES SILTY WITH SAND AND CLAY LENSES INTERMIXED 66 SAND WITH SILT, SB 5/1, DRY, HARD 68 2.1 70



Monitoring Well

00091608 29WW35

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Project Longhorn Army Ammunition Plant Owner USACE Location Karnack, Texas Proj. No. <u>117591</u> Description Graphic Log PID (mdd) Depth (ft.) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued - 70 72 SM 74 LIGNITE BED РΤ SAND WITH SILT 76 78 -SAND WITH SILT, SLIGHTLY DAMP, 10 GY, 5/1 0.5 80 82 84 86 88 -5 GY 4/1, SLIGHTLY MOIST 2.1 90 92 94 0,5 END OF BORING 96 98 100 102 104 106 108 110



Monitoring Well

00091609 29WW36 Page: 1 of 2

			munition Plant		_ c	owner <u>USACE</u>	COMMENTS
	Kamack,		·			Proj. No. <u>117591</u>	Hand augered 0 to 5 feet bgs.
						North 6956665.96 ft. East 3305879.737 ft.	
Top of Casing $\underline{234.02}$ Water Level Initial $\underline{\underline{\lor}}$ 28.0							
	Screen: Dia 4 in. Length 10 ft.						
Casing: E)ia <u>4 in.</u>		Length 27	ft.		TypeSch. 40 PVC	
Fill Mater	ial <u>NA</u>				_ R	ig/Core Mayhew 500	
Drill Co.	ETTL		Me	thod Ho	ollow (Stem	
Driller _	T. Cook		Log By A. I	Villmore		Date <u>8/25/06</u> Driller.# NA	
Checked	By <u>K. Eve</u>	rett		Licens	e No.	Texas 379	
.	Well Completion	. ←	Sample ID % Recovery	- -	USCS Class.	Description	
Depth (ft.)	Wel	PID (ppm)		Graphic Log	ဗ္ဗ	(Color, Texture, Structure)	ra)
	ပိ		SS'8	0	ĭ	Geologic Descriptions are Based on	, , , , , , , , , , , , , , , , , , ,
[0 -						CLAY, SANDY, LOW TO NO PLASTICITY	, DAMP (DUE TO
						RAIN), NO ODOR, BROWN	
├ ² ~		0.0					
-							
- 4 -			-			-BECOMES SILTY, HARD, NO PLASTICI	TV IRON STAINING
-						REDDISH-BROWN, RED TO BROWN MC	OTTLING, SOME
6 -						ORGANICS	·
		0.0					
L 8 -					CL		
ļ .							
10 -							
[₄₂]		0.0					
- 12 -							
† -							
- 14 -						-BECOMES LIGHT BROWN TO GRAY	
-					$\vdash \vdash \mid$	SAND, CLAYEY, DAMP, BROWN, DENSE	
- 16 -						ONITE, OLATET, DAME, DROWN, DENSE	אטעט טאל.
-		0.0			sc		
<u> </u>						 	
ļ						CLAY, SILTY, HARD, LOW TO NO PLAST	ICITY, BROWN TO
20 -						LIGHT BROWN, NO ODOR, DRY	
_ 22 _		0.0			CL		
I 1							
<u> </u>							
- 24 - - 26 -					sc	SAND, CLAYEY, DENSE, MOIST, MEDIUM	/I-SORTED, GRAY,
<u> </u>		0.0		m	РТ	┐ FINE-GRAINED, GRAY ┐ LĪĞNĪTĒ TO ŌRĞANIC CLAY, DRY, BLAC	E NO ODOB/
					sc	SAND, CLAYEY, DENSE, MOIST, MEDIUM	A-SORTED FINE
_ 28 ▽					\dashv	↑ GRAINED, BROWN TO GRAY	/ 1
1		0.0			CL	CLAY, SANDY, STIFF, NO PLASTICITY, B	ROWN TO GRAY,
30			ı	1111111	-	✓ DAMP, NO ODOR Continued Next Page	
ــــــــــــــــــــــــــــــــــــــ				и 11		Continued Next Page	



Monitoring Well

00091610

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Project Longhorn Army Ammunition Plant Owner <u>USACE</u> Location Karnack, Texas Proj. No. <u>11759</u>1 Well Completion USCS Class. Description Graphic Log Depth (ft.) PID (ppm) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 30 `-BECOMES DRY 32 0.0 CL 34 **END OF BORING** 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70



Monitoring Well

00091611 29WW37 Page: 1 of 3

Project _	Longhorn Army Ammunition Plant Owner USACE COMMENTS									
Location	Kamack,	Texas				Proj. No. <u>117591</u>	Hand augered 0 to 5 feet bgs.			
						North 6956663.149 ftast 3305871.659 ft.	Shallow Zone 12" Isolation Casing set at 34' bgs.			
Top of Ca	sing 234.	91	Water Level Initial <u>¥ 86.0</u>			ft. Static NA Diameter 8 in.				
Screen: D	ia <u>4 in.</u>		Length 10 f	t.	Type/Size Sch. 40 PVC/.01 in.					
Casing: D	ia <u>4 in.</u>	n. Length 84 ft.				Type Sch. 40 PVC				
Fill Materi	ial <i>NA</i>		~~~~~		_ R	ig/Core Mobil B5500				
Drill Co.	ETTL		Me	thod Mi	ıd Ro	tary				
Driller _7	. Cook		Log By A. V	Villmore		Date <u>9/8/06</u> Driller # <i>NA</i>				
Checked	By K. Eve	rett		Licens	e No.	Texas 379				
	c				υj					
Depth (ft.)	Well Completion	PID (mdd)	Sample ID % Recovery	Graphic Log	USCS Class.	Description				
g €	≯ mo	⊑ 8	Red	Ga	တ္တ	(Color, Texture, Structure)	re)			
	0		w/%		ž	Geologic Descriptions are Based on	the USCS.			
	ļ			***************************************						
- 0 -		<u> </u>				CLAY, SANDY, LOW TO NO PLASTICITY	, DAMP (DUE TO			
† -						RAIN), NO ODOR, BROWN				
- 2 -		0.0	. [
-										
- 4 -				<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>		DECOMES SILTY HARD NO DI ASTIGLI	EV IDON CTAINING			
ļ -						-BECOMES SILTY, HARD, NO PLASTICI' REDDISH-BROWN, RED TO BROWN MO	TY, IRON STAINING, DTTLING SOME			
L 6 -			1			ORGANICS	7 1 2 11 1 3 , 3 0 11 L			
		0.0								
					CL					
8 -										
- 10 -										
<u> </u>		0.0								
- 12 -										
<u> </u>										
- 14 -			-			-BECOMES LIGHT BROWN TO GRAY				
<u> </u>					ļ	SAND, CLAYEY, DAMP, BROWN, DENSE				
 16 –						OAND, OLATET, DAWIF, BROWN, DENSE	E, NO ODOK			
-		0.0			SC					
18 –					<u> </u>					
L						CLAY, SILTY, HARD, LOW TO NO PLAST ODOR, DRY	ICITY, BROWN, NO			
_ 20 _										
Ī ¯		0.0			CL					
_ 22 -										
-										
24 -										
<u>-</u>						SAND, CLAYEY, DENSE, MOIST, MEDIUI	MISORTED GRAV			
- 24 - - 26 -				1////	sc	↑ FINE-GRAINED, GRAY	· · · · · /-			
_		0.0		77777	PΤ	LIGNITE TO ORGANIC CLAY, DRY, BLAC				
- 28 -					sc	SAND, CLAYEY, DENSE, MOIST, MEDIUI GRAINED, BROWN TO GRAY	M-SORTED, FINE			
<u>}</u> -					CL	CLAY, SANDY, STIFF, NO PLASTICITY, E	BROWN TO GRAY /			
30 –		0.0				DAMP, NO ODOR				
취 1					l l	Continued Next Page				



Monitoring Well

00091612 29WW37

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Project Longhorn Army Ammunition Plant Owner USACE Location Kamack, Texas Proj. No. __117591 USCS Class. Description Graphic Log PID (mdd) Zepth (#.) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 30 >-BECOMES DRY 32 0.0 34 12" ISOLATION CASING SET AT 34' BGS 36 0.0 38 40 0.0 42 44 46 0.0 48 LIGNITE, BLACK, ORGANIC, HARD IN NORMAL DIRECTION, FLAKY IN COMPRESSED DIRECTION 50 SAND, SILTY, GRAY, SLIGHTLY MOIST, DENSE SM 0.0 SILT, SANDY, SLIGHTLY MOIST, DENSE 52 ML CLAY, SILTY, HARD, NO PLASTICITY, GRAY TO DARK GRAY, SLIGHTLY DAMP 54 56 58 0.0 60 62 64 66 68 0.0 Continued Next Page



Monitoring Well

00091613 29WW37

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Project Longhorn Army Ammunition Plant Owner USACE Location Karnack, Texas Proj. No. <u>117591</u> USCS Class. Well Completion Description Graphic Log PID (mdd) Depth (ft.) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 70 72 74 CL 76 78 0.0 80 SILT, SANDY, POORLY-SORTED, DENSE, MOIST 82 ML 84 86 \ SAND, CLAYEY, POORLY-SORTED, DENSE, GRAY, WET 88 SC 90 CLAY, SILTY, DAMP, GRAY, LOW TO NO PLASTICITY 0.0 CL END OF BORING 92 94 96 98 100 102 104 106 108



Monitoring Well

29WW38 Page: 1 of 2

Project Longhorn Army Location Kamack, Texa Surface Elev. 218.3370 Top of Casing 220.99 Screen: Dia 4 in. Casing: Dia 4 in. Fill Material NA Drill Co. ETTL	Total Hole Depth Water Level Initial Length 10 ft. Length 37 ft.	49.0 ft.	Type/Size <u>Sch. 40 PVC/.01 in.</u> Type <u>Sch. 40 PVC</u> Rig/Core <u>Mayhew 500</u>			
	Log By <u>S. Oller/</u>	A. Willmore				
Depth (ft.) (R.) Well Completion	Sample ID % Recovery	Log USCS Class.	Description (Color, Texture, Structur Geologic Descriptions are Based on	· ·		
- 4		CL CL SC	TOPSOIL, SANDY, ROOTED CLAY, SANDY, LOW PLASTICITY, DENS GRAY SAND, CLAYEY, LOW PLASTICITY, DAW CLAY, SANDY, DENSE, HIGH PLASTICIT SAND, CLAYEY, FINE-GRAINED, MEDIU WELL-SORTED, DAMP, BROWN CLAY, SANDY, LOW PLASTICITY, DAMP -BECOMES MORE CLAYEY -BECOMES MORE SANDY SAND, CLAYEY, FINE GRAINED, WELL-SBROWN, SOME IRON STAINING Continued Next Page	IP, LIGHT BROWN TY, DAMP, BROWN M- TO P, BROWN, DENSE		



Monitoring Well

00091615 29WW38

Page: 2 of 2

Project Longhorn Army Ammunition Plant Owner <u>USACE</u> Location Kamack, Texas Proj. No. <u>117591</u> Well Completion USCS Class. Description Graphic Log Depth (ft.) PID (ppm) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 30 -BECOMES MORE SANDY -BECOMES MOIST 32 0.0 34 36 0.0 38 SC 40 -BECOMES SATURATED 0.0 42 44 46 WELL SET AT 44' BGS; BORING BACKFILLED WITH 0.0 BENTONITE FROM 44' BGS TO 49' BGS 48 **END OF BORING** 50 52 54 56 58 60 62 64 66 68 70



Monitoring Well

00091616 29WW39

Page: 1 of 3

Project Longhorn Army Amr	munition Plant Owner	USACE	COMMENTS
Location Karnack, Texas	100 mg (1 _{11 mg 11}	Proj. No. <u>117591</u>	Hand augered 0 to 5 feet bgs.
Surface Elev. 218.25497	Total Hole Depth 87.0 ft.	North 6955363.733 feast 3307033.519 ft.	No isolation casing set. No discernable lithologic separation
Top of Casing <u>221.13</u>	Water Level Initial <u>₹ 78.0 ft.</u>	Static <u>NA</u> Diameter <u>8 in.</u>	of shallow and intermediate water-bearing zones
Screen: Dia 4 in.	Length 10 ft.	Type/Size Sch. 40 PVC/.01 in.	Backfilled with bentonite to 84'
Casing: Dia 4 in.	Length 80 ft.	Type _Sch. 40 PVC	bgs.
Fill Material NA	Rig/Co	re Mobil B5500	
Drill Co. <u>ETTL</u>	Method Mud Rotary		
Driller <i>J. Sartain</i>	Log By A. Willmore /D. Tibbals	Date <u>9/14/06</u> Driller# NA	
Checked By K. Everett	License No	xas 379	

Casing: Di			Length 80 ft						
Fill Materia				Rig/Core Rig/Core					
Drill Co.				hod Mu			.		
Driller <u>J</u>			Log By A. W			als Date 9/14/06 Driller # NA			
Checked E	By <u>K. Ever</u>	ett		License	e No.	Texas 379	-		
	uc		이상		SS.	Description			
Depth (ft.)	Well Completion	PID (ppm)	Sample ID % Recovery	Graphic Log	USCS Class.	·			
۵	Com	a d	Sam % Re	5	SC	(Color, Texture, Struc Geologic Descriptions are Based			
				<u> </u>		Coologic pescripating are passed to	on the 6666.		
L 0 -									
	X					TOPSOIL, SANDY, ROOTED CLAY, SANDY, LOW PLASTICITY, DEN			
- 2 -		0.0				GRAY	ISE, DRT, BROWN TO		
_									
- 4 -			<u> </u>				•		
-					CL				
6 -									
F =		0.0							
⊢ 8 ⊣									
-						SAND, CLAYEY, LOW PLASTICITY, DA	MP. LIGHT BROWN		
10 -					sc		, =		
† †	\aleph	0.0							
12						CLAY, SANDY, DENSE, HIGH PLASTIC	ITY, DAMP, BROWN		
					CL				
- 14 -						SAND, CLAYEY, FINE-GRAINED, MEDI	UM- TO		
1 1					-	WELL-SORTED, DAMP, BROWN			
− 16 −		0.0			SC				
18									
						CLAY, SANDY, LOW PLASTICITY, DAM	IP, BROWN, DENSE		
L 20 -									
20									
- 22 -		0.0			CL				
i 1						DECOMES MODE OF WEN			
24 -						-BECOMES MORE CLAYEY			
		İ				-BECOMES MORE SANDY			
26 -						SAND, CLAYEY, FINE GRAINED, WELL BROWN, SOME IRON STAINING	SORTED, DAMP,		
		0.0							
28 -					sc				
30 - J			H						
30 -		0.0							
.L	<u> </u>					Continued Next Page	·		



Monitoring Well

00091617 29ww39

Page: 2 of 3

Project Longhorn Army Ammunition Plant Owner USACE

Location Kamack, Texas Proj. No. 117591

Location	Karriack, I	0 ×00				Proj. No
Depth (ft.)	Well Completion	OIO (mdd)	Sample ID % Recovery	Graphic Log	USCS Class.	Description (Color, Texture, Structure) Geologic Descriptions are Based on the USCS.
- 30 - - 32 - - 34 - - 36 - 		0.0				Continued -BECOMES MORE SANDY -BECOMES MOIST
- 38 - 40 - 42 - 44		0.0			sc	-BECOMES SATURATED
- 46 - - 48 - - 50 -		0.0				
- 52 - - 54 - - 56 -		0.0				
- 58 - - 60 - - 62 -		0.0			SM	SAND, SILTY, SAND, GRAY, MOIST, FINE-GRAINED, WELL-GRADED -SOME LAYERING
20006 SITE 29.GPJ 11/13/07/27/2008 99 99 99 99 99 99 99 99 99 99 99 99 99				7.7.7.7.7.7	CL	CLAY, SILTY, GRAY, DRY, LOW PLASTICITY, HARD SAND, SILTY, SAND, GRAY, MOIST, FINE-GRAINED,
- 40 –		0.0			SM	WELL-GRADED Continued Next Page



00091618

Monitoring Well

29WW39 Page: 3 of 3

Project Longhorn Army Ammunition Plant Owner USACE Location Karnack, Texas Proj. No. 117591 Well Completion USCS Class. Sample ID % Recovery Description Graphic Log Depth (ft.) PID (mdd) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 70 72 74 SM 76 78 ∑ 9.0 LIGNITE, BLACK, LAYERED, ORGANIC 80 SAND, SILTY, SAND, GRAY, MOIST, FINE-GRAINED, WELL-GRADED SM 82 **WELL SET AT 83.5 FEET BGS** 84 LIGNITE, BLACK, LAYERED, ORGANIC РΤ 86 ČLAY, SILTY, LOW PLASTICITY, DARK GRAY, HARD, LAYERED CL END OF BORING - BACKFILLED TO 84' WITH BENTONITE 88 90 92 94 96 98 100 102 104 106 108



Continued Next Page

00091619

Sha	W					Monitoring vvei	Page: 1 of 5
Project _	Longhorn Ai	rmy Ami	munition Plant		_ 0	wner _USACE	COMMENTS
Location	Kamack, 7	exas				Proj. No. <u>117591</u>	Hand augered 0 to 5 feet bgs.
			Total Hole De		16" Shallow Zone Isolation Casing set at 50' bgs.		
Top of Ca	sing <u>232.4</u>	19	Water Level I	nitial 👱	8" Intermediate Zone Isolation		
			Length 10 ft		Casing set at 90' bgs		
Casing: D	ia <u>2 in.</u>		Length 152	ft.		Type Sch. 40 PVC	(Note: 12" Casing stuck at 82'
Fill Materi	al <u>NA</u>				_ Ri	g/Core Mayhew 500/ Mobil B5500	bgs.)
			Met				
						pals Date 9/18/06 Driller # NA	
Checked I	3y <u>K. Ever</u>	ett		Licens	e No.	Texas 379	
			-1>		ø		
Depth (ft.)	Well Completion	€۵	Sample ID % Recovery	를 p	USCS Class.	Description	
P B €	γγ dπο	PID (mdd)	Rec	Graphic Log	တ္တ	(Color, Texture, Structu	ге)
	٥		wl%		ŝ	Geologic Descriptions are Based on	the USCS.
						0' - 31' Description taken from log 29WW1	5, Appendix II of the
						Draft Site Characterization Summary Reports Group 2 Sites Remedial Investigation (RI)	ort for the Phase III
						(FS), Sverdrup, January 2000.	and reasibility Study
L 0 -				777777			
ļ						CLAY, SILTY, MEDIUM BROWN, MOTTL STAINING, BLACK STRIATION, MEDIUM	ED, ROOTS, IRON
L 2 -						MOIST TO MOIST, TRACE GRAVEL	TOTAT, GLICHTET
L 4 -							
4						-BECOMES SOFT AND WET	
 - 6 -					CL	-BECOMES VERY STIFF WITH RED STE	RIATION, SLIGHTLY
-						MOIST	
8 -							
† -					CL	-BECOMES MEDIUM-BROWN TO GRAY	WITH TRACE SAND
- 10 -						AND ROOTS	
† †							
12 -							
F -							
- 14 -							
F -							
16 -							
⊢ 18 −							
'-							
20 -						SAND, SILTY, MEDIUM BROWN WITH G	RAY LAYERS,
			i			MOIST, MEDIUM DENSE TO LOOSE	
[,,]		1					
22					SM		
					CIVI		
24 -							,
26	X X						
<u></u>					GP	GRAVEL, POORLY-GRADED, BROWN, V	
28 -		İ				CLAY, SILTY, MEDIUM-BROWN TO GRA SLIGHTLY MOIST, GOLDEN BROWN LA	Y, LAYERED,
4					CL	CEICHTET MOIOT, GOLDEN DROWN LA	11110



Monitoring Well

00091620 29WW40

Page: 2 of 5

 Project
 Longhorn Army Ammunition Plant
 Owner
 USACE

 Location
 Kamack, Texas
 Proj. No. 117591

Location						Proj. No
Depth (ft.)	Well Completion	PID (mdd)	Sample ID % Recovery	Graphic Log	USCS Class.	Description (Color, Texture, Structure)
	_				→	Geologic Descriptions are Based on the USCS.
- 30 -						Continued
-	\bowtie					31' - 88' Description taken from log 29WW16, Appendix II of the
- 32 -						Draft Site Characterization Summary Report for the Phase III
-						Group 2 Sites RI/FS, Sverdrup, January 2000.
– 34 –					CL	
-						
- 36 -						
-						
- 38 -					SC	
40					30	CLAY, SANDY, MEDIUM BROWN TO GRAY, LAMINATED, SLIGHTLY MOIST TO MOIST, SOME SILT, STIFF
- 40 -						CLAY, SILTY, DARK GRAY, VERY STIFF, TRACE SAND,
40						SLIGHTLY MOIST TO MOIST
- 42 -						
- 44 -						
444					CL	
- 46 -						
– 48 –						
'						
- 50 -						- 16" SHALLOW ZONE ISOLATION CASING SET AT 50' BGS
-					ML	SILT, CLAYEY, SOME SAND, MEDIUM GRAY, MOIST
– 52 –						CLAY, SILTY, SOME SAND, MEDIUM GRAY, MOIST, STIFF, ———
					CL ML	LAMINATED
- 54 -					PT	L LIGNITE, BLACK, LAYERED
						CLAY, SILTY, DARK BROWN WITH BLACK INTERMITTENT
- 56 -						ORGÁNIC CÓNTENT, VERY HARD, HIGH PLASTICITY, SLIGHTLY MOIST
						SEISTIE MOIOT
⊢ 58 ~						
 						
60 -						
		i				
<u></u>					CL	
¥ , 1						-PŁASTICITY INCREASES
= 64 						
SITE 29.GPJ 14/13/07						
86						
- 88						
÷ 70						Continued Next Page



Monitoring Well

00091621 29WW40

Page: 3 of 5

Project Longhorn Army Ammunition Plant Owner _USACE Location Karnack, Texas Proj. No. __117591 Well Completion USCS Class Description Graphic Log Zept (₹) PP (mdd (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued 70 72 74 76 SILT, SAND, MEDIUM GRAY, SLIGHTLY MOIST, DENSE CLAY, SILTY, DARK GRAY AND DARK GREENISH-GRAY. CL 78 TRACE SAND, SLIGHTLY MOIST, TRACE GRAVEL AND 29WW40 100% 129.2 SAND, SILTY, MEDIUM GRAY, WET, MEDIUM DENSE TO DENSE, TRACE GRAVEL 80 SAND, POORLY-SORTED, MEDIUM GRAY, WET DENSE SC 82 CLAY, SANDY WITH SILT, MEDIUM TO DARK GRAY. CL LAMINATED, MOIST ML CLAY, SILTY, MEDIUM GRAY, SLIGHTLY MOIST, VERY STIFF 84 SILT, SANDY, MEDIUM GRAY, TRACE CLAY, SLIGHTLY CL CLAY, SILTY, MEDIUM GRAY, TRACE SAND, SLIGHTLY MOIST, VERY STIFF, LAMINATED 86 SM SAND, SILTY, MEDIUM GRAY, MOIST CL CLAY, SILTY, MEDIÚM GRAY, SLIGHTLY MOIST 88 CLAY, SANDY, MEDIUM GRAY, SLIGHTLY MOIST Treatability St 105 - 8" INTERMEDIATE ZONE ISOLATION CASING SET AT 90' 90 3.2 **BGS** -BECOMES SILTY, LOW PLASTICITY, HARD 92 94 96 98 CL -INCREASING SILT 100 9.5 102 104 106 108 Continued Next Page



Monitoring Well

00091622 29WW40

Page: 4 of 5

Project Longhorn Army Ammunition Plant Owner USACE Location Kamack, Texas Proj. No. <u>117591</u> Well Completion USCS Class. Sample ID % Recovery Description Graphic Log Cft.) PID (mdd) (Color, Texture, Structure) Geologic Descriptions are Based on the USCS. Continued -110 SAND, SILTY, MOIST, FINE-GRAINED, WELL-GRADED, GRAY 2.5 112 -114 ŞМ 116 -118 120 CLAY, SILTY, GRAY, MOIST, LOW PLASTICITY, HARD 122 124 126 128 130 2.5 132 134 136 138 140 LIGNITE, HARD, BLACK, HIGHLY ORGANIC 2.0 142 144 146 SAND, SILTY, LIGHT GRAY, VERY FINE-GRAINED, MOIST 148 Continued Next Page



Monitoring Well

00091623 29WW40

Page: 5 of 5

Project Longhorn Army Ammunition Plant Owner USACE

Location Karnack, Texas Proj. No. 117591

Location	катаск, г	exas				Proj. No. <u>117591</u>
Depth (ft.)	Well Completion	OId (mdd)	Sample ID % Recovery	Graphic Log	USCS Class.	Description (Color, Texture, Structure) Geologic Descriptions are Based on the USCS.
- 150 152 154 154 156 160 160 160 160 160 160 160 160 160 170			Sal		OSN &M C	
Ę						

Attachment 2 Monitoring Well Development Records

WELL DEVELOPMENT RECORD

WELL/PIEZOMETER ID 21 WW 35
SHEET (OF)

		•		SHEET	_ OF
PROJECT NAME: Longh	PROJECT NO	o.: 117591. O	006 A 160 D	ATE: 4/18/	06
LOCATION: Karnack	Tx DATE INSTAL	LED:	06	<u> </u>	<u>.</u>
TOTAL DEPTH (FTOC)	CASING DIA	METER	4" PV	<u>د</u>	
METHODS OF DEVELOPMENT	<u>r</u>				
Swabbing Supplies Swabbing Swabbing Supplies Swabbing Supplies Swabbing Swa	Bailing Pum		escribe	lo .	
Describe					<u> </u>
EQUIPMENT NUMBERS pH Meter YS/ CASING VOLUME INFORMATION	EC Meter <u>Y\$/</u> ON:	Turbidity Mete	er <u>YS/</u>	Thermometer	<u>Y31</u>
	1.0 1.5 2.0 0.04 0.09 0.16	2.2 3.0 0.2 0.37	4.0 4.3 0.65 0.75	5.0 6.0 1.0 1.5	7.0 8.0 2.0 2.6
PURGING INFORMATION			111	artini (patagalasy)	- A consist or approximate a
Measured Well Depth B	95'	ft.] []	1
Measured Water Level Depth (C)	29.6	ft.		<u> </u>	***************************************
Length of Static Water Column (D)	95 - 29.6	= 65,4 ft.	W ₁ O]^	EVATION (FTOC)
Casing Water Volume (E)	(A) × 65.4	<u>'</u> = <u>42.57</u> ga	L		
Total Purge Volume =	gal 42.51 y	x5-213 gold	ens =	LEVATION	MEAN SEA

Date	Time	Water Level (FTOC)	Volume Removed (gal)	ρН	EC	Temperature F or C	Turbidity/ Sand (ppm)	Comments
9/18	11:19		5	8.39	497	21.99	400.2	
Ī	11:42		40	8,05	.832	71.73	1551.8	
	11.57		60	8.01	ROX	23.24	291.2	
	409		85	9.05	818	22 23	137.1	
	Hai		135	7.87	805	32.09	18,2	
	1441		160	7.85	.814	21.95	10.6	
	12:19		190	7,90	.દ્વરા	22.09	57.6	
	15:33		ا إ	7.8	.827	2161	8.9	
1	15:52		250	7.84	822	21.30	5.6	
	16:32		270	7.76	1818	21.23	47.1	
	16:45	•	280	7.85	.84K	20.56	19.7	

WELL DEVE	LOPMENT F	RECORD	WELL/PIE SHEET	ZOMETE	R ID 2º	1WW3
PROJECT NAME: Linehovn PROJECT NO LOCATION: LHANF-27 DATE INSTALL	D.: 117591.0	007A160 40L	DATE: _	9/15/	66	
TOTAL DEPTH (FTOC) CASING DIA	•	·				
METHODS OF DEVELOPMENT Swabbing Bailing Pum Equipment decontaminated prior to development Describe		Describe	No			
EQUIPMENT NUMBERS pH Meter YSI EC Meter YSI CASING VOLUME INFORMATION: Casing ID (inch) 1.0 1.5 2.0	2.2 3.0	er \\S\!		mometer _	YS 1	8.0
Unit Casing Volume (A) (gal/ft) 0.04 0.09 0.16 PURGING INFORMATION Measured Well Depth B Measured Water Level Depth (C) Length of Static Water Column (D) Casing Water Volume (E) Total Purge Volume = gal	ft = 0.02 ft $= 5.213 g$ $= 5.25 g$	al 213 = -	STATIC ELEVATION	1.5	ATION OC.	
	26.	065 Sallons				

Date	Time	Water Level (FTOC)	Volume Removed (gal)	рH	EC	Temperature F or C	Turbidity/ Sand (ppm)	Comments
416/06	lo; oc			608		20.85	13.2	
	10:33	-		6.79		1963	538,2	
Ц	10:53			681		195	407	
\Box	ii. 31	34.19		6.91		2156	830,7	
\Box	12.00	34.2		6.97		20.9	2593	
V	12:40	134.4		7.13		20,82	15367	
	13.11	34.55		9.87		10.51	259.5	
		9						
						! 		
	L							

37.95

	WELL/PIE SHEE	EZOMETER ID 29WW3
PROJECT NAME: Conshorn PROJECT NO.: 17591 LOCATION: Kay nack Tx Date Installed: 9/8/06	DATE: _	9/19/06
LOCATION: KGV nack, Tu DATE INSTALLED: 9/8/06		·
TOTAL DEPTH (FTOC) 85.25 CASING DIAMETER 4" PUC		
METHODS OF DEVELOPMENT		
Swabbing Bailing Pumping Describe		
Equipment decontaminated prior to development Yes	No	
Describe		·
EQUIPMENT NUMBERS		
pH Meter 45/ EC Meter 15/ Turbidity Meter 45/	Ther	mometer <u>YSI</u>
CASING VOLUME INFORMATION:		
Casing ID (inch) 1.0 1.5 2.0 2.2 3.0 4.0 4.3 Unit Casing Volume (A) (gal/ft) 0.04 0.09 0.16 0.2 0.37 0.65 0.75		6.0 7.0 8.0 1.5 2.0 2.6
PURGING INFORMATION		The state of the s
Measured Well Depth B \$5.25 ft.		
Measured Water Level Depth (C) 37.45 ft.	S CALLES TO MAKE THE REST	
Length of Static Water Column (D) 85.25 - 37.95 = 47.3 ft.	. 不甘	SLEVATION (PTOC)
Casing Water Volume (E) $\frac{.65}{(A)} \times \frac{.47.5}{(D)} = \frac{30.14}{gal}$		
Total Purge Volume = gal 30.74 47 od ums	ELEVATION	MEAN SEA
215 18		LEVEL

Date	Time	Water Level (FTOC)	Volume Removed (gal)	рH	EC	Temperature F or C	Turbidity/ Sand (ppm)	Comments
419/00	956		4	9.68	156	18.83	-12.3	***
	1033		45	8.61	<i>15</i> 7	19.33	1519.8	
	0.50		55	9.54	810	9.65	1524.3	·
	/l;\23		75	8.73	100	20.44	15344	
	1337	· · · · · · · · · · · · · · · · · · ·	90	8.42	669	21.81	1552.4	· · · · · · · · · · · · · · · · · · ·
	14:06		145	821	Wi	2/29	9564	
	56		185	82	570	22.78	1564.8	
	15:45	·	205	8.05	,586	10.33	278.5	
	16:15		235~	799	575	20.43	50.3	
	1640		250	811	510	2036	12.2	
4	17:04	*	280	9.04	.569	148	207	

WELL DEVE	-OPMENT	RECORD
------------------	----------------	--------

	WELL/PIEZOMETER ID 79いい38 SHEET OF 4
PROJECT NAME: Longhern PROJECT NO.: 117591.0007A 100	DATE:
LOCATION: LHAAP DATE INSTALLED: 8/26/06	
TOTAL DEPTH (FTOC) CASING DIAMETER	
METHODS OF DEVELOPMENT	
Swabbing Bailing Pumping Describe	
Equipment decontaminated prior to development Yes	No
Describe Equipment decounsed by 3-step ringe alkanox + water	er potable water, DI Water.
EQUIPMENT NUMBERS	<i>V</i> ₁ ,
OH Meter YSI Turbidity Meter YSI	Thermometer YS1
CASING VOLUME INFORMATION:	
Casing ID (inch) 1.0 1.5 2.0 2.2 3.0 4.0 4.3 Unit Casing Volume (A) (gal/ft) 0.04 0.09 0.16 0.2 0.37 0.65 0.75	
PURGING INFORMATION	The state of the s
Measured Well Depth B 45.44 ft. bgs	
Measured Water Level Depth (C) Z 7, 3 8	
Measured Water Level Depth (C) $\frac{27.30}{13.140}$ Length of Static Water Column (D) $\frac{40.44}{0.5} - \frac{27.30}{13.14} = \frac{8.544}{11.14}$ Casing Water Volume (E) $\frac{0.65}{(A)} \times \frac{13.14}{(D)} = \frac{3.544}{11.14}$ Casing Water Volume (E) $\frac{0.65}{(A)} \times \frac{13.14}{(D)} = \frac{3.544}{11.14}$	e ELEVATION (FIGE)
Casing Water Volume (E) $0.65 \times 13.14 = 42.505 \text{ gal}$	
Total Purge Volume = 42.79 Fal 8.341 * 5	STATIC ELEVATION MEAN
न पर ज़े व दुवी।	SEA LEVEL
1000	vy .

Date	Time	Water Level (FTOC) 77.30	Volume Removed (gal)	pH	EC	Temperature F or C	Turbidity/ Sand (ppm)	Comments
111604 114164 116766	10:31	7 Dry	P 501/095	6.801	0.6 <i>7</i> 5 5 <i>8</i> 3 7 1.041	18.99 19.21 19.5	20.68 14323. 1443.7	very silt
	12:10 12:40 13:35		24 32 40 7	7.84 5.55 5.1	0.733 0.74 05°	19.94 118.90 170.66	50.3 731.3	brownsit brownsit
						12	() () () () () () () () () ()	

20.73

WELL DEVEL	OPMENT.	RECORD
-------------------	---------	--------

						W	/ELL/PII SHEE	EZOMET	ER ID 4 OF	<u> </u>
PROJECT NAME: Longh LOCATION: Karrack TOTAL DEPTH (FTOC)	10(n P	ROJECT NO	.: 117	1591.0	006	160 D	ATE: _	9/18/1	06	
LOCATION: Karmack	₹\$ D	ATE INSTAL	LED:	9	1/14/0	6				
TOTAL DEPTH (FTOC)	5−95′ c	ASING DIA	METER		4	" PVC				
METHODS OF DEVELOPMEN										
Swabbing Equipment decontaminated pri	_	Pump Priment	oing	=	Describe 'es	N	0			
Describe		···								<u></u>
EQUIPMENT NUMBERS pH Meter YS/	EC Meter	451	. Turb	oidity Mete	er <u>7</u> 5	<u>/</u>	The	mometer	43,	
CASING VOLUME INFORMAT	<u>'ION;</u>									
Casing ID (inch) Unit Casing Volume (A) (gal/ft)	1.0 1.5 0.04 0.09		2.2 0.2	3.0 0.37	4.0 0.65	4.3 0.75	5.0 1.0	6.0 1.5	7.0	8.0 2.6
PURGING INFORMATION					, · <u> </u>		18 - 4	·	- 107 - Graza i j	
Measured Well Depth B	95	· /	fi	t.				*	T	
Measured Water Level Depth (C)		29.6				h 0 0				
Length of Static Water Column (D)	95	- 29.6	= 65	<u>, 4</u> ft.		н _г о	^ †	ELE (I	VATION PTOE)	4
Length of Static Water Column (D) Casing Water Volume (E)		x <u>65.4</u>	= 4	2.5 / ga	ř		J	\		
Total Purge Volume =	gal	42.51 ×	5-2	12/	9		EVATION		MEA	Ď.

Date	Time	Water Level (FTOC)	Volume Removed (gal)	Hq	EC	Temperature F or C	Turbidity/	0
9/18	11:14	(1,100)	5 981/	8.39	497	21.94	Sand (ppm)	Comments
71.4	11:42		40	8,05	832	21.72	15518	
	11.57		60	8.01	ROR	22.24	291.2	
	1402		85	8.05	818	<u> </u>	137.1	
	1421		135	7.87	805	32.09	18,2	
	1441		160	7.85	.814	21.95	10.6	
	12.0		190	7.90	.822	22,09	57.6	
	<i>15.33</i>		210	7.8	<u>.827</u>	2161	8.9	
	15:52	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	250	7.84	822	21:30	5.6	
	:6:32		270	7.76	18181	21.23	47.1	
	16:45		280	7.85	.84K	20.56	19,3	

WELL DEVELOPMENT RECORD Continued

1240 5.88 1.04 1062 7.56 C 1300 5.88 1.04 1062 7.56 C 1300 5.91 1.03 20.69 C.25 1	902.9 119.8 74.5 85.7
9/23 1) 00 53.48 1.01 20.73 6.33 6 1220 5.40 1.05 20.65 6.72 6 1240 5.88 1.04 2062 7.56 6 1300 5.91 1.03 20.69 (.25 1	119.8 74.5 95.7 81.7
1240 5.88 1.04 10362 7.56 5 1300 5.91 1.03 20.69 (.25 1	119.8 74.5 95.7 81.7
1240 5.88 1.04 10362 7.56 5 1300 5.91 1.03 20.69 (.25 1	74.5 95.7 81.7
1300 5.91 1.03 20.69 (.25)	81.7
1320 103 103 10055 784	81.7
	81.7
+ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$	21/2
14/10 5,9 1038 20.7 7.86 5	70.♥ +
	4.8 8.7
1990 5.9 103 20.13 7.89 3	28.7
1490 5.9 103 20.73 7.93 3 1500 4300 gal. 5.9 1.03 20.74 7.90 3	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
500 300 gal. 5,9 1,03 20.74 7.90 3	9.2

WELL DEVELOPMENT RECORD	WELL/PIEZOMETER ID 29649 SHEET OFOF
PROJECT NAME: Longhorn PROJECT NO.: 17591 LOCATION: Kannack TA DATE INSTALLED: 9/11/06	DATE: 9/20/06
TOTAL DEPTH (FTOC) 159' bg CASING DIAMETER 4 21 P	
METHODS OF DEVELOPMENT Swabbing Bailing Pumping Describe Equipment decontaminated prior to development Yes Describe	No
EQUIPMENT NUMBERS pH Meter YS	Thermometer Y51
Casing ID (inch) 1.0 1.5 2.0 2.2 3.0 4.0 4.3 Unit Casing Volume (A) (gal/ft) 0.04 0.09 0.16 0.2 0.37 0.65 0.75	5.0 6.0 7.0 8.0 1.0 1.5 2.0 2.6
PURGING INFORMATION Measured Well Depth B Measured Water Level Depth (C) Length of Static Water Column (D) Casing Water Volume (E) Total Purge Volume = gal 159 ft. 160 159 ft. 180 180 180 180 180 180 180 18	ELEVATION (FTOC) STATIC ELEVATION MEAN SEA LEVEL

Date	Time	Water Level (FTOC)	Volume Removed (gal)	pH //90	EC	Temperature F or C	Turbidity/ Sand (ppm)	Comments
)	11:04 11:30 11:30		100	3.75 8.57 8.36 9.29 9.19		(9.74 21-17 20.00 19.8 14.7	70.3 229.3 3.9 3.6	
							201	

Attachment 3

Activated Persulfate Oxidation Treatability Study Report



ACTIVATED PERSULFATE OXIDATION TREATABILITY STUDY REPORT

LHAAP-29

Prepared By:

Shaw Environmental, Inc.

Technology Development Laboratory
304 Directors Drive
Knoxville, TN 37923

Project No. 117591.0006A200

00091634

Acronyms and Abbreviations

°C degrees Celsius

μg/kg micrograms per kilogram

BTEX benzene, toluene, ethylbenzene, and xylenes

Cl⁻ chloride ion

E° reduction potential

FeEDTA Iron (II) ethylenediamine tetra acetic acid

g gram

g/L grams per liter

GC/FID gas chromatography with flame ionization detector

HSO₄ hydrogen sulfate

ISCO in-situ chemical oxidation

kg kilogram

MCL maximum contaminant level

MeCl₂ methylene chloride meq milliequivalents

mg/kg milligrams per kilogram mg/L milligrams per liter

mL milliliter

Na₃PO₄ sodium phosphate OH• hydroxyl radical

Shaw Environmental, Inc.

 $(S_2O_8)^{-2}$ persulfate ion SO_4^{-2} sulfate ion $SO_4\bullet^-$ sulfate radical

SOD soil oxidant demand

SOP standard operating procedures

TDL Technology Development Laboratory

UV ultraviolet V volts

VOC volatile organic compound

1.0 Introduction

The groundwater in the intermediate water-bearing zone at the LHAAP-29 site is contaminated with methylene chloride. Shaw Environmental, Inc. (Shaw) conducted a bench-scale treatability study to evaluate the effectiveness of in-situ chemical oxidation (ISCO) using activated sodium persulfate to treat the methylene chloride at the site. The treatability study was performed at Shaw's Technology Development Laboratory (TDL) in Knoxville, TN. This report describes treatability testing procedures and presents the results.

2.0 Technology Description

Persulfate ion $(S_2O_8^{-2})$ is a strong oxidant capable of oxidizing most organic compounds to carbon dioxide and other mineral products. The standard reduction potential for the half reaction shown below is +2.01 volts (V).

$$S_2O_8^{-2} + 2e^- \rightarrow 2SO_4^{-2}$$
 $E^{\circ} = +2.01 \text{ V}$

It is on the same order as ozone and higher than for permanganate and hydrogen peroxide, but less than the hydroxyl radical (Fenton's reagent intermediate). As shown in the half reaction above, the product of persulfate reduction is sulfate ion (SO₄-2), which is a relatively benign species. Sulfate ion has a secondary federal drinking water standard maximum contaminant level (MCL), which is a recommended but unenforceable limit, of 250 milligrams per liter (mg/L). During in situ treatment the solubility of sulfate may be limited by natural calcium concentrations, which can precipitate a fraction of the aqueous sulfate concentration as calcium sulfate dihydrate.

It is believed that persulfate reacts with organic compounds primarily by the sulfate radical $(SO_4\bullet^-)$, which can be generated in solution by several mechanisms. The sulfate radical, shown in the reaction below, is a powerful oxidizing species with a standard electrode reduction potential of +2.6 V, which is similar to that for the hydroxyl radical $(OH\bullet)$ species (+2.8 V).

$$SO_4^{\bullet^-} + e^- \rightarrow SO_4^{-2}$$
 $E^{\circ} = +2.6 \text{ V}$

The hydroxyl radical is a powerful oxidizing species that is generated with catalyzed hydrogen peroxide systems. The persulfate anion radical in contrast to the hydroxyl radical has a longer lifetime in solution and is more selective in its reactions (P. Neta, 1987). Generation of the sulfate radical may be accomplished by homolytic scission of the persulfate ion, which can be

activated by heat or ultraviolet (UV) radiation (G. E. Hoag, 2000; P. Neta, 1987 and C. Liang, 2001):

$$S_2O_8^{-2}$$
 or $O_4S-SO_4 \rightarrow 2SO_4^{-1}$

Heat activation can be accomplished at temperatures in the range of 20°C to 60°C, which can be accomplished in situ without extreme heat generation processes. Steam heating has been used as a practical means to provide persulfate activation for in situ treatment.

Sulfate radicals may also be generated by one-electron oxidation reactions, such as with metals (C. Liang, 2001; FMC, 2001 and G. E. Hoag, 2000):

$$S_2O_8^{-2}$$
 or $O_4S-SO_4^{-1} + M^{+n} \rightarrow SO_4^{-1} + SO_4^{-2} + M^{+(n+1)}$

Recently, new methods of persulfate reaction activation have been developed using: chelated metals, such as iron (II) ethylenediamine tetraacetic acid (FeEDTA), hydrogen peroxide addition, or an alkaline pH (P. Block, 2004). These new methods most likely also involve the generation of the sulfate radical and possibly the hydroxyl radical and related species for reaction with organic compounds.

Metal complex activation of persulfate has been effective in treating aromatics and chlorinated ethenes, but chlorinated ethanes and chlorinated methanes have proven to be somewhat resistant to persulfate with this form of activation (P. Block, 2004). The chemistry of peroxide activation of persulfate is not clearly understood and results with the reagent combination mixture seem to be promising.

Alkaline activation of persulfate has been shown to be most effective for the treatment of chlorinated ethane and chlorinated methane compounds. Alkaline activation uses a base such as sodium hydroxide to adjust initial pH in the range of 11 to 12.5. The alkaline conditions are typically neutralized during treatment by the generation of hydrogen sulfate anion (HSO₄⁻), which is an acid. This occurs during natural decomposition of the persulfate reagent that is catalyzed by high pH and species present in the soil. The equation for the decomposition reaction is shown below.

$$\mathrm{S_2O_8}^{-2} \ + \ \mathrm{H_2O} \ \rightarrow \ 2\mathrm{HSO_4}^{-} \ + \ {}^{1}\!\!/_{2} \, \mathrm{O_2}$$

Testing results show that persulfate can be effective on recalcitrant organics. Specifically, persulfate has been shown to degrade BTEX, chlorinated ethenes, chlorinated ethanes and

chlorinated methane compounds such as the methylene chloride detected at LHAAP-29 (C. Liang, 2001 and P. Block, 2004).

The persulfate reagent is very soluble in water to concentrations of 30 to 40 percent and the solutions are relatively stable especially at lower concentrations (1 to 10 percent). These properties allow for optimum delivery and distribution to the subsurface matrix without the solubility limitations encountered with potassium permanganate. The reagent is similar to permanganate with respect to safety issues (e.g., handling and reactivity); however, there are materials of compatibility consideration due primarily to the potential for low pH from persulfate reactions

3.0 Treatability Study and Approach

Testing was conducted to evaluate activated persulfate oxidation for the treatment of methylene chloride in soil and groundwater slurries. The two activation methods tested were heat activation and alkaline activation.

4.0 Objectives

The objectives of the bench-scale treatability tests were the following:

- Evaluate treatment effectiveness of heat-activated persulfate and alkaline activated persulfate for destruction of methylene chloride in soil/groundwater slurries;
- Provide an estimate of the oxidant dosing requirements by measuring the soil oxidant demand (SOD);
- Measure the alkaline buffering capacity of the soil to determine the dose of caustic required to increase pH to above 10.5 for persulfate activation.

5.0 Experimental Design and Procedures

The experimental approach was as described below and entailed site soil preparation, characterization of test soils and groundwater, SOD tests, acid/base titration of site soil and reagent treatment effectiveness tests on soil and groundwater mixtures.

5.1 Treatability Study Sample Collection and Homogenization

Monitoring well 29WW16 is an intermediate zone well approximately 90 feet deep and contains an extremely high concentration of methylene chloride. Water from this well was collected for the treatability study to ensure that the water contained high concentrations of methylene

chloride. The soil for the treatability study was collected during drilling for deep well 29WW40, from the same soil interval where 29WW16 is installed.

Soil and groundwater samples were received at the TDL on September 12 and September 22, 2006 respectively. The samples were shipped on ice and stored at the TDL at 4°C until used in treatability testing. Samples were identified as follows:

Client Sample ID	<u>Type</u>	Amount	TDL Lab #
29WW40	SOIL	5 KG	10762
29WW16	GW	10×1 -LITER	10828

The samples of soil received for batch slurry testing were mixed manually in the plastic container to apparent homogeneity at 4°C in a manner to minimize volatile organic compounds (VOC) loss. The 10 liters of site groundwater collected were homogenized in a sterile chilled glass container. Samples were stored with zero headspace at 4°C prior to testing. The homogenized site groundwater and site soil was sampled for VOCs of concern using a modified EPA SW-846 Method 8015, which uses purge-and-trap gas chromatography with flame ionization detection methodology (GC/FID).

The soil sample was also analyzed for alkalinity/buffering capacity at the TDL using laboratory standard operating procedures (SOP). These measurements were used to determine the amount of base needed to adjust pH conditions of the alkaline activated test systems to desired values and were used to determine sodium hydroxide dose for SOD and treatment effectiveness tests.

5.2 Soil Oxidant Demand Testing

SOD tests were performed to measure the amount of oxidant consumed in the course of treatment to destroy the target VOCs. The amount and rate of oxidant consumption is used to determine oxidant dosing and reaction condition requirements for treatment. The soil composite was used to measure the SOD with alkaline activated persulfate. Tests were performed on soil/groundwater slurries containing 200 g of soil and 200 mL of groundwater in 500-mL polyethylene sample bottles. The soil sample was also analyzed for percent solids. Two SOD tests were set up: alkaline activated persulfate SOD by adding 10 g of sodium persulfate and 2 mL of 50% (by weight) sodium hydroxide solution, resulting in a starting concentration of 50 g/L sodium persulfate and 0.5% sodium hydroxide, and peroxide activated persulfate SOD with 50 g/L persulfate and 119 g/L hydrogen peroxide (molar ratio of persulfate to peroxide = 1:5). The test bottles were capped, placed onto a temperature controlled oscillating shaker table at 15°C and mixed periodically for the duration of the test. The sodium persulfate concentration

was measured on a weekly basis by titrating 0.5 mL aliquots of the sample following laboratory SOP. Another 5 g of sodium persulfate was added on day 12 when its concentration dropped to 6.045 g/L.

Periodically, a small portion of the liquid (0.5-1 mL) from each test was sampled for persulfate analysis to determine the amount of oxidant consumed as a function of time to define the consumption characteristics for each oxidant system. Because of the impact of pH on persulfate and the potential for a pH decrease during treatment resulting from persulfate degradation, the pH of the sample was also monitored every two to three days and more sodium hydroxide solution (50% by weight) was added when the pH dropped to below 10. Tests were monitored for about a 4 week time period using sample points of 5, 7, 9, 12, 14, 21, 29 and 36 days.

5.3 Oxidation Effectiveness Tests

Slurry tests using alkaline and/or heat activated persulfate were performed on site soil and groundwater mixtures. The bench scale testing designed to evaluate the two activation methods is described in detail below.

The test samples were prepared by mixing 100 g site soil and 150 mL groundwater in 210 mL test bottles. A small volume of headspace was left in each bottle to allow for slurry mixing. Initial characterization of site soil and groundwater indicated the methylene chloride concentration was 7 g/L in groundwater and non detectable in soil (10 µg/kg detection limit). The stoichiometric demand for 7 g/L methylene chloride oxidation is 42 g/L sodium persulfate. Considering the SOD, a persulfate dose of 50 g/L was used in this test. All test bottles were allowed to equilibrate overnight before adding any reagent. All bottles were hand mixed periodically at 24 to 72 hour intervals by gently turning each bottle end over end. Test bottles were temperature controlled at 15°C for the test duration.

Alkaline activation

Four bottles were prepared for alkaline activated persulfate oxidation. One bottle was amended with 7.5 g sodium persulfate and 1.5 mL 50% sodium hydroxide, one bottle was amended with 1.5 mL 50% sodium hydroxide alone to serve as an alkaline control, and another two without any amendment to serve as initial and final time point controls.

At pre-determined sampling points, T-0 and T-14 days, the reaction was quenched by placing the test bottle in the refrigerator at ~4°C. The low temperature also helps to minimize the volatilization loss of VOC of concern. A portion of the water phase was transferred to 50 mL plastic vials for analysis for remaining persulfate and pH. Both the soil and groundwater phases

were sampled for VOC analysis. The soil phase was also analyzed for moisture content. **Table 5-1** below describes the slurry batch tests and sampling schedule.

Table 5-1
Alkaline-Activated Persulfate Oxidation Batch Test Experimental Details

Test	Sodium persulfate conc.	Temperature (°C)	Sample Points (Days)		Soil (g)	Water (ml)	Sodium persulfate	50% Sodium hydroxide
	(g/L)		T-0	T-14			(g)	(mL)
С	0	15	X	X	100	150	0	0
СВ	0	15		X	100	150	0	1.5
В	50	15		X	100	150	7.5	1.5

Heat activated persulfate oxidation at 60°C

Three bottles (2 sampling points and one control) were prepared for heat activated persulfate oxidation at 60°C. Two of them were amended with 7.5 g sodium persulfate to result in a nominal concentration of 50 g/L. The third had no amendment to serve as a heated control. All three test bottles were placed in the oven set at 60°C. The temperature inside the oven was monitored on a daily base and it varied between 59°C and 61°C.

Once the pre-determined treatment time had elapsed, the test bottle(s) was placed in the refrigerator at \sim 4°C to quench the persulfate reaction. The sample was then prepared for analyses as detailed above for the alkaline activation tests. **Table 5-2** below describes the slurry batch tests and sampling schedule for the heat activated tests.

Table 5-2 Heat-Activated Persulfate Oxidation (60°C) Batch Test Experimental Details

Test	Sodium persulfate conc.	Temperature (°C)	_	Sample Points (Days)		Water (ml)	Sodium persulfate
	(g/L)		T-7	T-14			(g)
СН	0	60		X	100	150	
Н	50	60	X	X	100	150	7.5

Heat and alkaline activated persulfate oxidation at 40°C

The above two treatment options were not very successful in oxidizing the methylene chloride in groundwater. Therefore, another batch of tests was setup to evaluate the combined persulfate activation methods of heat and alkaline. However, to reduce the rate of persulfate degradation, in an attempt to increase the persulfate radical longevity, the heat was reduced from 60°C to 40°C. Four bottles were prepared in this batch, one was set at room temperature to serve as a control without amendments to monitor volatilization loss, one heated control was setup without amendment to monitor if heat accelerated the loss of methylene chloride, and the remaining two

bottles were established for heat activated persulfate with alkaline catalysts of sodium phosphate (Na₃PO₄) and sodium hydroxide, respectively. The two treated samples were amended with 9.0 g sodium persulfate to result in a nominal concentration of 60 g/L. Sodium phosphate was added to get a concentration of 62 g/L. For sodium hydroxide activation, the dose was double that of the previous batch by adding 3 mL of 50% sodium hydroxide solution to get a concentration of 15 g/L (density of 50% sodium hydroxide is 1.5 g/mL). The doses of both alkaline catalysts were equal to the stoichiometric demand to neutralize the protons released from the degradation of 60 g/L sodium persulfate. The heated control and the two treated samples were placed in an incubator set at 40°C.

The sampling point for all tests in this batch was 7 days. After 7 days, all the test bottles were placed in the refrigerator at \sim 4°C to quench the persulfate reaction. The samples were then prepared for analyses as detailed above for the alkaline activation tests. **Table 5-3** below describes the slurry batch tests and sampling schedule for the heat and alkaline activated tests.

Table 5-3
Heat and Alkaline Activated Persulfate Oxidation (40°C) Batch Test Experimental Details

Test	Sodium persulfate conc. (g/L)	Temperature (°C)	Sampling point 7 days	Soil (g)	Water (ml)	Sodium persulfate (g)	Alkaline catalyst
C-7	0	22	X	100	150	0	NA
CH-7	0	40	X	100	150	0	NA
PP-7	60	40	X	100	150	9	21.6 g Na ₃ PO ₄ •12H ₂ O
PH-7	60	40	X	100	150	9	3 mL 50% NaOH

6.0 Results

6.1 Sample Characterization Results

Results from the VOC analyses of site soil and groundwater sample composites determined there was 7,113 mg/L (~7 g/L) methylene chloride in the groundwater and non-detectable VOCs in soil, which is consistent with the previously reported contaminant levels. Soil buffering capacity test indicated sodium hydroxide dose of 120 milli-equivalents (meq) per kg soil increased the pH of the soil/groundwater slurry to 11.46. A sodium hydroxide dose of 125 meq per kg soil was used in the alkaline activated SOD and treatment effectiveness tests. Measurement data for the soil buffering capacity are included in **Attachment 1**.

6.2 Soil Oxidant Demand Results

Results from the SOD tests are tabulated below in **Table 6-1** and included in **Attachment 2**. The value given is the total grams of persulfate consumed per kilogram of wet soil.

The SOD tests indicated rapid oxidant consumption. On day 12, the persulfate concentration in the alkaline-activated sample dropped from the initial 41.3 g/L to 6.05 g/L. The sample was then redosed with another 5 g of persulfate. As measured on day 36, the SOD was 54.7 g persulfate per kg of wet soil.

Table 6-1
Summary of Persulfate Consumption Rates in SOD Tests

Test	Description ^a	Oxidant consumption g oxidant / kg wet soil		
Alkaline activation	50 g/l persulfate + 50 g/L sodium hydroxide	54.7 ^b		
Peroxide activation	50 g/L persulfate + 119 g/L hydrogen peroxide	> 50°		

^aBoth tests in 200 g soil composite: 200 mL GW;

The pH behavior from the persulfate tests is typically characterized by a shift to low pH over time. This is caused by the acid product from persulfate decomposition and the low site soil buffering capacity. This is particularly of concern in alkaline-activated persulfate oxidation. The pH of the alkaline-activated sample dropped to 7.22 on day 7, so 2 mL of 50% sodium hydroxide solution was added to increase the pH. Sodium hydroxide was again re-dosed on day 9 and day 28 by adding 1 mL 50% sodium hydroxide. This is consistent with the high persulfate SOD, which produces protons and lowers the pH of the system.

A SOD sample with hydrogen peroxide activated persulfate was set up with 50 g/L persulfate and 119 g/L hydrogen peroxide (molar ratio of persulfate to peroxide = 1:5). The persulfate was depleted to non-detectable levels (detection limit 30 mg/L) on day 6 and the pH dropped to 2.44, due to the rapid decomposition of persulfate with the presence of peroxide. As a result, this activation option was eliminated in the subsequent treatment effectiveness test. Nevertheless, this SOD sample was analyzed for methylene chloride and inorganic anions and the results were discussed in this report.

^bBased on measurement on day 29;

^cbased on measurement on day 6 when no persulfate was detected in the sample and this sample was terminated.

6.3 Batch Slurry Test Results

The analytical results are summarized below in **Table 6-2**. Initial sample characterization indicated that the percent solids on the site soil composite was 79.0%, and that methylene chloride concentration was 7,113 mg/L in the groundwater composite, and 56.2 µg/kg in the soil composite. The methylene chloride concentration measured in the initial baseline control sample decreased to 5,611 mg/L, probably due to systematic loss during test set up and sampling procedure. This value was used as the initial methylene chloride level to calculate the treatment efficiency.

Table 6-2
Analytical Results of Methylene Chloride Treatment Effectiveness Tests

Treatment	Sample ID	Chloride	Sulfate	Persulfate	pН		ylene ride
Treatment	Sample 13	mg/L	mg/L	mg/L	pii	water mg/L	dry soil mg/kg
0 day control	C-0				8.05	5611	0
14 days control	C-14	217.5	290.27	0	7.92	4133	0
14 days base control	CB-14	221.72	81.06	0	12.58	5762	0
14 days base-activated persulfate	B-14	284.72	17408.72	16,452	9.22*	5279	0
14 days heated control	CH-14	274.2	40.43	0	7.25	90.1	0
7 days heat activated persulfate	Н-7	1274.63	29221.23	<20	2.02	24.2	0
14 days heat-activated persulfate	H-14	1303.91	23910.68	<20	2.59	46.6	0
6 days, peroxide- activated persulfate	P-6	763.16	28001.11	<20	2.44	622	0

^{* 1} mL 50% sodium hydroxide added on day 6.

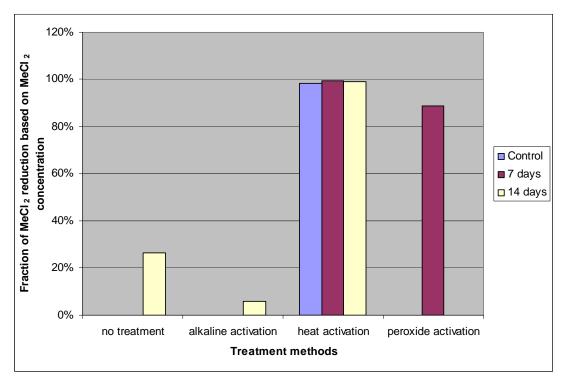


Figure 6-1. Methylene chloride (MeCl₂) reductions with different treatment methods, based on MeCl₂ concentrations

Figure 6-1 presents a plot of the methylene chloride reduction based on methylene chloride measured at the end of each test. The 14 days control (C-14) sample had 4,133 mg/L methylene chloride, indicating a 26% loss compared to the 0 day control, possibly due to volatilization, hydrolysis, or intrinsic biodegradation.

Heat Activation at 60°C

The heat activated persulfate samples had very low pH (2.02 for 7 days sample H-7, and 2.59 for 14 days sample H-14) due to the rapid decomposition of persulfate. Correspondingly, persulfate concentration dropped to below the detection limit (20 mg/L) at the end of each test. Methylene chloride concentrations decreased to less than 1% of the initial level both for 7 days and 14 days treatment. However, the heated control (CH-14) also showed 98% reduction of methylene chloride. So the decrease in methylene chloride concentration in H-7 and H-14 are due to volatilization loss as well as oxidation by persulfate. To differentiate the oxidation from volatilization loss, one of the oxidation products from methylene chloride, chloride ion, was used as the indicator. **Figure 6-2** presents a plot of the methylene chloride reduction for different treatment methods based on chloride concentrations. This figure indicates that with heat activated persulfate, approximately 23% of the methylene chloride was oxidized to chloride within either 7 days or 14 days of treatment. The heated control (CH-14) also showed a slight

increase in chloride concentrations (5%), probably due to accelerated hydrolysis of methylene chloride at the elevated temperatures.

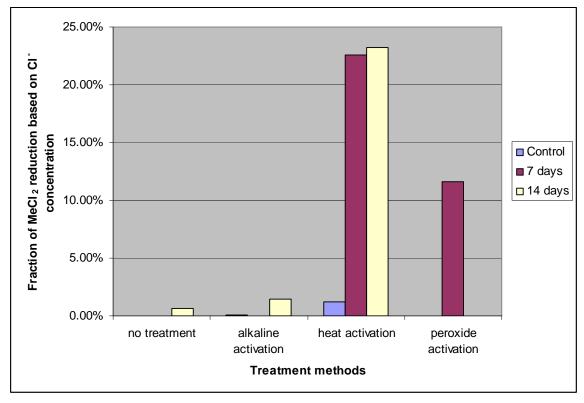


Figure 6-2. Methylene chloride (MeCl₂) reduction with different treatment methods, based on chloride (Cl⁻) concentration

Alkaline Activation

The pH of the alkaline activated persulfate oxidation sample (B-14) was 11.38 on day 4, and 1 mL 50% sodium hydroxide was added when the pH dropped to 8.35 on day 6. The pH was then increased to 12.68 as measured on day 11, but dropped to 9.22 on day 14 at the end of test. This treatment resulted in a 6% reduction in methylene chloride concentration. The persulfate concentration at the end of test was 16.45 g/L, which is not too low to treat the contaminant. Therefore the possible reasons for the failure of significant treatment efficiency are: 1) low pH. As stated above, the pH of the sample dropped dramatically due to reaction between persulfate and methylene chloride, and the alkaline activation requires a pH above 10.5. 2) Recalcitrance of methylene chloride to alkaline-activated persulfate oxidation, or slow reaction kinetics. Chloride analysis showed there was 63 mg/L more chloride in B-14 than in C-14, which translates to 1.44% reduction of methylene chloride. This indicates that oxidation of methylene chloride did occur in B-14, but just at a too slow rate to show significant reduction within the time frame tested.

The 14 days base control (CB-14) which was amended with sodium hydroxide showed slightly increased methylene chloride concentration (5,762 mg/L), indicating the systematic losses are minimal (plotted as 0% reduction on **Figure 6-1**). The pH of this alkaline control was 12.70 on day 4, and dropped slightly to 12.58 on day 14.

Peroxide Activation

The peroxide activated persulfate SOD sample was also analyzed for inorganic anions and methylene chloride and the results were plotted in **Figure 6-1** and **Figure 6-2**. It showed 89% reduction by looking at methylene chloride concentrations, and 12% reduction based on chloride concentrations, and the pH of the sample was 2.44 on day 6 when the test was terminated.

Alkaline and Heat Activation at 40°C

The above test results indicated that alkaline or peroxide activation was not effective on methylene chloride contamination, and that heat activation alone resulted in a too acidic condition and short longevity of persulfate. So an additional batch of test was performed with combined heat and alkaline activation. The temperature of heat activation was also lowered to 40°C to increase the longevity of persulfate and mitigate volatilization loss of methylene chloride.

Table 6-3
Analytical Results of Heat and Alkaline Activated Persulfate Oxidation Tests

Treatment	sample ID	Cl-, mg/L	Sulfate, mg/L	persulfate, mg/L	pН	Methylene chloride (mg/L)
7 day room temperature control	C-7	235.23	49.76	NA	7.72	5458
7 day heated control	CH-7	233.47	63.47	NA	7.59	5338
Phosphate activated persulfate	PP-7	1385.57	33402.34	7,854	7.55	4039
hydroxide activated persulfate	PH-7	2435.19	49672.46	12,733	6.39	3382

The analytical results (**Table 6-3**) showed that the volatilization loss of methylene chloride at 40°C heated condition was negligible (2.2% relative to the control at room temperature), and the decomposition rate of persulfate was much slower compared to 60°C, as there were 13% and 21% of the original persulfate left after 7 days in the phosphate activated (PP-7) and hydroxide activated (PH-7) persulfate samples, respectively.

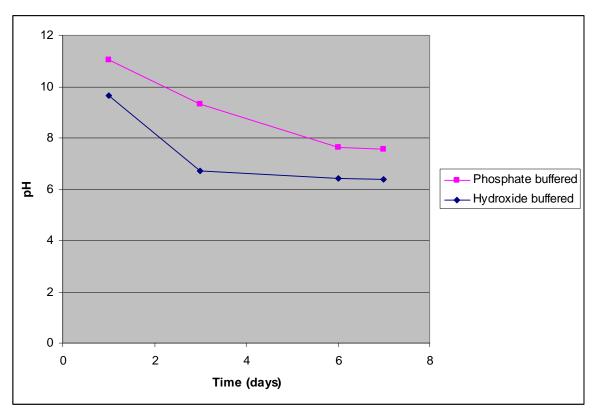


Figure 6-3. pH change over time in heat and alkaline activated persulfate oxidation tests

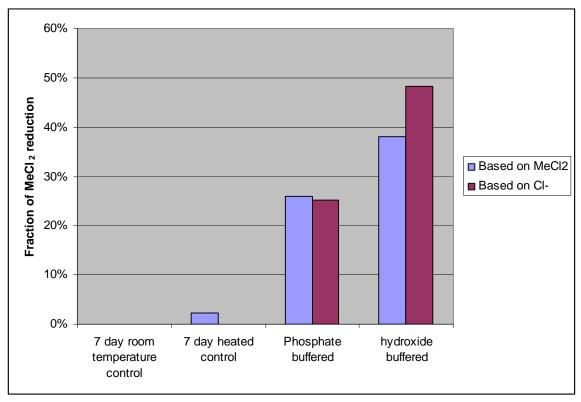


Figure 6-4. Methylene chloride reduction with heat and alkaline activated persulfate oxidation, based on methylene chloride analysis and chloride ion analysis.

Figure 6-3 indicated the pH dropped over time in hydroxide activated and phosphate activated samples. Apparently phosphate performed better as a pH buffering reagent since the pH in phosphate activated treatment was always higher than that of the hydroxide activated. However, the treatment efficiency was not positively correlated with the pH buffering capacity, as hydroxide activated persulfate treatment achieved 48% methylene chloride removal compared to 26% removal of phosphate activated. More importantly, treatment efficiency calculated based on chloride analysis showed similar results, indicating the removal of methylene chloride is through oxidation to carbon dioxide and chloride, rather than volatilization.

7.0 Conclusions and Recommendations

This treatability study determined that alkaline activated persulfate did not result in significant reduction of methylene chloride found at the Longhorn site within 14 days. Heat activated persulfate treatment at 60°C achieved 99% reduction of methylene chloride concentration. However, the majority of this reduction was due to volatilization loss, and oxidation accounted for no more than one fourth of this reduction. The treatment efficiency of peroxide activated persulfate was moderate with 89% reduction of methylene chloride concentration, but only a 12% reduction due to oxidation when considering chloride concentrations. The peroxide activation also resulted in rapid loss of oxidants, which would limit treatment effectiveness.

Combined heat at 40°C and alkaline activated persulfate oxidation appear to be the best treatment option for methylene chloride at the Longhorn site. Two alkaline catalysts were tested, phosphate and hydroxide. Between two of the alkaline catalysts tested, the hydroxide buffered treatment achieved more removal of methylene chloride through oxidation. The hydroxide removed 48% of methylene chloride through oxidation whereas phosphate removed 26% in 7 days. The dosage of 60 g/L persulfate and 15 g/L sodium hydroxide is recommended for the site. A lower temperature of heat activation, 40°C instead of 60°C, is recommended as it minimized the volatilization of methylene chloride and extended the longevity of persulfate. However, re-dosing of both persulfate and alkaline catalyst will likely be necessary after 7 to 10 days, as the pH dropped to neutral, and more than 80% of persulfate was consumed in 7 days in the test samples. The rate of persulfate and caustic consumption is expected to decrease upon subsequent treatment, due to depletion of methylene chloride reactant and natural oxidant demand

8.0 References

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Attachment 1

Soil Alkalinity Measurement Data

Notes:

Project/No.: Long Horn/117591			Date: 9/27/2006	
Sample	TDL 10762		Reagent/G.W.	TDL 10828
Sample Wt. (g):	100		Water Volume (mL)	150
Base Reagent/Conc.:	NaOH	1 N	Initials	XZ

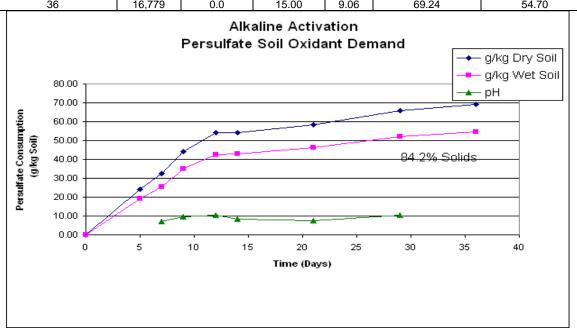
Reading No.	Time	Base Add'n (mL)	Total Vol Base (mL)	рН	Base meq. per kg Soil	Comments
1		0	0	8.03	0.00	
2		2.6	2.6	10.06	26.00	
3		0.4	3	10.19	30.00	
4		0.5	3.5	10.3	35.00	
5		0.5	4	10.5	40.00	
6		1	5	10.73	50.00	
7		1	6	11	60.00	
8		1	7	11.15	70.00	Slurry appears to be thickened
9		1	8	11.35	80.00	
10		1	9	11.35	90.00	
11		1	10	11.39	100.00	
12		1	11	11.42	110.00	,
13		1	12	11.46	120.00	
14						
15						
16						
17						
18						
19			рН	vs Bas	e Addit	tion
20						
21		14				
22		I .				
23		10	***	++++	** *	
24						
25	돐	8				— pH
26		6				
27		4 +				
28		2 +				
29		0 +		- I		
30		0 20	40	60	80	100 120
31			Base	Δddition	n (meq/L	
32			Dase	kg)		
33				∧g.	'	
	1 1					
34						

Attachment 2

Soil Oxidant Demand Test Data

Project Name:	Long Horn	Date Started:	9/27/2006
Project Number:	117591.0006A200	Analyst Initials:	XZ
Client Sample No. (Soil):	29WW40 Silty soil.	Client Sample No. (Water):	29WW16 Groundwater,
Description:	dark grey	Description:	smells solvent
TAL Sample No.:	10762	TAL Sample No.:	10828
Solids (%):	79.00%	Volume Used (mL):	200
Fraction -4 mm particle size :	NA		
Weight Used (g):	200	Initial Weight Na ₂ S ₂ O ₈ (g):	10.00
Test Temp (°C)	15	Initial Conc. Na ₂ S ₂ O ₈ (mg/L):	50,000
NaOH at 0.5%			

144011410.576			Total			
Time	Persulfate Conc.	Persulfate Addition	persulfate Added	рН	Persulfate Consumed	Persulfate Consumed
(Days)	(mg/L)	(g)	(g)	(SI)	(g/kg Dry Soil)	(g/kg Wet Soil)
0	41,322	0.0	10.00		0.00	0.00
5	25,466	0.0	10.00		24.29	19.19
7	20,230	0.0	10.00	7.22	32.31	25.52
9	12,376	0.0	10.00	9.4	44.34	35.03
12	6,045	0.0	10.00	10.36	54.03	42.69
14	26,537	5.0	15.00	8.4	54.29	42.89
21	23,847	0.0	15.00	7.67	58.41	46.15
29	19,040	0.0	15.00	10.32	65.77	51.96
36	16,779	0.0	15.00	9.06	69.24	54.70



Notes:

NaOH was redosed with 50% NaOH solution as following:

2 mL on day 7,

1 mL on day 9,

1 mL on day 28.

Attachment 4 Groundwater Sampling Forms



Sheet 1 of Z

IREATABIL								JTY .	SAMPLE		
Operable	Unit/Site II	D: 291	VWIL			Sampling	location II): 29WW	/)(,		
	larne/#:			117591		Sample ID: 29WWIL					
Weather:	<u>Cleow</u>	70	<u>s 70 805</u>	<u> </u>		Collection	n Time/Dat	e: 4/2	1/06		
				Pum	n Inst	allation					
Pump ins	tallation cre	w: A. W.	Il man / A	. Gilchris	le mach	. inetallatio	n data/haa	linnina tima	9/21/2		
PID/FID r	eading (we	ll head/bacl	kground):	0 D	Le. Milo	inetallation y	on date/seg	pletion time	2:412.12		
Casing di	ameter (inc	hes): 4	ii	<u> </u>		Screen In	ntervel (ft. F	STUC). Spicatori ami	80,41 to	<u> </u>	
			90.41		_	Pump int	ake denth (ft BTOC):	QE W.	10.41	
			9: 44.14		ود د	Post-Insta	allation DT\	N/time:	Os		
	er pump prin				-					70	
Free prod	luct (circle):	LNA	PL/DNAPI		_	Appearar	ice of prodi	ıct:	_/min): <u> /</u> <u> </u>		
Volume o	f water rem	oved during	priming (m	L):		Discharge	e tube diam	eter (3/8" o	г 1/4"): 1/4	H	
	tube lengt		~100'			Inlet redů	cer.used ()	//N):	_ N		
	ic Controll						·	-			
Initial air p	ressure = l	i (ft.) X 0.4	3= <u>50</u>	psi							
-		Initial	2	3	4	5	6	7		Final	
Pressure (ps	si)	_								1,	
Refill Setting		 		<u> </u>			1				
Discharge S					<u> </u>	/	AV.				
Flow rate (m	L/min)			<u> </u>	<u> </u>						
Initial (pre- Calculated Pneumati	purging) D I tubing + pr c Controlle	TW (ft. BTC ump volume r Tuning:	9/21/06 0C): 3:	NA	<u>.</u>	Final (pos	t-purging) E	OTW (ft. BTo volumes pu	9/2// OC): irged:		
	700010	· · · · · · · · · · · · · · · · · · ·		_ har	·						
Organism (ma)		Initial	2	3	4	5 .	6	7	8	Final	
Pressure (psi Refill Setting)	50	45 10	50 -			<u> </u>		└	56	
Discharge Se	tilna	4	10	 			ļ	 		11	
Flow rate (m)		纮	120	170	 		<u> </u>		<u></u>	4	
		1 133	· · · · · · · · · · · · · · · · · · ·					1	<u> </u>	170	
1944		F	ł	Quality Pa	ramete	r Measure	ments	T			
Time	DTW MEDICAL	Purge Rate		Temp.	ŀ	ectrical	pH₁	Eh	· DO	Turbidity	
	(ft. BTOC)	(ml./min)	Volume	(degree C)	Con	ductivity MS/cm ^C hos/cm)		(mv)	(mg/L)	(NTU)	
09:48	44.32	100	Purged (L)	10 62				30	A-3		
09:53	44,32	170	850	19,53	1.51		7.04	-72.1	0.71	1.7	
99:58	44.32	180	766	19.42	1.50		7.04	-95.6	0.69	1.3	
10:03					7.04	-913	0.51	1.2			
10:03 44.32 176 3400 19.21 1.48 10:08 44.32 170 42.5 19.16 1.47				7.03	- 96.	0.80.89	0.5				
10/13	44.32	170	49.0	19.09			7.02	-99.4	-49.495	0.3	
10:18	44.32	170	51.5	19.36	1.48°		7.03	-103,2	0.77	0.2	
(0			. 113	11.16	<u>(. 78</u>		7.05	∽ 99.7	0.78	0.1	
الب ندسيين											



Sheet 7 of Z

Time	DTW	Dames D.			er Measurement		eu)		_
IIMIG	(ff. BTOC	Purge Rate (mL/min)	Cumulative Volume	(degree C)	士 3号ectrical Conductivity	Hq	Eh (mv)	DO (mg/L)	Turbid
			Purged (L)	生10%	(uMhos/cm)	±0.1	±10	士10%	± 10%
				·					
				1/1/2					
		<u> </u>				3			
					- a/12/				
				Sai	npling				
ampling	beginning tin	ne: <u> 6;5</u>		Quality Para	Sampling c meter Measurer	ompletion ti	me: <u>[]'</u>	<u>3</u> d	-
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	Hq	Eh	DO	70
	(fit BTOC)	(mL/min)	Volume Purged (L)	(degree C)	Conductivity (uMhos/cm)		(mv)	(mg/L)	Turbidity (NTU)
(40	44.32			19.39	1,491	7.04	~100.1	0.72	0,1
									-
				Sample h	nformation				
mple ID:	IZWY	4.16			Sample colle	ection date/	ime: 9/z	1/06	•
piicate s lit sampl	ample collec e collected (ted (Y/N): Y/N):	N _o		Sample colle Duplicate sa	mple ID:	Hone		
C No(s)	<u>`</u>		(16)		Split sample	iD: <u> </u>	201	<u> </u>	
quested Racter		Method	Conf	ainers	Requested /	Analysis	Method	Contair	ers
voc.			3.40m	10-1 L L VOAS AM	16h2				
									-
nments:									
						•			,

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; ml - milifiter: 1 Liter



Sheet <u>1</u> of <u>2</u>

Operabl	e Unit/Site II	29/1	135			Samplin	a location II	- 201n	W 85	· · · · · · · · · · · · · · · · · · ·		
	Name/#;			17591		Sampling location ID: 29Ww35 Sample ID: 29ww35						
Weather	7		4015	1.0.11	-	Collection Time/Date: 9/26/coc						
<u> </u>								^				
1		1 0.1	1.	Pym	ip Inst	tallation						
Pump in:	stallation cre	w: <u>H. Gilc</u>	hrist	J. Kocky	uiez	Installatio	on date/beg	inning time	= 9/	26/06		
				0.0	_	Installatio	on date/com	pletion time	e: 9/2	6/06		
Casing d	liameter (inc	hes): <u> </u>			_	Screen li	nterval (ft. B	TOC):	8 8 to	98		
Total we	ll Depth (ft. I	3TOC):	9832			Pump int	take depth (t	ft BTOC):	93'			
Ilnitial (pr	e-installation	ı) DTW/time	: <u> </u>	0848	_	Post-inst	allation DTV	V/time:	41,25	0920		
	er pump prir			······	_	Max. sus	tainable pur	np rate (ml	/min): _	10		
	duct (circle):				-	Appearar	nce of produ e tube diam	ict:	None			
1	of water rem			ıL):	•	Discharg	e tube diam	eter (3/8" o	r 1/4"):	1/4"		
	e tube lengti		~110			Inlet redu	icer used (Y	/N):	N_			
	tic Controlle	**	<u>۔</u> م ہے									
initial air	pressure = H	1 (R.) X 0.43	5 = <u>5 5</u>	psi								
		initial	2	3	4	5	6	7	8	Final		
Pressure (p					4	1						
Refill Setting	~								_			
Discharge S				<u>↓\</u>				7	<u> </u>			
Flow rate (n	nL/min)	<u> </u>	1	<u> </u>	<u>Y </u>	\ -		<u> </u>				
Calculated Pneumati	e-purging) Di d tubing + p ic Controlle pressure = H	ımp volume r <mark>Tuning:</mark>	:	NA	-		t-purging) D ing + pump					
initial and	7 000010 - 11	,	· · · · ·	T hai		,	· r · · · · · · · · · · · · · · · · · ·		-1			
D /		Initial	2	3	 4	5	6	7	8	Final		
Pressure (ps	· · · · · · · · · · · · · · · · · · ·	5 5					 			55		
Refill Setting Discharge Se	······	10				<u> </u>	 		//	10		
Flow rate (mi		20	<u> </u>	<u> </u>					ļ	5		
i ion rate (iii	D. Viller)	1 100	Li	<u> </u>	L				l <u>. </u>	1 280		
	1			Quality Pa	ramete	er Measure	ments			,		
Time	DTW	-	Cumulative		l '	ectrical	рН	Eh	DO	Turbidity		
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Cor	iductivity c hostom		(mv)	(mg/L.)	(UTM)		
A) C project	111.00	- 100	Purged (L)	0.0.00								
0955	41.32	280	1.25	20.62		.07	9.46		7.19	4.5		
1000	41.80	280	1.90	20.65		.04	9.29		7,92	1.7		
1005	41.84	280	2.0	20.69	L	03	7.25		9.41	2,3		
1010	41.85	280	2.5	10.19	<u> </u>	<i>0</i> 2	9.03		10.47	8		
1015	41.96	280	2.7	208		0 (8.98		10.76			
1020	41.86	280	3	20.85		7]	8.95		12,36	0		
1035	41.86	280	3,4	20.89	1.0		8.92		11.68	0		
いつじ	41.26	280	3.7	50.98	1.0	<i>)</i>	8,89		13,20	0		



Sheet Z of Z

(ft. BTOC) (ml/min) Volume (degree C) Conductivity ± 0.1 ± 10 ± 10 ± 10 ± 10 ± 10 ± 10 ± 1			1	Water Gual	tre Donama	ar Magazzzzzzzzzzzzzzzzzzzzzzzzzzzzzzzzzzz	- 1	-f)		
(ft. BTOC) (ml./min) Volume (degree C) Englicitivity English E	Time	WTQ	Purge Rate	Cumulative						T
10:40		ł		.1		±3%	рн	ł	1	Turbidity
10:40 146 280 4.0 21.48 1.0 8.86 13.46		1'		1		trillbaddom)	1±0.1	1 (mv) 1 1 1 0	(mg/L)	(NTU) 土10亿
Sampling beginning time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct Sampling completion time: Oct O		41.87	280				. 1	1=10		(3)
mpling beginning time: {Oct Sampling Sampling completion time: [O, 'Y.5] Water Quality Parameter Measurements Time DTW (ft. BTOC) Purge Rate (mL/min) Purged (L) (degree C) Conductivity (mV) (mg/L) (NT) (MN) (MN) (MN) (MN) (MN) (MN) (MN) (MN	10:40						9.85	 	13 79	1
Sampling beginning time: IOA7 Sampling completion time: IOA7 Water Quality Parameter Measurements			0.0-				7.20.5	 	12.51	
Sampling completion time:							1			
Water Quality Parameter Measurements Time DTW (ft. BTOC) (mL/min) Volume (degree C) Conductivity (mv) (mg/L) (NTI (MTI)		<u> </u>								l
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume Purged (L) (uMhos/cm) (my) (mg/L) (NT) OUS 41.86 280 4/.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collected (Y/N): Sample collection date/time: 104.5 9/3 cicate sample collected (Y/N): Split sample ID:			<u> </u>							
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume Purged (L) (uMhos/cm) (my) (mg/L) (NT) OUS 41.86 280 4/.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collected (Y/N): Sample collection date/time: 104.5 9/3 cicate sample collected (Y/N): Split sample ID:		<u> </u>	<u> </u>							
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume Purged (L) (uMhos/cm) (my) (mg/L) (NT) OUS 41.86 280 4/.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collected (Y/N): Sample collection date/time: 104.5 9/3 cicate sample collected (Y/N): Split sample ID:			<u> </u>				-			,
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume Purged (L) (uMhos/cm) (my) (mg/L) (NT) OUS 41.86 280 4/.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collected (Y/N): Sample collection date/time: 104.5 9/3 cicate sample collected (Y/N): Split sample ID:					[·		
Sampling completion time: CO, US Water Quality Parameter Measurements Time DTW (ft. BTOC) (mL/min) Volume (degree C) Conductivity (mv) (mg/L) (NT) DUS 41.86 280 4/.5 21.37 1.0 3.36 12.76 0 Sample Information Sample collected (Y/N): Sample collected (Y/N): Split sample ID:										
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume Purged (L) (uMhos/cm) (my) (mg/L) (NT) OUS 41.86 280 4/.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collected (Y/N): Sample collection date/time: 104.5 9/3 cicate sample collected (Y/N): Split sample ID:	.	<u> </u>				<u> </u>				
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume (degree C) Conductivity (mv) (mg/L) (NTI (num) Purged (L) (uMhos/cm) D45 41.86 280 47.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collection date/time: 104.5 9/3 icate sample collected (Y/N): Sample collected (Y/N): Split sample ID: Split					-					
Sampling completion time: 10.°45 Water Quality Parameter Measurements Time DTW Purge Rate (ML/min) Volume (degree C) Conductivity (mv) (mg/L) (NT) D'45 41.86 280 47.5 21.37 1.0 8.32 12.76 0 Sample Information Ple ID: 29 5 21 5 Sample collected (Y/N): Sample collected (Y/N): Split sample ID	····									
Sampling completion time: 1047 Water Quality Parameter Measurements Time DTW Purge Rate Cumulative Temp. Electrical pH Eh DO Turbi (mL/min) Volume (degree C) Conductivity (mv) (mg/L) (NTI (num) Purged (L) (uMhos/cm) D45 41.86 280 47.5 21.37 1.0 8.36 12.76 0 Sample Information Sample collection date/time: 104.5 9/3 icate sample collected (Y/N): Sample collected (Y/N): Split sample ID: Split			<u> </u>							
Purged (L) Purged (L) Purged (L) (uMhos/cm) (inv) (inv) (inv) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (ing) (inv) (inv) (ing) (inv) (in	fime		- 1	Cumulative	Temp,	Electrical		1	1	Turbidity
Sample Information Sample Collected (Y/N): Sample collected (Y/N): Sample collected (Y/N): Sample collected (Y/N): Sample collected (Y/N): Split sample ID: Sp				1	aegrae ()			(mv)	(mg/L)	(UTN)
Sample Information ple ID: 29 ULI 35 licate sample collected (Y/N):	045	41.86			21.37	10	8.36		127/	<u></u>
ple ID: 29 UU 35 icate sample collected (Y/N): Duplicate sample ID: Split sample ID: Split sample ID: No(s): Requested Analysis Method Containers Requested Analysis Method Containers							•	-		<u></u>
pipe ID:										
ple ID:	1	<u> </u>								
GONTAINERS INCOME AND A CONTRINERS	licate sa sample	mple collected ()	ted (Y/N):	···		Sample colle Duplicate sar	mpie iD;		1045	9/26/0
Treducted Analysis Method Containers	uested /	Analysis	Method	Conf	ainers '	Reguested A	nalycia	Madhad	C4-1	
1000 (60,1641)						Requested A	lialy515 I	Memod	Contain	ers
					LONTONIS.					
						1				
									·	
	,									· · · · · · ·
ments:	ments:		7							

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of /

Operable Unit/Site ID: CHAMP-30 29WW 36 Sampling location ID: Project Name/#: Sample ID: 29ww 36 Weather: Collection Time/Date: 9/22/06 Pump Installation Pump installation crew: C. Make, A. Gilchrist Installation date/beginning time: PID/FID reading (well head/background): A. O installation date/completion time:_ Casing diameter (inches); . 4 26.7 Screen Interval (ft. BTOC): to Total well Depth (ft. BTOC); Pump intake depth (ft BTOC): Initial (pre-installation) DTW/time: 28,50 Post-installation DTW/time: Final (after pump priming) DTW/fime: Max. sustainable pump rate (mL/min): Free product (circle): ___ LNAPL / DNAPL Appearance of product: Volume of water removed during priming (mL):_ Discharge tube diameter (3/8" or 1/4"): Discharge tube length (ft.): Inlet reducer used (Y/N); Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = Initial Ź 5 7 Final Pressure (psi) Refill Setting Discharge Setting Ftow rate (mL/min) Purging Purging/sampling crew: C. Mabe A. Gilchrist PID/FID reading (well head/background):_ Purge date/beginning time:_ Purge date/completion time: 9/22/06 Initial (pre-purging) DTW (ft. BTOC): Final (post-purging) DTW (ft. BTOC): Calculated tubing + pump volume: NA No. of tubing + pump volumes purged: Pneumatic Controller Tuning: 50 Initial air pressure = H (ft.) X 0.43 = Initial 5 Final Pressure (psi) **5**0 50 Refill Setting 10 70 Discharge Setting Flow rate (mL/min) 230 Water Quality Parameter Measurements DTW Time Purge Rate Cumulative Temp, **Electrical** DO Eh Turbidity (ff. BTOC) (mL/min) Volume Conductivity (uMhestern) (degree C) (mv) (mg/L) (NTU) Purged (L) 920 29*0* 20.47 20 7,44 0. 23*0* 9,9 5.378 7.5 230 19.96 5.343 **7.27** 230 4.5 20.13 130 b.0 20.07



Sheet __of Z

Time	ptw			 	er Measurement		1	1. 50	Taxation.
111116	(fr. BTOC)	Purge Rate (mL/min)	Volume	(degree C)	± 3 [jectrical Conductivity	±0.1	Eh (mv)	(mg/L)	Turbidity (NTU)
		 	Purged (L)	±10%	(uMhos/cm)	1-0,1	±10	上10%	110%
	 						 		
	1	-				-			
				·					<u> </u>
·	ļ <u>.</u>				<u> </u>	<u> </u>	<u> </u>	<u> </u>	
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	-	<u> </u>		- '	·	 -	 	 	
		 				 	 	<u>- [</u>	
		ļ				 		-	<u> </u>
			·						
	·					}			
				Sa	mpling				
ampling i	oeginning til	ne:9	50	· ·	Sampling o	completion t	ime: <i>[</i>	900	
			Water	Quality Par	ameter Measure	ments	ė		
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	00	Turbidity
	(fi. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
955	29.89	230	Purged (L)	0	(uMhos/cm)	5.50		70 22	
-35	29.81	250	6.3	20.09	5.38	6.58		1/35	0
						<u> </u>		 	
		·	,	Commiste	lufo um ette u				
mnlė.li)	3	9.663	<u>(</u>	-	Information	liantian data	Bima na	0455	9/00/0
plicate s	ample colle	cted (Y/N):_	9	· · · · · · · · · · · · · · · · · · ·	Sample col Dunticate s	ample ID:	/ume:	<u>~30</u>	TAROS
lit sampl	e collected	(Y/N):				e ID:			
OC No(s)					• • • • • • • • • • • • • • • • • • • •				
musetor	Analysis	Method	Car	talmana	Requested	Anabraia	Madhad	Canta	
VOC		8260		tainers		i Analysis	Method	Conta	iners
		3000	5 000	Conta nec	5				
<u> </u>									
		·						······································	
-		i							
			.						
mments		,							

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of _

Oporobil	n l Init/Otio II	n. //J//	40 50			O			· ~	
Operable Unit/Site ID: CHARY - 29 Sampling location ID: 19ww37 Project Name/#: Longhorn //759! Sample ID: 29ww37 Weather: Clear 80'5 Collection Time/Date: 9/22/66										
		Clear	1000 (201/	<u> </u>	<u> </u>					
Weather		Clear	30 5			Collectio	n Time/Date);	9/22/66	
				Pun	ın İnst	allation		•		
Pump ins	stallation cre	A Cost	loved Ch	nala	יף וווטנ		an data/hawi		- 9/nn /	
PIN/FID	reading (we	I bood/book	karound).	0.0			on date/begi			
	lameter (inc			0.0	_		on date/com			
	Depth (ft. I					Screen in	ntervar (it. 15	100):	82.12 to	95.15
Initial (on	e-installation	3 100; 3 DTW#im		7 50	-	Pump int	ake depth (f allation DTV	tBIOC):	11/2 70	
Final (att	er bamb buji	nina) DTM	timo:) 1/7						
	duct (circle):					Max. sus	tainable pun	np rate (mi	L/min):	
	of water rem				-	Piochara	nce of produ	CU	none	1/4"
	e tube lengt			II- J	-		e tube diame			1/4"
	tic Controll		<u> </u>		_	metreau	cer.used (Y	/N/;		<u>_</u> _
	pressure = l		3 <u>-</u> ⊂⊄	nei					4	- ,
	prodout 0 - 1	1 (10.) 10.4	J	hai						
		Initial	2	3	4	5	6	7	8	Final
Pressure (p			<u> </u>	<u> </u>	$\perp \downarrow_{\Lambda}$	<u> </u>				
Refill Setting	·				1111	<u> </u>				
Discharge S		ļ		11	1/11/					
Flow rate (m	oL/min)			+	<u> L'</u>	<u> </u>		<u> </u>		
Initial (pre Calculated Pneumati	e/beginning -purging) Di I tubing + pu c Controlle	FW (ft. BTC imp volume r Tuning:)C): ::	NA.	- -	Final (pos	e/completion t-purging) D ing + pump	TW (ft. BT	OC):	
Initial air p	ressuré = H	(ft.) X 0.43	= 55	_ psi						9
		Initial	2	3	4	5	6	. 7	T 8	Final
Pressure (ps	i)	55	 		1				 	55
Refili Setting		:10								10
Discharge Se	etting	5							 	5
low rate (mt	Jmin)	110	. 4						 	110
	-		Water	Quality Pa	ramete	r Measure	ments		-{	1110
Time	WTO	Purge Rate	Cumulative		3	ectrical	рН	Eh	DO	Turbidity
	(fft. BTOC)	(mL/min)	Volume	(degree C)	Con	ductivity		(mv)	(mg/L)	(NTU)
		·	Purged (L)		(1114	hos/em)S/cm		• • • • • • • • • • • • • • • • • • • •	(57	, ,,,,,
1100	49.0	110	1.110	21.31	1.0	14	11.19		5.37	0
1105	49.12	10	3.02	91.59	1.0	717	11.10		4.71	Ŏ
1110	49.20	110	5.33	21.65		211	11.09		4.62	\times
115	49.537	110	7.44	21.6		176	11.02			170
1120	49,22	110	9,55	21.62		62	10.95		5.09	0
125	49.26	110	19.88	21.73		146	10.86		4.79	õ
130	77 32						11/10[/			
135	49.35	110	11.5	21.7		44	10.79		4.7	7)



Sheet **2** of **2**

77						s (continue	<u> </u>		
Time	DTW (ft. BTOC)	Purge Rate (mt/min)	Cumulative Volume	Temp. (degree C)	士 3 Electrical Conductivity	Нq	Eh	DO (mall)	Turbidit (NTU)
······································	1.2.5.00)	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Purged (L)		(uMhos/cm)	±0.1	士10	生 10%	±10%
	<u> </u>	 	<u> </u>				<u> </u>		
· · · · · · · · · · · · · · · · · · ·	 	<u> </u>	 						
			<u> </u>					 	
	-					Intilo			
·				7	91	770			
	 	<u> </u>			#	· · · · · ·		 	
				- H	10/			1	<u> </u>
								1	
						· · ·			
					mpling			<u> </u>	
	eginning tin	· · · · · · · · · · · · · · · · · · ·		Quality Par	Sampling c ameter Measure			, , , ,	
Time	DTW (ft. BTOC)	Purge Rate	Cumulative	Temp.	Electrical	На	Eh	DO	Turbidity
İ	(ILBIOL)	(mL/min)	Volume Purged (L)	(degree C)	Conductivity (uMhos/cm)		(mv)	(mg/L)	(UTM)
1040	49,34	110	~3.254	21.68	,945	10.74		4,63	0
								*	
·Ol.elor	<u> </u>	9/1/-12~		Sample	Information	ootion data	simo. Ci	innime i	1 (125)
mple ID:	ample collec	94437 ted (Y/N):		Sample	Sample colle	ection date/	time: 억/	122/06	40
it sample	: collected (`	ない3 ted (Y/N): Y/N):	1		Sample colle	ample ID:		122/06 1	40
mple ID: olicate sa it sample C No(s):	: collected (`	9いい3~, ted (Y/N):_ Y/N):_			Sample colle Duplicate sa	ample ID:		122/06 1	•40
it sample C No(s): quested	Analysis	ない3 [*] ted (Y/N):_ Y/N):_ Method	Cor		Sample coll Duplicate sa Split sample	ample ID:		(23/06 (
it sample C No(s):	Analysis	Y/N):	Cor		Sample colle Duplicate sa	ample ID:			
it sample C No(s): quested	Analysis	Y/N):	-	atainers	Sample coll Duplicate sa Split sample	ample ID:			
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it sample C No(s): quested	Analysis	Y/N):	Cor	atainers	Sample coll Duplicate sa Split sample	ample ID:			

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of 2

Project Namel#: Lower Modern Modern Lower Modern Lower Modern Mode	Operal	ole Unit/Site	ID:	29443	7		Sampli	na location	in 294	111138	
Pump installation crew: A Coloriest Pump installation Pump i	Project	: Name/#:	Long	OT O	11759	1	Sample	ID: 241	ปพรล	4 00	
Pump installation crew: A Gickiest J Robridge Pump installation provided in the property of the provided in th	Weath	or	clear	80'5						17. 9/2	23/06
Pump installation craw: A Glock of J Refrigeria Installation date/completion time: Albahot oyou Installation date/completion time: Albahot oyou Installation date/completion time: Albahot oyou Installation date/completion time: Albahot oyou Installation date/completion time: Albahot oyou Installation Installatio					Pur	np ins	tallation				
PIDIFID reading (well head/background):	Pump i	nstallation o	rew:_AG	Closest	J. Rolling	est à			ainnina tim	. alan	al ner
Casing diameter (inches)	PID/FID	reading (w	/ell head/ba	ckaround).	00	<u>,, , , , , , , , , , , , , , , , , , ,</u>					OR ON CO
Total well Depth (ft. BTOC):	Casing	diameter (ir	nches):	4"							
Final (affer pump printing) DTW/time: Tree product (circle): LNAPL / DNAPL DNAPL DNAPL Volume of water removed during printing (mL): Discharge tube length (ft.): ~55! Inlet reducer used (Y/N): // I	Total we	ell Depth (ft	BTOC):	45	2		Octeen	merval (II.	D100);	95	
Final (affer pump printing) DTW/time: Tree product (circle): LNAPL / DNAPL DNAPL DNAPL Volume of water removed during printing (mL): Discharge tube length (ft.): ~55! Inlet reducer used (Y/N): // I	Initial (p	re-installati	on) DTW/fin	ne: 307	3,						0'
Free product (circle): LNAPL/DNAPL	Final (al	ter pump p	rimina) DTM	//time·	d						4.6
Volume of water removed during priming (mL):	Free pro	oduct (circle): LN	APL / DNAF) 		Max. su	stainable bi	ımp rate (m	ıL/min):	100
Discharge tube length (ft.):	Volume	of water rea	noved dusin	a primina (s	nl l		Appeara	ince of prod	luci:	hone.	5 3 A
Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = 20 psi	Dischard	re tube lend	ith (ft):	ر سيساع (ر عاميساع (nu.j	_	Dischar	je tube djan	neter (3/8" (or 1/4"):	1/4"
Initial air pressure	Pneuma	tic Contro	ller Tupina				iniet rea	ucer used (Y/N):	<i>N</i>	
Pressure (pst)	Initial air	pressure =	H (ft.) X 0.4	3 = 2 Ø	psi	-	-	•			
Pressure (pst) Refit Setting Purging/sampling crew: # 6. lowes J. R. John Purging Purge date/beginning time: Purging Purge date/beginning time: Purge date/beginning time: Purge date/beginning time: Purge date/beginning time: Purge date/beginning time: Purge date/beginning time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time: Purge date/beginning time: Purge date/completion time: Purge date/beginning time			···								·
Purging Purg	Pressure (j	osi)		- 	┤╌╌	- -4	- 5	- 6	7	8	Final
Purging Purg					41.7		- -				
Purging Purg	Discharge :	Selting	-		MIL	1				<u> </u>	7
Purging Purging Crew: # 6. 6. 6. 6. 6. 6. 6. 6.			- N		- 	-	-			+	
PID/FID reading (well head/background):											_1
Initial 2 3 4 5 6 7 8 Final	neumat	ic Controll	er Tuning:			_	No. of tub	ing + pump	volumes pu	ırged:	- 1
Persure (psi) 2.0 2.0 3.0	•				_ psi		·	· · · · · · · · · · · · · · · · · · ·			
### Setting ### Se	meniro (na	.X				4	5	. 6	7	8	Final
Scharge Setting					30	1	·	<u> </u>			
Water Quality Parameter Measurements Time						ļ		<u> </u>		شسر	7
Water Quality Parameter Measurements								<u> </u>			
Time	अर्थ ।तास् (मा	-//nji/j	1 4 100	C 100	1 100						
Time		1		Water	Quality Pa	ramete	r Measure	ments			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Time	1		Cumulative		•		1	Eh	DO	Turbidity
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		(ft BTOC)	(mL/min)	Volume	(degree C)	Con	ductivity,		(mv)		-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	dus			Purged (L)		(A M a)	nis/en nos/em)-	-	,,	(***91=)	(1110)
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4			ي 5	18.28					7.36	100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$, , , , , , , , , , , , , , , , , , , 		[00					/ · ~ - J		50	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		30.18	100	.9	14.57			6.20		100	
010 31.19 100 1.2 20.0 0.757 6.22 6.03 11.9 0.15 31.19 100 1.9 20.11 0.755 6.22 2.90			100								
015 31.19 100 1.9 20.11 0.755 6.22 2.40 545 020 31.20 100 1.5 20.26 0.752 6.22 3.40 545	010	31,191		1,2		<u> </u>	_	7 27			
020 31.20 100 1.5 20.26 0.752 6.22 3.40 127.6	015	31.19				<u></u>		영경하			11.4
025 31.14 100 20 30 41 6700 6.30 3. 10 02/1	1020	31.20									5 4.5
	025	31.14	100								4127.0



Sheet C of C

		ed)	-						
Time	DTW	Purge Rate	Gumulative			рН	Eh	DO	Turbidit
	(ft. BTOC)	(mL/min)	Volume	(degree C)	士 3 % Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	110%	(uMhos/cm)	±0.1	±10	±10% 3.30	10%
7030		100	2.5	20,54	0,748	6,23		3.30	1662.1
1035		100	2.75	² Ø,57	0,743	6,23		4.06	1663.5
10,40	31,19	100	3,0,0	20,70	6.742	6.23		4.06	1665
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				Sa	mpling		1		
ampling b	eginning tin	ne: 10	<u>142</u>	 .	Sampling o		ime: <i>Ì()</i>	55	, ;
	D714				ameter Measurer	ments	·	,	
Time	DTW		Cumulative	Temp.	Electrical	Нq	Eh	DO	Turbidity
	(fL BTOC)	(mL/min)		(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
1055	31.2	100	Purged (L)	22.01	(uMhos/cm)		······································	64.63	
1037	21.0	100	-3"U-1.	2 271	0.749	6.25		5.43	0_
	i						·····		·····
molė ID.	0.0	WW 38	,	Sample I	information			مستوسری و	
ເກຣິດate sa ເກຣິດate sa	mple colleg	ted (Y/N):		- :	Sample colle	ection date/	'time:	1055	4/23/0
lit sample	collected (Y/N):	<u> </u>		Duplicate sa Split sample	imple ID;			
C No(s):	(• • • • • • • • • • • • • • • • • • • •	<u> </u>		Split sample	(ID:		 	
						· · · · · · · · · · · · · · · · · · ·	·		
quested	Analysis	Method	Con	tainers	Requested.	Analysis	Method	Contai	ners
JOC	<u> </u>	8260	<u>3 001</u>	4 Container				•	
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				·			<u>L</u>		
mments:		<u>_</u>				,			

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of C

Project			DW 39			Samplin	g location IE): <u>24</u> 4	υωვη	
	Name/#:	_Lanho	(0)	P 11'	1591	Sample	ID:29	ww34		
Weather	r:	čle	<u>a</u>				n Time/Date		<u> </u>	
				Duse	n Ingi	allation				
Dump in	etalistian or	AP1	6.4	J. Rolrige	ւի աջւ				0	in and and
DID/CID	scanding (9W. <u>/1 (0.1</u> 0	VICET S	- Kadrigu	χZ,				: 9/	
Cooing	reading (we	ali nead/baci	kgrouna): c <i>x 6i</i>	0,0	_	Installatio	on date/com	pletion tim	e: <i>¶</i> /	21/06
Total wa	diameter (ind	nes):	00 0			Screen I	nterval (ft. B	TOC):	82 to	92
Initial (or	ell Depth (ft.	DIUU);	78 K , C	2 1310	-		take depth (f			
				4 1310					31.4	
	ter pump pri duct (circle)				.	Max, sus	tainable pun	np rate (m	L/min):	130
Volume o	anner fannie)	LIVA	EL/ DINAP	1L):	~~	Appearai	nce of produ	ct:	ne	<u>ب</u>
Dischara	e tube lengi	iovea aarrig	; priming (n	714);	-	Discharg	e tube diame	eter (3/8" c	or 1/4"):	14"
Prouma	tic Controll	or Tuning	~105			inlet redu	icer.used (Y	/N):	IV	· · · · · · · · · · · · · · · · · · ·
	pressure =		- 	w:						
all	hi coonie – i		. ,	psi						
		Initial	2	3	4	5	6	7	8	Flnal
Pressure (p		\			1.					
Refill Setting					$\perp \perp \perp$	<u> </u>				
Discharge S				17	$\perp \perp$	1				
Flow ráte (n	nL/min)			7 7		<u> </u>	<u> </u>		i	
`	-	1]	Purgir	ıg				
Purging/s	ampling cre	w. <i>H. G.</i> l	christ .	I. Redrig	1727-	PID/FID re	eading (well	head/back	ground):	0.0
Purge dat	e/beginning	tima-	- 5 - 2							
	.cg	mire	_4/27/0	6		Purge dat	e/completion	ı time:	972760	
Initial (pre	-purging) D	TW (ft. BTO	_ <i>4/37/0</i> C):	6	_	Purge dat	e/completion	ı time:	9/27/00	-
Initial (pre Calculated	e-purging) Di d tubing + p	TW (ft. BTO ump volume	_ <i>4/37/0</i> C):	6	- -	Purge dat Final (pos	e/completion	r time: TW (ft. BT	_ <i>9]27/60</i> OC):	-
Initial (pre Calculated Pneumati	-purging) D d tubing + p ic Controlle	TW (ft. BTO ump volume e <mark>r Tuning:</mark>	<i>4/37/0</i> C): o:	NA.	- -	Purge dat Final (pos	e/completior t-purging) D	r time: TW (ft. BT	_ <i>9]27/60</i> OC):	-
Initial (pre Calculated Pneumati	e-purging) Di d tubing + p	TW (ft. BTO ump volume e <mark>r Tuning:</mark>	<i>4/37/0</i> C): o:	NA.	- -	Purge dat Final (pos	e/completior t-purging) D	r time: TW (ft. BT	_ <i>9]27/60</i> OC):	-
Initial (pre Calculated Pneumati	-purging) D d tubing + p ic Controlle	TW (ft. BTO ump volume er Tuning: I (ft.) X 0.43	<i>9/37/0</i> c): :: = <i>50</i>	NA _ psi	-	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	
Initial (pre Calculated Pneumati Initial air p	-purging) D d tubing + p ic Controlle oressure = F	TW (ft. BTO ump volume or Tuning: I (ft.) X 0.43	<i>4/37/0</i> C): o:	NA.	4	Purge dat Final (pos	e/completior t-purging) D	r time: TW (ft. BT	_ <i>9]27/60</i> OC):	Final
Initial (pre Calculated Pneumati Initial air p Pressure (ps	e-purging) Did tubing + price Controller oressure = F	TW (ft. BTO ump volume or Tuning: I (ft.) X 0.43	<i>9/37/0</i> c): :: = <i>50</i>	NA _ psi	-	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 50
Initial (pre Calculated Pneumati	e-purging) Did tubing + price Controlle pressure = F	TW (ft. BTO ump volume or Tuning: I (ft.) X 0.43	<i>9/37/0</i> c): :: = <i>50</i>	NA _ psi	-	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 50
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se	e-purging) Did tubing + price Controlle pressure = F	TW (ft. BTO ump volume or Tuning: I (ft.) X 0.43	<i>9/37/0</i> c): :: = <i>50</i>	NA _ psi	-	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 5-0 10 5
Initial (pre Calculated Pneumati Initial air p Pressure (ps Refill Setting	e-purging) Did tubing + price Controlle pressure = F	TW (ft. BTO ump volume or Tuning: I (ft.) X 0.43	= 50	NA psi	4	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 50
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (ml	e-purging) Did tubing + price Controlle pressure = Fig. 1) atting Limin)	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 60	### ##################################	NA psi 3 Quality Pa	4	Purge dat Final (pos No. of tubi	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 5-0 10 5
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se	e-purging) D d tubing + p ic Controlle pressure = F ii) etting L/min)	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 0 Furge Rate	### Wate Cumulative	NA psi 3 r Quality Pa Temp.	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure	e/completion t-purging) D ing + pump v	n time:_ TW (ft. BTo	<i>9]3.7/60</i> OC): urged:	Final 5-0 10 5
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (ml	e-purging) Did tubing + price Controlle pressure = Fig. 1) atting Limin)	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 0 Furge Rate	Water Cumulative Volume	NA psi 3	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure	e/completion t-purging) D ing + pump v 6 ments	n time: TW (ft. BT- volumes po	9/37/60 OC): urged: 8	Final 50 10 5
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mi	e-purging) D d tubing + p ic Controlle pressure = F ii) etting L/min) DTW (ft. BTOC)	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 10 5 180 Purge Rate (mL/min)	Water Cumulative Volume Purged (L)	psi 3 r Quality Pa Temp. (degree C)	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure ectrical ductivity	e/completion t-purging) D ing + pump v 6 ments	n time: TW (ft. BT- volumes po	9/37/60 OC): urged:	Final 50 10 5 180 Turbidity
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mi	e-purging) Did tubing + price Controlle pressure = Historian DTW (ft. BTOC)	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 10 5 180 Purge Rate (mL/min)	Water Cumulative Volume Purged (L)	PSi 3 Quality Pa Temp. (degree C)	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure	e/completion t-purging) D ing + pump v 6 6 ments	n time: TW (ft. BT- volumes po	9/37/60 OC):	Final 50 10 5 180 Turbidity
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mt) Time	e-purging) D d tubing + p ic Controlle pressure = F ii) etting Umin) DTW (ft. BTOC) 31-35	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 80 I 80 I 80 I 80	Water Cumulative Volume Purged (L)	Quality Pa	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure ectrical ductivity	e/completion t-purging) D ing + pump v 6 ments	n time: TW (ft. BT- volumes po	9/37/60 OC): urged:	Final 50 10 5 190 Turbidity (NTU)
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mt) Time 1340 1345	e-purging) Did tubing + price Controlle pressure = Final Price Pressure = Final Price Pressure = Final Price Pressure = Final Price	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 60 Purge Rate (mL/min) ISO ISO	Water Cumulative Volume Purged (L)	NA psi 3 r Quality Pa Temp. (degree C) 22.39 21.66 21.55	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure actrical ductivity hos/cm 1.135	e/completion t-purging) D ing + pump v 6 ments pH 7, 40	n time: TW (ft. BT- volumes po		Final 50 10 5 180 Turbidity (NTU) 16.0 18.3
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mt Time 1340 1345 1350 1355	e-purging) Did tubing + price Controlle pressure = Final Price Pri	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 80 I 80 I 80 I 80	Water Cumulative Volume Purged (L)	PSi 3 Quality Pa Temp. (degree C)	4 uramete	Purge dat Final (pos No. of tubi 5 r Measure ectrical ductivity hos/cm 1, 135	e/completion t-purging) D ing + pump v 6 ments pH 7.42 6.24	n time: TW (ft. BT- volumes po	DO (mg/L) 12.58 2,07	Final 5 0 10 5 180 Turbidity (NTU) 16.0 18.3 21.7
Initial (pre Calculated Pneumati Initial air p Pressure (ps Refill Setting Discharge Se Flow rate (mt Time 1340 1345 1355 1400	e-purging) Did tubing + price Controlle pressure = Final Price Pressure = Final Price Pressure = Final Price Pressure = Final Price	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 I 0 5 I 60 Purge Rate (mL/min) ISO ISO	2 2 Water	Psi 3 r Quality Pa Temp. (degree C) 22.29 21.66 21.55 21.77	4 uramete	r Measure ectrical ductivity 1, 135	e/completion t-purging) D ing + pump v 6 ments pH 7. 42 6.24	n time: TW (ft. BT- volumes po	9/37/60 OC):	Final 5-0 10 5 180 Turbidity (NTU) 16.0 18.3 21.7 27.7
Initial (pre Calculated Pneumati Initial air p Pressure (psi Refill Setting Discharge Se Flow rate (mt Time 1340 1345 1350 1355 1400	e-purging) Did tubing + price Controlle pressure = Final Price Pri	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 IO 5 IGO Purge Rate (mL/min) ISO ISO ISO	2 2 Water	NA psi 3 r Quality Pa Temp. (degree C) 22.99 21.66 21.55 21.74	4 uramete	r Measure extrical duritivity	e/completion t-purging) D ing + pump v f f f f f ments pH 7. 42 6.24 6.26 6.26	n time: TW (ft. BT- volumes po	9/37/60 OC):	Final 5-0 10 5 180 Turbidity (NTU) 16.0 18.3 21.7 27.1 30.0
Initial (pre Calculated Pneumati Initial air p Pressure (ps Refill Setting Discharge Se Flow rate (mt Time 1340 1345 1355 1400	p-purging) Did tubing + price Controlle pressure = Historian DTW (ft. BTOC) 31.35 31.35 31.36 31.36 31.36	IW (ft. BTO ump volume or Tuning: I (ft.) X 0.43 Initial 50 IO 5 ISO ISO ISO ISO ISO ISO ISO ISO	Wate 2 2	Psi 3 r Quality Pa Temp. (degree C) 22.29 21.66 21.55 21.77	4 uramete	r Measure ectrical ductivity 1, 135	e/completion t-purging) D ing + pump v 6 ments pH 7. 42 6.24	n time: TW (ft. BT- volumes po	9/37/60 OC):	Final 5-0 10 5 180 Turbidity (NTU) 16.0 18.3 21.7 27.7



Sheet Z of Z

									
			Water Qual		ter Measurements	s (continu	ed)		
Time	DTW	Purge Rate	Cumulative				Eh	DO	Turbic
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Electrical 2 % Conductivity (UMinusicin)	·	(mv)	(mg/L)	(NTL
470-		<u> </u>	Purged (L)	±10%	(UMHUSTOR)	±0.1	1 10	±10%	+109
1420	31.21	180	2.5	22.64	1.66	6,25	-	12	215
1425	31.19	180	3.0	22.87	1.16	624	T	139	20
1430	31.17	180	3,25	22.45	1.171	6.22		1.85	1913
1435	31.16	180	3.7	23.09	1.17	6.20		2.26	18.
1440	31.18	180	3.9	23.18	17	618		3.08	17.5
1445	31, 19	180	4.0	12.34	117	6.17		3.34	15.
1450	31.18	180	4.3	23,23	1.17	617		3.87	
						——		- - >,0/ -	17.5
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					*				 -
									
						•	-		
		*;*****************		Sar	npling				
Time	eginning tim		Water C		Sampling co		me:	<u> </u>	
Table	(ft. BTOC)	(mUmin)	Cumulative	Temp.	Electrical	рН	Eħ	DO	Turbidity
	(120100)		Volume (Purged (L)	(degree C)	Conductivity		(mv)	(mg/L)	(UTV)
1500	31.19	130		23.42	(uMhos/cm)	T # C			\ Zl_ ==
			7.0 	47. (d		66		3.72	19.8
					-				
		·						 	
				<u> </u>			. ,	<u> </u>	
plicate sa it sample	29 mple collect collected (Y	ed (Y/N):		Sample II	nformation Sample collect Duplicate san Split sample I	nple ID:	ime:	1500	9/21/0
C No(s):_					·				
hoteau	Analysis I	Viethod	0	_ t				I	
VC			Cont	ainers	Requested A	nalysis	Method	Contair	ners
	7	8260	_200A	Containes					
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ments:									
nments:									

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - millifiter; L - Liter



Sheet 1 of 3

Operable	Unit/Site ID	: LHAAP	-29			Sampling	location ID	29WW	*40	
Project N	lame/#: L	HAP	//	759		Sample II): 29WW	40		
		loudy 3	2015				Time/Date		12:4	8
	<u> </u>			Dring	n line4	allation				
Dump inc	tallation cre	w A Dilit	A O			ananon Jactollofio	n date/begi	ning time	9/21/06	11.29
Lamb me	eading (wel	w. 11.001/0	word in the	V V	- Irrefort	Installatio	n date/comp	anny ame	9/21/06	11:31
				0.0	-	Pareen In	terval (ft. B	neggi dine.		159
Casing of	ameter (incl Depth (ft. B	nes):	59' bas				tervai (it. b ike depth (fl			
	: Depth (ft. E e-installation						ike depiti (ii MTO noball			
	er pump prin			5 bes	-		ainable pun			· ·
B	uct (circle):				-		ce of produ		, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	f water remo				-	Discharge	tuha diama	tor (3/8" or	1/4"): Y-3	7
	tube length			- <i>/</i>		Inlet redu	cerused (Y/	N): 144	1/4 / <u>1</u> }	
	ic Controlle		1-		-	illiet reuu	vei ,uaeu (13	147	<u> </u>	
	ressure = F		= 350) _{nei}						
botton on p	, COOG 10 1		,	·r		,		1		
<u> </u>		Initial	2	3	4	5	6	7 ·	8	Final
Pressure (ps		ļ		 	-/x-	ļ <u>.</u>	·	<u> </u>	ļ. <u>`</u>	<u> </u>
Refill Setting		ļ	 -	$+/\setminus$	$// \downarrow$	ļ		ļ		<u> </u>
Discharge S		 	<u> </u>	/ - /	4/51	 	 	ļ. —		
Flow rate (m	r1111111)		<u> </u>		urgir				<u> </u>	
Initial (pre Calculated Pneumati	e/beginning -purging) Dī I tubing + pu c Controlle ressure = H	TW (ft. BTO imp volume r Tuning:	c):! :!	Y Q √A psi	•	Final (post	e/completion t-purging) D ng + pump	TW (ft. BTC	C):(C)	58
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps	i)	250					· · · ·			250
Refili Setting		10								10
Discharge Se	etting	20							<u> </u>	20
Flow rate (ml		300								300
			Water	Quality Pa	ramete	r Measure	monts	·		
Time	DTW	Purge Rate	Cumulative			ectrical	pH	Eh	DO	Turbidity
,	(ft. BTOC)	(mL/min)	Volume	(degree C)		ductivity	ļ , , ,	(mv)	(mg/L)	(NTU)
	(-1, -1, -1,	(Purged (L)	(3)		hos/cm)	•		(5)	W /
	<u> </u>		3-41-7		. (4.5	31043 0111				

			~~~	1/ 0.2	1					
		J	see	Nex	-	- F 6	HC-			
-							·			
				·		-				
		· · · · ·								
									<u> </u>	



Sheet Z of S

		1	Water Quali	ity Paramet	ter Measurement	e leontinue	alt		· · · · · · · · · · · · · · · · · · ·
Time	DTW	Purge Rate	Cumulative			Hq		T	1
1	(fi. BTOC	, .	Volume		士。Electrical Conductivity) pii	Eh	DO	Turbidity
	' '	, , , , , , ,	Purged (L)		(uMhos/cm)	±0.1	士10	生 10%	(NTU) 土10%
11:44	51,25	300	3 - 4 - 7	24.4	2.0	9,93	98.7	146.2	110,6
1152	51,32	/		24.22	2.6	8.96	124.7	106.3	95.6
11:57	51.26			2421	9.7	813	127.1	97.7	59.7
12:00	51.28			24,22	2.8	2.8	127.6	93,2	37.2
1207	51.30			24.22	2.9	8,77	128.1	7.97	23.7
1913	51.38			2424	2,135	8.75	127.5	7.27	15.8
1217	51,37			24.24	3.19	8.79	26.4	7.19	1.2
1333	5140	<u> </u>		2421	. 3.2	8.73	125.4	7.08	
1327	51.32	V		24,27	3,24	8.72	125.6	7.05	7.G 4.0
1232	51.30			24.2	3,25	8.71	124.5	7.01	3.0
			35 L				123.2		
									
							\		
						·			
Sampling b	eginning tir	ne: 2:	36	· 	•	ompletion ti	me: 12	;40	·,
77	72738É				ameter Measure	ments			
Time	WTO		Cumulative	Temp.	Electrical	Hq	Eh	DO	Turbidity
	(ff. BTOC)	(mL/mln)	Volume 3	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
12:50	51.30	300	Purged (2)	711 01	(uMhos/cm)		<u></u>		
7-110		500	4 gal.	24.26	3.28	8.72		7.06	4.2
					·		· .		· · · · ·
									·
<u> </u>									
uplicate sa	29ww40 imple collected (sted (Y/N): Y/N):	No No	Sample	Information Sample coll Duplicate sa Split sample	ample ID:	N/A /	06 z::	35
equested		Method		tainers	Requested	Analysis	Method	Contair	ners
VOCs .		8260	3 soa	uple					
				· · ·					
···		<u> </u>							
. 6								· · · · · · · · · · · · · · · · · · ·	
								<u></u>	.
omments:									
		•							ł
					•				

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliter; L - Liter



Sheet <u>1</u> of <u>2</u>

Operable Unit/Site ID: LHAAD - 29						Sampling location ID: 24ww 35 - 214					
Project Name/#: LHAAP //759/						Sample ID: 29W W35 - 2 ⁻⁴					
Weather: clear, 68's						Collection Time/Date: 15:25 11/20/66					
Pump Installation											
Pump installation crew: A. William / S. Becringer						installation	date/begin	ning time:	1/20/06	14:52	
PID/FID reading (well head/background):						Installation date/completion time: 1/20/06 14:54					
Casing diameter (inches):						Screen Interval (ft. BTOC): 89 to 78					
Total well Depth (ft. BTOC): 93.30						Pump intake depth (ft BTOC):					
Initial (pre-installation) DTW/time: 4.14						Post-installation DTW/time: 41.10					
Final (after pump priming) DTW/time: 41.10						Max. sustainable pump rate (mL/min):					
Free product (circle): LNAPL / DNAPL						Appearance of product: None					
Volume of water removed during priming (mL):N						Discharge tube diameter (3/8" or 1/4"): 1/4"					
Discharge tube length (ft.): N Inlet reducer used (Y/N): N											
Pneumatic Controller Tuning:											
Initial air pressure = H (ft.) X 0.43 = <u>N</u> L psi											
		Initial	2	3	4	5	6	7	8	Final	
Pressure (psi)				1 1			.				
Refill Setting			1	1.11							
Discharge Setting			101	RIL			111	ASISI-			
Flow rate (mL/min)							4	100	L		
Purging											
Purging/sampling crew: A. Willmox S. Basinger PID/FID reading (well head/background): 6.0											
Purge date/beginning time: 11/20/06 1754 P							Purge date/completion time: 11/20/6¢ 1535				
Initial (pre-purging) DTW (ft. BTOC): NR						Final (post-purging) DTW (ft. BTOC):					
Calculated tubing + pump volume: NA No. of tubing + pump volumes purged:											
Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = N psi											
Initial air pressure = H (ft.) X 0.43 = NL psi											
		Initial	2	3	4	5	6	7	8	Final	
Pressure (psi)		156 -								150	
Refill Setting		10				·				10	
Discharge Setting		8							ļ	5	
Flow rate (mL/min)		150		L				<u></u>		150	
Water Quality Parameter Measurements											
Time	Time DTW Purge Rate Cumulative		Temp.	emp. Electrical		рH	Eh	DO	Turbidity		
ŀ	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity			(mv)	(mg/L)	(NTU)	
_	Purged (L)			(uMhos/cm)							
14:5 f	41.09	150	6.75	20.05	0.824		8.32	- 222.	6.96	14,	
15:02	41.08	150	1.5	20.04	0.824		8.32	-217.1	۵,95	13.1	
15.07	41.08	150	2.25	20.04	0.923		8.31	-205.4	0.92		
5:12	41.08	150	3.0	19.99	0.322		8.22	-210.5	0.80	10.3	
15:17	41.08	150	3.75	9.7	6,822		8.20	-213.3	6.84	10.8	
				,							
						ノレーノ					



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Sheet 2 of 2

Water Quality Parameter Measurements (continued) Purge Rate DO Turbidity DTW Cumulative Electrical Eh Temp. Time Conductivity (NTU) (ft. BTOC) (mL/min) Volume (degree C) (mv) (mg/L) Purged (L) (uMhos/cm) Sampling Sampling completion time: Sampling beginning time: **Water Quality Parameter Measurements** Cumulative DTW Electrical DO Turbidity Time Purge Rate Temp. Eh (ft. BTOC) Volume (degree C) Conductivity (mv) (mg/L) (NTU) (mL/min) (uMhosicm) Purged (L) ~~15.3 1530 0.82 0.50 41.08 150 5.0 Sample Information 29wws5 -2nd Sample collection date/time: W120/06 Sample ID: Duplicate sample collected (Y/N): Duplicate sample ID: Nem Split sample collected (Y/N): Split sample ID:_ NR COC No(s):_ Requested Analysis Method Containers Requested Analysis Method Containers 8266 Voc 40 mL Comments:

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1_of Z

Operable L						Sampling location ID: 29いいるとっていっ Sample ID: マロールいるとっていっ				
Project Nar			1173	591		•				
Weather:	clear	Hi 56's	co bos			Collection	Time/Date:_			
				Pump	Insta	llation				
Pump insta	lation crew	r 1. Wi	wares	5 B - 1.			date/begin	ning time:	11.6	117/4
PlD/FID rea	ading (well l	nead/backg	round): \	·9),				11:17 1	
Casing dia	neter (inche	es): HA	(E) "F			Screen Inte	erval (ft. BT6	OC : \sim	?? to ≏	
Total well I	lenth (ff Ri	.00). 	9669			Pump intal	ke denth (ft l	BTOC):	.32	
Initial (pre-i	netallation)	DT\W/time	29.70)		Pump intake depth (ft BTOC): 437				
			ne: 3641				inable pum			
Free produ				· · · · · · · · · · · · · · · · · · ·			e of produc			,
			oriming (mL)): N/A			tube diamet		1/4"): 3/8	<u>u</u>
Discharge				<i>J</i>		_	er used (Y/N		,	
Pneumatic	_						•	,		
Initial air pr		_	= <u>MM</u>	_psi						
<u> </u>		Initial	2	3,	, 4	5	6	7	8	Final
Pressure (psi	 \		- h				1_			
Refill Setting				N/J			7			
Discharge Se	ttina	****		1-6-6	0					
Flow rate (mL									·	
				P	urgin	a				,
Puraina/ea	mnling crew	. A Will	۱۵ سده ۲.	Becsinge	w. g	-	ading (well l	head/backo	round):(2.0
Purce date	/heainnina i	time: Wit	10h 11.	20			completion			
		W (ft. BTO							C): 36.3	a
		mp volume:	-/	IA.					ged:\/	
	: Controller	-					, g F F			· · · · · · · · · · · · · · · · · · ·
Initial air pr	essure = H	(ft.) X 0.43	= NR	psi						
			r			-		7	8	Final
D		Initial	2	. 3	4	5	6	· ' ·	<u> </u>	عح"
Pressure (psi)	<u> '</u> 					 		\	11
Refill Setting Discharge Se	Hina									4
Flow rate (ml.		100								100
i low rate (mic	21091)	100							I	
	<u> </u>	f		Quality Pa						
Time	DTW		Cumulative	Temp.		ectrical	Hq	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)		nductivity		(mv)	(mg/L)	(NTU)
	27 in	11 *	Purged (L)	M 20		lhos/cm)	101	m 1	-7 Ga	1.2
11.29	36.48	110	0.5	17.28		442	6.36	57.	299	13
11.34	36.39	100	10	17.33		479	6.38	\$5.0	785	
11:39	3639	100	1.5	17.27	<u>۲.</u>	488	6.39	54.0 52.9	7.64	0.1 8.0
11:44	36.39	100	2.0	17.46		496	V-39	51.1	2.55	
11:49	36.39	100	20	17.17		.496	6.39	<u> </u>	6.35	1.0
<u> </u>				,	<u> </u>		 			
<u> </u>					<u> </u>	·····		ι		
1					<u> </u>		<u> </u>		l	



Sheet Z of Z

		٧	Vater Quali	ty Paramet	er Measurements	(continue))		
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume	Temp. (degree C)	Electrical Conductivity (uMhos/cm)	рН	Eh (mv)	DO (mg/L)	Turbidity (NTU)
		<u> </u>	Purged (L)		(unnosiem)				
						1)
						1			
						W	m 160		-
						UV			
							MO. 4		
	<u> </u>		<u> </u>	S	ampling				
Sampling t	egînning tir	ne: <u>\\</u>	.ენ Water			completion to	ime: <u>\\</u>	5 Î	
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume	Temp. (degree C)	Electrical Conductivity	рH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
1200	36.58	100	Purged (L) べる.ち	17.14	(uMhos/cm) 4,441	6,39	50.9	7.31	1.0
			,	Sample	Information				
	ample colle e collected		No No		Sample col Duplicate s Split sampl	llection date ample ID:_ e ID:	/time:	1106 11	.50
COC No(s)		ΝΛ							
· · · · · · · · · · · · · · · · · · ·	l Analysis	Method		ntainers	Requested	l Analysis	Method	Conta	iners
Vocs		8260	7.40m	L Voas					
									<u>.</u>
Comment	3:								

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of 2

Operable U	Init/Site ID:	LHIAAP	- 29			Sampling le	ocation ID:_	29ww3] - 2 ^{no}	
Project Nar	ne/#: _ \- ^\	19-29	117	591	•	Sample ID:	290	0W37		
Weather:	clear,	503				Collection	Time/Date:_	10:50 11	117/00	
				Dum	Inoto	llation				
L		A	. ,	•	IIISta		ما مناه ما الما مناه	.: ši li	liniār is	_
Pump insta	illation crew	: <u> </u>	Marke 7.	Decrinacy				ning time: \frac{\frac{1}{2}}{2}		
			round):0	1.0		Installation	date/compl	etion time: i	47/06 10	
	meter (inche					Screen Inte	erval (ft. B10	OC): ලිදු	90' to	95
Total well D	Depth (ft. B1	OC): ~ 4:) 					BTOC):		
	nstallation)							time: <u>47.</u> 2		
	pump primi							rate (m∐n	nin):	
Free produ	ct (circle): _	LNAP	L / DNAPL	A		Appearance	e of produc	t: None	7106	
Volume of v	water remo	ved during p	oriming (mL)): <u>NB</u>		Discharge	tube diamet	ter (3/8" or 1	/4"): <u> </u>	
	tube length		<i>y</i> 6'			Inlet reduce	er used (Y/N	V);		
	: Controlle		114							
Initial air pr	essure = H	(ft.) X 0.43	=	_ psi						
		initial	2	, 3	A	5	6	7	8	Final
Pressure (psi)	}		1			1 ^	1			
Refill Setting				1.11	70_					
Discharge Sei	tting						WITH) <i>(</i>		
Flow rate (mL	/min)						WELL.			
				P	urgin	a				<u> </u>
Purging/sal	mpling crew	r A. usti	S. 200	Beesing	H 9-4-	-	ading (well l	head/backg	round): 0	-0
	/beginning t			- occation	v			time: \\[1]		
Initial (pro-	nuraina) DT	WAY OF FITO	C): 47 8.	3		Final (nost	-nuraina) D	rw (ft. BTO	c) 47.9	<u></u>
Calculated	tubing + pu	mn volume	·	 IA				olumes pur		
1	Controlle	-		···	•	710. 01 (00)	·g · pump ·	olumoo pu	9	
			= <u>NA</u>	nsi						
indui dii pi	000070 77				·					
		Initial	2	3	4	5	6	7	8	Final
Pressure (psi)	66 _								60
Refill Setting	·	11								
Discharge Se		4					_	i		
Flow rate (mL										4
Water Quality Parameter Measurements										4
	/min)	200	Water	Quality Pa	ramete	er Measure	ments			9
Time								Eh	ρO	
Time	DTW	Purge Rate	Cumulative	Temp.	El	ectrical	ments pH	Eh (my)		Turbidity
Time			Cumulative Volume		El Cor	ectrical ductivity		Eh (mv)	DO (mg/L)	
	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative	Temp. (degree C)	El Cor (uN	ectrical iductivity Ihos/cm)	рН	(mv)	(mg/L)	Turbidity (NTU)
10:17	DTW (ff. BTOC)	Purge Rate	Cumulative Volume Purged (L)	Temp. (degree C)	El Cor (uN	ectrical iductivity lhos/cm) 22.916	pH [2.07	(mv) -134.2	(mg/L)	Turbidity (NTU)
10:17 10:22	DTW (ft. BTOC) 41.86 41.86	Purge Rate (mL/min)	Cumulative Volume Purged (L)	Temp. (degree C)	El Cor (uN	ectrical iductivity (hos/cm) 22.9% 44.2.145	pH [2.07 [2.09	(mv) -134.2 -135.	(mg/L) -/.83 -/.68	Turbidity (NTU) 73 2 74.8
10:17 10:22 10:21	DTW (ff. BTOC) 41.86 47.86 47.86	Purge Rate (mL/min)	Cumulative Volume Purged (L) 1 2 3	Temp. (degree C) (6. 66 10.12	El Cor (uN ———————————————————————————————————	ectrical inductivity (hos/cm) 22.9/L 44.145 300	pH [2.07 [2.09 [2.13]	(mv) - 34,2 - 35. - 45.8	(mg/L) 83 68 24	Turbidity (NTU) 73.2 74.8 27.9
10:17 10:22 10:21	DTW (ff. BTOC) 41.86 47.86 47.86	Purge Rate (mL/min)	Cumulative Volume Purged (L) 2 3	Temp. (degree C) (6.66 (6.72 (6.73 (7.03	El Cor (uN ———————————————————————————————————	ectrical aductivity (hos/cm) 29 29 16 4 2 145 300 272	PH [2.07 [2.09 [2.13 [2.13	(mv) - 34.2 - 35. - 45.8 - 45.7	(mg/L) 1.83 1.68 1.24 1.24	Turbidity (NTU) 73 2 74.0 27.9 -29.7
10:17 10:22 10:27 10:37	DTW (ff. BTOC) 41.86 47.86 47.86 47.86	Purge Rate (mL/min)	Cumulative Volume Purged (L) 1 2 3 4	Temp. (degree C) 16.66 10.72 10.03 17.03	El Cor (uN 14 15 3.	ectrical inductivity (Inos/cm) 28 2.9 L 43 2.145 500 272	PH [2.07 [2.09 [2.13 [2.13 [2.14	(mv) - 34.2 - 35. - 45.8 - 45.7 - 52.7	(mg/L) 1.83 1.68 1.24 1.24 1.10	Turbidity (NTU) 73.2 74.8 27.9 24.7 77.1
10:17 10:22 10:21	DTW (ff. BTOC) 41.86 47.86 47.86	Purge Rate (mL/min)	Cumulative Volume Purged (L) 2 3	Temp. (degree C) (6.66 (6.72 (6.73 (7.03	El Cor (uN ———————————————————————————————————	ectrical inductivity (thos/cm) 2 2.9 // 2 3.00 2 7 2	PH [2.07 [2.09 [2.13 [2.13	(mv) - 34.2 - 35. - 45.8 - 45.7	(mg/L) 1.83 1.68 1.24 1.24	Turbidity (NTU) 73 2 74.0 27.9 -29.7
10:17 10:22 10:27 10:37	DTW (ff. BTOC) 41.86 47.86 47.86 47.86	Purge Rate (mL/min)	Cumulative Volume Purged (L) 1 2 3 4	Temp. (degree C) 16.66 10.72 10.03 17.03	El Cor (uN 14 15 3.	ectrical inductivity (Inos/cm) 28 2.9 L 43 2.145 500 272	PH [2.07 [2.09 [2.13 [2.13 [2.14	(mv) - 34.2 - 35. - 45.8 - 45.7 - 52.7	(mg/L) 1.83 1.68 1.24 1.24 1.10	Turbidity (NTU) 73.2 74.8 27.9 24.7 77.1



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		V	Vater Qualit	v Paramet	er Measurements	(continued	1)		
Time	DTW (ft. BTOC)	Purge Rate (mL/min)		Temp. (degree C)	Electrical Conductivity (uMhos/cm)	рН	Eh (mv)	DO (mg/L)	Turbidity (NTU)
		1				7 Ob			
Sampling b	eginning tir	ne: 10:5			ampling Sampling o rameter Measure	ompletion ti	me: 1C	5.54	,
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume Purged (L)	Temp. (degree C)	Electrical Gonductivity (uMhos/cm)	рH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
11:05	47.86	200	a	JL.56	3.201	12.14	-159.0	1.06	19.6
Sample ID: Duplicate s Split sampl COC No(s)	ample colle e collected	cted (Y/N):		Sample	e Information Sample col Duplicate s Split sampl	llection date ample ID: e ID:	/time: Ho No	7/06 (1	D: 56
Requested \\∂0	l Analysis	Method %265	US WL	ontainers	Requested	l Analysis	Method	Conta	niners
							, , , , , , , , , , , , , , , , , , ,		
Comments):								

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



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Operable L	Jnit/Site ID:	내	MAP-24			Sampling location ID: 29ww38-2-				
Project Nar	me/#: し	HMAP	1175	591	_	Sample ID: 24WW38 - 2M9				
Weather:	cha	v, 60%		•	_	•	Time/Date:			
				D	1	11_4!				
		6 . 1	-11 1	Pump	msta	llation				
Pump insta	illation crev	v. <u>β.ω</u>	Ill More	S. Becsin	vg-c-b	Installation date/beginning time: 11/20/06 3:52				
PID/FID rea	ading (well	head/backg	round):	0.0	•	Installation date/completion time: 1/20/06 13:54 Screen Interval (ft. BTOC): 36 to 45				
	(,					Screen Int	terval (ft. BT	FOC): 5	<u>ና</u> 'to_	45
Total well E	Depth (ft. B	тос): <u>"</u>	6			Pump inta	ke depth (ft	BTOC):	<u>-40'</u>	
		DTW/time:						//time: 3 /		
Final (after	pump prim	ing) DTW/ti	me: <u>3(_3</u>	7		Max. susta	ainable purr	ip rate (mL/i	miń): 229	<u> </u>
Free produ	ct (circle): _	LNAP	L / DNAPL			Appearance	ce of produc	ct: Non-	ι	
Volume of v	blume of water removed during priming (mL): NI- ischarge tube length (ft.): HP (MV U5' neumatic Controller Tuning: itial air pressure = H (ft.) X 0.43 = NI- psi						tube diame	eter (3/8" or	1/4"): //Y"	
Discharge t	neumatic Controller Tuning: itial air pressure = H (ft.) X 0.43 = NIP psi						er used (Y/	N):		
	charge tube length (ft.): HP (W 45') eumatic Controller Tuning: ial air pressure = H (ft.) X 0.43 = NP psi Initial 2 3 4									
Initial air pr	essure = H	(ft.) X 0.43	= <u>VIR</u>	_ psi						
										
Pressure (psi))		-	1	1		<u> </u>	 	<u> </u>	* ##di
				1	1//					
	lting	<u> </u>			1		<u> </u>	111261	4.0	
							 	11 50	<u> </u>	
								<u> </u>	<u> </u>	
		A . 111	1.10		Purgin	_				_
Purging/sar			more V	Bersing	V				round): c	3,0
Purge date/				1400		~	e/completion			
Initial (pre-p								TW (ft. BTC	,	
Calculated		•	;	NA		No. of tubi	ng + pump	volumes pui	rged:	
Pneumatic										
initial air pre	essure = H	(ft.) X 0.43	=	_ psi						
		Initial	2	3	4	5	6	7	8	Final
Pressure (psi))	@5 ~							>	35
Refill Setting		10								10
Discharge Set	ting	5				-				5
Flow rate (mL/	/min)	220								250
			Makey	Oustin Da					,	
T	DTW	I n		Quality Pa			I	1	r	
Time		i .	Cumulative			ectrical	pH	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	ł	ductivity	1	(mv)	(mg/L)	(NTU)
1000	2. 01	224	Purged (L)	12 44		hos/cm)				- A -
1402	31.3/	276		17.91		69;	9,9	-92.3	0.91	9,6
M67	31.3	226	3	17.90	<u>, 0,</u>	(8)	9.7	-92.0	0.96	9.5
1412	31.3	226		17.87	O,	582	9.7	-92,7	0.89	4.5
네구	3 31	230	ម	17.84	L 0,	65	9.6	-92.7	0.88	9.5
								 	- · DO -	740
		4							U.Do	710
	\$./\$								0.06	740
			~~						0.00	7.0



Sheet 2 of 2

117591

	-	V	Vater Quali	ty Paramet	er Measurements	s (continue	d)	·	
Time	pTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume Purged (L)	Temp. (degree C)	Electrical Conductivity (uMhos/cm)	рĦ	Eh (mv)	DO (mg/L)	Turbidity (NTU)
· · · · · · · · · · · · · · · · · · ·									
•									
Sampling	beginning tir	ne:				completion t	ime:	1	
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume	Quality Pa Temp. (degree C)	rameter Measure Electrical Conductivity	pH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
1435	31.30	25 Z20	Purged (L)	13.61	(uMhos/cm) 0.654	9.5	-93./	8.92	9.7
				Sample	Information				
Duplicate :	z 214 sample colle le collected):	cted (Y/N):_ (Y/N):	N		Sample co Duplicate s	llection date sample ID:_ le ID:	/time: [/ /Von-	120/06	14:25
	d Analysis	Method 8260		ontainers	Requester	d Analysis	Method	Conta	iiners
•				, Þ.					
Comment	s;								

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



Sheet 1 of 2

117591

	Unit/Site ID:				= .	Sampling location ID: LHAAP-27 296639-2					
		myhorn l	Priny Any	nation when	Plu	Sample ID	: 29w				
Weather:_	dear,	00 60	<u> </u>			Collection	Time/Date:	13:40		24/06	
				Pumr	Insta	llation	,				
Pump inet	allation crev	v A ldi	More S	Bessinge).).		. data/bagir	mina timo: I	1/20 IA.	15:10	
4 `		head/backg	morning).	4 V	V	Installation date/beginning time: \(\frac{1/20}{60.} \) \(\frac{15.'(c)}{60.} \) \(15.'					
	meter (inch		round)	<u> </u>		Coroon Int	on of /# DT		1 to	91	
_	Depth (ft. B		~9.61			Screen Interval (ft. BTOC): 81 to 91 Pump intake depth (ft BTOC): 867					
		DTW/time:		· ·		Post-installation DTW/time: 3.68					
		ing) DTW/ti	mo. 31	. 18		Max. sustainable pump rate (mL/min): 276					
•		LNAF		. 60		Apparan	anable putt	ip iate (iiitiii	10111)		
			priming (mL	\- 1 64		Appearance of product: Nen Discharge tube diameter (3/8" or 1/4"): /// "					
Discharge	tuba lanath	(ft.):~	ង់ ពុទ្ធ	·)AIA					1/4): 77		
_	c Controlle		17	······································	-	met read	er used (Y/	N):			
		(ft.) X 0.43	- 11/6	noi							
инцагал р	ressure – n	(11.) 1 0.43	- 101	_ psi	·			-			
		Initial	2	3	4	5	6	7	8	Final	
Pressure (psi	i)	·									
Refill Setting					<u> </u>						
Discharge Se								<u> </u>			
Flow rate (ml	/min)		<u> </u>	<u> </u>			<u> </u>			·	
Purge date Initial (pre- Calculated	Purging/sampling crew: A·Williage PID/FID reading (well head/background): O. 6 Purge date/beginning time: 11/20/06 Purge date/completion time: 11/20/06 Initial (pre-purging) DTW (ft. BTOC): Final (post-purging) DTW (ft. BTOC): No. of tubing + pump volumes purged: Pneumatic Controller Tuning:										
Initial air pr	ressure = H	(ft.) X 0.43	=	_ psi		y					
		Initial	2	3	4	5	6	7	8	Final	
Pressure (psi)	35 -								>	
Refill Setting		10				<u> </u>					
Discharge Se		5									
Flow rate (ml.	/min)	220	<u></u>					<u> </u>			
			Water	Quality Pa	ramete	er Measure	ments				
Time	DTW	Purge Rate	Cumulative	Temp.		ectrical	рН	Eh	DO	Turbidity	
	(ft. BTOC)	(mL/min)	Volume	(degree C)	i i	ductivity	•	(mv)	(mg/L)	(NTU)	
			Purged (L)		l	lhos/cm)			, , ,		
13:18	31.68	726		18.12		814	4.40	-212.4	0.7/	6./	
13:25	31.68	226	2.	18.11		813	4.41	-217.6	0.61	1.5	
13:28	31.68	120	3	18.11		808	4.41	-215.5	0.54	5.4	
13:33	31.68	550	4	18.12		808	9.41	-217.7	0.51	5.4	
13:38	31.68	220	5	18.20		808	9.40	- 2/9.2	1.49	5.6	
							· · · · · ·		 		
								·	and the same	· · · · · · · · · · · · · · · · · · ·	



Sheet Z of Z

117591

		γ	Vater Quali	ty Paramet	er Measurements	(continue	d)		· · ·
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume Purged (L)	Temp. (degree C)	Electrical Gonductivity (uMhos/cm)	рΗ	Eh. (mv)	DO (mg/L)	Turbidity (NTU)
			1						
		0	1		11/20/0		·		
(
<u> </u>				S:	mpling	1			
Sampling b	eginning tir	ne: 1):			, -	completion t	ime:		
Time	DTW (ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume Purged (L)	Temp. (degree C)	Electrical Conductivity (uMhos/cm)	На	Eh (mv)	DQ (mg/L)	Turbidity (NTU)
13:45	31.69	Bens	28	12.19	0.888	9.41	-218.	0.50	5.3
Sample ID: Duplicate s Split sampl COC No(s)	24ww ample colle e collected	31 - 2nd cted (Y/N):_ (Y/N):	Na	Sample	Duplicate s	llection date sample ID:/	e/time: 11/2 Han Venu	<i>o</i> / d6	13:41
Requested	l Analysis	Method \$266		ontainers ML Voas	Requested	d Analysis	Method	Cont	ainers

Comments	> .							· · · · · · · · · · · · · · · · · · ·	

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter

2.2

17

121.6

123.2

8.77

7.14



0925

0930

49.00

49.00

300r

360

10.5

12.0

70

21-21

z. 231

3.237

GROUNDWATER SAMPLING FORM

Sheet 1 of 2

LHAAP-29 Operable Unit/Site ID: Sampling location ID: 29Ww 40 - 2nd Project Name/#: LHABP Sample ID: 2966 46. 744 11/21/00 Weather: Sunny cool 40% to 503 Collection Time/Date: 0950 **Pump Installation** Pump installation crew: A. MushorE Robert Owens Installation date/beginning time: "Valloe PID/FID reading (well head/background): Installation date/completion time: 11/21/06 0843 Casing diameter (inches): Screen Interval (ft. BTOC): 149 159 695 Total well Depth (ft. BTOC): Pump intake depth (ft BTOC): 154 bas Initial (pre-installation) DTW/time: 49.00 Post-installation DTW/time: Final (after pump priming) DTW/time: NR Max. sustainable pump rate (mL/min): 300 Free product (circle): LNAPL / DNAPL Appearance of product: Non-NK Volume of water removed during priming (mL): Discharge tube diameter (3/8" or 1/4"): Discharge tube length (ft.): Inlet reducer used (Y/N): Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = \(\mathcal{D}\mathcal{L}\) Initial 3 5 6 7 8 Final Pressure (psi) Refill Setting Discharge Setting K Flow rate (mL/min) Purging Willmore, tu Robert Owens Purging/sampling crew: Allen 0.0 PID/FID reading (well head/background): Purge date/beginning time: Purge date/completion time: Initial (pre-purging) DTW (ft. BTOC); 49.00 Final (post-purging) DTW (ft. BTOC): Calculated tubing + pump volume: NA No. of tubing + pump volumes purged: Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = NP Initial 5 6 Final Pressure (psi) Refill Setting Discharge Setting Flow rate (mL/min) Water Quality Parameter Measurements DTW Time Purge Rate Cumulative Temp. Electrical Εħ DO Turbidity (ft. BTOC) (mL/min) Volume (degree C) Conductivity (mv) (mg/L)(NTU) Purged (L) (uMhos/cm) 0835 49.00 300 1.5 21.06 ८.94 3.241 <u>.79</u> 1-3.6 713 0960 49.00 30¢ 3.0 3.240 122.9 75 7.12 0905 49.00 300 4.5 3.239 8.76 120.1 7.14 4.3 0910 49.00 300 6.0 21.18 3 237 8.78 121.3 2.13 4.4 0915 49.00 300 7.5 21.21 3.737 2.40 122.4 7.14 0920 3-237 49.00 300 9.6 2(18 . 18 121.4 7.16



Sheet Z of Z

		V	Vater Quali	ty Paramet	er Measurements	(continue	d)	-	·····
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uMhos/cm)				' '
0935	49.00	306	13.5	21.28	3,238	6,77	124.1	7.19	[-]
0940	49.00	30 5	15.0	21.21	3 230	9.78	123,9	7.15	0,4
1945	49.00	350	16.5	21,72	3,239	8.78	123.7	7.15	6.3
		~							
			//						
<u> </u>			/		1				
<u> </u>			$ \Lambda$	$\Lambda V \Lambda$					
		!		,000	- 115	11/16			
		/ _		7/	/// ,	L U			
	1		•		\				
					· · · · · · · · · · · · · · · · · · ·				
		·							
									<u> </u>
		•	• •	Sa	ampling		_		
Sampling t	eginning tin	ne: <u>0</u> 6	<u> 150 </u>		Sampling c	ompletion t	ime: <i>0</i> 9	55	
			Water	Quality Pa	rameter Measure	ments			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рH	Eh	DO	Turbidity
İ	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
<u> </u>			Purged (L)		(uMhos/cm)	- A-A			
9957	49-00	300	13.5	21.06	3.238	8.78	23.4	7.10	0.1
<u> </u>				,					
			ŕ	Sample	Information				
Sample ID:	ଌ୳୷୷	0-2nd			Sample col Duplicate s	lection date	/time: 0°	950 W	4/06
Duplicate s	ample colle	cted (Y/N):_	Yes		Duplicate s	ample ID:_	29ww464	DUP #6	MS/MSD
	e collected	(Y/N): <u> </u>			Split sample	e ID:/\ ^{\textstyle}	A		
COC No(s)	:	NR							l
Requester	l Analysis	Method	r.	ntainers	Requested	Analysis	Method	Conta	inore
	. Midly 313	8266		L Voa V		Allalysis	Menioa	COME	inters
10.5	·	0	10 1	· Dec VI	<u>""</u>				
Comments	i:	٠٠,	ن	_					
~ ~ 11111111111111111111111111111111111		1001-	FIELD	Dopuci	HES O MS/N	بر (له ۱۶			j
				.,,	· · ·	- •			

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliter; L - Liter



Sheet 1 of 2

Operable Unit/Site ID: LHAR F Snc 29 Project Name/#: Wew Sampung @ 29 //759/						Sampling location ID: Size 29						
Project Na	ıme/#: <u>Ν€</u>	ul Samplin	19 e 29	_//759/	· -	Sample ID: 29 WW46						
Weather:_	wet 7	٠٥,				Collection Time/Date: 12-19-01/1536						
			·	Pumr	Inst	allation						
Pump inst	allation crev	w A. W	LI MADE	S. McAdoo	, 1110tt		n date/begir	nina timo:	12-10-81	1 1426		
DID/FID ro	adina /wall	hood/back	round).	4 A								
Capina dia	motor (inch	head/backo	inguina).	<u> </u>		Installation date/completion time: 12·19·06 / /42² Screen Interval (ft. BTOC):/53to 163						
Total wall	Donth (# D	TOC):	1.2 /							163		
) DTW/time:					ke depth (ft		158			
				10		Post-installation DTW/time: 48.99						
		ning) DTW/ti		14			ainable pum			<u> </u>		
£		LNAF		· · · · ·			ce of produc			it		
		ved during		-): <u>NA</u>			tube diame		1/4"): <u>"14</u>			
-	_	(ft.): <u>\</u>	96		-	iniet reduc	er used (Y/	N): <u>No</u>				
	neumatic Controller Tuning: itial air pressure = H (ft.) X 0.43 =NR psi											
initial air p	ressure = H	(ft.) X 0.43	= <u>NK</u>	_ psi								
		Initial	2	3	4	5	6	7	8	Final		
Pressure (ps	i)	<u> </u>	<u></u>	<u> </u>	<u> </u>							
Refill Setting	- Alexandria		<u> </u>									
Discharge Se	etting					11.	A		1/			
Flow rate (ml	_/min)	100.00										
		········		P	urgin	a						
Purging/sa	ımplina crev	v: A.Wi	Ilmore 5	S. McAdoo		_	ading (well	bead/backo	aronad). \), c)		
		time: [42					e/completion	~	- ,	<i>,,</i> <u> </u>		
		W (ft. BTO		,					OC): 48.9	4		
		ımp volume		NA			ng + pump י			<u> </u>		
	c Controlle	•	·	37.	-	IVO. OF LADI	ng i pump	volumes pu	igeu. 14			
		(ft.) X 0.43	= 112	nsi								
		(111) 71 01 10		_ poi						···		
		Initial	2	3	4	5	6	7	8	Final		
Pressure (psi)	256 -							>	250		
Refill Setting		10								10		
Discharge Se	tting	\$								5		
Flow rate (ml	/min)	350		<u> </u>			<u> </u>	<u> </u>	<u> </u>	356		
			Water	Quality Pa	ramete	er Measure	ments		•			
Time	DTW	Purge Rate	Cumulative			ectrical	pН	Eh	DO	Turbidity		
	(ft. BTOC)	(mL/min)	Volume	(degree C)	1	ductivity		(mv)	(mg/L)	(NTU)		
		, ,	Purged(L)	`		hos/cm)	[(,	(****3***)	(,,,,,,,		
1430	48.48	356	700	21.63	3.2		2.80	124.7	7.09	02		
1935	48.98	350	2450	21.04		18	8.91	123.2	7.08	6.		
1440	48.95	356	4200	21.07		39	8.92	12-3.1	7.05	4.5		
1445	48.91	350	5950	21.06	3.2		8.80	122.9	7 06			
1450	49,98	350	1700	21.07	3, 2		8.80	135'0	9.11	9.1		
1955	48.98	350	9450	21.67	3,2		8.81	Ls. 8	7.12			
1500	4 8.48	350	11200	21.07	3.2		8.80		712	5.0		
1565	48.98	350	12 950		3.5			123.4	7.13	2.1		
1 103	עייטו	77.	16 11-	21.04	1, 4,	<u>, , , , , , , , , , , , , , , , , , , </u>	8.8>	1.43.17	7.9	1.6		



Sheet of 2

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	•	V	Vater Quali	y Paramet	er Measurements	(continued	l)			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рĦ	Eh	DO	Turbidity	
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)	
			Purged (L)		(uMhos/cm)					
1516	40.98	350	14700	21.0b	323 8	2.85	124.1	7.08	6,0	
1615	49.98	350	16450	21.06	3.237	6.30	79.9	7.09	გ.∂	
1520	48, 98	3 50	18200	21.00	7,237	\$.30	123 V	ጉወ3	6.6	
			1	,						
			1 11							
	1	1	k \ \							
· 			$\mathcal{N}_{\mathcal{N}}$	7						
		\ · ·				10 1 Ma				
		\mathcal{V}			1/2	1/2/0				
	J					1				
ļ						-				
						<u> </u>			1	
				S	ampling					
Sampling b	eginning tir	ne: <u> 5.2</u>	0		Sampling of	completion t	me: <u>ເຽງ?</u>	<u></u>		
Water Quality Parameter Measurements										
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity	
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)	
			Purged (L)		(uMhos/cm)					
1540	48.98	350	~20	21.63	3.240	8,79	124.0	7.01	0.0	
				Sample	e Information					
Campia ID	SITE	29		Jumpn	Sample co	illection date	/time: 12	19.06 x	: 36	
		ected (Y/N):			Duplicate:	ollection date sample ID:_ ole ID:	NV	-1-1	+ 30	
		(Y/N):			Split samp	le ID:	NA			
COC No(s)		(· / · / ·	YIR.							
 		1							_	
	l Analysis	Method		ontainers		d Analysis	Method	Cont	ainers	
Voc		8240	3. 40 ml	You vie	LJS					
<u> </u>		ļ						ļ		
<u> </u>				<u> </u>						
Comment	s:				,					
1					-					
l										

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

			RFA / COC Numb	er:1	0957
Location Code:				Task:	MNA_EVENT_FEB07
Sample Number:	29WW06- Feb :	2007	Collect	on Date:	2-22-07
Sample Name:	29WW06-GW-29	WW06REG			1500
Sampling Method:	SP				32.5
Sample Type:	GW	Sample Purpose: R			29.85
	tainles Ste	el Bladder	Remp Sampl	e Matrix:	WATER
rtners: B)	(ER)	(<u>FB</u>)	Samp	le Team:	Willemore, W.Fldor
Analytical Suite	Containe Flt Frtn Qty Size	T		ERPIM	IS Values: Sacode:
VOC-FULL	N A 3 40	Court of the Control of Control of the Control of Contr		Lo	t Control#:
ANIONS	N B 1 500	mL HDPE			
PERC	N C 1 500	mL HDPE			
GASES	N D 2 40	mL VOA Vial			
ALKALINITY	N E 1 100	mL HDPE			
TOC_415	N F 1 100	mL HDPE			
DHC	N G 1 1	L Amb. Glass			
Groundwater Info Measured Wo Comments:	ormation: ell Depth: <u>35.1</u>	9 Depth To V	Water: <u>29.81</u>	·····	
			<i>p</i> 113		

Logged BY / Date: Reviewed BY / Date: ______



00091684

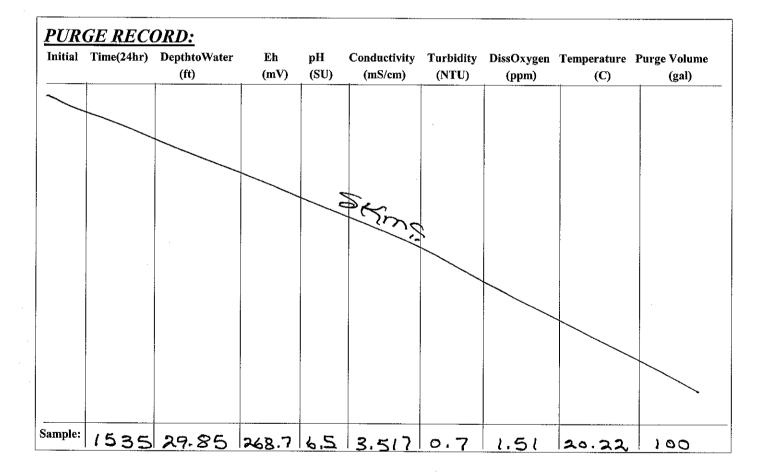
Page 2 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW06

Sample Number: 29WW0676b2007



Logged BY / Date: Sherry M. F. Plan 2-22-07

Reviewed BY / Date:



00091685 Sheet <u>1</u> of 2

Operable	Unit/Site ID	LONG	horn,	Sites	9	Sampling	location ID	: 29 W	J06	
Project N	Unit/Site ID ame/#:	, Nghoi	AA US	ર્				W P 6 -		507
Weather.	SULLIN	พัธร	. •					2-22-		500
				Pum	n Inst:	allation				
Dump ins	tallation cre	b):11a	- a- W		-		1	• ••		
						Installatio	n date/pegii	nning time:	3-22-01	, 1430
Casina di	eading (well	i nead/back(grouna). <u></u>	0/5/0	_	installatio	n date/com	pletion time	2-22-8	<u>1430</u>
	ameter (incl				-			TOC):2		35.19
	Depth (ft. B			<u> </u>				t BTOC): 🟒		
	-installation				-			V/time: a		
	er pump prim				<u>-</u>			np rate (mL/		
	uct (circle):				-	Appearan	ce of produ	ct: yell	nich	<u> </u>
	f water remo			L):		Discharge	e tube diame	eter (3/8" or	1/4"):_ -7/8	**
	tube length		<u> </u>		_	Inlet reduc	cer used (Y	/N):_ _\		
	ic Controlle	_								
Initial air p	ressure = F	I (ft.) X 0.43	; =	_ psi	_					
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps						CIA				
Refill Setting					<u> </u>	akn	15:	T		
Discharge Se								+	+	
Flow rate (m	L/min)				Τ				1	
Pneumati	l tubing + pu c Controlle ressure = H	r Tuning:		NA psi	-	No. of tubi	ng + pump	volumes pu	rged:	
		Initial	2	T	1 4	· _	1 _			r
Pressure (psi	n	ag ag	20	3	30	5	6	7	8	Final
Refill Setting)	10	-	20	20		 	<u> </u>	 	
Discharge Se	Hina	85	5	<u>10</u>	5		ļ	ļ <u>.</u>		
Flow rate (mL						<u> </u>	 			<u> </u>
TOW TOTAL	7600)	100	100	100	100	<u>L</u>		I		<u> </u>
	T	ı		Quality Pa	1		ments			
Time	DTW	Purge Rate	Cumulative	Тетр.	I.	ectrical	рH	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Con	ductivity		(mv)	(mg/L)	(NTU)
	-0.65	ļ	Purged (L)			lhos/cm)				
144-2	29.85	100	100	1991		510	6.41	224.6	1.81	2.3
1450	29.85	₹00	200	19.89		50¥	6.41	227.6	1.61	a.3
1455	29.85	100	300	19.89	3,5	501	6,44	234.6	1.42	1.5
1500	29,85	100	400	19.94	3.5	400	6.45	240.1	1,39	1.4
	 -			·						
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l l	i i	l l			İ	1				



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		1	Vater Quali	tv Parame	ter Measurements	(continue	ed)	· · · · · · · · · · · · · · · · · · ·	
Time	DTW	Purge Rate		Temp.	±3% Electrical	Hq	Eh	DO	Turbidity
	(ft. BTOC)		Volume	(degree C)	エクル Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	± 10%	100%
	1	***************************************	J	_ 10 10	(2,,,,,,,,	 	- ,	- 10 /6	1
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	 	\rightarrow		2				ļ	
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		ļ	<u> </u>						
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	<u> </u>	ļ							
									
			<u> </u>						
				S	ampling				
Time	DTW	Purge Rate	Water Cumulative	Quality Pa	rameter Measure Electrical	ments pH	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uMhos/cm)		, ,	(***3)	()
1535	29.85	100	500	4	3,517	6.5	248.7	1.51	0.7
			SKIM	20.22				1 - 1 !	<u> </u>
				5 ,					

····				<u> </u>	1		<u> </u>		
ال خامسة	. 70. 1. 1		1 -		Information				
ample iD.	: <u>೩೪ ಬ ಬ</u> sample colle	106- FE	<u>D 2007</u>				e/time: <u>2 - 2</u>	2-07	
	sample colle le collected		N		Duplicate s				
PIR Sampi): 109	(1/N):	14		Split sampl	e ID:]	N		
OC NO(S))	<u> </u>							
equester	d Analysis	Method	Co	ntainers	Requested	Analveie	Method	Conta	inore
1100		82603		<u></u>	Perchio		3(4.0	/ Jointa	miers
				₹					
LACEC		415.1		<u> </u>	B(KA)		310.0	<u></u>	
	7			>	Explo	Zinez		<u> </u>	
SASES TOC				<u>t</u>					
TOC	S	300.0	· · · · · · · · · · · · · · · · · · ·	. 1	i i				
TOC PUISION	es Les	376.2		1					
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TOC WISION	es Les	376.2	ellow	ish ?	tannia				



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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

•			RF	'A / COC Number:	
Location Code: Sample Number: Sample Name: Sampling Method: Sample Type: Sampling Equip:	29WW15- 29WW15-GW-2 SP		REG ple Purpose: REG	Task: Collection Date: Collection Time: Start Depth:	MNA_EVENT_FEB07
rtners: B)	(ER)		(FB)	-	AW/cu
Analytical Suite VOC-FULL ANIONS PERC GASES ALKALINITY TOC 415 DHC		e Units mL 0 mL 0 mL 0 mL	Type VOA VIAL HDPE HDPE VOA VIAI HDPE WOA VIAI HDPE HDTEVDA Amb. Glass	ERPIM:	S Values: Sacode: Control#:
Groundwater Int Measured W Comments:	formation: /ell Depth:		Depth To Water:	Explosi	ves ~ 1 L Amb.



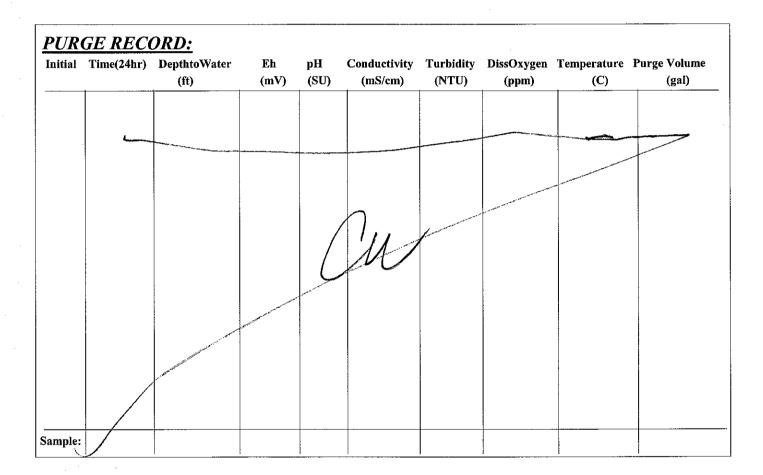
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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW15
Sample Number: 29WW15-



Logged BY / Date: (. Winser 7/14/, Reviewed BY / Date:



 $\underset{\text{Sheet} \underline{\textbf{1}} \text{ of } \underline{\textbf{M}}}{\textbf{1}}$

Operable	Unit/Site ID	LAAZ	P			Sampling	location ID:	19 111	11.16	
Proiect N	ame/#: 🗘	ILAAP	-29			Sample II	location ID: D: 29 W	NIS	CER	2007
Weather:	ame/#:_L Overcas	F, Rain	y 65-	-70°	- -		Time/Date		rep (20/
				Pum	o Inst	allation				
Pump ins	tallation cre	w: <u>A W:11</u> ,	nore /C.b	Uinzev .	•	Installatio	n date/begiı	nnina time:	NA	
lPID/FID n	eading (well	l head/back	around).	ρ			n date/com			,
Casing di	ameter (incl	nes): 4 "	Stain	ers Stee	Ì		terval (ft. B]			23 89
Total well	Depth (ft. B	TOC): 33	32		·1		ike depth (fi			
	-installation					•	llation DTW	, _		
	er pump prin				•		ainable pun			Λ
	uct (circle):				•		ce of produ			<u> </u>
	f water remo				•		tube diame			A
	tube length			,			cer used (Y/			
Pneumat	ic Controlle	er Tuning:					(1)			
Initial air p	ressure = H	f (ft.) X 0.43	i =	_ psi						
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps	si)	ļ <u>.</u>			<u> </u>					
Refill Setting			12.	()		Dod				
Discharge S			D	MCC2	<u> </u>	PHI				
Flow rate (m	L/min)									
Calculated Pneumati	-purging) DT I tubing + pu c Controlle ressure = H	ımp volume <mark>r Tuning:</mark>	:	VA	-		-purging) D ng + pump י			
miliai ali þ	ressure – n	· · · · · · · · · · · · · · · · · · ·	1	_ psi						
5 /		Initial	2	3	4	5	6	7	8	Final
Pressure (ps				<u> </u>					<u> </u>	
Refill Setting		<	1	1897 -		·				<u> </u>
Discharge Se Flow rate (ml			7	עשיי						
riow rate (IIII	<i>-21000)</i>	<u></u>	<u> </u>	<u> </u>	<u>. </u>		<u> </u>			<u> </u>
		·	Water	Quality Pa	ramete	er Measure	ments			
Time	DTW	Purge Rate	Cumulative	Temp.	EI	ectrical	рH	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Con	ductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uM	lhos/cm)		_	, , ,	
								4		
				\ <u>.</u>		1				
				III()	44			9		
				, <u> </u>			h	J		
							VL	7		
		i	i	į			Y			



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Sheet ___of ___

		1	Nater Quali	ty Paramet	ter Measurements	s (continue	d)		
Time	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	= 10%	± 10%
						<u> </u>			
···									
	<u></u>			1					
								77.0	
									
								<u> </u>	
									*
					*****	-			
									
				9.	ampling		<u> </u>		
Sampling b	eainnina tir	ne: D : -	ő	•		completion t	ime.		
	3	t		Ovelity De					
Time	DTW	B B.4.	1		rameter Measure	,	·	T	
irne		Purge Rate	Cumulative	Temp.	Electrical	рΗ	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uMhos/cm)				
					- THE PART OF THE	The state of the s	A STATE OF THE STA		
					A				
		And Should be seen							
	Mark W. Sand Steff and St. of	_		Sample	Information				
Sample ID:	29 W	W15		•	Sample col	lection date	/time: 2/	24/07/	p(35
Duplicate s	ample colle	cted (Y/N):_	\mathcal{N}		Duplicate s	ample ID:	No.	<u> </u>	
Split sampl	e collected	(Y/N): _	/		Duplicate s Split sampl	e ID:	10		
COC No(s)	• •				, , ,				
Paguagia d	Analysis	Madhad						_	
				ntainers	Requested		Method	Conta	iners
<u> 100</u>		8260B		<u>3</u>	PERCHI		314.0		
<u>Gases</u>	~ CO2	502175		3	- HIKAL		310.0		
Toc		415.1	·	3	Explos	جن دخ		<u> </u>	<u> </u>
ANior		300.0		}					
<u>sulfi</u>	des	376.2		1					
Comments	of w	ater in	well.	Bailed	dry @ 3:301	on. 2/20	1/07		
	541	L.	rr. 2.3	7	7	, , , ,	/ .		
		, ,		<u> </u>					



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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

		RFA /	/ COC Number: 10957
Sample Name: ampling Method: Sample Type: ampling Equip: S	29WW35-Feb; 29WW35-GW-29 SP GW	*	Task: MNA_EVENT_FEB07 Collection Date: 2-22-07 Collection Time: 1245 Start Depth: 42.70 Sample Matrix: WATER
ners:	(E <u>R)</u>	(<u>FB)</u>	Sample Team: Willemore Ms Ado
Analytical Suite	Containe Flt Frtn Qty Size		ERPIMS Values: Sacode:
VOC-FULE ANIONS PERC GASES ALKALINITY FOC 415 DHC	N A 3 40 N B 1 500 N C 1 500 N D 2 40 N E 1 100 N F 1 100 N G 1 1	mL HDPE mL HDPE mL VOA Vial mL HDPE	Lot Control#:
Groundwater Info Measured W	ormation: ell Depth: <u>95</u>	Depth To Water: _3	u. 45 42.84

Logged BY / Date: Sperry MEAdoo

Reviewed BY / Date:



00091692

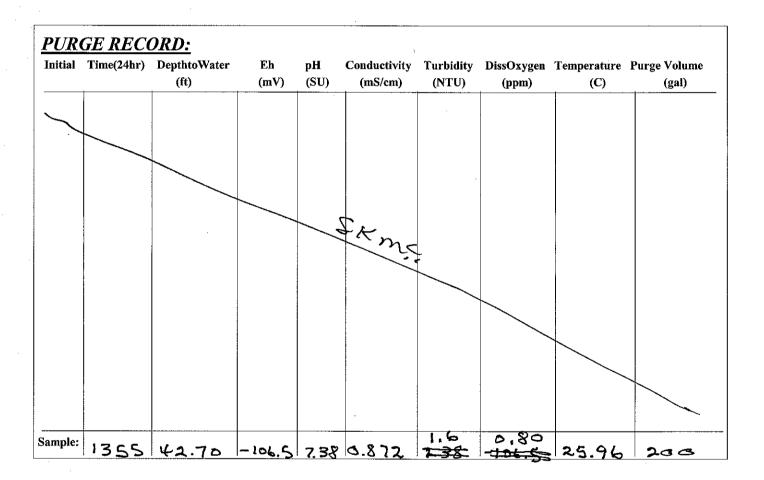
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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW35

Sample Number: 29WW35-Feb2007



Logged BY / Date: Sherry MEAles

Reviewed BY / Date:



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Sheet 1 of 2

	Unit/Site ID	LONSO	hores,	5, te 29	<u>}</u>	Sampling	location ID:	29WL	135			
Project Na	Project Name/#: Langhorn AAP Veather: Suny 605 Sampling location ID: 29ww35 Sample ID: 29ww35 Collection Time/Date: 2-22-57, 1245											
Weather:_	Sun	44 60	≤									
				Pumi	a Ineta	allation						
Dumn inct	tallation area		· Y				1					
DID/EID **	tallation cre	w. <u>w.u.</u>	Malee 17	11-1	3	installatio	n date/begir	nning time:	x12-07	, 1125		
	eading (well		ground): 🛂 .	2(01.	-	Installation	n date/comp	oletion time:	2-2207	,05		
	ameter (inch		3 - 1							<u>45</u>		
	Depth (ft. B			21		· · · · · · · · · · · · · · · · · · ·	• •	BTOC):				
	-installation							//time:_ <u>ሦ</u> ৯				
	r pump prim			SKW	15			ıp rate (m∐		<u> </u>		
	uct (circle):				•	Appearan	ce of produc	ct:	J			
	f water remo			_):				eter (3/8" or	1/4"): 3/ &	<u>" </u>		
_	tube length	· · —	<u>1' </u>		_	Inlet reduc	er used (Y/	N): 				
	c Controlle	-										
Initial air p	ressure = F	f (ft.) X 0.43	=	_ psi								
		Initial	2	3	4	5	6	7	8	Final		
Pressure (ps	i)						i i	 	 	11101		
Refill Setting					2	Km:		 				
Discharge Se	etting					Lie						
Flow rate (ml	L/min)		<u> </u>									
				r). remain		<u> </u>					
Duraina/co	mpling arou	.11 / 14	^		urgin							
							77 / 17	1 11 11		; e/		
Duran data	ampining cicy	4:mo: 2	Vase 11	SAdoa_				head/backg				
Purge date	e/beginning	time: <u>2-2</u>	2-07, 11	30		Purge date	e/completion	n time: _2_2	2-07 15	140		
Purge date Initial (pre-	e/beginning -purging) D1	time: <u> </u>	2-07, 11 C): 42.	30 20		Purge date Final (post	e/completion -purging) D	n time: <u>2-2</u> TW (ft. BTC	2-67, 12 (C): \$2	140		
Purge date Initial (pre- Calculated	e/beginning -purging) D1 I tubing + pu	time: <u>2 – 2</u> FW (ft. BTO ump volume	2-07, 11 C): 42.	30		Purge date Final (post	e/completion -purging) D	n time: _2_2	2-67, 12 (C): \$2	140		
Purge date Initial (pre- Calculated Pneumatie	e/beginning -purging) Dī I tubing + pu c Controlle	time: <u>2 - 2</u> FW (ft. BTO ump volume r Tuning:	<u>ス-07, 1)</u> C): <u>七名.</u> :	30 ?o NA	-	Purge date Final (post	e/completion -purging) D	n time: <u>2-2</u> TW (ft. BTC	2-67, 12 (C): \$2	140		
Purge date Initial (pre- Calculated Pneumatie	e/beginning -purging) D1 I tubing + pu	time: <u>2 - 2</u> FW (ft. BTO ump volume r Tuning:	<u>ス-07, 1)</u> C): <u>七名.</u> :	30 ?o NA	-	Purge date Final (post	e/completion -purging) D	n time: <u>2-2</u> TW (ft. BTC	2-67, 12 (C): \$2	140		
Purge date Initial (pre- Calculated Pneumatie	e/beginning -purging) Dī I tubing + pu c Controlle	time: <u>2 - 2</u> FW (ft. BTO ump volume r Tuning:	<u>ス-07, 1)</u> C): <u>七名.</u> :	30 ?o NA	4	Purge date Final (post	e/completion -purging) D	n time: <u>2-2</u> TW (ft. BTC	2-67, 12 (C): \$2	140		
Purge date Initial (pre- Calculated Pneumatie	e/beginning -purging) D1 I tubing + pu c Controlle ressure = H	time: 2-2 FW (ft. BTO ump volume r Tuning: (ft.) X 0.43	2-07, 11 C): 42. : = NR	30 70 NA psi	4 55	Purge date Final (post No. of tubin	e/completion -purging) D ng + pump	n time: <u>2-2</u> TW (ft. BTC volumes pu	2-67, 13 0C): \2 rged:	70		
Purge date Initial (pre- Calculated Pneumation Initial air po	e/beginning -purging) D1 I tubing + pu c Controlle ressure = H	time: 2 - 2 FW (ft. BTO) ump volume r Tuning: (ft.) X 0.43	2-07, 1) C): 42, : NR	30 70 NA psi 3		Purge date Final (post No. of tubin 5	e/completion -purging) D ng + pump v	time: <u>2-2</u> TW (ft. BTC volumes pui	2-67, 13 0C): \\2 rged: 8 55	70		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H	time: 2 - 2 FW (ft. BTO) ump volume r Tuning: (ft.) X 0.43 Initial	2-07.11 C): \(\frac{1}{2}\). \(\frac{2}{55}\)	30 70 NA psi 3 55	55	Purge date Final (post No. of tubin	e/completion -purging) D ng + pump	r time: 2-2 TW (ft. BTC volumes put	2-67, 13 0C): \2 rged:	70		
Purge date Initial (pre- Calculated Pneumatic Initial air po Pressure (psi Refill Setting	e/beginning -purging) DT I tubing + pu c Controlle ressure = H	time: 2 - 2 FW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20	2-07.11 C): 42.	30 NA psi 3 55 20	55 20	Furge date Final (post No. of tubin	e/completion-purging) Ding + pump	7 55	8 55 20 8	70		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se	e/beginning -purging) DT I tubing + pu c Controlle ressure = H	time: 2 - 2 FW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20	2-07.11 C): \(\frac{1}{2}\).	30 NA psi 3 55 20 10	55 20 10 200	Furge date Final (post No. of tubin 5 55 20 10	e/completion -purging) D ng + pump	7 55	8 55 200): 42 200): 42 200	140		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt.)	e/beginning -purging) DT I tubing + pu c Controlle ressure = H i) etting /min)	time: 2-2 TW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 10 200	2-07-11 C): \(\psi \alpha\). = NR 2 55 20 10 200 Water	30 NA psi 3 55 20 10 200	55 20 10 200 ramete	Furge date Final (post No. of tubin 5 5 5 20 10 200 er Measure	6 55 20 20 20	Time: <u>2-2</u> TW (ft. BTC volumes pure 55	8 55 20 10 8 55 20 10	Final		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H i) etting _/min)	time: 2-2 TW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 10 200 Purge Rate	2-07, 11 C): \(\frac{1}{2}\).	30 VA psi 3 55 20 10 200 Quality Pa	55 20 10 200 200 ramete	Furge date Final (post No. of tubin 5 55 20 10 200 er Measure	e/completion -purging) D ng + pump	Time: 2-2 TW (ft. BTC volumes pur 7 55 20 10 200	8 55 20 10 200	Final Turbidity		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt.)	e/beginning -purging) DT I tubing + pu c Controlle ressure = H i) etting /min)	time: 2-2 TW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 10 200	2-07.11 C): \(\frac{1}{2}\). \[\frac{2}{55}\) \(\frac{2}{20}\) \[\frac{1}{0}\) \[\frac{2}{00}\) \[\text{Water}\] Cumulative Volume	30 NA psi 3 55 20 10 200	55 20 10 200 ramete	Furge date Final (post No. of tubin 5 55 20 10 200 r Measure ectrical ductivity	6 55 20 20 20	Time: <u>2-2</u> TW (ft. BTC volumes pure 55	8 55 20 10 8 55 20 10	Final		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt.)	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H i) etting _/min) DTW (ft. BTOC)	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min)	2-07.1) C): \(\(\frac{1}{2} \). \(\frac{2}{55} \) 20 10 200 Water Cumulative Volume Purged (L)	PSi 3 55 20 10 200 Quality Pa Temp. (degree C)	10 200 10 200 ramete Con (uM	Furge date Final (post No. of tubin 5 55 20 10 200 r Measure ectrical ductivity hos/cm)	6 55 20 20 20 ments	Time: 2-2 TW (ft. BTC volumes pur 7 55 20 10 200 Eh (mv)	8 55 20 10 200 10 200 mg/L)	Final Turbidity		
Purge date Initial (pre- Calculated Pneumation Initial air post Pressure (psi Refill Setting Discharge Se Flow rate (m.) Time	e/beginning purging) DT I tubing + pu c Controlle ressure = H i) etting /min) DTW (ft. BTOC)	time: 2-2 TW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 10 200 Purge Rate (mL/min)	2-07.11 C): \(\frac{1}{2}\). \(\frac{2}{55}\) \(\frac{2}{20}\) \(\frac{1}{2}\) \(\frac{2}{200}\) \(\fr	30 PSi 3 55 20 10 200 Quality Pa Temp. (degree C)	70 70 70 70 70 ramete Con (uM	Furge date Final (post No. of tubin 5 5 5 2 0 2 0 er Measure ectrical ductivity hos/cm)	6 55 20 200 ments pH	Time: 2-2 TW (ft. BTC) volumes pur 7 55 20 10 200 Eh (mv)	8 55 20 10 200 (mg/L)	Final Turbidity		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt.) Time	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H i) etting _min) DTW (ft. BTOC) 42.70	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min)	2-07.11 C): \(\frac{1}{2}\). \(\frac{2}{55}\) \(\frac{2}{50}\) \(\frac{1}{5}\) \(\frac{2}{50}\) \(\frac{1}{5}\) \(\frac{2}{50	30 Poi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.66	255 20 10 200 ramete Con (uM	Purge date Final (post No. of tubin 5 5 5 20 10 200 Pr Measure ectrical ductivity hos/cm) 875	e/completion-purging) Ding + pump ving + p	7 55 20 (mv) Eh (mv)	2-67, 13 PC): \\2 Tged: 8 55 20 10 200 DO (mg/L) 0.63 0.55	Final Turbidity (NTU)		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt.) Time	ploeginning purging) D7 I tubing + pu c Controlle ressure = H i) etting _min) DTW (ft. BTOC) 42.70	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min)	2-07.1) C): \(\(\frac{1}{2} \) \(\frac{5}{5} \) \(\frac{2}{5} \) \(\frac{5}{2} \) \(\frac{1}{0} \) \(\frac{2}{0} \) \(\frac{1}{0} \) \(\frac{2}{0} \) \(\frac{1}{0}	30 70 NA psi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.64 20.65	255 20 10 280 aramete Con (uM 0.	Furge date Final (post No. of tubin 5 55 20 10 200 Per Measure ectrical ductivity hos/cm) 875 861	6 55 20 200 ments pH	7 55 20 10 200 Eh (mv)	8 55 20 10 20 10 20 10 20 (mg/L) 0.63 0.55	Final Turbidity (NTU)		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt. Time 1235 1215 1239	e/beginning purging) DT I tubing + pu c Controlle ressure = H i) etting /min) DTW (ft. BTOC) 42.70 42.70 42.70	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min)	2-07.11 C): \(\frac{1}{2}\). \(\frac{2}{55}\) \(\frac{2}{50}\) \(\frac{1}{5}\) \(\frac{2}{50}\) \(\frac{1}{5}\) \(\frac{2}{50	30 Poi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.66	255 20 10 280 aramete Con (uM 0.	Purge date Final (post No. of tubin 5 5 5 20 10 200 Pr Measure ectrical ductivity hos/cm) 875	6 55 20 200 ments pH 8.63 7.77 7.49	7 55 20 10 200 Eh (mv) 166.8 78.5	2-67, 13 PC): \\2 Tged: 8 55 20 10 200 DO (mg/L) 0.63 0.55	Final Turbidity (NTU) 14.6		
Purge date Initial (pre- Calculated Pneumation Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (ml.) Time 1205 1215 1339 1235	e/beginning purging) DT I tubing + pu c Controlle ressure = H i) etting /min) DTW (ft. BTOC) 42.70 42.70 42.70 42.70	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min)	2-07.1) C): \(\(\frac{1}{2} \) \(\frac{5}{5} \) \(\frac{2}{5} \) \(\frac{5}{2} \) \(\frac{1}{0} \) \(\frac{2}{0} \) \(\frac{1}{0} \) \(\frac{2}{0} \) \(\frac{1}{0}	30 70 NA psi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.64 20.65	255 20 10 280 aramete Con (uM 0.	Furge date Final (post No. of tubin 5 55 20 10 200 er Measure ectrical ductivity hos/cm) 375 945	6 55 20 200 ments pH 8.63 7.77 7.49	7 55 20 10 200 Eh (mv)	8 55 20 10 20 10 20 10 20 (mg/L) 0.63 0.55	Final Turbidity (NTU) 14.4 1.4		
Purge date Initial (pre- Calculated Pneumatic Initial air pre- Pressure (psi Refill Setting Discharge Se Flow rate (mt. Time 1205 1215 1230 1235 1230	beginning purging) DT I tubing + pu c Controlle ressure = H by tting min) DTW (ft. BTOC) 42.70 42.70 42.70 42.70 42.70	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 LO 200 Purge Rate (mL/min) 200 200 200 200	2-07.11 C): \(\frac{1}{2}\).	30 70 NA psi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.66 20.65 20.65	70 70 70 70 70 ramete Con (uM 0.1	Furge date Final (post No. of tubin 5 5 5 2 0 10 2 0 r Measure ectrical ductivity hos/cm) 875 861 875	6 55 20 200 ments pH 8.63 7.77 7.49	7 55 20 10 200 Eh (mv) 166.8 78.5	8 55 20 10 200 10 200 10 (mg/L) 0.63 0.55 0.52	Final Final Turbidity (NTU) 14.6 1.4 1.1 1.3		
Purge date Initial (pre- Calculated Pneumation Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (ml.) Time 1205 1215 1339 1235	e/beginning purging) DT I tubing + pu c Controlle ressure = H i) etting /min) DTW (ft. BTOC) 42.70 42.70 42.70 42.70	time: 2-2 TW (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 55 20 10 200 Purge Rate (mL/min)	2-07.1) C): \(\frac{1}{2}, \] \[\frac{2}{55} \] \[\frac{2}{50} \] \[\frac{1}{0} \] \[\frac{2}{00} \] \[\frac{1}{0} \] \[\frac{2}{00} \] \[\frac{1}{0} \] \[\frac{2}{00} \] \[\frac{1}{0} \] \[\frac{2}{00} \] \[\f	30 70 NA psi 3 55 20 10 200 Quality Pa Temp. (degree C) 20.65 20.72 20.72 20.72	55 20 10 280 ramete Con (uM 0.1	Furge date Final (post No. of tubin 5 5 5 2 0 10 2 0 r Measure ectrical ductivity hos/cm) 875 861 875	6 55 20 20 20 20 20 20 20 20 20 7.77 7.49 7.43	7 55 20 10 200 Eh (mv) 166.8 266.4 -78.5	8 55 20 10 200 10 200 0.63 0.55 0.55 0.47	Final Final Turbidity (NTU) 14.6 19.6 1.4 1.1		



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Sheet 2_of 2_

77	DEN	1	·	T	er Measurement	1	1	I	F
Time	DTW	Purge Rate	ľ	Temp.	±3% Electrical	Hq	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity	L	(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	10	= 10%	± 10%
\	ļ								
	<u> </u>					ļ			
					<u> </u>		<u> </u>		
	 					<u> </u>	<u> </u>		
							<u> </u>		
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···							<u> </u>		
						<u> </u>			
		<u> </u>						<u> </u>	
Time	(ft. BTOC)	Purge Rate (mL/min)	Cumulative Volume	Temp. (degree C)	Electrical Conductivity	рН	Eh (mv)	DO (mg/L)	Turbidity (NTU)
	11	ನಾರ	Purged (L)	29.96	(uMhos/cm) のみつる	7.38	-106.5	0.80	, ,
1355	1 YZ.70		1 700	70	<u> </u>		I 106. 3	1 シ・ヘン・	
1355	¥2.70	200			_ •	1.20			1.6
1355	Y2.76	200			- •				1.56
1355	YZ. 75	200				36			1.56
1355	¥2.76	200		Sample	Information	58			1.5
ample ID	29w1	ω35-	Feb 20		Information Sample co	llection date	e/time: <u>2- 2</u>	2-87	
ample ID	コラマン Sample colle	ム35 cted (Y/N):_	Feb 20		Sample co	llection date		2-87	
Sample ID Ouplicate s	: タマ い sample colle	ム35~ cted (Y/N):_ (Y/N):_ ト	Feb 20		Sample co Duplicate s	llection date	e/time: <u>ス- ス</u> 対ステ <u>い</u>	2-87	
Sample ID Ouplicate s	コラマン Sample colle	ム35~ cted (Y/N):_ (Y/N):_ ト	Feb 20		Sample co Duplicate s	llection date	e/time: <u>ス- ス</u> 対ステ <u>い</u>	2-57	
Sample ID Duplicate s Split samp COC No(s	sample colle le collected	ム35 - cted (Y/N):_ (Y/N):_ N 57	Feb 20	207	Sample co Duplicate s Split samp	llection datesample ID:_	e/time: 2-2 ₩29₪	.2-07 W35-Feb	2007-
Sample ID Ouplicate s Split sampl COC No(s	E み9 いいsample colleted i: 109	ム35 - cted (Y/N):_ (Y/N):_ ト 57	Feb 20	ontainers	Sample co Duplicate s Split samp Requeste	llection datesample ID:_ le ID:_	e/time: 2-2 ⋈ 29ພ N Method	.2-07 W35-Feb	
ample ID Juplicate s plit samp COC No(s	ample collected	235 - cted (Y/N):N (Y/N):N 57 Method 8360 B	Feb 20	entainers	Sample co Duplicate s Split samp Requested	llection datesample ID:_ le ID:_ d Analysis	# 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.2-07 W35-Feb	2007-
ample ID duplicate s plit sample OC No(s) dequested	E み9 いいsample colleted i: 109	ル35 - cted (Y/N):_ (Y/N):_ N 57 Method 8240 B Sep 175	Feb 20	ontainers	Sample co Duplicate : Split samp Requester Feach!	llection date sample ID:_ le ID:_ d Analysis o Rみと	e/time: 2-2 ⋈ 29ພ N Method	. 2 - 57 い35 - たと Conta	2007-
ample ID Duplicate s Split sample OC No(s) Requested VOC GASES	Sample college collected: 109	235- cted (Y/N):_ (Y/N):_ 1 57 Method 8260 B Sep 175 415.1	Feb 20	entainers	Sample co Duplicate : Split samp Requester Feach!	llection datesample ID:_ le ID:_ d Analysis	# 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.2-07 W35-Feb	2007-
Sample ID Duplicate s Split samp COC No(s) Requested	ample collected in the	ル35 - cted (Y/N):_ (Y/N):_ N 57 Method 8240 B Sep 175	Feb 20	ontainers	Sample co Duplicate : Split samp Requester Feach!	llection date sample ID:_ le ID:_ d Analysis o Rみと	# 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	. 2 - 57 い35 - たと Conta	2007-

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

	RFA / C	OC Number: 10495
Location Code: Sample Number:	29WW36 29WW36-Feb 2007	Task: MNA_EVENT_FEB07
•	29WW36-GW-29WW36REG	Collection Date: 2-21-07 Collection Time: 1515
Sampling Method:	SP	Start Depth: 31'
Sample Type:	I I	End Depth: 28.88
Sampling Equip: Sertners:	tainless Steel Bladder	Sample Matrix: WATER
ГВ)	(ER) · (FB)	Sample Team: Willemore M. Ad
Analytical Suite	Containers Flt Frtn Qty Size Units Type	ERPIMS Values: Sacode:
VOC-FULL	N A 3 40 mL VOAVIAL	Lot Control#:
ANIONS	N B 1 500 mL HDPE	
PERC	N C 1 500 mL HDPE	
GASES	N D 2 40 mL VOA Vial	
ALKALINITY	N E 1 100 mL HDPE	
TOC_415	N F 1 100 mL HDPE	
DHC	N G 1 1 L Amb, Glass	
Groundwater Inf Measured W Comments:	ormation: ell Depth: 36,70 Depth To Water: 28	. 9
Sketch Locat	ion:	

Logged BY /	Date: Berry M. Polos
	2-21-07



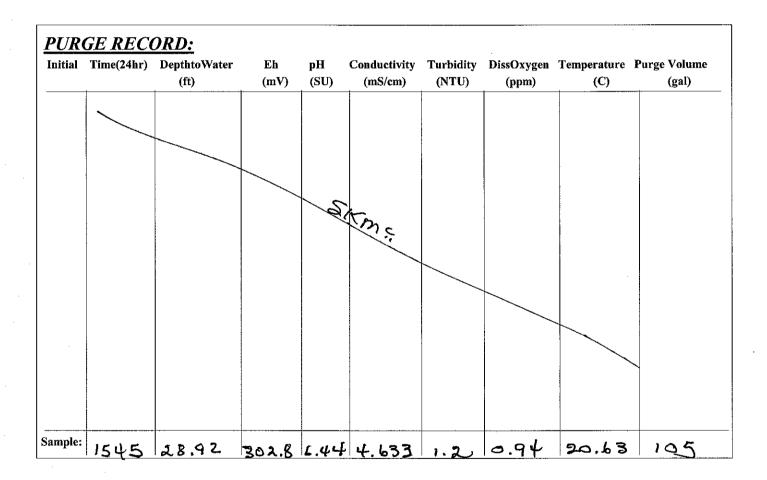
00091696

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW36

Sample Number: 29WW36Feb 2007



Logged BY / Date: Serry M. Teloo 2-21-07

Reviewed BY / Date:



00091697

Sheet 1 of 2.

	Unit/Site ID				<u>_</u>			29W U		
	<u>ما :</u> #			۲	_	•			PO 500	
Weather:_	Surn	1 80		·	_	Collection	Time/Date:	2-21-0	7/15	15
				Dumi	Inct	allation				
D	-11-4:)+						.	1
	allation crev					Installatio	n date/begir	nning time:	2-21-07	1年30
PID/FID re	eading (well	head/back	ground): <u>o</u>	0/0/0		Installatio	n date/comp	oletion time:	<u> 2-21-07</u>	1450
•	ameter (inch		<u> </u>				terval (ft. B1	,	to _	
1	Depth (ft. B							BTOC): 🎅		
•	-installation							//time: ኋ ና		
	r pump prim			38		Max. susta	ainable pun	ip rate (mL/	min):	
	uct (circle):					Appearan	ce of produc	ct:		. , ,
Volume of	water remo	ved during	priming (ml	_):		Discharge	tube diame	eter (3/8" or	1/4"): 3/g	r,
Discharge	tube length	(ft.):	·		_		er used (Y/			
Pneumati	c Controlle	r Tuning:								
Initial air p	ressure = H	l (ft.) X 0.43	=	_ psi						
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps	i)		 	<u> </u>	 			 	1	Final
Refill Setting			 		 	SKn	DS.		 	
Discharge Se			 		 				 	
Flow rate (m				 	 					<u> </u>
' 		<u> </u>	<u></u>		urgin					
Initial (pre- Calculated Pneumati	e/beginning -purging) Dī I tubing + pu c Controlle ressure = H	TW (ft. BTO) imp volume r Tuning:	C): ス多。() :		· -	Final (post	-purging) D		<u>ス1-ロ7/</u> DC): ス会.9 rged:	
		Initial	2	T					Т .	
Pressure (psi	;)	21	عرا	3	21-	5	6	7	8	Final
Refill Setting)	10	10	21				ļ	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	71
Discharge Se	etting	5	-5	5	1 <u>D</u> S				/	5
Flow rate (ml			105	·					-	<i>)</i>
riow rate (inc	21111117	105	105	105	105			<u> </u>	<u> </u>	105
			Water	Quality Pa	ramete	er Measure	ments			
Time	WTG	Purge Rate	Cumulative	Temp.	E	ectrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Con	ductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uM	lhos/cm)				
1455	28.88	105	105	20.06	4.	704	6.4	2698	1.49	<u>ئ</u> ن
1500	28.88	105	入! D	20.00		<u>675</u>	6.4	275.5	124	2.0
1505	28.88	105	315	19,92		659	6.40	280.9	1.00	1.7
1510	28.92	105	420	19.86		647	6.41	284.2	0-92	1,2
						* *			,,,,	
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				· · · · · · · · · · · · · · · · · · ·					<u>. </u>	



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Sheet 2_ of 2_

-		I	Nater Quali	ty Paramet	ter Measurements	s (continue	d).	 	·
Time	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	±10%	100%
								13	
									
			<u> </u>			 			
								 	
	1								
	 					 	 		 _
					\sim	 	<u> </u>		
	 	 	<u> </u>		<i>(1)</i>	-	-		
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		ļ				<u> </u>	· · · · · · · · · · · · · · · · · · ·		
	 						<u> </u>		
	ļ								
									
			·						/
				S	ampling	······································			
Sampling I	beginning tir	ne: <u>15</u>		Quality Pa	Sampling o		ime: <u>15</u>	15	
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity	, , ,	(mv)	(mg/L)	(NTU)
	`		Purged (L)	((uMhos/cm)		,,,,,	(1119/12)	(1410)
1545	28.92	105	ちなく	20.63	4.633	6.44	302,8	A Gull	1.0
	707.12	5	~ ~ >	<u> </u>	4,633	6.47	207,8	U. 17	1.2
 									
······································									
						<u> </u>			
			•	Sample	Information				
Sample ID	<u> </u>	36-Fe	2007	•		llection date	/time: 2~	21-07	
Suplicate s	sample colle	cted (Y/N):	7	****	Duplicate s	ample ID:_	N		
					Split sampl		<u> </u>		
COC No(s)	le collected): <u>10</u> サ	95			Opin odinipi				
					L				
	d Analysis	Method		ntainers		l Analysis	Method	Conta	iners
<u> </u>		5260B		<u> </u>		prate			
(PAC .		50P175		<u>}</u>		(tivil)	310.1	1	
		415.1			Explos	ives!			
TOC		300.0	1						
FOC ANIE									
ANI TO C					1				
SW15 EN12	rides	376.2							<u>.</u>
ANI TO C	rides								:
SW15 ENIS	rides								



00091699

Page 1 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 2 Sample Number: 2 Sample Name: 2 sampling Method: S Sample Type: G	9WW38- Feb = 9WW38-GW-29		Colle	Task:	MNA_EVENT_FEB07
Sample Name: 2 ampling Method: S	9WW38-GW-29		Colle		
ampling Method: S		WW38REG		ction Date:	2-22-07
1 0	P				0930
Sample Type: G	-			tart Depth:	_
. ,,	W	Sample Purpose: RE			30.64
Sampling Fauin∙ < ⊁		L Bladder Pu		_	
tners:	rinkeso) <u>lei</u>	L Bladur Pu	Sam ₂	ple Matrix:	WATER
)	(ER)	(<u>FB</u>)	San	nple Team:	Willemore, M. Ad
Analytical Suite	Containe Fit Frtn Qty Size			ERPIM	S Values: Sacode:
VOC-FULL	N A 3 40	mL VOA VIAL		Lot	Control#:
ANIONS	N B 1 500	mL HDPE			
PERC	N C 1 500	mL HDPE			
GASES	N D 2 40	mL VOA Vial			
ALKALINITY	N E 1 100	mL HDPE			
TOC_415	N F 1 100	mL HDPE			
DHC	N G 1 1	L Amb, Glass			
Groundwater Information Measured Well Comments:	mation: Depth: <u></u>	P Depth To Wa	ater: <u>30.64</u>		
Sketch Location	· 1•				
Sketch Bocado	.K.•				

Logged BY / Date: Spenn M. Quloo	Reviewed BY / Date:	f
SVIENT TO THE LOS		



00091700

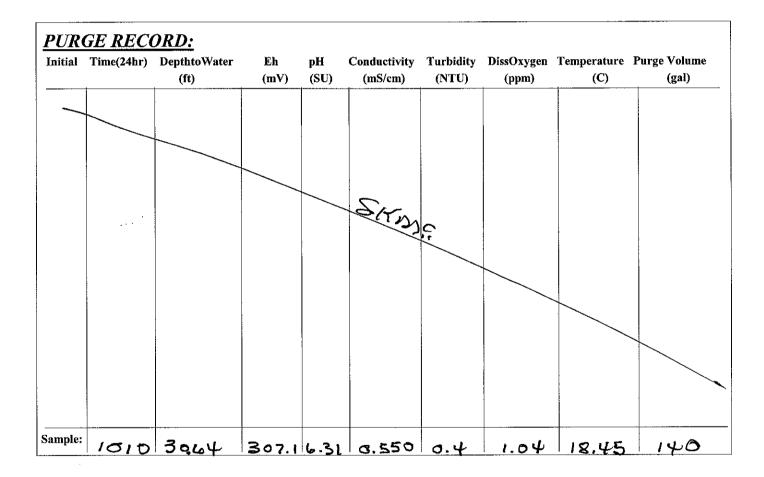
Page 2 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW38

Sample Number: 29WW38-Feb 2007



Logged BY / Date: Sern M.F. Adoo	Reviewed BY / Date:	
2-22-07		



00091701

Sheet <u>1</u> of <u>2.</u>

*Operable	Unit/Site ID	Longh	982 - 5	Arc. 29		Sampling	Incation ID	· 2 9ca)r. 1 =	2 O	
Project Na	ame/#: Lo	Nahori	SAAP	<u> </u>		Sampling location ID: <u>29ພພ38</u> Sample ID: <u>29ພພ38 - Feb</u> 2007				
Weather:	ame/#: <u>Lo</u> i	1-(1)p	AR -5	0-	_	Collection Time/Date: 2-12-07/0930				
							Time/Date	<u> </u>	3 // 0-2	30
						allation				
Pump inst	tallation crev	N: Willen	nore, M	15Adoo		Installatio	n date/begi	nning time:	2-22-07	840
PID/FID reading (well head/background): o. o / o %.					Installation	n date/com	pletion time:	2-42-07	0908	
	Casing diameter (inches):							TOC): 3		
	Depth (ft. B	· ———	-W'			Pump inta	ke denth (fi	t BTOC): 3	41	<u> </u>
	-installation							//time: 3		
	r pump prim							np rate (m∐		
	uct (circle):			- 7				ct: Clea	,	
	water remo			١٠	•			eter (3/8" or		11
	tube length			-,					1/4]:_ -/8	
	c Controlle			·	-	mier read	er used (Y	/IN/: I_X		
Į.	ressure = F	_	=	nei						
- P		1 (16) / 0.43		_ hai						
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps					<u> </u>					
Refill Setting						LW:				
Discharge Se					ļ			-		
Flow rate (ml	L/min)		<u> </u>				<u> </u>			
				F	urgin	q		·		
in										
Purging/sa	ampling crev	v:Willem	ORE W	E Adap		PID/FID re	ading (well	head/backo	iround). 🗸	1/20%
Purging/sa Purge date	ampling crev e/beginning	v: <u>W illem</u> time: ス- ス	3-07 0	405		PID/FID re	ading (well	head/backg د ع time: ع	ر (round): <u>م. ه</u> ا 2 م - 2 م	1020
Purge date	e/beginning	time: 2-2	3-07,0	905		Purge date	completion	n time: <u> ጄ</u> -	22-07/	1020
Purge date Initial (pre-	e/beginning -purging) D1	time: 2 - 2 FW (ft. BTO	2-07,0 :30,6	90 <u>5</u> 4		Purge date Final (post	e/completion -purging) D	n time: בַּבְּבָּ TW (ft. BTC	22-07/ C): 3d.	1020
Purge date Initial (pre- Calculated	e/beginning -purging) D1 I tubing + pu	time: 2 - 2 TW (ft. BTO) Imp volume	2-07,0 :30,6	905	-	Purge date Final (post	e/completion -purging) D	n time: <u> ጄ</u> -	22-07/ C): 3d.	1020
Purge date Initial (pre- Calculated Pneumation	e/beginning -purging) Dī I tubing + pu c Controlle	time: <u>2 - 2</u> TW (ft. BTO) Imp volume r Tuning:	3-07,0 C): 30,6	905 VA		Purge date Final (post	e/completion -purging) D	n time: בַּבְּבָּ TW (ft. BTC	22-07/ C): 3d.	1020
Purge date Initial (pre- Calculated Pneumation	e/beginning -purging) D1 I tubing + pu	time: 2-2 FW (ft. BTO) imp volume r Tuning: (ft.) X 0.43	2-07,000:30.60: = NR	905 W NA psi		Purge date Final (post No. of tubi	e/completion -purging) D ng + pump	n time: בַּבְּבָּ TW (ft. BTC	22-07/ C): 3d.	1020
Purge date Initial (pre- Calculated Pneumation Initial air p	e/beginning -purging) D1 I tubing + pu c Controlle ressure = H	time: 2 - 2 TW (ft. BTO) imp volume r Tuning: (ft.) X 0.43	2-07.0 C): 30.6 : NR	905 4 NA psi	4	Purge date Final (post No. of tubi	e/completion -purging) D	n time: בַּבְּבָּ TW (ft. BTC	22-07/ C): 3d.	1020
Purge date Initial (pre- Calculated Pneumatie Initial air po Pressure (psi	e/beginning -purging) D1 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27	2-07 0:30,4 = NR	905 ル NA psi 3 ネ7	4 27	Purge date Final (post No. of tubi	e/completion -purging) D ng + pump	n time: <u>3 - 3</u> TW (ft. BTC volumes pu	922-67/ DC): 3d rged:	1020 64
Purge date Initial (pre- Calculated Pneumatie Initial air properation Pressure (psi Refill Setting	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial	2-07 30.4 - NR 2 27 10	905 L NA psi 3 27	27	Purge date Final (post No. of tubin 5	e/completion -purging) D ng + pump	n time: <u>3 - 3</u> TW (ft. BTC volumes pu	922-67/ DC): 3d rged:	1020 64
Purge date Initial (pre- Calculated Pneumatic Initial air po Pressure (psi Refill Setting Discharge Se	e/beginning purging) D7 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTOO Imp volume r Tuning: (ft.) X 0.43 Initial 27 05	2 2 2 2 2 2 2 5	905 ル NA psi 3 3 37 10 5	27 10 5	Furge date Final (post No. of tubin 5 27	e/completion -purging) D ng + pump	n time: <u>3 - 3</u> TW (ft. BTC volumes pu	922-67/ DC): 3d rged:	1020 64
Purge date Initial (pre- Calculated Pneumatie Initial air properation Pressure (psi Refill Setting	e/beginning purging) D7 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial	2-07 30.4 - NR 2 27 10	905 L NA psi 3 27	27	Purge date Final (post No. of tubin 5	e/completion -purging) D ng + pump	n time: <u>3 - 3</u> TW (ft. BTC volumes pu	922-67/ DC): 3d rged:	1020 64
Purge date Initial (pre- Calculated Pneumatic Initial air po Pressure (psi Refill Setting Discharge Se	e/beginning purging) D7 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTOO Imp volume r Tuning: (ft.) X 0.43 Initial 27 05	2 2 2 2 2 10 140	905 4 psi 3 27 10 5 140	27 10 5 140	Furge date Final (post No. of tubin 5 27 10	e/completion -purging) D ng + pump	n time: <u>3 - 3</u> TW (ft. BTC volumes pu	922-67/ DC): 3d rged:	1020 64
Purge date Initial (pre- Calculated Pneumatie Initial air po Pressure (psi Refill Setting Discharge Se Flow rate (mL	e/beginning -purging) DT I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 UD 55	2 2 2 2 2 2 10 5 140 Water	Po5 ル NA psi 3 ネフ リロ 5 リセロ	27 10 5 140	Furge date Final (post No. of tubin 5 27 10 5 1 40 er Measure	e/completion-purging) Ding + pump	n time: 2 - 2 TW (ft. BTC volumes pu	82-67/ DC): 3d . rged:	ip 20 6サ Final
Purge date Initial (pre- Calculated Pneumatic Initial air po Pressure (psi Refill Setting Discharge Se	e/beginning -purging) D7 I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 IS INFO Purge Rate	2 27 10 5 140 Water Cumulative	905 JA psi 3 3 37 10 5 140 Quality Pa	27 10 5 140 ramete	Furge date Final (post No. of tubin 5 27 10 1 40 er Measure	e/completion -purging) D ng + pump	n time: 2 - 2 TW (ft. BTC volumes put	82-67/ DC): 34. rged:	Final Turbidity
Purge date Initial (pre- Calculated Pneumatie Initial air po Pressure (psi Refill Setting Discharge Se Flow rate (mL	e/beginning -purging) DT I tubing + pu c Controlle ressure = H	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 UD 55 U+O Purge Rate (mL/min)	2 27 10 5 140 Water Cumulative Volume	Po5 ル NA psi 3 ネフ リロ 5 リセロ	27 10 5 140 ramete	Furge date Final (post No. of tubin 5 27 10 5 r Measure ectrical ductivity	e/completion-purging) Ding + pump	n time: 2 - 2 TW (ft. BTC volumes pu	82-67/ DC): 3d . rged:	ip 20 6サ Final
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL	e/beginning purging) D7 I tubing + pt c Controlle ressure = H etting /min) DTW (ft. BTOC)	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 UD 55 U+O Purge Rate (mL/min)	2 27 10 5 140 Water Cumulative Volume	PO5 A PSi 3 A7 10 5 (4の Quality Pa Temp. (degree C)	27 10 5 140 ramete Con (uM	Furge date Final (post No. of tubin 5 27 10 5 I U D er Measure ectrical ductivity hos/cm)	e/completion-purging) D ng + pump 6 ments pH	TW (ft. BTC volumes pur	BO (mg/L)	Final Turbidity (NTU)
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL	e/beginning purging) DT I tubing + pu c Controlle ressure = H i) biting _/min) DTW (ft. BTOC)	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 ID SS IVO Purge Rate (mL/min)	2 27 10 5 140 Water Cumulative Volume Purged (L) 140	PSi A PSi 3 ネフ 10 S 140 Quality Pa Temp. (degree C) 16.63	27 10 5 140 aramete Con (uM	Furge date Final (post No. of tubin 5 27 10 5 1 40 er Measure ectrical ductivity hos/cm) 5 30	e/completion-purging) Ding + pump 6 ments pH	TW (ft. BTC volumes pure function of the funct	DO (mg/L)	Final Turbidity (NTU) 2.9
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL Time	e/beginning purging) D7 I tubing + pt c Controlle ressure = H i) otting /min) DTW (ft. BTOC) 30.64	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 2.7 (0 5 L+0 Purge Rate (mL/min)	2 27 10 5 140 Water Cumulative Volume Purged (L) 140 280	905 4 psi 3 27 10 5 140 Quality Pa Temp. (degree C) 16.68	27 10 5 140 aramete Con (uM	Purge date Final (post No. of tubin 5 27 10 sr Measure ectrical ductivity hos/cm) 530 519	e/completion-purging) D ng + pump 6 ments pH 6.41	Eh (mv)	DO (mg/L)	Final Turbidity (NTU) 2.9 3.2
Purge date Initial (pre- Calculated Pneumatic Initial air properties Refill Setting Discharge Se Flow rate (mL Time 0910 9915	e/beginning purging) D7 I tubing + pt c Controlle ressure = H etting /min) DTW (ft. BTOC) 30.64 30.64	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 ID S IV-O Purge Rate (mL/min)	2 2 2 2 2 10 5 140 Water Cumulative Volume Purged (L) 140	905 4 psi 3 37 10 5 (40 Quality Pa Temp. (degree C) (0.63 10.68	27 10 5 140 aramete Con (uM 0.4	Purge date Final (post No. of tubin 5 27 10 5 140 er Measure ectrical ductivity hos/cm) 530 519 524	e/completion-purging) D ng + pump 6 ments pH 6.41 6.40 6.39	Eh (mv) 274.2 280.9	BO (mg/L) (A80 1.49 1.38	Final Final Turbidity (NTU) 2.9 3.2 3.1
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL Time 0910 9915 9925 9925	Properties of the properties o	time: 2-2 W (ft. BTOO Imp volume r Tuning: (ft.) X 0.43 Initial 27 LD 55 LHO Purge Rate (mL/min) LHO LHO LHO LHO	2 2 2 2 2 2 10 5 140 Water Cumulative Volume Purged (L) 140 280 420 560	905 ル NA psi 3 ネフ 1D 5 (40 Quality Pa Temp. (degree C) 16.63 17.67 17.32	27 10 5 140 aramete Con (uM 0.4	Purge date Final (post No. of tubin 5 27 10 5 140 er Measure ectrical ductivity hos/cm) 530 519 524 529	e/completion-purging) D ng + pump 6 ments pH 6.41 6.40 6.39 6.37	TW (ft. BTC volumes pure ft. 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	DO (mg/L) 1.38 1.26	Final Turbidity (NTU) 3.9 3.2 3.1 2.6
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL Time 0910 9915 9925 9925	e/beginning purging) D7 I tubing + pt c Controlle ressure = H etting /min) DTW (ft. BTOC) 30.64 30.64	time: 2-2 W (ft. BTO) Imp volume r Tuning: (ft.) X 0.43 Initial 27 ID S IV-O Purge Rate (mL/min)	2 2 2 2 2 10 5 140 Water Cumulative Volume Purged (L) 140	905 4 psi 3 37 10 5 (40 Quality Pa Temp. (degree C) (0.63 10.68	27 10 5 140 aramete Con (uM 0.4	Purge date Final (post No. of tubin 5 27 10 5 140 er Measure ectrical ductivity hos/cm) 530 519 524	e/completion-purging) D ng + pump 6 ments pH 6.41 6.40 6.39	Eh (mv) 274.2 280.9	BO (mg/L) (A80 1.49 1.38	Final Final Turbidity (NTU) 2.9 3.2 3.1
Purge date Initial (pre- Calculated Pneumatic Initial air properties Pressure (psi Refill Setting Discharge Se Flow rate (mL Time 0910 9915 9925 9925	Properties of the properties o	time: 2-2 W (ft. BTOO Imp volume r Tuning: (ft.) X 0.43 Initial 27 LD 55 LHO Purge Rate (mL/min) LHO LHO LHO LHO	2 2 2 2 2 2 10 5 140 Water Cumulative Volume Purged (L) 140 280 420 560	905 ル NA psi 3 ネフ 1D 5 (40 Quality Pa Temp. (degree C) 16.63 17.67 17.32	27 10 5 140 aramete Con (uM 0.4	Purge date Final (post No. of tubin 5 27 10 5 140 er Measure ectrical ductivity hos/cm) 530 519 524 529	e/completion-purging) D ng + pump 6 ments pH 6.41 6.40 6.39 6.37	TW (ft. BTC volumes pure ft. 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	DO (mg/L) 1.38 1.26	Final Turbidity (NTU) 3.9 3.2 3.1 2.6
Purge date Initial (pre- Calculated Pneumatic Initial air properties Refill Setting Discharge Se Flow rate (mL Time 0910 9915 9925 9925	Properties of the properties o	time: 2-2 W (ft. BTOO Imp volume r Tuning: (ft.) X 0.43 Initial 27 LD 55 LHO Purge Rate (mL/min) LHO LHO LHO LHO	2 2 2 2 2 2 10 5 140 Water Cumulative Volume Purged (L) 140 280 420 560	905 ル NA psi 3 ネフ 1D 5 (40 Quality Pa Temp. (degree C) 16.63 17.67 17.32	27 10 5 140 aramete Con (uM 0.4	Purge date Final (post No. of tubin 5 27 10 5 140 er Measure ectrical ductivity hos/cm) 530 519 524 529	e/completion-purging) D ng + pump 6 ments pH 6.41 6.40 6.39 6.37	TW (ft. BTC volumes pure ft. 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	DO (mg/L) 1.38 1.26	Final Turbidity (NTU) 3.9 3.2 3.1 2.6



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Sheet a of a

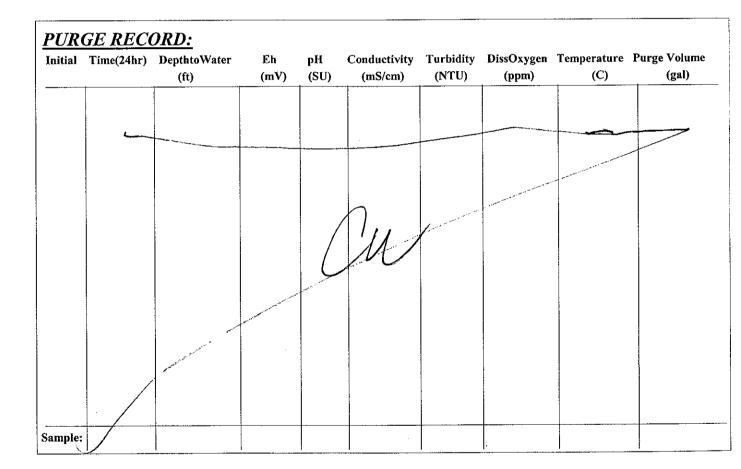
			Matar / hitar	tu Darama	とのと おほんべん・・レヘンペーート	n (nambiu			
Time	DTW	Purge Rate	Cumulative	Temp.	ter Measurement		- · · · · · · · · · · · · · · · · · · ·	T 50	1
71110	(ft. BTOC)	(mL/min)	Volume	(degree C)	±3% Electrical Conductivity	рH	Eh	DO	Turbidity
	(1.2.2100)	(11111111111111111111111111111111111111	Purged (L)	± 10%	(uMhos/cm)	± 0.1	(mv) 土 10	(mg/L)	100%
$\overline{}$			ruigeu (L)	- 10 6	(ulwinos/cm)		= 10	= 10%	10 to
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		<u> </u>			ampling	<u> </u>	<u> </u>		
Sampling I	beginning tir	ne: 09	3 0			completion	time: °	930	
			Water	Quality Pa	rameter Measure	ements			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
								1 .	
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
	(ft. BTOC)	(mL/min)	Volume Purged (L)	(degree C)	Conductivity (uMhos/cm)		(mv)	(mg/L)	(NTU)
1010	(ft. BTOC)	(mL/min)		(degree C)	(uMhos/cm)	6.31			
1010			Purged (L)		(uMhos/cm)	6.31	(mv)	(mg/L)	(UTИ) 4. 0
1010			Purged (L)		(uMhos/cm)	6.31			
1010			Purged (L)		(uMhos/cm)	6.31			
1010			Purged (L)	18.45	(uMhos/cm) ロ・558	6.31			
	30.6¢	140	Purged (L) 名中の	18.√5 Sample	(uMhos/cm) の、ちちゅ		307.1	1.04	
Sample ID	30.6¢	140 38-1-el	Purged (L) 名中の	18.√5 Sample	(uMhos/cm) つ・55点 Information Sample co	llection dat	307. 1	1.04	
Sample ID Duplicate s	30.64 30.64	38-Fell	Purged (L) 多少の ふるのう	18.√5 Sample	(uMhos/cm) つ・55点 Information Sample co Duplicate s	llection dat	307.1 e/time: 2-1	1.04	
Sample ID Duplicate s Split samp	30.6¢	38-1-el cted (Y/N):_	Purged (L) 多少の ふるのう	18.√5 Sample	(uMhos/cm) つ・55点 Information Sample co	llection dat	307.1 e/time: 2-1	1.04	
Sample ID Duplicate s Split samp COC No(s	30.64 30.64 : 29 ww sample colle le collected): 10 4	38-I-el cted (Y/N): (Y/N):	Purged (L) 名中の 2007 ハ	I8.⊮5 Sample	(uMhos/cm) つ・5 5 a Information Sample co Duplicate s Split samp	llection dat sample ID:_ le ID:	307.1 e/time: 2	22-07	0.4
Sample ID Duplicate s Split samp COC No(s Requeste	30.64 30.64 Sample collected by 1045 Analysis	38-1-el cted (Y/N):_ (Y/N): ? \	Purged (L) 名中の つ えののフ ソ	Sample	(uMhos/cm) つ・55点 Information Sample co Duplicate s Split samp	llection dat sample ID:_ le ID:_	307. 1 e/time: 2-	1.04	0.4
Sample ID Duplicate s Split samp COC No(s Requested	30.64 30.64 Sample colleted or 1045 I Analysis	38 - I-el cted (Y/N):_ (Y/N):_ Y \(\frac{1}{2}\) Method 8260B	Purged (L) 多少の ころのフ ン	Sample	(uMhos/cm) O. 550 Information Sample co Duplicate s Split samp Requested	llection dat sample ID: le ID: d Analysis	### 307.1 ###################################	22-07	0.4
Sample ID Duplicate s Split samp COC No(s Requested VOC	30.64 30.64 Sample colleted or 1045 I Analysis	38-1-el cted (Y/N): (Y/N): ? \ Method 8260B Sep175	Purged (L) 840	Sample	(uMhos/cm) O・555 Information Sample co Duplicate s Split samp Requested Recとは	llection dat sample ID:_ le ID:_ d Analysis seats	### ### ##############################	1.04 22-07 Conta	o.Ψ
Sample ID Duplicate s Split samp COC No(s Requested VOC GASES	30.64 30.64 29 ww sample colle le collected 10 40 Analysis - CO2	38-1-el cted (Y/N):_ (Y/N):_ ?\ Method 8260B \$260B \$175 \\	Purged (L) 多少の ころのフ ン	Sample	(uMhos/cm) O・555 Information Sample co Duplicate s Split samp Requested Recとは	llection dat sample ID: le ID: d Analysis	### ### ##############################	22-07	o.Ψ
Sample ID Duplicate s Split samp COC No(s Requested VOC GASES	30.64 30.64 Sample collected or 1049 d Analysis - CO2	38-1-el cted (Y/N): (Y/N): ? \ Method 8260B Sep175	Purged (L) 名中の えつのフ ン	Sample	(uMhos/cm) O・555 Information Sample co Duplicate s Split samp Requested Recとは	llection dat sample ID:_ le ID:_ d Analysis seats	### ### ##############################	1.04 22-07 Conta	o.Ψ



117591 - Longhorn Army Ammunition Plant

Praveen Srivastav Manager:

Location Code: 29WW15 Sample Number: 29WW15-



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GROUNDWATER SAMPLING FORM

Sheet _1_of ___

Operable Unit/Site ID: LHAAP Project Name/#: LHAAP—29					Sampling location ID: 19 WW 5 Sample ID: 19 WW 5 - FEB 2007					
Project Nan	ne/#:_ <i>_L-[-</i>]	AA r =	•21	2. 2		Collection Time/Date:				
Weather:_{	Nevest	- Nainy	(4)-	/0		Collection	rime/Date			
		<u></u>		Pump	Insta	llation				
Pump instal	llation crew:	AWilm	ore/C.W	inzer		Installation	date/begini	ning time:	NA	
PID/FID reading (well head/background):						Installation	date/compl	letion time:	WH CO	
Casing diameter (inches): 4" / Stain less Stee						Screen Inte	erval (ft. BT	OC): 23	3.37 to -	3.52
Total well D							ce depth (ft			
Initial (pre-i	nstallation)	DTW/time:_	31.46				ation DTW/			
Final (after	pump primi	ng) DTW/tin	ne:			Max. susta	inable pum	p rate (mL/r	nin): <u>UN</u>	· !
Free produc	ct (circle): _	LNAPI	<u>/DNAPL</u>				e of produc			
Volume of v	water remov	ed during p	riming (mL)):		Discharge	tube diame	ter (3/8" or	1/4"): NA	\
Discharge t						Inlet reduce	er used (Y/N	۷):		
Pneumatic										
Initial air pro			=	psi .						,
		Initial	2	3	4	5	6	7	8	Final
Pressure (psi)							<u></u>			ļ
Refill Setting			0.			1 Josh				
Discharge Set	ting		NG	(CC)		NK!		<u> </u>		
Flow rate (mL	/min)					<u></u>	<u> </u>		<u> </u>	
F				P	urgir	na				
Initial (pre-p Calculated Pneumatic Initial air pr	tubing + pu : Controller	mp volume: r Tuning:		IA					DC):_ <u>D7R</u> rged:	
militar an pr		Initial	2	3	4	5	6	7	8	Final
Pressure (psi)	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \									
Refill Setting	<u></u>		7			1				
Discharge Set	ttina		7	イバシ						
Flow rate (mL										
. ion rate (inc			Water	· Quality Pa	ramet	er Measure	ments			
Time	DTW	Purge Rate	Cumulative	Temp.	E	lectrical	рН	Eh (my)	DO (ma/l.)	Turbidity (NTU)
	(ft. BTOC)	(mL/min)	Volume	(degree C)		nductivity		(mv)	(mg/L)	(1410)
		ļ	Purged (L)		(ul	Mhos/cm)		 		
				<u> </u>				 	 	
									 	
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Water Quality Parameter Measurements (continued)									
Time	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity	1.	(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	±10%	± 10%
			!						
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	200								
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				Sa	ampling				
Sampling b	eainnina tir	ne: [0:3	, <u>v</u>		· -	completion t	ime [,]		
oumpung c	ogiiiiiiiig tii			Ovality Da	•				······································
Time	DTW	Purge Rate	Cumulative		rameter Measui Electrical		- EL	DO.	Turkidibe
inne	(ft. BTOC)	(mL/min)	Volume	Temp. (degree C)	Conductivity	pH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
	(it. broc)	(1112311111)	Purged (L)	(degree c)	(uMhos/cm)		(,,,,,	(iiig/L)	(1410)
					(0111100,011)				
					11/	and a process of the second		** ***********************************	
			and the second s						
	a market have been a			Sample	Information	· · · · · · · · · · · · · · · · · · ·			
Sample ID:	29 W	4115		Sample	nomannonn: a elama2	ollection date	Itima: 1	44/121	n!35
		cted (Y/N):_	M					2 (/ 0 1)	0130
	-	(Y/N): _			Split sam	sample ID:_ ple ID:	1/6		
COC No(s)		· /			•	, —			
							Method		
Requested			Co	ontainers		Requested Analysis		Conta	iners
10C		8260B		<u> </u>		IsRAte	314.0		
GASUS	- 002	502175		<u>3</u>		1.0.44	310.0	-	
ANIO	36	415.1 300.0		3	- Lexpla	مکابہ دچ		2	
544;		376.2		1					
		276.74							
Comments	E ()	in an in	, 11	by (t i		~ /	,		
4	. of u	rater in	well.	Douled	dry & 5:30	on, 2/2	1/07.		
	541	L	err- 7.3	57	1				
2' of water in well. Bailed dry & 8:30 cm, 2/24/07. 541 ferr- 2.33 Abbreviations: BTOC-Below top of casing; DTW-Depth to water; H-head above pump intake; mL-milliliter; L-Liter									

MNA GROUNDWATER SAMPLING FORM Sheet _____ of ____

Site ID <u>29</u>	Sampling Event	FEB 2007
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Well ID . 29WW 15	Date	Ferrous Iron 2.33	Salinity	Sample Crew
29WW 15	2/24/07	2.33		AW/CU
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		_		
			·	
				



117591 - Longhorn Army Ammunition Plant

Praveen Srivastav

						KFA	/ COC Number:	
Location Code:	29W	VW:	15					MNA_EVENT_FEB0
Sample Number:	29W	VW:	15-				Collection Date:	
Sample Name:	29 V	VW:	15-G	W-29V	VW15	REG		
Sampling Method:	SP							
Sample Type:	GW	7			Sam	ple Purpose: REG	-	
Sampling Equip:							Sample Matrix:	
rtners:							-	
B)		(ER)			(FB)	Sample Team:	AW/CW
Analytical Suite	Flt	Frt		itainer Size		Туре	ERPIM	S Values: Sacode:
VOC-FULL		A		40		VOA VIAL	Lot	Control#:
1	N	В	1	500	mL	HDPE		
PERC	N	С	1	500	mL	HDPE		
GASES	N	D	3	40	mL	VOA Vial		
ALKALINITY	N	E	1	1000	mL	HDPE		
TOC_415	N	F	1	40	mŁ	HOPEVOA		
DHC	N	G	1	1	L	Amb. Glass	Sulfide) ~
Groundwater Inf	forma	tion	<u>:</u>				Explosi	ves ~ LA.
Measured W	ell De	epth	:			Depth To Water:		
Comments:								

Shaw.

Project Name/#: Longhorn AAP						Sampling location ID: 24Ww38				
Project N	<u>ما</u> :#ame/#	Ngnor	D HH P	• •	Sample ID: 29 w w 38 - Feb 2007					
Weather:	SULTA	sy-Cle	AR -5	o _s	Collection Time/Date: ユーユューロフ/0930					
	''			Pumi	o Insta	allation	·- <u>-</u>			
Pump ins	tallation cre	w.Willer	mare M	•			n date/hedi	inning time:	2 - 29 - 40	1=81/10
		l head/back			•	Installatio	n date/com	pletion time:	· O - A 2 A 7	1990
	ameter (incl		ground). <u>w.</u>	0 1 0 11	-			TOC):		39
		TOC): \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	LU'		-		-	ft BTOC):		<u> </u>
) DTW/time						V/time: 3		
		ning) DTW/t			-			np rate (mL/		
		LNAF			•		•	ict: Clea	, 	
		oved during		_);	-	Discharge	tube diam	eter (3/8" or	1/4"): 3/5	2 11
		n (ft.): 🗳		-/-				/N): /		
_	ic Controlle				-		•	/		
Initial air p	ressure = F	I (ft.) X 0.43	=	psi						
		Initial	2	- · · · · · · · · · · · · · · · · · · ·	T .	T -	1 _	Т	1	1
Pressure (ps	·i)	JIIII III		3	4	5	6	7	8	Final
Refill Setting				 	5	Mr.	 	 	 -	-
Discharge S		 		 				<u> </u>		
Flow rate (m			<u> </u>	.to en la colonia. En	<u> </u>	<u> </u>				
								<u> </u>		
Pneumati	c Controlle	ump volume r Tuning: I (ft.) X 0.43						OTW (ft. BTC volumes pu		
'		Initial	2	 [1 .		1 4	1	Τ .	T =: .
Pressure (ps	il	27	27	3 タフ	27	5 27	6	7	8	Final
Refill Setting	<u>'</u>	(0	10	10	10	10	<u> </u>	 	 -	
Discharge Se	ettina	5	5	5	5	5		1	 	
Flow rate (ml		140	140	140	140	140		 	-	ļ
								1	<u>. </u>	
Time	DTW	Purge Rate	Cumulative	Quality Pa		er measure ectrical	T		1 20	T
THITE	(ft. BTOC)	(mL/min)	Volume	(degree C)		ectrical iductivity	рН	Eh	DO	Turbidity
	(11. 11.00)		Dommand (1.)	(uegree C)		lhos/cm)		(mv)	(mg/L)	(NTU)
0910	30.64	140	140	16.02			1. 1.1	2714 2	180	2 0
0915	30.64	28042	280	16,68		<u>530</u> 519	6.40	<u> አ7 ሂ. ዲ</u> ኦ 71.5	1.49	3.2
	30.64	140	420	17.07		524	6.39	280.9	1.38	3.1
	30.64	140	560	17.32		5 29	6.37	282.4	1.26	2.6
	30.64	140	700	17. 45		5∋7	4.34	284.7	1.21	2.5
<u>~ U </u>		T. T.				<u> </u>	٠. ت	707.1	1,~:	~-3
						······································	· · · · · · · · · · · · · · · · · · ·			
		<u> </u>	***					<u> </u>		



00091709

Sheet a of a

						<u> </u>			
J	· · · · · · · · · · · · · · · · · · ·			ty Parame	ter Measurement	s (continu	ed)		
Time	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity	1.	(mv)	(mg/L)	(NTU)
	<u> </u>		Purged (L)	± 10%	(uMhos/cm)	土 0.1	± 10	± 10%	100%
									<u> </u>
		+					<u> </u>		
				S			† 		
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	·	<u> </u>				 			
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	1	<u> </u>	<u> </u>				<u> </u>	<u>L</u>	
				Sa	ampling				
Sampling b	peginning ti	me: 09	3 -0		Sampling	completion	time: ^	930	
				Ouglity Da	rameter Measure		<u> </u>		
Time	DTW	Purge Rate	Cumulative		········				
Time		1	ŀ	Temp.	Electrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity	ļ	(mv)	(mg/L)	(NTU)
15.0	2- 1-1	1.16	Purged (L)		(uMhos/cm)				
1010	30.64	140	840	18.45	0.550	6.31	307.1	1.0+	4.0
		 			· · · · · · · · · · · · · · · · · · ·				
					····				
						<u> </u>			
			<u> </u>	Sample	Information				
Sample ID:	29 6161	38-1-01	5 2007			llection date	e/time: 2 - 1		
		cted (Y/N):_			Dunlicate s	ample ID:_	γume. <u> </u>	<u> </u>	
	e collected		7			le ID:			
COC No(s)	: 104	714			ори запр		<u>N</u>		
	·	¥ .1						· · · · · · · · · · · · · · · · · · ·	
Requested	I Analysis	Method	Co	ntainers	Requested	l Analysis	Method	Contai	ners
VOC		82603	-		Perchi)	.,,,,,
GASES		Sep175	<u> </u>	<u> </u>	Alkal		310.0	*	
TOC		415.1	<u></u>				210.0	2	
Anion	, c	300.0			Explo	>1 VEZ		<i>,</i> , ,	
Sulfi		376.2	<u>r</u>						
)16·A							
Comments	:								
									ļ
hbreviations:	DTOO D I								

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Lite



00091710

Page 1 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

		RFA	/ COC Number: 10494
Sample Name: Sampling Method: Sample Type: Sampling Equip: stners:	29WW38-Feb 2007 29WW38-GW-29WW38- SP GW Sample I	-REG Purpose: REG Lder Peimp	Task: MNA_EVENT_FEB07 Collection Date: ユーユネーロア Collection Time: つり30 Start Depth: 39 End Depth: 30.64 Sample Matrix: WATER
)	(ER)	(FB)	Sample Team: Willemore, M. Ac
Analytical Suite	Containers Flt Frtn Qty Size Units Ty	pe .	ERPIMS Values: Sacode:
VOC-FULL	N A 3 40 mL VOA	VIAL	Lot Control#:
ANIONS	N B 1 500 mL HDF	'E	<u>: </u>
PERC	N C 1 500 mL HDF	'E	
GASES	N D 2 40 mL VOA	Vial	
ALKALINITY	N E 1 100 mL HDF	'E	
TOC_415	N F 1 100 mL HDF	E .	
DHC	N G 1 1 L Amb	. Glass	
Groundwater Int		Depth To Water: _3	30.64



00091711

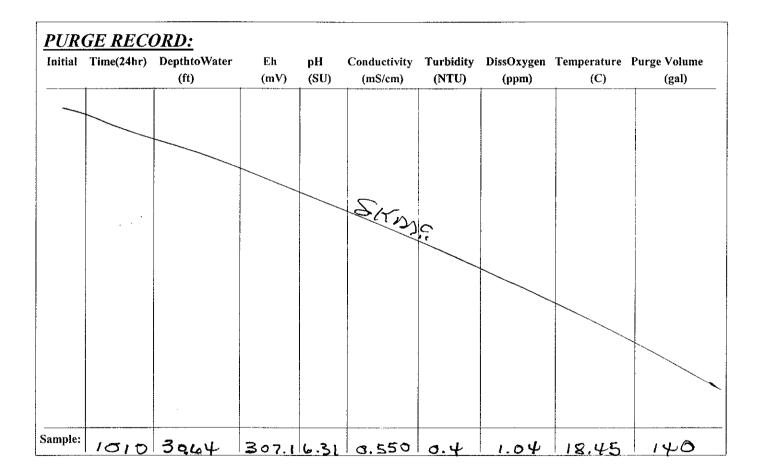
Page 2 of 2

117591 - Longhorn Army Ammunition Plant

Praveen Srivastav

Location Code: 29WW38

Sample Number: 29WW38-Feb 2007



Logged BY / Date: Serry M.F. Adoo Reviewed BY / Date:



 $00091712 \atop \text{Sheet} \ \underline{1} \ \text{of} \ \underline{z}$

Project Name/#: Langhorn Site29						Sampling location ID: 29 WWO6				
Project N	ame/#:	25 NO	SN HB	بع	_	Sample ID: 29 WW 06 - Feb 2007 Collection Time/Date: 2-22-07, 1500				
vveatner:	SULLI	27 8 c	<u> </u>			Collection	n Time/Date	e: <u>ス-スス</u> _	07,1	5 <u>00</u> _
7 11			······································	Pum	p Inst	allation	<u></u>			
Pump ins	tallation cre	wild Her	~ @ e. W				n date/hedi	و:inning time	9. 22 5-	7 01 500
PID/FID r	eading (wel	I head/back	around): a.	2/20/	=	Installatio	in data/com	pletion time	2-22-	1420
Casing di	ameter (inc	hes): 🇘 ''	ground). <u>91</u>	<u> </u>	_			TOC): <u>2</u> 5		
Total well	Depth (ft. E	STOC): 3 4	191		-			ft BTOC):		دا ۱۰دد
Initial (pre	e-installation) DTW/time	29.81	1				V/time: 2		
	er pump prin				~			mp rate (mL		~
	luct (circle):				-	Appearan	ice of produ	ict: <u>sell</u>	11111)	<u> </u>
	f water rem				_	Discharge	e tube diam	eter (3/8" or	1/4"1. 3/2	77
	tube lengtl			- <i>y</i>			cer used (Y		17 7) <u> </u>
	ic Controlle					***************************************	00. 0000 (1	// //- <u></u>		
1	oressure = F	_	; =	psi						
<u> </u>		1	1	1	1	1	. 1		7	
Pressure (ps	-1)	Initial	2	3	4	5	6	7	8	Final
Refill Setting			 		 	SKn	1			-
Discharge S	<u> </u>	 	 	· · · · · · · · · · · · · · · · · · ·		1 0 1/1/	4.7			<u></u>
Flow rate (m	<u> </u>		 	V	In the					-
					Albania.		<u> </u>		<u> </u>	
Pneumati	d tubing + po c Controlle ressure = H	r Tuning:		nei		i oi	ng + pump	volumes pu	rged:	
			1	1						· · <u> </u>
D	: \	Initial	2				· · · · · ·	γ	.	
Pressure (psi Refill Setting	<u> </u>	20	· ~ -	3	4	5	6	7	8	Final
Discharge Se	ettina		20	20	20	5	6	7	8	Final
Flow rate (ml	zung	10	10	10 50	20	5	6	7	8	Final
1 low rate (int	/min)	5	10 5	20 10 5	20 10 5	5	6	7	8	Final
	L/min)	-	10	10 50	20	5	6	7	8	Final
	1	5	100 100	20 10 5	20 10 5 100			7	8	Final
Time	рту	5	100 100	10 5 100	20 10 5 100			7 Eh	8 DO	Final
Time	1	100	/ D 5 / O Ø Water	2.0 10 5 100 Quality Pa	20 10 5 100 sramete	er Measure	ments			
	DTW (ft. BTOC)	Purge Rate	/ D 5 / OG Water Cumulative	100 5 100 Quality Pa Temp. (degree C)	20 19 5 100 ramete Con (uM	er Measure ectrical ductivity hos/cm)	ments	Eh	DO	Turbidity
1445	DTW (ft. BTOC)	Purge Rate (mL/min)	/ D S Vater Cumulative Volume Purged (L) / OO	2.0 10 5 100 Quality Pa Temp. (degree C)	20 19 5 100 ramete Con (uM	er Measure ectrical ductivity	ments	Eh	DO	Turbidity
1445	DTW (ft. BTOC) 29.85 29.85	Purge Rate (mL/min)	/ D S / OO Water Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.91 19.89	20 10 5 100 sramete Con (uM	er Measure ectrical ductivity hos/cm)	ments pH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
1445 1450 1455	DTW (ff. BTOC) 29.85 29.85 29.85	Purge Rate (mL/min) IDO IDO	/ D S Vater Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.89	20 10 5 100 tramete Con (uM 3.5 3.5	er Measure ectrical ductivity hos/cm)	ments pH	Eh (mv)	DO (mg/L)	Turbidity (NTU)
1445	DTW (ft. BTOC) 29.85 29.85	Purge Rate (mL/min)	/ D S / OO Water Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.91 19.89	20 10 5 100 tramete Con (uM 3.5 3.5	er Measure ectrical ductivity hos/cm)	ments pH 6.41	Eh (mv) 224.6 227.6	DO (mg/L)	Turbidity (NTU) 2.3 2.3
1445 1450 1455	DTW (ff. BTOC) 29.85 29.85 29.85	Purge Rate (mL/min) IDO IDO	/ D S Vater Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.89	20 10 5 100 tramete Con (uM 3.5 3.5	er Measure ectrical ductivity hos/cm)	ments рН 6.41 6.41 6.44	Eh (mv) 227-6 234.6	DO (mg/L) 1.81 1.61	Turbidity (NTU) 2.3 2.3 1.5
1445 1450 1455	DTW (ff. BTOC) 29.85 29.85 29.85	Purge Rate (mL/min) IDO IDO	/ D S Vater Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.89	20 10 5 100 tramete Con (uM 3.5 3.5	er Measure ectrical ductivity hos/cm)	ments рН 6.41 6.41 6.44	Eh (mv) 227-6 234.6	DO (mg/L) 1.81 1.61	Turbidity (NTU) 2.3 2.3 1.5
1445 1450 1455	DTW (ff. BTOC) 29.85 29.85 29.85	Purge Rate (mL/min) IDO IDO	/ D S Vater Cumulative Volume Purged (L) / OO 200	20 10 5 100 Quality Pa Temp. (degree C) 19.89	20 10 5 100 tramete Con (uM 3.5 3.5	er Measure ectrical ductivity hos/cm)	ments рН 6.41 6.41 6.44	Eh (mv) 227-6 234.6	DO (mg/L) 1.81 1.61	Turbidity (NTU) 2.3 2.3 1.5



00091713

Sheet 2_of 2_

		1	Water Quali	ity Parame	ter Measurement	s (continu	ed)	·	
Time	DTW	Purge Rate	1		±3% Electrical	pH	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	エッル Conductivity		(mv)	(mg/L)	(NTU)
	İ		Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	+10%	
						 	1	1 10 16	-
			<u>-</u> -			-			
							 	 	<u> </u>
		1				 	-		
						 	 	 	
				SKM			 	 	
		·		(4.V)			 	 	ļ
	<u> </u>					 -	 -	 -	
						 		 	
	 	1				\leftarrow	 	ļ <u>.</u>	
		<u> </u>						<u> </u>	<u> </u>
		 				 	 		
	 	 			<u> </u>	 			
	 	 					 		
***************************************		<u>.l</u>						<u> </u>	
				Sa	ampling				
ampling t	peginning ti	me: <u>150</u>		Quality Pa	Sampling o rameter Measure		time: <u>15</u>	30	
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uMhos/cm)] ' '	('3'-/	()
1535	29.85	100	500	77	3.517	6.5	248.7	1.51	0.7
			21/4	70.22			1		
				4					
				Sample	Information		<u> </u>		
ample ID:	29 WW	06-Fe	b 2007		Sample col	lection date	e/time: <u>2−2</u>	2-07	
uplicate s	ample colle	cted (Y/N):_	<i>N</i>		Duplicate s	ample ID:	N		
	e collected		N		Split sample				
OC No(s)	109	57	·····	<u> </u>					
equested	Analysis	Method	Coi	ntainers	Requested	Analysis	Method	Contai	inore
NOC		82603		₹	Perchlo		314.0	1	
	-002	S-0175		3	BIKAL		310.0	1	
TOC		415.1		<u> </u>	Explo		3,0.0	<u>, , , , , , , , , , , , , , , , , , , </u>	
Nion		300.0			- 1 3 P 10	31062		<u> </u>	
ulfid	es	376.2		Ì					
omments	nale	مخره د	ellow	col 7	annie				
breviations.	RTOC - Relo	w ton of casing	DTW Dooth	to work and I h					



00091714

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

	RF	A / COC Number: <u>l (</u>	2951
Location Code:			MNA_EVENT_FEB07
Sample Number:	29WW06- Feb 2007	Collection Date:	
Sample Name:	29WW06-GW-29WW06REG	Collection Time:	
Sampling Method:			32.5
Sample Type:		End Depth:	29.85
Sampling Equip:	tainless Seel Bladden Pun		
B)	(ER) (FB)	Sample Team:\	dillemore MSAdo
Analytical Suite	Containers Flt Frtn Qty Size Units Type		S Values: Sacode:
VOC-FULL	N A 3 40 mL VOA VIAL	Lot	Control#:
ANIONS	N B 1 500 mL HDPE		
PERC	N C 1 500 mL HDPE		
GASES	N D 2 40 mL VOA Vial		
ALKALINITY	N E 1 100 mL HDPE		
TOC_415	N F 1 100 mL HDPE		
DHC	N G 1 1 L Amb. Glass		
Groundwater Int Measured W Comments:	Formation: Vell Depth: 35.19 Depth To Water:	29.81	
Sketch Locat	ion:		

Logged BY / Date: Reviewed BY / Date:



00091715

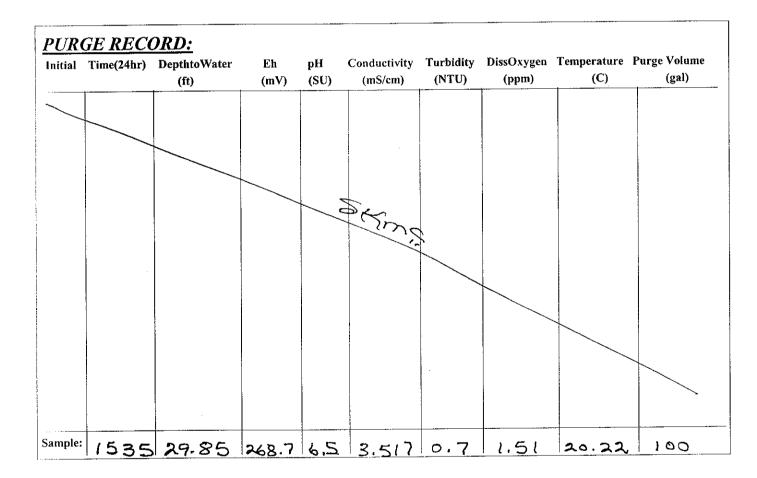
Page 2 of 2

117591 · Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW06

Sample Number: 29WW0676b2007



Logged BY / Date: Sherry M. Per

Reviewed BY / Date:

00091716 Sheet 1 of 2



eb 20 7, 12	D7							
7, 12								
,	Collection Time/Date: 2-22-57, 1245							
Pump Installation								
<u>- ユス-07</u>	,1125							
A-2207 5 to)							
5to	45							
<u>, o</u>								
. 7o								
nin):								
ر4"): 3/	<u>'</u>							
8	Final							
	1 1/101							
	 							
	<u></u>							
C):_ <u>_2</u> ged:	. 70							
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8	Finaí							
55								
<u> </u>								
10								
200								
	Turbidity							
200								
2 00	Turbidity							
DO (mg/L)	Turbidity (NTU)							
DO (mg/L)	Turbidity (NTU)							
DO (mg/L) 0,43	Turbidity (NTU)							
DO (mg/L) 0.63 0.55	Turbidity (NTU) 14.4 .19.4							
DO (mg/L) 0,63 0,55 0.52	Turbidity (NTU) 14.6 19.6							
200 DO (mg/L) 0.63 0.55 0.52 0.43	Turbidity (NTU) 14.6 .19.6 1.4 1.1							
DO (mg/L) 0,63 0,55 0.52	Turbidity (NTU) 14.6 19.6							
	8 bund):3,2 cound):3,2 ed:							

00091717



GROUNDWATER SAMPLING FORM

Sheet 2 of 2

Time	(ft. BTOC)	Purge Rate (mL/min)		Temp.	±3% Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	I		1126		1		I raibiaity
			Volume	(degree C)	Conductivity	1.	(mv)	(mg/L)	(NTU)
	1		Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	± 10 %	
									
									1
							<u> </u>		
								· · · · · · · · · · · · · · · · · · ·	
				27	\$35C		 		
					3 50				
						 	 	- [
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		i					 		
						 	 	 	
							 	 	
		<u> </u>			mpling	<u> </u>	<u></u>		
		ne: <u>)ス</u> ↓	Water		rameter Measure		time:	1220	
Time	DTW	i	Cumulative	Temp.	Electrical	Нq	Eh	DO	Turbidity
	(ft. BTOC)	(mL/mîn)	Volume	(degree C)	Conductivity	ļ	(mv)	(mg/L)	(NTU)
1355	42.70		Purged (L)		(uMhos/cm)				
.927	42.10	200	1800	25.96	<u>০.১</u> 7২,	7.38	-106.5	0.80	1.6
ample ID:	29 600	035-F		Sample	Information				
tunlicate sa	ample collec	cted (Y/N):_		<u>vo 7</u>	Sample col	ection date	/time: 2 - 2	2-57	
opiidato oc	collected (Y/N): <u>\</u>			Duplicate s	ampie ເນ:	14 YAM	W35-Feb:	2007-
OC No(s):	109	57			Split sampl	e ID:	N		
equested	Analysis	Method	Co	ntainers	Requested	Analysis	Method	Contai	inore
VOC		8260 B		3	Perchl			1	
GASES	- 002	500175		3	AIKAL		310.0	1	
TOC		415.1		₹	Explo	E . / • C	3.0.0	2	
ANION		300.0	[- CAPIO	3. V C			
Julfide	es :	376.2		1					
omments:									
									j

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Liter



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117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

			RFA/	COC Number:	10957
Location Code:	29WW35			Task:	MNA EVENT FEB07
Sample Number:	29WW35- F	3002 ومعرطا			2-22-07
Sample Name:	29WW35-GV	V-2 9WW35	-REG	Collection Time:	
Sampling Method:	SP				90'
Sample Type:		San	iple Purpose: REG		42.70
Sampling Equip: S Partners:	tainless	Steel	ladder Pump	Sample Matrix:	
TB)	(ER)		(FB)	Sample Team:	Willemore MEAdo
Analytical Suite	Con Flt Frtn Qty	tainers Size Units	у Туре		S Values: Sacode:
VOC-FULL	N A 3	40 mL	VOA VIAL	Lot	Control#:
ANIONS	N B 1	500 mL	HDPE		
PERC	N C 1	500 mL	HDPE		
GASES	N D 2	40 mL	VOA Vial		
ALKALINITY	N E 1	100 mL	HDPE		
TOC_415	N F 1	100 mL	HDPE		
DHC	N G 1	1 L	Amb. Glass		
	ormation: ell Depth: 4	5′	Depth To Water: 3	1 45 42.84	
Comments:					
Sketch Locati	on:				

Logged BY / Date: Sperry MEDdoo Reviewed BY / Date:



00091719

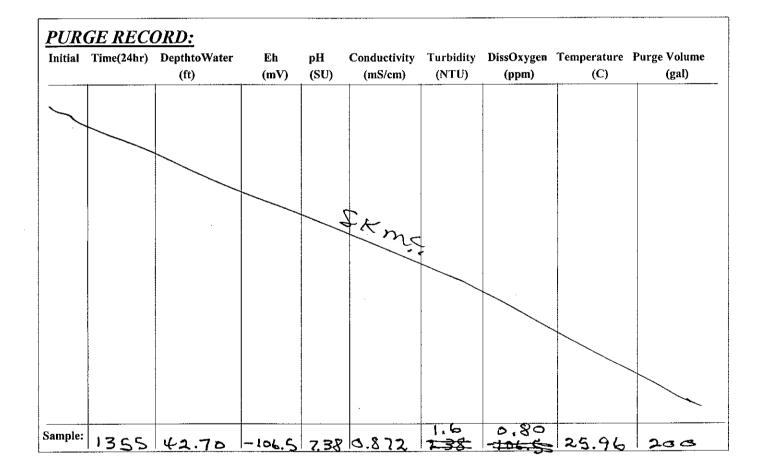
Page 2 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW35

Sample Number: 29WW35-Feb 2007



Logged BY / Date: Sherry M. Aleo

Reviewed BY / Date:



00091720

Page 1 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code:		COC Number: 10495
		Task: MNA_EVENT_FEB07
Sample Number:	29WW36-Feb 2007	Collection Date: 2-21-07
Sample Name:	29WW36-GW-29WW36REG	Collection Time: 1515
Sampling Method:	SP	Start Depth: 31'
Sample Type:		End Depth: 28.88
Sampling Equip:	Stainless Steed Pladder	Sample Matrix: WATER
artners: B <u>)</u>	(ER) (FB) Pumps	Sample Team: Willemore M.S.A.
Analytical Suite	Containers Flt Frtn Qty Size Units Type	ERPIMS Values: Sacode:
VOC-FULL	N A 3 40 mL VOAVIAL	Lot Control#:
ANIONS	N B 1 500 mL HDPE	
PERC	N C 1 500 mL HDPE	
GASES	N D 2 40 mL VOA Vial	
ALKALINITY	N E 1 100 mL HDPE	`
TOC_415	N F 1 100 mL HDPE	
DHC	N G 1 1 L Amb. Glass	
Groundwater In Measured W	formation: Vell Depth: <u>36.70</u> Depth To Water: <u>2</u> &	₹.9
Comments:		

Logged BY /	Date: Berr	ym Poloo
	n - m ,	- ~



00091721

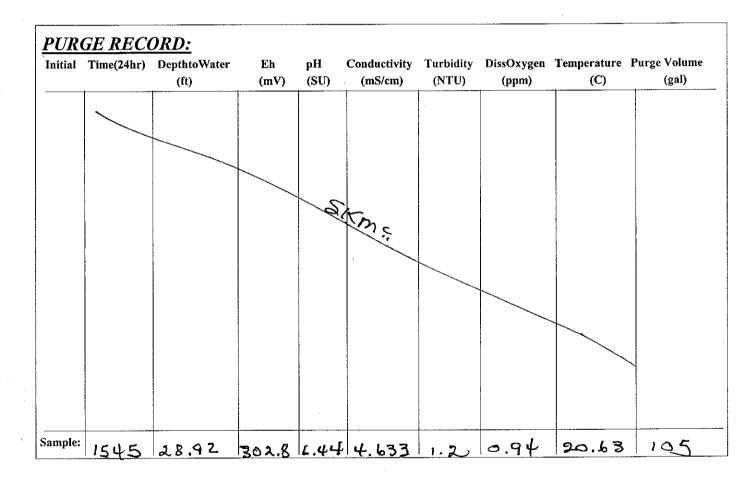
Page 2 of 2

117591 - Longhorn Army Ammunition Plant

Manager: Praveen Srivastav

Location Code: 29WW36

Sample Number: 29WW36Feb 2007



Logged BY / Date: Sherry M. Feloo

Reviewed BY / Date:



00091722 Sheet 1 of 2.

Operable	Unit/Site ID:	LONG	hoRN,	5.7029	2	Sampling	location ID:	29W U	<u> 3と</u>					
	<u>اصا</u> :#:ame								200	7				
Weather:_	Supp	J 80.			-	•			7/15					
			`			allation								
Pump inst	allation crev	v: Willer	more/1	M. Ado	6	Installation	n date/begir	nning time:	2-21-07/	14230				
PID/FID re	eading (well	head/backg							<u> 2-21-07</u>					
	ameter (inch		1				terval (ft. BT		to					
Total well	Depth (ft. B	TOC): 34						BTOC): ᢃ	7 1					
	-installation)							//time: ユミ						
Final (after	r pump prim	ing) DTW/ti	ime: <u>28.8</u>	58				ip rate (mL/i						
-	uct (circle):						ce of produc			·				
Volume of	water remo	ved during	priming (mL	-):		Discharge	tube diame	eter (3/8" or	1/4"): 3/ g	1,				
4	tube length			·	_		cer used (Y/							
Pneumatic Controller Tuning: Initial air pressure = H (ft.) X 0.43 = psi														
lnitial air p	ressure = H	(ft.) X 0.43	=	_ psi										
		Initial	2	3	4	5	6	7	8	Final				
Pressure (ps					ļ									
Refill Setting						DVII	P.S.	<u> </u>	<u> </u>					
Discharge Se					ļ	<u> </u>			<u> </u>					
Flow rate (ml	Jmin)	<u></u>	<u> </u>		<u> </u>	<u> </u>				<u> </u>				
Initial (pre- Calculated Pneumation	-purging) DT I tubing + pu c Controlle	TW (ft. BTO) Imp volume: r Tuning:	C): <u>スき, 8</u> : <u>N</u>	38		Final (post	t-purging) D	TW (ft. BTO	Purging/sampling crew: \(\begin{align*} \lambda \lamb					
		Initial	2	3	<u> </u>	k and a second s								
Pressure (psi			<u> </u>		4	5	6	7	1 ₈	Final				
Refill Setting	- 7	21	ובי											
							6	7	8	Final 721				
Discharge Se)	10	21 10 5	21	5	6	7	8	· · · · · · · · · · · · · · · · · · ·				
Discharge Se Flow rate (mL	etting	10	10	21	21		6	7	8	71				
	etting	10 5	10 5 105	21 10 5	21. 10 S 10.5			7	8	21 10 5				
	etting	10 5	10 5 105	31 10 5 105	21: 10 S 105			7 Eh	8 DO	21 10 5				
Flow rate (mL	etting /min)	105	10 5 105 Water	21 10 5 105 Quality Pa	21 10 S 105 ramete	er Measure	ments			21 10 5 105				
Flow rate (mL	etting _/min)	10 5 105	1 € 5 10 5 Water	2 10 5 10 5 Quality Pa	ID S Io.5 ramete	er Measure	ments	Eh	BO	Zi io 5 105				
Flow rate (mL	onting Jermin) DTW (ff. BTOC)	10 5 105	L O S Water Cumulative Volume Purged (L)	2 10 5 10 5 Quality Pa	ID S I > 5 Iramete Con (uM	er Measure ectrical aductivity	ments	Eh	DO (mg/L)	Zi io 5 105				
Flow rate (mL Time	Arting Armin) DTW (ft. BTOC)	Purge Rate (mL/min)	Vater Cumulative Volume Purged (L) 1 0 5	21 10 5 105 Quality Pa Temp. (degree C)	ID S 105 ramete Con (uM 4.	er Measure ectrical aductivity lhos/cm)	ments pH	Eh (mv)	DO (mg/L)	Z1 10 5 105 Turbidity (NTU)				
Flow rate (mL Time	DTW (ff. BTOC)	Purge Rate (mL/min)	Vater Cumulative Volume Purged (L) 105	21 5 105 Quality Pa Temp. (degree C)	10 Saramete Con (uM 4.	er Measure ectrical aductivity Ihos/cm)	ments pH	Eh (mv)	DO (mg/L) 1.49	Zi (° 5 105 Turbidity (NTU)				
Time 1455	DTW (ff. BTOC) 28.88	105 105 Purge Rate (mL/min)	Volume Purged (L) 105 210 315	21 105 105 Quality Pa Temp. (degree C) 20.04	21: 10 S ramete Con (uM 4. 4.	er Measure ectrical aductivity (hos/cm) 704 675 659	ments pH 6.4	Eh (mv) 2-698 275.5	DO (mg/L)	21 10 5 105 Turbidity (NTU) 2.0 2.0				
Time 1455 1500	DTW (ff. BTOC) 28.88 28.88 28.88	Purge Rate (mL/min)	Vater Cumulative Volume Purged (L) 105	21 10 5 105 Quality Pa Temp. (degree C) 20.06 20.00	21: 10 S ramete Con (uM 4. 4.	er Measure ectrical aductivity (hos/cm)	ments pH 6.4 6.4 6.4 6.4	Eh (mv) 2.692 275.5 280.9	DO (mg/L) 1.49 1.24 1.00	21 10 5 105 Turbidity (NTU) 2.0 2.0				
Time 1455 1500	DTW (ff. BTOC) 28.88 28.88 28.88	Purge Rate (mL/min)	Volume Purged (L) 105 210 315	21 10 5 105 Quality Pa Temp. (degree C) 20.06 20.00	21: 10 S ramete Con (uM 4. 4.	er Measure ectrical aductivity (hos/cm) 7 0 4 6 7 5 6 5 9	ments pH 6.4 6.4 6.4 6.4	Eh (mv) 2.692 275.5 280.9	DO (mg/L) 1.49 1.24 1.00	21 10 5 105 Turbidity (NTU) 2.0 2.0				
Time 1455 1500	DTW (ff. BTOC) 28.88 28.88 28.88	Purge Rate (mL/min)	Volume Purged (L) 105 210 315	21 10 5 105 Quality Pa Temp. (degree C) 20.06 20.00	21: 10 S ramete Con (uM 4. 4.	er Measure ectrical aductivity (hos/cm) 7 0 4 6 7 5 6 5 9	ments pH 6.4 6.4 6.4 6.4	Eh (mv) 2.692 275.5 280.9	DO (mg/L) 1.49 1.24 1.00	21 10 5 105 Turbidity (NTU) 2.0 2.0				



00091723

Sheet 2_of 2_

			Nater Quali	ity Parame	ter Measurement	s (continue	ad)		-
Time	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	На	Eh	DO	Turbidity
	(ft. BTOC)		Volume	(degree C)	±3% Conductivity		(mv)	(mg/L)	(NTU)
İ			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	= 10%	± 10%
/					,	 		10 10	-
V						ļ	<u> </u>		
				-					
				5.			· · · · · · · · · · · · · · · · · · ·		
				$\leq \langle \nabla V \rangle$	na				
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: 	<u> </u>								
	<u> </u>	<u> </u>							
··· · · · ·		<u> </u>		<u> </u>					
		<u> </u>			······		<u> </u>		
				Sa	mpling				
Sampling b	eginning tii	ne: <u> 15</u>	15		Sampling o	ompletion t	time: <u>15</u>	15	
		· · · · · · · · · · · · · · · · · · ·	Water	Quality Pa	rameter Measure	ments			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	pН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		(uMhos/cm)				
<u>1545 </u>	28.72	105	525	20.63	4.633	6.44	3028	0.94	1.2
		ļ							
									
		_		Sample	Information				
Sample ID:	29WW	36-Fe<u>F</u> cted (Y/N):_	2007		Sample col	lection date	/time: 2~	70-15	
Duplicate s	ample colle	cted (Y/N):_	7		Duplicate s	ample ID:_	/time: 2 -		
Split sampl	e collected	(Y/N): •	7		Split sample	e ID:	7		
COC No(s)	104	45							
Requested	Analysis	Method	Co	ntainers	Requested	Analysis	Method	Camtai	
VOC		3260B	3		Reachli			Contai	ners
CASE		50P175	<u>~</u>		Alkal				
Toc		415.1			Explos		310.		
ANIO		300.0	<u></u>		Cubiaz	, , ,		<u> </u>	
Suls		376.2	<u>;</u>	·····				· ··· · · · · · · · · · · · · · · · ·	
Comments									
Joinments	•								
	PTOC Rolo								

Abbreviations: BTOC - Below top of casing; DTW - Depth to water; H - head above pump intake; mL - milliliter; L - Lite





Opposible	Unit/Site II	1 114	no			C 1:	1 (1)	C:10	50	
	lame/#:			0.00				o: Site		
Monthor	SUNNY	11591	00046	800				W37-0		01/100
vveatrier.	ZUNNY	1 30°F			*****	Collectio	on Time/Dat	e: i	33 6	+11/08
				Pun	np Inst	allation			1 1	
Pump ins	tallation cre	ew: 5	lesus			Installati	on date/bed	jinning time	2/1/08	12:15
	eading (we			The second second second		Installati	on date/con	pletion time	5/1/08	12:30
1	ameter (inc		411			Screen I	nterval (ft. F	BTOC): _ \(\xi \)	35 0010	95.00
	Depth (ft. E		95 00					ft BTOC): _		
	e-installation				-	Post-inst	allation DT\	W/time:	40 11)
	er pump prir							mp rate (ml		
	luct (circle):						nce of produ			
	f water rem					223 (8		neter (3/8" o	r 1/4")·	
	e tube lengtl		5 (-		icer used (Y		1 1/4)	
	ic Controlle					mict rede	7001 U30U (1	/14)		
1	nitial air pressure = H (ft.) X 0.43 =psi									
		Initial	2			T -		Т _	T	T
Pressure (ps	ai)	Hilliai	2	3	4	5	6	7	8	Final
Refill Setting						-	-			
Discharge S						-				
Flow rate (m				+		-			-	
					<u> </u>					
Initial (pre Calculated Pneumati	e/beginning -purging) D d tubing + pu c Controlle ressure = H	TW (ft. BTO ump volume e r Tunin g:	c): 48	3.10 NA	-	Final (pos	st-purging) [on time: 2 DTW (ft. BT0 volumes pu	OC):4	8.35
		T (11.) 7. 0.40	1	_ psi	· · · · · · · · · · · · · · · · · · ·	·		-		
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps	i)	50			-	1				
Refill Setting		48								
Discharge Se		45								
Flow rate (ml	Jmin)	150								
			Water	Quality P	aramete	er Measure	ements			
Time	DTW	Purge Rate	Cumulative	Temp.	T	ectrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	1	ductivity		(mv)	(mg/L)	(NTU)
			Purged (L)		1	lhos/cm)		(((1110)
12:35	48.20	150	750	16.29	0 /	65	8.36	144.5	3,43	3.4
12:40	48.25	150	1500	16,62	0.1	100	7.94	1496	2.73	2,3
12:45	48.30	150	2250	17.02	0,1	069	7.48	157.8	2,34	1.7
12:50	48.32	150	3000	17.26	0.1	270	7.11	158.7	1.99	1.3
12:55	48.34	150	3750	17.35	0,1	072	6,98	147.3	1,76	0.9
1:00	48.35	150	4500	17.38	0.1	071	6.85	125,3	1.67	0.9
1105	48.35	150	5250	17.49	0:6	_7 :	6.78	111.7	1.60	0.10
1:10	48.35	150	6000	17.54		77	6.77	100 9	1.57	08





Time			Nater Quali	ty Paramet	er Measurement	s (continue	d)	_	
1	DTW	Purge Rate	Cumulative	Temp.	±3% Electrical	рН	Eh	DO	Tentachty
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	± 10%	(uMhos/cm)	± 0.1	± 10	±107c	= 100%
1:15	48.35	150	6750	17.32	0.674	6.68	81.3	1.57	0.6
1:20	48.35	150	7500	16.87	0.674	6,58	72,5	1,56	0.6
11,25	48.35	150	8250	16.98	0.672	6.56	60.7	1.48	0.6
1:30	48.35	150	9000	17.09	0.672	6.55	59.8	1.44	0.5
1:35	48.35	150	9750	17.11	0.673	6.55	57.6	1.43	0.3
							4		
									NATIONAL PROPERTY OF THE PERSON NAMED IN
Sampling b	eginning tin	ne(:35		mpling Sampling	completion t	ime:/.	37	
			Water	Quality Par	ameter Measure	ements			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	MITTER
			Purged (L)		(uMhos/cm)				
									-
									The second secon
					the Lagrangian management of the lagrangian and the				
Sample ID:_ Duplicate sa Split sample COC No(s):	ample collected (cted (Y/N):_	20108	Sample	Duplicate s	Illection date sample ID: le ID:	·	08 /;	35
Requested	Analysis	Method	Co	ntainers	Requested	d Analysis	Method	Conta	iners
				nt glass				50	
VIII			1 1	71003					
VOC									
VUC		- 1							
VVC					1		- 1		
VUC					-				
									PROGRAMMENT OF THE PROGRAMMENT O
Comments	:								
	:								

Shaw G

Operable	Unit/Site II	D: LH	AAP	*		Samplin	g location II	o: Sit	e 29	
Project N	ame/#:	17591.	0009	B800		Sample	ID: 291	NW39	-0201	08
Weather:	SUN	NY 59	JOF			Collectio	on Time/Dat	e: 3:3	30 2/	1/08
				Dum	n Inot					
		Do	^ .	run	ip inst	allation			-110	·
1	tallation cre		l Senger	>		Installati	on date/beg	inning time	2/1/00	2:05
1	eading (wel					Installati	on date/con	pletion time	e: 2/1/0	2:05
Casing di	ameter (inc		411			Screen I	nterval (ft. E	BTOC): 7	1.22 to	81.22
	Depth (ft. E					Pump int	take depth (ft BTOC): _	82,00	0
•	e-installation			12		Post-inst	tallation DT\	N/time:		
	er pump prir					Max. sus	stainable pu	mp rate (ml	/min):	
Free product (circle): LNAPL / DNAPL						Appeara	nce of produ	uct:		
Volume of water removed during priming (mL):						Discharg	e tube diam	eter (3/8" o	r 1/4"):	
Discharge tube length (ft.):							ucer used (Y			
Pneumatic Controller Tuning:										
Initial air pressure = H (ft.) X 0.43 = psi										
		Initial	2	3	4	5	6	7	8	Final
Pressure (ps	si)									Ciria
Refill Setting								 		+
Discharge S										
Flow rate (m								+		
					 Purgin					
Initial (pre- Calculated Pneumati	e/beginning -purging) D I tubing + pu c Controlle	TW (ft. BTO ump volume r Tuning:	C): 32	2120 .08	-	Final (pos	te/completio st-purging) E ing + pump	TW (ft. BT	OC): 37	3:30
Initial air p	ressure = H	(tt.) X 0.43		_ psi					,	
-		Initial	2	3	4	5	6	7	8	Final
Pressure (psi	i)	50								
Refill Setting		50								
Discharge Se	etting	45								
Flow rate (mL	_/min)	100								
			Water	Quality Pa	aramete	r Measure	ements			1
Time	DTW	Purge Rate	Cumulative	Temp.	1	ectrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	1	ductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	, ,	ł	hos/cm)		(,	(mg/c)	(1410)
2:25	32.15	100	500	17,58		20	10.37	21.2	1.33	3.5
2:30	32.17	100	1000	17.79	0,6	t- 1	10.32	15.5		2,3
2:35	32.19	100	1500	17.84	0.6	20	10.28	17.9	0,89	
2:40	32,20	100	2000	17.81	0.6		10.20	14.5	0.62	2.2
21,45	32.20	100	2500	17.79		004			0.48	2.5
21,50	32,20	100	3000	1700		594	9,98	16.8	0.38	1.7
21.55	32.20	100	3500	17/0		585	9.88	19.7	0.29	3.6
3:00	32,20	100	4000	1710		500	9.88	22.4	0.24	4.1
0,00	200	1-0	- 1000	1/6	(3)	7 % ()	17,801	111.51	012	771





	T			(er Measurement	s (continue	a)	Ţ	T
. Time	DTW	Purge Rate	1		±3% Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mUmin)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
	-		Purged (L)	± 10%	(uMhos/cm)	± 0.1	±10	±107c	100%
3:05	32,20		4500	17,60	0.574	9.73	25,9	9120	3.4
3'.10	32.20	100	5000	17.58	0,568	9.67	27.1	0,19	3.6
3:15	32,20		5500	17,55	0.564	9.60	28,6	0,18	5.1
3:20	32,20		6000	17.54	0.560	9.58	30,3	0.17	5.3
3:25	32,20	100	6500	17.53	0,566	9,55	30.1	0.17	5.0
3:30	32,20	100	7000	17,53	0.559	9.53	29.5	0.17	5.5
	-	-	-						
						-			
		-			***************************************				
<i>u</i>									
	<u> </u>								
		-	. 0	Sa	mpling		`	1 -	
Sampling b	eginning tir	ne:3	: 30		Sampling (completion ti	me: 3	. 32	
			Water	Quality Par	rameter Measure	ements			
Time	DTW	Purge Rate	Cumulative	Temp.	Electrical	рН	Eh	DO	Turbidity
	(ft. BTOC)	(mL/min)	Volume	(degree C)	Conductivity		(mv)	(mg/L)	(NTU)
			Purged (L)	1 3	(uMhos/cm)		()	(9.2)	11107
					1 6 4:				
0 1 10	10.	21		Sample	Information		~ 1	100	,
Sample ID:	24MM	239-0	20108		Sample col	llection date	time: 2//	108 3	.50
	ample colle	()//// ()			Duplicate s	ample ID:			
Split sample COC No(s)	e collected ((1/14):			Split sampl	e ID:			
						γ-			
Requested	Analysis	Method	Со	ntainers	Requested	Analysis	Method	Contai	ners
VOC				niglas				Ootitai	1013
				7					
			-						
C									
Comments	:								
									-

Attachment 5

Laboratory Reports

Available on the attached CD



156 Starlite Drive, Marietta, OH 45750 • TEL 740-373-4071 • FAX 740-373-4835 • http://www.kemron.com

Laboratory Report Number: L0609004

Please find enclosed the analytical results for the samples you submitted to KEMRON Environmental Services.

Review and compilation of your report was completed by KEMRON's Sales and Service Team. If you have questions, comments or require further assistance regarding this report, please contact your team member noted in the reviewed box bleow at 800-373-4071. Team member e-mail addresses also appear here for your convenience.

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Kathy Albertson - Team Chemist/Data Specialist

kalbertson@kemron-lab.com

This report was reviewed on September 13, 2006.

Stephanie Mossburg

STEPHANIE MOSSBURG - Team Chemist/Data Specialist

I certify that all test results meet all of the requirements of the NELAP standards and other applicable contract terms and conditions. All results for soil samples are reported on a 'dry-weight' basis unless specified otherwise. Analytical results for water and wastes are reported on a 'as received' basis unless specified otherwise. A statement of uncertainty for each analysis is available upon request. This laboratory report shall not be reproduced, except in full, without the written approval of KEMRON Environmental Services.

This report was certified on September 13, 2006.

David Vandenberg - Vice President

FL DOH NELAP ID: E8755

David & Vande berg

This report contains a total of $\underline{44}$ pages.

Protecting Our Environmental Future

KEMRON ENVIRONMENTAL SERVICES REPORT NARRATIVE

00091730

KEMRON Login No.: L0609004

CHAIN OF CUSTODY: The chain of custody number was 10407.

SHIPMENT CONDITIONS: The chain of custody forms were received sealed in a cooler. The cooler temperature

was 3 degrees C.

SAMPLE MANAGEMENT: All samples received were intact.

I certify that this data package is in compliance with the terms and conditions agreed to by the client and KEMRON Environmental Services, both technically and for completeness, except for the conditions noted above. Release of the data contained in this hardcopy data package has been authorized by the Laboratory Manager or designated person, as verified by the following signature.

Approved: 05-SEP-06

Stephanie Mossburg

Laboratory Data Package Cover Page

This data Package consists of:

This signature page, the laboratory review checklists, and the following reportable data:

- R1 Field chain-of-custody documentation;
- R2 sample identification cross-reference;
- R3 Test reports (analytical data sheets) for each enviornmental sample that includes:
 - a) Items consistant with NELAC 5.13 or ISO/IEC 17025 Section 5.10
 - b) dilution factors.
 - c) preparation methods,
 - d) Cleanup methods, and
 - e) If required for the project, tentatively identified compounds (TICs)
- R4 Surrogate recovery data including:
 - a) Calculated recovery (%R) for each analyte, and
 - b) The laboratory's surrogate QC limits.
- R5 Test reports/summary forms for blank samples;

R6 Test reports/summary forms FOR laboratory control samples (LCSs) including:

- a) LCS spiking amount,
- b) Calculated %R for each analyte, and
- c) The laboratory"s LCS QC limits.

R7 Test reports for project matrix spike/matrix spike duplicates (MS/MSDs) including:

- a) Samples associated with the MS/MSD clearly identified,
- b) MS/MSD spiking amounts,
- c) Concentration of each MS/MSD analyte measured in the parent and spiked samples,
- d) Calculated %R and relative percent differences (RPDs), and
- e) The laboratory's MS/MSD QC limits

R8 Laboratory analytical duplicate (if applicable) revocery and precision:

- a) the amount of analyte measured in the duplicate,
- b) the calculated RPD, and
- c) the laboratory's QC limits for anlytical duplicates.

R9 List of method quantitation limits (MQLs) for each analyte for each method and matrix;

R10 Other problems or anomalies.

The exception Report for every "No" or "Not Reviewed (NR)" item in laboratory review checklist.

Release statement: I am responsible for the release of this laboratory data package. This data package has been reviewed by the laboratory and is complete and technically compliant with the requirements of the methods used, except where noted by the laboratory in the attached exceptions reports. By my signature below, I affirm to the best of my knowledge, all problems/anomalies, observed by the laboratory as having the potential to affect the quality of the data, have been identified by the laboratory in the Laboratory Review Checklist, and no information or data have been knowingly withheld that would affect the quality of the data.

Check, If applicable: [] This laboratory is an in-house laboratory controlled by the person repsonding to rule. The official signing the cover page of the rule-required report (for example, the APAR) in which these data are used is responsible for releasing this data package and is by signature affirming the above release statement is trus.

DEANNA I. HESSON	Inmalpsson	Conventional Lab Supervisor	September 12, 2006
Name (Printed)	Signature	Official Title (printed)	DATE

RG-366/TRRP-13 December 2002

Α1

00091731

00091732

KEMRON Environmental Services

Laboratory Review Checklist

Laboratory Name:
Laboratory Log Number:
Project Name:

Method:
Prep Batch Number(s):
Reviewer Name:
LRC Date:

KEMRON
L0609004
798-LONGHORN
PCTSOLIDS
WG221779
DEANNA I. HESSON
September 12, 2006

Description	Yes	No	NA(1)	NR(2)	ER(3)
Chain-Of-Custody (C-O-C)					
Did samples meet the laboratory's standard conditions of sample acceptability upon	√				
receipt?					
Were all departures from standard conditions described in an exception report?	√				
Sample and quality control (QC) identification					
Are all field sample ID numbers cross-referenced to the laboratory ID numbers?	√				
Are all laboratory ID numbers cross-referenced to the corresponding QC data?	√				
Test reports					
Were all samples prepared and analyzed within holding times?	√				
Other than those results <mql, all="" bracketed="" by="" calibration="" other="" raw="" standards?<="" td="" values="" were=""><td></td><td></td><td>√</td><td></td><td></td></mql,>			√		
Were calculations checked by a peer or supervisor?	√				
Were all analyte identifications checked by a peer or supervisor?			√		
Were sample quantitation limits reported for all analytes not detected?			√		
Were all results for soil and sediment samples reported on a dry weight basis?	√				
Were % moisture (or solids) reported for all soil and sediment samples?	√				
If required for the project, TICs reported?			√		
Surrogate recovery data					
Were surrogates added prior to extraction?			√		
Were surrogate percent recoveries in all samples within the laboratory QC limits?			√		
Test reports/summary forms for blank samples					
Were appropriate type(s) of blanks analyzed?			√		
Were blanks analyzed at the appropriate frequency?			√		
Were method blanks taken through the entire analytical process, including preparation and, if applicable, cleanup procedures?			√		
Were blank concentrations <mql?< td=""><td></td><td></td><td>√</td><td></td><td></td></mql?<>			√		
Laboratory control samples (LCS):			V		
Were all COCs included in the LCS?			√		
Was each LCS taken through the entire analytical procedure, including prep and cleanup			V		
steps?			'		
Were LCSs analyzed at the required frequency?			\		
Were LCS (and LCSD, if applicable) %Rs within the laboratory QC limits?			√		
Does the detectability data document the laboratorys capability to detect the COCs at the			V		
MDL used to calculate the SQLs?			'		
Was the LCSD RPD within QC limits?			√		
Matrix spike (MS) and matrix spike duplicate (MSD) data			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		
Were the project/method specified analytes included in the MS and MSD?			√		
Were MS/MSD analyzed at the appropriate frequency?			∨ ✓		
Were MS (and MSD, if applicable) %Rs within the laboratory QC limits?			√		
were wis (and wisb, if applicable) 70 ks within the laboratory QC inflits?			V		

Description	Yes	No	NA(1)	NR(2)	ER(3)
Were MS/MSD RPDs within laboratory QC limits?			√ _		4
Analytical duplicate data			0	009°	1733
Were appropriate analytical duplicates analyzed for each matrix?	√				
Were analytical duplicates analyzed at the appropriate frequency?	√				
Were RPDs or relative standard deviations within the laboratory QC limits?	√				
Method quantitation limits (MQLs):					
Are the MQLs for each method analyte included in the laboratory data package?			√		
Do the MQLs correspond to the concentration of the lowest non-zero calibration standard?			√		
Are unadjusted MQLs included in the laboratory data package?			√		
Other problems/anomalies					
Are all known problems/anomalies/special conditions noted in this LRC and ER?	√				
Were all necessary corrective actions performed for the reported data?	√				
Was applicable and available technology used to lower the SQL minimize the matrix			√		
interference affects on the sample results?					
Were response factors and/or relative response factors for each analyte within QC limits?			√		
Were percent RSDs or correlation coefficient criteria met?			√		
Was the number of standards recommended in the method used for all analytes?			√		
Were all points generated between the lowest and highest standard used to calculate the			√		
curve?					
Are ICAL data available for all instruments used?			√		
Has the initial calibration curve been verified using an appropriate second source standard?			√		
Initial and continuing calibration verification (ICV and CCV) and continuing					
calibration blank (CCB):					
Was the CCV analyzed at the method-required frequency?			√		
Were percent differences for each analyte within the method-required QC limits?			√		
Was the ICAL curve verified for each analyte?			√		
Was the absolute value of the analyte concentration in the inorganic CCB <mdl?< td=""><td></td><td></td><td>√</td><td></td><td></td></mdl?<>			√		
Mass spectral tuning:					
Was the appropriate compound for the method used for tuning?			√		
Were ion abundance data within the method-required QC limits?			√		
Internal standards (IS):					
Were IS area counts and retention times within the method-required QC limits?			√		
Raw data (NELAC section 1 appendix A glossary, and section 5.12 or ISO/IEC 17025					
section 4.12.2)					
Were the raw data (for example, chromatograms, spectral data) reviewed by an analyst?	√				
Were data associated with manual integrations flagged on the raw data?			√		
Dual column confirmation					
Did dual column confirmation results meet the method-required QC?			√		
Tentatively identified compounds (TICs):					
If TICs were requested, were the mass spectra and TIC data subject to appropriate checks?			√		
Interference Check Sample (ICS) results:					
Were percent recoveries within method QC limits?			√		
Serial dilutions, post digestion spikes, and method of standard additions					
Were percent differences, recoveries, and the linearity within the QC limits specified in the			√		
method?					
Method detection limit (MDL) studies					
Was a MDL study performed for each reported analyte?			√		
Is the MDL either adjusted or supported by the analysis of DCSs?			√		
Proficiency test reports:					
Was the laboratory's performance acceptable on the applicable proficiency tests or			√		
evaluation studies?					

Description	Yes	No	NA(1)	NR(2)	ER(3)
Standards documentation					4 – 0
Are all standards used in the analyses NIST-traceable or obtained from other appropriate			√ 0	0091	1734
sources?					
Compound/analyte identification procedures					
Are the procedures for compound/analyte identification documented?			√		
Demonstration of analyst competency (DOC)					
Was DOC conducted consistent with NELAC Chapter 5C or ISO/IEC 4?	√				
Is documentation of the analyst's competency up-to-date and on file?	√				
Verification/validation documentation for methods (NELAC Chap 5 or ISO/IEC					
17025 Section 5)					
Are all the methods used to generate the data documented, verified, and validated, where	√				
applicable?					
Laboratory standard operating procedures (SOPs):					
Are laboratory SOPs current and on file for each method performed?	√				

00091735

KEMRON Environmental Services

Laboratory Review Checklist

Laboratory Name: KEMRON
Laboratory Log Number: L0609004
Project Name: 798-LONGHORN
Method: PCTSOLIDS
Prep Batch Number(s): WG221779
Reviewer Name: DEANNA I. HESSON
LRC Date: September 12, 2006

EXCEPTIONS REPORT

ER# - Description

Footnotes:

- (1) NA = Not applicable to method or project
- (2) NR = Not reviewed
- (3) ER# = Exception report number

LABORATORY REPORT

L0609004

09/13/06 08:30

00091736

Submitted By

KEMRON Environmental Services 156 Starlite Drive Marietta, OH 45750 (740)373-4071

For

Account Name: Shaw E & I. Inc.
ABB Lummus Biulding

3010 Briarpark Houston, TX 77042

Attention: Diane Mever

Account Number: 2773

Work ID: LHAAP/TRANSIT LIVE/KARNACK.TX

P.O. Number: 200328

Sample Summary

Client ID	Lab ID	Date Collected	Date Received
29-WL-12	L0609004-01	31-AUG-06	01-SEP-06
32-WL-05	L0609004-02	31-AUG-06	01-SEP-06
29-SD-48	L0609004-03	31-AUG-06	01-SEP-06
29-SD-49	L0609004-04	31-AUG-06	01-SEP-06
29-SD-47	L0609004-05	31-AUG-06	01-SEP-06
29-SD-49-QC	L0609004-06	31-AUG-06	01-SEP-06

KEMRON FORMS - Modified 11/30/2005 Version 1.5 PDF File ID: 564135 Report generated 09/13/2006 08:30

1 OF 1

Report Number: L0609004

Report Date : September 13, 2006

00091737

Sample Number: L0609004-01 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 29-WL-12
 Prep Method: METHOD
 Prep Date: 09/07/2006 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006 19:30

 Workgroup Number: WG221826
 Analyst: JLS
 Run Date: 09/08/2006 18:26

Analyte	CAS. Numb	er	Result	Qual		PQL	SQL
1,3,5-Trinitrobenzene	99-35-4		0.554		0	.249	0.0995
1,3-Dinitrobenzene	99-65-0)	0.386		0	.249	0.0995
2,4,6-Trinitrotoluene	118-96-	7	25.6	I	0	.249	0.0995
2,4-Dinitrotoluene	121-14-	2	6.25		0	.249	0.0995
2,6-Dinitrotoluene	606-20-	2		U	0	.259	0.0995
2-Amino-4,6-dinitrotoluene	35572-78	-2		υ	0	.259	0.0995
2-Nitrotoluene	88-72-2	2		υ	0	.249	0.0995
3-Nitrotoluene	99-08-1			υ	0	.249	0.0995
4-Nitrotoluene	99-99-0)		υ	0	.249	0.0995
4-Amino-2,6-dinitrotoluene	19406-51	-0		υ	0	.259	0.0995
HMX	2691-41-	.0		U	1	2.19	0.0995
Nitrobenzene	98-95-3	3		υ	0	.259	0.129
RDX	121-82-	4		υ	0	.995	0.0995
Tetryl	479-45-	8		υ	0	.647	0.199
Surrogate	% Recovery	Lower	r Upj	per	Qual		1
3,4-Dinitrotoluene	93.6	50	1	50			

I Semiquantitative result (out of instrument calibration range)

Sample Number: L0609004-01 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 29-WL-12
 Prep Method: METHOD
 Prep Date: 09/07/2006 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006 19:30

 Cup Number: WG221826
 Analytical Method: TIS
 Pup Date: 09/11/2006 16:57

Workgroup Number: WG221826 Analyst: JLS Run Date: 09/11/2006 16:57
Collect Date: 08/31/2006 11:30 Dilution: 10 File ID: 4L009152.F

Sample Tag: <u>DL1</u> Units: <u>mg/kg</u> File 1D: <u>4L009152.F</u>

Analyte	CAS. Numb	er	Result	Qual		PQL	SQL
1,3,5-Trinitrobenzene	99-35-4			υ	1 2	2.49	0.995
1,3-Dinitrobenzene	99-65-0			υ	1	2.49	0.995
2,4,6-Trinitrotoluene	118-96-7	7	38.2		1 2	2.49	0.995
2,4-Dinitrotoluene	121-14-2	2	8.81		1	2.49	0.995
2,6-Dinitrotoluene	606-20-2	2		υ	1 2	2.59	0.995
2-Amino-4,6-dinitrotoluene	35572-78-	-2		U	1	2.59	0.995
2-Nitrotoluene	88-72-2			υ	1 2	2.49	0.995
3-Nitrotoluene	99-08-1			U	1	2.49	0.995
4-Nitrotoluene	99-99-0			U	1	2.49	0.995
4-Amino-2,6-dinitrotoluene	19406-51-	-0		υ	1	2.59	0.995
HMX	2691-41-	0		υ	1 2	21.9	0.995
Nitrobenzene	98-95-3			U	1	2.59	1.29
RDX	121-82-4	4			2	9.95	0.995
Tetryl	479-45-8	3		U	-	5.47	1.99
Surrogate	% Recovery	Lower	Upp	er	Qual		•
3,4-Dinitrotoluene	13.9	50	15	0	*		

^{*} Surrogate or spike compound out of range

U Not detected at or above adjusted sample detection limit

J Not detected at or above adjusted sample detection limit

Report Number: L0609004

Report Date : September 13, 2006

00091738

Sample Number: L0609004-01 PrePrep Method: NONE Instrument: OVEN

 Client ID: 29-WL-12
 Prep Method: D2216-90
 Prep Date: 09/08/2006 08:20

 Matrix: Soil
 Analytical Method: D2216-90
 Cal Date:

Workgroup Number: WG221779

Collect Date: 08/31/2006 11:30

Dilution: 1

Units: weight %

Run Date: 09/08/2006 08:20

File ID: 0V.0609080820-08

Analyte	CAS. Number	Result	Qual	PQL	SQL
Percent Solids	10-02-6	51.5		1.00	1.00

Sample Number: L0609004-02 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 32-WL-05
 Prep Method: METHOD
 Prep Date: 09/07/2006 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006 19:30

 Workgroup Number: WG221826
 Analyst: JLS
 Run Date: 09/08/2006 19:03

Collect Date: 08/31/2006 10:50 Dilution: 1 File ID: 4L009142.F

Sample Tag: 01 Units: mg/kg

Analyte	CAS. Numb	er	Result	Qual		PQL	SQL
1,3,5-Trinitrobenzene	99-35-4			υ	0	.245	0.0980
1,3-Dinitrobenzene	99-65-0			Ū	0	.245	0.0980
2,4,6-Trinitrotoluene	118-96-7	7		υ	0	.245	0.0980
2,4-Dinitrotoluene	121-14-2	2		υ	0	.245	0.0980
2,6-Dinitrotoluene	606-20-2	2		Ū	0	.255	0.0980
2-Amino-4,6-dinitrotoluene	35572-78-	-2	27.8	I	0	.255	0.0980
2-Nitrotoluene	88-72-2			Ū	0	.245	0.0980
3-Nitrotoluene	99-08-1			υ	0	.245	0.0980
4-Nitrotoluene	99-99-0			Ū	0	.245	0.0980
4-Amino-2,6-dinitrotoluene	19406-51-	-0		υ	0	.255	0.0980
HMX	2691-41-	0		Ū	1	2.16	0.0980
Nitrobenzene	98-95-3			υ	0	.255	0.127
RDX	121-82-4	4		υ	0	.980	0.0980
Tetryl	479-45-8	В		υ	0	.637	0.196
Surrogate	% Recovery	Lower	Upj	per	Qual		1
3,4-Dinitrotoluene	97.3	50	15	50			

I Semiquantitative result (out of instrument calibration range)

U Not detected at or above adjusted sample detection limit

Sample Number: L0609004-02 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 32-WL-05
 Prep Method: METHOD
 Prep Date: 09/07/2006
 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006
 19:30

 Workgroup Number: WG221826
 Analyst: JLS
 Run Date: 09/11/2006
 17:34

Collect Date: 08/31/2006 10:50 Dilution: 10 File ID: 4L009153.F
Sample Tag: DL1 Units: mg/kg

Analyte CAS. Number Result Qual PQL SQL 1,3,5-Trinitrobenzene 99-35-4 U 2.45 0.980 υ 1,3-Dinitrobenzene 99-65-0 2.45 0.980 2,4,6-Trinitrotoluene 118-96-7 U 2.45 0.980 2,4-Dinitrotoluene 121-14-2 U 2.45 0.980 2,6-Dinitrotoluene 606-20-2 U 2.55 0.980 2-Amino-4,6-dinitrotoluene 35572-78-2 72.4 2.55 0.980 88-72-2 2.45 0.980 2-Nitrotoluene U 99-08-1 2.45 0.980 3-Nitrotoluene U

2 of 6

Report Number: L0609004

Report Date : September 13, 2006

00091739

Sample Number: L0609004-02 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 32-WL-05
 Prep Method: METHOD
 Prep Date: 09/07/2006
 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006
 19:30

 Workgroup Number: WG221826
 Analyst: JLS
 Run Date: 09/11/2006
 17:34

CAS. Number Result Analyte Qual PQL SQL 4-Nitrotoluene 99-99-0 U 2.45 0.980 19406-51-0 0.980 4-Amino-2,6-dinitrotoluene U 2.55 HMX 2691-41-0 U 21.6 0.980 1.27 Nitrobenzene 98-95-3 2.55 U 121-82-4 9.80 RDX TT 0.980 479-45-8 6.37 1.96 Tetryl TT % Recovery Surrogate Upper Qual 3,4-Dinitrotoluene 11.4

U Not detected at or above adjusted sample detection limit

Sample Number: 10609004-02 PrePrep Method: NONE Instrument: OVEN

 Client ID: 32-WL-05
 Prep Method: D2216-90
 Prep Date: 09/08/2006 08:20

 Matrix: Soil
 Analytical Method: D2216-90
 Cal Date:

 Workgroup Number: WG221779
 Analyst: TMM
 Run Date: 09/08/2006 08:20

Collect Date: 08/31/2006 10:50

Dilution: 1

Units: weight %

 Analyte
 CAS. Number
 Result
 Qual
 PQL
 SQL

 Percent Solids
 10-02-6
 80.9
 1.00
 1.00

 Sample Number: L0609004-03
 PrePrep Method: NONE
 Instrument: HPLC4

 Client ID: 29-SD-48
 Prep Method: METHOD
 Prep Date: 09/07/2006 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006 19:30

Workgroup Number: WG221826 Analyst: JLS Run Date: 09/08/2006 19:40
Collect Date: 08/31/2006 09:15
Sample Tag: 01 Units: mg/kg

Analyte CAS. Number Result Qual PQL SQL 99-35-4 1,3,5-Trinitrobenzene 0.239 0.0957 U 0.0957 1,3-Dinitrobenzene 99-65-0 TT 0.239 118-96-7 TT 0.239 0.0957 2,4,6-Trinitrotoluene 121-14-2 0.239 0.0957 2,4-Dinitrotoluene U 2,6-Dinitrotoluene 606-20-2 U 0.249 0.0957 2-Amino-4,6-dinitrotoluene 35572-78-2 U 0.249 0.0957 2-Nitrotoluene 88-72-2 U 0.239 0.0957 3-Nitrotoluene 99-08-1 U 0.239 0.0957 4-Nitrotoluene 99-99-0 4.88 0.239 0.0957 4-Amino-2,6-dinitrotoluene 19406-51-0 U 0.249 0.0957 HMX 2691-41-0 J 2.11 0.0957 Nitrobenzene 98-95-3 υ 0.249 0.124 121-82-4 υ 0.957 0.0957 RDX Tetryl 479-45-8 υ 0.622 0.191

3 of 6

^{*} Surrogate or spike compound out of range

Report Number: L0609004

Report Date : September 13, 2006

00091740

Sample Number: L0609004-03

Client ID: 29-SD-48 Matrix:**Soil**

Workgroup Number: WG221826 Collect Date: 08/31/2006 09:15

Sample Tag: 01

PrePrep Method: NONE

Prep Method: METHOD Prep Date: 09/07/2006 08:00 Analytical Method: 8330

Analyst:**JLS**

Dilution: 1 Units:mg/kg

____ Instrument:<u>HPLC4</u>

Cal Date: 08/10/2006 19:30 Run Date: 09/08/2006 19:40

File ID: 4L009143.F

Surrogate	% Recovery	Lower	Upper	Qual
3,4-Dinitrotoluene	105	50	150	

J The analyte was positively identified, but the quantitation was below the RL

U Not detected at or above adjusted sample detection limit

Sample Number: L0609004-03

Client ID:29-SD-48 Matrix:**Soil**

Workgroup Number: WG221779

Collect Date: 08/31/2006 09:15

PrePrep Method: NONE

Analytical Method: D2216-90

Analyst: TMM Dilution: 1

Units:weight %

____ Instrument: OVEN

Prep Method: D2216-90 Prep Date: 09/08/2006 08:20

Cal Date:_

Run Date: 09/08/2006 08:20

File ID: OV. 0609080820-10

Analyte	CAS. Number	Result	Qual	PQL	SQL
Percent Solids	10-02-6	75.3		1.00	1.00

____ Instrument: HPLC4 Sample Number: **L0609004-04** PrePrep Method: NONE

Client ID: 29-SD-49

Matrix: Soil

Workgroup Number: WG221826 Collect Date: 08/31/2006 09:30

Sample Tag:01

Prep Method: METHOD Analytical Method: 8330 Analyst:**JLS**

Dilution: 1 Units:mg/kg

Prep Date: 09/07/2006 08:00 Cal Date: 08/10/2006 19:30

Run Date: 09/08/2006 20:17

File ID: 4L009144.F

Analyte	CAS. Numbe	er I	Result	Qual	PQL	SQL
1,3,5-Trinitrobenzene	99-35-4			U	0.246	0.0985
1,3-Dinitrobenzene	99-65-0			υ	0.246	0.0985
2,4,6-Trinitrotoluene	118-96-7	'		U	0.246	0.0985
2,4-Dinitrotoluene	121-14-2	1		U	0.246	0.0985
2,6-Dinitrotoluene	606-20-2	1		U	0.256	0.0985
2-Amino-4,6-dinitrotoluene	35572-78-	2		U	0.256	0.0985
2-Nitrotoluene	88-72-2			υ	0.246	0.0985
3-Nitrotoluene	99-08-1			U	0.246	0.0985
4-Nitrotoluene	99-99-0			υ	0.246	0.0985
4-Amino-2,6-dinitrotoluene	19406-51-	0		U	0.256	0.0985
нмх	2691-41-)		υ	2.17	0.0985
Nitrobenzene	98-95-3			υ	0.256	0.128
RDX	121-82-4				0.985	0.0985
Tetryl	479-45-8	1			0.640	0.197
Surrogate	% Recovery	Lower	Upp	er	Qual	
3,4-Dinitrotoluene	96.3	50	15	0		

U Not detected at or above adjusted sample detection limit

ο£ 6

Report Number: L0609004

Report Date : September 13, 2006

00091741

Sample Number: L0609004-04 PrePrep Method: NONE Instrument: OVEN

Workgroup Number: WG221779 Analyst: TMM Run Date: 09/08/2006 08:20
Collect Date: 08/31/2006 09:30 Dilution: 1 File ID: 0V.0609080820-11

Units: weight %

Analyte	CAS. Number	Result	Qual	PQL	SQL
Percent Solids	10-02-6	79.1		1.00	1.00

Sample Number: L0609004-05 PrePrep Method: NONE Instrument: HPLC4

 Client ID: 29-SD-47
 Prep Method: METHOD
 Prep Date: 09/07/2006 08:00

 Matrix: Soil
 Analytical Method: 8330
 Cal Date: 08/10/2006 19:30

 Workgroup Number: WG221826
 Analyst: JLS
 Run Date: 09/08/2006 20:55

Collect Date: 08/31/2006 09:00 Dilution: 1 File ID: 4L009145.F

| Dilution: 1 | File 1D: 4E009145.F

Analyte	CAS. Numb	er	Result	Qual		PQL	SQL
1,3,5-Trinitrobenzene	99-35-4			υ	(0.249	0.0995
1,3-Dinitrobenzene	99-65-0			U	(0.249	0.0995
2,4,6-Trinitrotoluene	118-96-7	7		U	(0.249	0.0995
2,4-Dinitrotoluene	121-14-2	2		U	(0.249	0.0995
2,6-Dinitrotoluene	606-20-2	2		U	(0.259	0.0995
2-Amino-4,6-dinitrotoluene	35572-78-	-2		U	(0.259	0.0995
2-Nitrotoluene	88-72-2			U	(0.249	0.0995
3-Nitrotoluene	99-08-1			U	(0.249	0.0995
4-Nitrotoluene	99-99-0			U	(0.249	0.0995
4-Amino-2,6-dinitrotoluene	19406-51-	-0		U	(0.259	0.0995
HMX	2691-41-	0		U		2.19	0.0995
Nitrobenzene	98-95-3			U	(0.259	0.129
RDX	121-82-4	4		U	(0.995	0.0995
Tetryl	479-45-8	В		U	(0.647	0.199
Surrogate	% Recovery	Lowe	er	Upper	Qual		•
3,4-Dinitrotoluene	97.8	50		150		1	

U Not detected at or above adjusted sample detection limit

Sample Number: L0609004-05 PrePrep Method: NONE Instrument: OVEN

Workgroup Number: WG221779 Analyst: TMM Run Date: 09/08/2006 08:20

Collect Date: 08/31/2006 09:00 Dilution: 1 File ID: 0V.0609080820-12 Units: weight %

 Analyte
 CAS. Number
 Result
 Qual
 PQL
 SQL

 Percent Solids
 10-02-6
 78.7
 1.00
 1.00

5 of 6

Report Number: L0609004

3,4-Dinitrotoluene

Report Date : September 13, 2006

00091742

Sample Number: L0609004-06 PrePrep Method: NONE Instrument: HPLC4

Prep Date: 09/07/2006 08:00 Client ID: 29-SD-49-QC Prep Method: METHOD Matrix: Soil Analytical Method:8330 Cal Date: 08/10/2006 19:30 Workgroup Number: WG221826 Analyst:**JLS** Run Date: 09/08/2006 21:32

Collect Date: 08/31/2006 09:30 Dilution: 1 File ID:4L009146.F Sample Tag:01 Units:mg/kg

CAS. Number Result SQL Analyte Qual PQL 1,3,5-Trinitrobenzene 99-35-4 U 0.242 0.0966 0.242 0.0966 1,3-Dinitrobenzene 99-65-0 U 0.242 0.0966 2,4,6-Trinitrotoluene 118-96-7 U 121-14-2 0.242 0.0966 2,4-Dinitrotoluene U 606-20-2 0.251 0.0966 2,6-Dinitrotoluene TT 35572-78-2 2-Amino-4,6-dinitrotoluene 0.251 0.0966 TT 2-Nitrotoluene 88-72-2 U 0.242 0.0966 3-Nitrotoluene 99-08-1 U 0.242 0.0966 4-Nitrotoluene 99-99-0 U 0.242 0.0966 4-Amino-2,6-dinitrotoluene 19406-51-0 U 0.251 0.0966 2691-41-0 0.880 2.13 0.0966 J Nitrobenzene 98-95-3 υ 0.251 0.126 RDX 121-82-4 U 0.966 0.0966 Tetryl 479-45-8 U 0.628 0.193 Surrogate % Recovery Qual

U Not detected at or above adjusted sample detection limit

Sample Number: L0609004-06 PrePrep Method:NONE Instrument: OVEN

95.1

Client ID: 29-SD-49-QC Prep Method: D2216-90 Prep Date: 09/08/2006 08:20 Matrix:**Soil** Analytical Method: D2216-90 Cal Date:

Lower

50

Upper

150

Workgroup Number: WG221779 Analyst: TMM Run Date: 09/08/2006 08:20 Collect Date: 08/31/2006 09:30 Dilution:1 File ID:0V.0609080820-13 Units: weight %

Analyte CAS. Number Result Qual PQL SQL Percent Solids 10-02-6 79.6 1.00 1.00

> ο£ 6

The analyte was positively identified, but the quantitation was below the RL

WORKGROUP SUMMARY BY METHOD

WORKGROUP SUMMARY BY METHOD

00091744

Analysis: Explosives

Extraction Method:METHOD

Workgroup:WG221670

Lab ID	Client ID	Tclp Date	Prep Date	Analysis Date	Tag	Inst Id	Analyst
L0609004-01	29-WL-12		09/07/06 08:00			SONICATION	CEB
L0609004-02	32-WL-05		09/07/06 08:00			SONICATION	CEB
L0609004-03	29-SD-48		09/07/06 08:00			SONICATION	CEB
L0609004-04	29-SD-49		09/07/06 08:00			SONICATION	CEB
L0609004-05	29-SD-47		09/07/06 08:00			SONICATION	CEB
L0609004-06	29-SD-49-QC		09/07/06 08:00			SONICATION	CEB

Analysis:Percent Solids

Analytical Method: D2216-90

Workgroup:WG221779

Lab ID	Client ID	Tclp Date	Prep Date	Analysis Date	Tag	Inst Id	Analyst
L0609004-01	29-WL-12			09/08/06 08:20		OVEN	TMM
L0609004-02	32-WL-05			09/08/06 08:20		OVEN	TMM
L0609004-03	29-SD-48			09/08/06 08:20		OVEN	TMM
L0609004-04	29-SD-49			09/08/06 08:20		OVEN	TMM
L0609004-05	29-SD-47			09/08/06 08:20		OVEN	TMM
L0609004-06	29-SD-49-QC			09/08/06 08:20		OVEN	TMM

Analysis:Explosives

Analytical Method:8330

Workgroup:WG221826

Lab ID	Client ID	Tclp Date	Prep Date	Analysis Date	Tag	Inst Id	Analyst
L0609004-01	29-WL-12		09/07/06 08:00	09/08/06 18:26	01	HPLC4	JLS
L0609004-01	29-WL-12		09/07/06 08:00	09/11/06 16:57	DL1	HPLC4	JLS
L0609004-02	32-WL-05		09/07/06 08:00	09/08/06 19:03	01	HPLC4	JLS
L0609004-02	32-WL-05		09/07/06 08:00	09/11/06 17:34	DL1	HPLC4	JLS
L0609004-03	29-SD-48		09/07/06 08:00	09/08/06 19:40	01	HPLC4	JLS
L0609004-04	29-SD-49		09/07/06 08:00	09/08/06 20:17	01	HPLC4	JLS
L0609004-05	29-SD-47		09/07/06 08:00	09/08/06 20:55	01	HPLC4	JLS
L0609004-06	29-SD-49-QC		09/07/06 08:00	09/08/06 21:32	01	HPLC4	JLS

Kemron Environmental Services Analyst Listing September 13, 2006

ARA - ADRIAN R. ACHTERMANN CAF - CHERYL A. FLOWERS CAK - CHERYL A. KOELSCH CEB - CHAD E. BARNES CEB - CHAD F. BOOK CLC - CHRYS L. CRAWFORD CLS - CARA L. STRICKLER CLW - CHARISSA L. WINTERS CPD - CHAD P. DAVIS CPC - CARLA R. COCHRAN CSA - LUCINDA S. ARNOLD CSH - CHRIS S. HILL DAS - DALLAS A. SULLIVAN DD - DIANE M. DENNIS DDE - DEBRA D. ELLIOTT DEL - DON E. LIGHTFRITZ DEV - DAVID E. VANDENBERG DGB - DOUGLAS G. BUTCHER DLP - DOROTHY L. PAYNE DLP - DOROTHY L. PAYNE DRF - DAVE R. PITZER DSM - DAVID S. MOSSOR DST - DENNIS S. TEPE ECL - ERIC C. LAWSON ED - EMILY E. DECKER HAV - HEMA VILASAGAR JAL - JOHN A. LENT JUS - JANICE L. SCHIMMEL JWR - JOHN W. RICHARDS JWS - JACK W. SHEAVES KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MAREN M. BEERY MSW - MATI S. WILSON MDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SKM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER VAR - WALTER F. MARTIN	AJF - AMANDA J. FICKIESEN	ALB - ANNIE L. BOCK	ALT - ANN L. THAYER
CFB - CHAD F. BOOK CLC - CHRYS L. CRAWFORD CLS - CARA L. STRICKLER CLW - CHARISSA L. WINTERS CM - CHARLIE MARTIN CMS - CRYSTAL M. STEPHENS CPD - CHAD P. DAVIS CRC - CARLA R. COCHRAN CSA - LUCINDA S. ARNOLD CSH - CHRIS S. HILL DAS - DALLAS A. SULLIVAN DD - DIANE M. DENNIS DDE - DEBRA D. ELLIOTT DEL - DON E. LIGHTFRITZ DEV - DAVID E. VANDENBERG DGB - DOUGLAS G. BUTCHER DIH - DEANNA I. HESSON DLB - DAVID L. BUMGARNER DLP - DOROTHY L. PAYNE DLR - DIANNA L. RAUCH DR - DEANNA ROBERTS DRP - DAVE R. PITZER DSM - DAVID S. MOSSOR DST - DENNIS S. TEPE ECL - ERIC C. LAWSON ED - EMILY E. DECKER FJB - FRANCES J. BOLDEN HAV - HEMA VILASAGAR JAL - JOHN A. LENT JKT - JANE K. THOMPSON JLS - JANICE L. SCHIMMEL JNB - JOSHUA N. BOOTH JS - JENNIFER L. SOUTHALL JWR - JOHN W. RICHARDS JWS - JACK W. SHEAVES KRA - KATHY R. ALBERTSON KEB - KATHRYN E. BARNES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MES - MARY E. SCHILLING MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON MJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	ARA - ADRIAN R. ACHTERMANN	BRG - BRENDA R. GREGORY	CAA - CASSIE A. AUGENSTEIN
CLW - CHARISSA L. WINTERS	CAF - CHERYL A. FLOWERS	CAK - CHERYL A. KOELSCH	CEB - CHAD E. BARNES
CPD - CHAD P. DAVIS CRC - CARLA R. COCHRAN CSA - LUCINDA S. ARNOLD CSH - CHRIS S. HILL DAS - DALLAS A. SULLIVAN DD - DIANE M. DENNIS DDE - DEBRA D. ELLIOTT DEL - DON E. LIGHTFRITZ DEV - DAVID E. VANDENBERG DGB - DOUGLAS G. BUTCHER DIH - DEANNA I. HESSON DLB - DAVID L. BUMGARNER DLP - DOROTHY L. PAYNE DLR - DIANNA L. RAUCH DR - DEANNA ROBERTS DRP - DAVE R. PITZER DSM - DAVID S. MOSSOR DST - DENNIS S. TEPE ECL - ERIC C. LAWSON ED - EMILY E. DECKER HAV - HEMA VILASAGAR JAL - JOHN A. LENT JKT - JANE K. THOMPSON JLS - JANICE L. SCHIMMEL JWB - JOHN W. RICHARDS KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MKZ - MARILYN K. ZUMBRO MKR - MARY L. ROCHOTTE MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	CFB - CHAD F. BOOK	CLC - CHRYS L. CRAWFORD	CLS - CARA L. STRICKLER
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HAV - HEMA VILASAGAR JAL - JOHN A. LENT JKT - JANE K. THOMPSON JLS - JANICE L. SCHIMMEL JWR - JOHN W. RICHARDS KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KHR - KIM H. RHODES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MMS - MAREN M. BEERY MSW - MATT S. WILSON MDB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP RKK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	DRP - DAVE R. PITZER	DSM - DAVID S. MOSSOR	DST - DENNIS S. TEPE
JLS - JANICE L. SCHIMMEL JWR - JOHN W. RICHARDS JWS - JACK W. SHEAVES JYH - JI Y. HU KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MDA - MIKE D. ALBERTSON MC - MICHAEL D. COCHRAN MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	ECL - ERIC C. LAWSON	ED - EMILY E. DECKER	FJB - FRANCES J. BOLDEN
JWR - JOHN W. RICHARDS KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KHR - KIM H. RHODES KRA - KATHY R. ALBERTSON MCC - MICHAEL D. COCHRAN MES - MARY E. SCHILLING MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE TMM - TAMMY M. MORRIS VC - VICKI COLLIER	HAV - HEMA VILASAGAR	JAL - JOHN A. LENT	JKT - JANE K. THOMPSON
KCZ - KEVIN C. ZUMBRO KEB - KATHRYN E. BARNES KHR - KIM H. RHODES KRA - KATHY R. ALBERTSON MDC - MICHAEL D. COCHRAN MES - MARY E. SCHILLING MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE TMM - TAMMY M. MORRIS VC - VICKI COLLIER	JLS - JANICE L. SCHIMMEL	JNB - JOSHUA N. BOOTH	JS - JENNIFER L. SOUTHALL
KRA - KATHY R. ALBERTSON MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MES - MARY E. SCHILLING MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	JWR - JOHN W. RICHARDS	JWS - JACK W. SHEAVES	JYH - JI Y. HU
MDA - MIKE D. ALBERTSON MDC - MICHAEL D. COCHRAN MES - MARY E. SCHILLING MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	KCZ - KEVIN C. ZUMBRO	KEB - KATHRYN E. BARNES	KHR - KIM H. RHODES
MKZ - MARILYN K. ZUMBRO MLR - MARY L. ROCHOTTE MLS - MICHAEL L. SCHIMMEL MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	KRA - KATHY R. ALBERTSON	LKN - LINDA K. NEDEFF	LSB - LESLIE S. BUCINA
MMB - MAREN M. BEERY MSW - MATT S. WILSON NJB - NATALIE J. BOOTH PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	MDA - MIKE D. ALBERTSON	MDC - MICHAEL D. COCHRAN	MES - MARY E. SCHILLING
PAS - PATRICK A. STREET PJM - PAUL J. MILLER RB - ROBERT BUCHANAN RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	MKZ - MARILYN K. ZUMBRO	MLR - MARY L. ROCHOTTE	MLS - MICHAEL L. SCHIMMEL
RDC - REBECCA D. CUTLIP REK - ROBERT E. KYER RNP - RICK N. PETTY RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	MMB - MAREN M. BEERY	MSW - MATT S. WILSON	NJB - NATALIE J. BOOTH
RWC - RODNEY W. CAMPBELL SCM - SUSAN C. MOELLENDICK SLM - STEPHANIE L. MOSSBURG SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	PAS - PATRICK A. STREET	PJM - PAUL J. MILLER	RB - ROBERT BUCHANAN
SLP - SHERI L. PFALZGRAF SMH - SHAUNA M. HYDE SRM - SAMUEL R. MCFEE TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	RDC - REBECCA D. CUTLIP	REK - ROBERT E. KYER	RNP - RICK N. PETTY
TMB - TIFFANY M. BAILEY TMM - TAMMY M. MORRIS VC - VICKI COLLIER	RWC - RODNEY W. CAMPBELL	SCM - SUSAN C. MOELLENDICK	SLM - STEPHANIE L. MOSSBURG
	SLP - SHERI L. PFALZGRAF	SMH - SHAUNA M. HYDE	SRM - SAMUEL R. MCFEE
WFM - WALTER F. MARTIN	TMB - TIFFANY M. BAILEY	TMM - TAMMY M. MORRIS	VC - VICKI COLLIER
W W	WFM - WALTER F. MARTIN		

List of Valid Qualifiers September 13, 2006

Qualkey: STD 00091746

Qualifier	Description
*	Surrogate or spike compound out of range
+	Correlation coefficient for the MSA is less than 0.995
<	Result is less than the associated numerical value.
>	Result is greater than the associated numerical value.
A	See the report narrative
В	Analyte present in method blank
С	Confirmed by GC/MS
CG	Confluent growth
DL	Surrogate or spike compound was diluted out
E	Estimated concentration due to sample matrix interference
EDL	Elevated sample reporting limits, presence of non-target analytes
EMPC	Estimated Maximum Possible Concentration
FL	Free Liquid
1	Semiquantitative result (out of instrument calibration range)
J	The analyte was positively identified, but the quantitation was below the RL
J,B	Analyte detected in both the method blank and sample above the MDL.
J,P	ESTÍMATE & COLUMNS DON'T AGREE TO WITHIN 40%
Ĺ	Sample reporting limits elevated due to matrix interference
M	Matrix effect; the concentration is an estimate due to matrix effect.
N	Tentatively identified compound(TIC)
NA	Not applicable
ND	Not detected at or above the reporting limit
NF	Not found by library search
NFL	No free liquid
NI	Non-ignitable
NR	Analyte is not required to be analyzed
NS	Not spiked
Р	Concentrations >40% difference between the two GC columns
Q	One or more quality control criteria fail. See narrative.
QNS	Quantity of sample not sufficient to perform analysis
RA	Reanalysis confirms reported results
RE	Reanalysis confirms sample matrix interference
S	Analyzed by method of standard addition
SMI	Sample matrix interference on surrogate
SP	Reported results are for spike compounds only
TIC	Library Search Compound
TNTC	Too numerous to count
U	Undetected; the concentration is below the reported MDL.
UJ	Undetected; the MDL and RL are estimated due to quality control discrepancies.
W	Post-digestion spike for furnace AA out of control limits
X	Exceeds regulatory limit
Z	Cannot be resolved from isomer - see below

- ***Special Notes for Organic Analytes

 1. Acrolein and acrylonitrile by method 624 are semi-quantitative screens only.

 2. 1,2-Diphenylhydrazine is unstable and is reported as azobenzene.

- N-nitrosodiphenylamine cannot be separated from diphenylamine.
 3-Methylphenol and 4-Methylphenol are unresolvable compounds.
 m-Xylene and p-Xylene are unresolvable compounds.
 The reporting limits for Appendix II/IX compounds by method 8270 are based on EPA estimated PQLs referenced in 40 CFR Part 264, Appendix IX. They are not always achievable for every compound an are matrix dependent.

Organic QA/QC

KEMRON Environmental Services Data Checklist

00091748

Date:	10-AUG-2006
Analyst:	JLS
Analyst:	NA
Method:	8330
Instrument:	HPLC4
Curve Workgroup:	NA
Runlog ID:	11718
Analytical Workgroups:	L0607001,002 QMDL'S L0607333 DUE 8/1/06

Initial Calibration	X
Average RF	X
Linear Reg or Higher Order Curve	X
Second Source standard % Difference	X
Continuing Calibration /Check Standards	X
Project/Client Specific Requirements	X
Special Standards	NA NA
Blanks	X
TCL's	X
Surrogates	X
LCS (Laboratory Control Sample)	X
Recoveries	X
Surrogates	X
MS/MSD/Duplicates	Х
Samples	X
TCL Hits	X
Confirmations	Х
Surrogates	Х
Calculations & Correct Factors	Х
Dilutions Run	NA
Reruns	NA
Manual Integrations	Х
Integrations digitally signed	Х
Case Narrative	NA
KEMRON .pdf forms	X
Results Reporting/Data Qualifiers	X
KOBRA Workgroup Data	X
Check for Completeness	X
Primary Reviewer	JLS
Secondary Reviewer	MDC
Check for compliance with method and project specific requirements	X
Check the completeness of reported information	X
Check the information for the report narrative	NA
Check the resonableness of the results	X
Comments	

Primary Reviewer: 14-AUG-2006 Janier Schimmel Michel Coder

Secondary Reviewer: 14-AUG-2006

Generated: AUG-14-2006 13:02:33

KEMRON Environmental Services Data Checklist

00091749

Date:	08-SEP-2006
Analyst:	JLS
Analyst:	NA
Method:	8330
Instrument:	HPLC4
Curve Workgroup:	NA
Runlog ID:	12176
Analytical Workgroups:	L0608643 DUE 9/8, L0609004 DUE 9/12 F3

Initial Calibration	X
Average RF	X
Linear Reg or Higher Order Curve	X
Second Source standard % Difference	X
Continuing Calibration /Check Standards	X
Project/Client Specific Requirements	Х
Special Standards	NA NA
Blanks	X
TCL's	X
Surrogates	X
LCS (Laboratory Control Sample)	X
Recoveries	X
Surrogates	X
MS/MSD/Duplicates	X
Samples	X
TCL Hits	X
Confirmations	X
Surrogates	X
Calculations & Correct Factors	X
Dilutions Run	X
Reruns	X
Manual Integrations	X
Integrations digitally signed	X
Case Narrative	NA
KEMRON .pdf forms	X
Results Reporting/Data Qualifiers	X
KOBRA Workgroup Data	X
Check for Completeness	X
Primary Reviewer	JLS
Secondary Reviewer	MDC
Check for compliance with method and project specific requirements	X
Check the completeness of reported information	X
Check the information for the report narrative	NA
Check the resonableness of the results	X
Comments	

Primary Reviewer: 11-SEP-2006 Janies Schimmel Michel Coder

Secondary Reviewer: 11-SEP-2006

Generated: SEP-11-2006 13:00:21

KEMRON Environmental Services Data Checklist

00091750

Date: <u>11-SEP-2006</u>	
Analyst: <u>JLS</u>	
Analyst: NA	
Method: <u>8330</u>	
Instrument: HPLC4	
Curve Workgroup: NA	
Runlog ID: <u>12216</u>	
Analytical Workgroups: L0609004 DHE 9/12 F3	

Initial Calibration	X
Average RF	X
Linear Reg or Higher Order Curve	X
Second Source standard % Difference	X
Continuing Calibration /Check Standards	X
Project/Client Specific Requirements	X
Special Standards	NA
Blanks	X
TCL's	X
Surrogates	X
LCS (Laboratory Control Sample)	X
Recoveries	X
Surrogates	X
MS/MSD/Duplicates	X
Samples	X
TCL Hits	X
Confirmations	X
Surrogates	X
Calculations & Correct Factors	X
Dilutions Run	NA
Reruns	NA
Manual Integrations	X
Integrations digitally signed	X
Case Narrative	NA
KEMRON .pdf forms	X
Results Reporting/Data Qualifiers	X
KOBRA Workgroup Data	X
Check for Completeness	X
Primary Reviewer	JLS
Secondary Reviewer	MDC
Check for compliance with method and project specific requirements	X
Check the completeness of reported information	X
Check the information for the report narrative	NA
Check the resonableness of the results	X
Comments	

Janies Schimmel Michel Coder

Primary Reviewer: Secondary Reviewer: 12-SEP-2006 12-SEP-2006

Generated: SEP-12-2006 15:55:36

Instrument Run Log

00091751

Instrument:	HPLC4	Dataset:	081006			
Analyst1:	JLS	Analyst2:	NA			
Method:	8330	SOP: HPLC02			Rev: 8	
Maintenance Log ID:	15141					
			Caluma 0 ID.	NIA		
	Column 1 ID: ULTRACARB 5	ODS	Column 2 ID:	NA		
Workgroups: WG219024, WG	217741					
Interr	nal Standard: NA	Su	rrogate Standard:	STD13480		
Comments:						

Seq.	File ID	Sample Information	Mat	Dil	Reference	Date/Time
1	4L008947.F	WG219506-01 STD6	1	1		08/10/06 16:24
2	4L008948.F	WG219506-02 STD5	1	1		08/10/06 17:01
3	4L008949.F	WG219506-03 STD4	1	1		08/10/06 17:38
4	4L008950.F	WG219506-04 STD3	1	1		08/10/06 18:16
5	4L008951.F	WG219506-05 STD2	1	1		08/10/06 18:53
6	4L008952.F	WG219506-06 STD1	1	1		08/10/06 19:30
7	4L008953.F	WG219506-07 ALT	1	1		08/10/06 20:07
8	4L008954.F	WG218108-01 BLK	1	1		08/10/06 20:44
22	4L008955.F	WG218108-02 LCS	1	1		08/10/06 21:22
23	4L008956.F	WG218108-03 LCS2	1	1		08/10/06 21:59
11	4L008957.F	L0607001-01	1	1		08/10/06 22:36
12	4L008958.F	L0607002-01	1	1		08/10/06 23:13
13	4L008959.F	L0607333-01	1	1		08/10/06 23:50
14	4L008960.F	L0607333-02	1	1		08/11/06 00:28
24	4L008961.F	WG216614-01 BLK	7	1		08/11/06 01:05
25	4L008962.F	WG216614-02 LCS	7	1		08/11/06 01:42
17	4L008963.F	WG216614-02 LCS	7	1		08/11/06 02:19
18	4L008964.F	WG219523-01 CCV	1	1		08/11/06 02:56
19	4L008965.F	L0607003-01	7	1		08/11/06 03:34
20	4L008966.F	L0607004-01	7	1		08/11/06 04:11
21	4L008967.F	WG219523-02 CCV	1	1		08/11/06 04:48

Comments

Seq.	Rerun	Dil.	Reason	Analytes
11	Х			
	To confi	rm the blo	b at the end of the run.	

Page: 1 of 1 Approved: 14-AUG-06 Michael

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Instrument Run Log

00091752

							0009173
	Instrument:	HPLC4	Dataset:	090806			
	Analyst1:	JLS	Analyst2:	NA			
	Method:	8330	SOP:	HPLC02		Rev: <u>8</u>	_
	Maintenance Log ID:	15564					
Worko	roups: <u>WG221826/WG2</u>	Column 1 ID: <u>ULTRACARB 5</u>	ODS	Column 2	ID: NA		
Internal	STD: NA	Surrogate STD:	SID145	513	Cal	bration STD	
	Comments:						
Seq.	File ID	Sample Info	rmation	Ma	at Dil	Reference	Date/Time
1	4L009134.F	WG221825-01 CCV		1	1		09/08/06 13:57
2	4L009135.F	L0608643-09 MS		7	1		09/08/06 14:43
3	4L009136.F	L0608643-10 MSD		7	1		09/08/06 15:20
4	4L009137.F	WG221825-02 CCV		1	1		09/08/06 15:57
5	4L009138.F	WG221670-01 BLK		7	1		09/08/06 16:34
6	4L009139.F	WG221670-02 LCS		7	1		09/08/06 17:11
14	4L009140.F	WG221670-03 LCS2		7	1		09/08/06 17:49
7	4L009141.F	L0609004-01		7	1		09/08/06 18:26
8	4L009142.F	L0609004-02		7	1		09/08/06 19:03
9	4L009143.F	L0609004-03		7	1		09/08/06 19:40
10	4L009144.F	L0609004-04		7	1		09/08/06 20:17
11	4L009145.F	L0609004-05		7	1		09/08/06 20:55
12	4L009146.F	L0609004-06		7	1		09/08/06 21:32
13	4L009147.F	WG221825-03 CCV		1	1		09/08/06 22:09

Comments

Seq.	Rerun	Dil.	Reason	Analytes
6	Х			
7	X	10	Over Calibration Range	2,4,6-Trinitrotoluene
8	X	10	Over Calibration Range	4-amino-4,6-dinitrotoluene
			1	

Page: 1 of 1 Approved:

Run Log ID: 12216

KEMRON Environmental Services

Instrument Run Log

00091753

	Instrumer	nt: <u>HPLC4</u> Da	taset: 091106		_	
	Analyst	1: <u>JLS</u> Ana	alyst2: NA		_	
	Method	d: <u>8330</u>	SOP: HPLC02		Rev: 8	_
	Maintenance Log II					_
Work	groups: WG221826	Column 1 ID: <u>ULTRACARB 5 ODS</u>	Column 2 ID:	NA		
Interna		Surrogate STD: S	TD14513	Calibra	ition STD	
	Comments:					
Seq.	File ID	Sample Information	Mat	Dil	Reference	Date/Time
1	4L009150.F	WG221972-01 CCV	1	1		09/11/06 15:40
2	4L009151.F	WG221670-02 LCS	7	1		09/11/06 16:20
3	4L009152.F	L0609004-01 10X	7	10		09/11/06 16:57
4	4 4L009153.F L0609004-02 10X		7	10		09/11/06 17:34
5	5 4L009154.F WG221972-02 CCV		1	1		09/11/06 18:11
		<u>C</u> c	omments			
Seq.	Rerun Dil.	Reason			Analytes	

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Document Control No.: EE0006 rage: 32 of 50

Sample Extraction Log Sheet – Method 8330 / Explosives

Analyst:	EB			Extract Relinquished By:
•	7-00 00	හිර		Extract Received By:
SOP#:	EXTATZ	REV 6		Date Extract Received: 4-8-06
Spike Analyst:	CEB	Witness	s: <u>Ed</u>	_
Sample Matrix:	SOIL			Matrix Spike # / Conc: STD 14512 Q
Ext Solvent:	CHOCN	_ Lot#:	co4825	Surrogate Spike # / Conc: 57014513 (
Ext Solvent:		_ Lot#:		- 1.10 - 2011-70
Ext Disk:	_	Lot#:	-	Extraction Work Group: W622167
Other:	caci	Lot#:	EX0017-92	Analytical Work Group:

RNG	18847
Sonic Bath On – D	Pate: 69-07-06
Time (1) 1300	Temp (1) Ctrl 3,5
	Bath 18°C
Time (2) 1500	Temp (2) Ctrol 3.5°c
	Bath 12°C
Sonic Bath Off – I	Date: 09-08-06
Time (3) 720	Temp (3) Ctrl 3.50
	Bath 12°C

	Project ID	Sample ID	Sample Wt (g) / Vol (mL)	Surrogate Amount (uL)	Matrix Spike Amount (uL)	Extract F. Volume (mL)	Comments
1		BLK	2.00 g	lu 0001		20.0mL	W6221670-01
2		US.	1 7	1	10000	1	
3		LCS OUP	1		لم		-03
4		09-004-01	2.01				
5		-02	2-04				
6		-03	2-09				
7		-04	2-03				
8		-05	2.01				
9		-06	2-07	4		1	
10							
11							
12							
13							
14							
15					\sim		
16	-				5 001		
17					010	2/0/	
18						2/06	
19							
20							
21		-					
22							
23							
24							

All soil samples are air dried to a constant weight prior to extraction All extracts are filtered through a 0.45 um teflon **ACRODISC** prior to analysis Reviewed by:

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KEMRON Environmental Services HOLDING TIMES

EQUIVALENT TO AFCEE FORM 9

00091755

Analytical Method:8330 Login Number: L0609004 AAB#: WG221826

	Date	Date	Date	Max Hold	Time Held	Date	Max Hold	Time Held	
Client ID	Collected	Received	Extracted	Time Ext.	Ext.	Analyzed	Time Anal	Anal.	Q
29-WL-12	08/31/06	09/01/06	09/07/06	14	6.85	09/08/06	40	1.43	
29-WL-12	08/31/06	09/01/06	09/07/06	14	6.85	09/11/06	40	4.37	
32-WL-05	08/31/06	09/01/06	09/07/06	14	6.88	09/08/06	40	1.46	
32-WL-05	08/31/06	09/01/06	09/07/06	14	6.88	09/11/06	40	4.40	
29-SD-48	08/31/06	09/01/06	09/07/06	14	6.95	09/08/06	40	1.49	
29-SD-49	08/31/06	09/01/06	09/07/06	14	6.94	09/08/06	40	1.51	
29-SD-47	08/31/06	09/01/06	09/07/06	14	6.96	09/08/06	40	1.54	
29-SD-49-QC	08/31/06	09/01/06	09/07/06	14	6.94	09/08/06	40	1.56	

^{*} EXT = SEE PROJECT QAPP REQUIREMENTS

^{*}ANAL = SEE PROJECT QAPP REQUIREMENTS

SURROGATE STANDARDS

00091756

Login Number:L0609004
Instrument Id:HPLC4
Workgroup (AAB#):WG221826

Method:8330

CAL ID: HPLC4-10-AUG-06

Matrix:SOLID

Sample Number	Dilution	Tag	1
L0609004-01	1.00	01	93.6
L0609004-01	10.0	DL1	<u>13.9</u>
L0609004-02	1.00	01	97.3
L0609004-02	10.0	DL1	11.4
L0609004-03	1.00	01	105
L0609004-04	1.00	01	96.3
L0609004-05	1.00	01	97.8
L0609004-06	1.00	01	95.1
WG221670-01	1.00	01	96.0
WG221670-02	1.00	01	95.6
WG221670-03	1.00	01	94.6

Surrogates

Surrogate Limits

1 - 3,4-Dinitrotoluene

50 - 150

Underline = Result out of surrogate limits

DL = surrogate diluted out
ND = surrogate not detected

METHOD BLANK SUMMARY

00091757

Work Group: WG221826
Blank Sample ID: WG221670-01
Instrument ID: HPLC4
Method: 8330

This Method Blank Applies To The Following Samples:

Client ID	Lab Sample ID	Lab File ID	Time Analyzed	TAG
LCS2	WG221670-03	4L009140.F	09/08/06 17:49	01
29-WL-12	L0609004-01	4L009141.F	09/08/06 18:26	01
32-WL-05	L0609004-02	4L009142.F	09/08/06 19:03	01
29-SD-48	L0609004-03	4L009143.F	09/08/06 19:40	01
29-SD-49	L0609004-04	4L009144.F	09/08/06 20:17	01
29-SD-47	L0609004-05	4L009145.F	09/08/06 20:55	01
29-SD-49-QC	L0609004-06	4L009146.F	09/08/06 21:32	01
LCS	WG221670-02	4L009151.F	09/11/06 16:20	01
29-WL-12	L0609004-01	4L009152.F	09/11/06 16:57	DL1
32-WL-05	L0609004-02	4L009153.F	09/11/06 17:34	DL1

METHOD BLANK REPORT

00091758

 Login Number: L0609004
 Run Date: 09/08/2006
 Sample ID: WG221670-01

 Instrument ID: HPLC4
 Run Time: 16:34
 Prep Method: METHOD

 File ID: 4L009138.F
 Analyst: JLS
 Method: 8330

 Workgroup (AAB#): WG221826
 Matrix: Solid
 Units: mg/kg

Contract #:DACA56-94-D-0020 Cal ID: HPLC4-10-AUG-06

Analytes	SQL	PQL	Concentration	Dilution	Qualifier
1,3,5-Trinitrobenzene	0.100	0.250	0.100	1	υ
1,3-Dinitrobenzene	0.100	0.250	0.100	1	υ
2,4,6-Trinitrotoluene	0.100	0.250	0.100	1	Ū
2,4-Dinitrotoluene	0.100	0.250	0.100	1	υ
2,6-Dinitrotoluene	0.100	0.260	0.100	1	Ū
2-Amino-4,6-dinitrotoluene	0.100	0.260	0.100	1	υ
2-Nitrotoluene	0.100	0.250	0.100	1	Ū
3-Nitrotoluene	0.100	0.250	0.100	1	υ
4-Nitrotoluene	0.100	0.250	0.100	1	υ
4-Amino-2,6-dinitrotoluene	0.100	0.260	0.100	1	υ
HMX	0.100	2.20	0.100	1	υ
Nitrobenzene	0.130	0.260	0.130	1	υ
RDX	0.100	1.00	0.100	1	υ
Tetryl	0.200	0.650	0.200	1	U

Surrogates	% Recovery	Surro	gate L	imits	Qualifier	
3,4-Dinitrotoluene	96.0	50	-	150	PASS	

MDL Method Detection Limit

RL Reporting/quantitation Limit

* Analyte concentration > RL

LABORATORY CONTROL SAMPLE (LCS)

		LCS			LCS2			%Rec	RPD	
Analytes	Known	Found	% REC	Known	Found	% REC	%RPD	Limits	Lmt	Q
1,3,5-Trinitrobenzene	0.500	0.500	100	0.500	0.499	99.8	0.155	75 - 125	40	Г
1,3-Dinitrobenzene	0.500	0.505	101	0.500	0.500	100	1.03	80 - 125	40	T
2,4,6-Trinitrotoluene	0.500	0.407	81.3	0.500	0.410	82.0	0.849	55 - 140	40	
2,4-Dinitrotoluene	0.500	0.535	107	0.500	0.499	99.9	6.96	80 - 125	40	T
2,6-Dinitrotoluene	0.500	0.527	105	0.500	0.554	111	5.08	80 - 120	40	
2-Amino-4,6-dinitrotoluene	0.500	0.554	111	0.500	0.669	134	18.9	80 - 125	40	*
2-Nitrotoluene	0.500	0.511	102	0.500	0.492	98.3	3.84	80 - 125	40	
3-Nitrotoluene	0.500	0.517	103	0.500	0.495	99.1	4.32	75 - 120	40	T
4-Nitrotoluene	0.500	0.526	105	0.500	0.467	93.4	11.9	75 - 125	40	
4-Amino-2,6-dinitrotoluene	0.500	0.468	93.7	0.500	0.504	101	7.34	80 - 125	40	T
нмх	0.500	0.475	94.9	0.500	0.440	88.1	7.45	75 - 125	40	
Nitrobenzene	0.500	0.499	99.8	0.500	0.491	98.2	1.57	75 - 125	40	Т
RDX	0.500	0.559	112	0.500	0.484	96.8	14.3	70 - 135	40	
Tetryl	0.500	0.428	85.6	0.500	0.418	83.7	2.35	20 - 130	40	T

	LCS	LCS2		
Surogates	% Recovery	Recovery % Recovery Su		Qualifier
3,4-Dinitrotoluene	95.6	94.6	50 - 150	PASS

* FAILS %REC LIMIT

FAILS RPD LIMIT

INITIAL CALIBRATION SUMMARY

Login Number:L0609004

Analytical Method:8330

ICAL Workgroup:WG219506

Instrument ID:HPLC4 00091760

Initial Calibration Date:10-AUG-06 19:30

Column ID:F

Analyte	AVG RF	% RSD	LINEAR	QUAD
1,3,5-Trinitrobenzene	2.503	4.27		
1,3-Dinitrobenzene	1.853	3.46		
2,4,6-Trinitrotoluene	2.638	3.49		
2,4-Dinitrotoluene	2.418	22.8	0.818	
2,6-Dinitrotoluene	4.408	9.45		
2-Amino-4,6-Dinitrotoluene	3.515	9.00		
2-Nitrotoluene	5.169	5.73		
3-Nitrotoluene	4.530	3.94		
4-Amino-2,6-Dinitrotoluene	4.280	3.91		
4-Nitrotoluene	6.317	8.42		
HMX	6.155	6.57		
Nitrobenzene	2.891	4.22		
RDX	6.185	14.6		
Tetryl	3.472	4.15		

INITIAL CALIBRATION DATA

Login Number:L0609004

Analytical Method:8330

Instrument ID:HPLC400091761
Initial Calibration Date:10-AUG-06 19:30

Column ID:F

		WG219506-0	1		WG219506-0	2		WG219506-0	3
Analyte	CONC	RESP	RF	CONC	RESP	RF	CONC	RESP	RF
1,3,5-Trinitrobenzene	1000	410.116058	2.438	500	207.627075	2.408	100	42.0826988	2.376
1,3-Dinitrobenzene	1000	548.319336	1.824	500	277.595795	1.801	100	56.5400391	1.769
2,4,6-Trinitrotoluene	1000	386.420624	2.588	500	195.437485	2.558	100	39.5971184	2.525
2,4-Dinitrotoluene	1000	240.642197	4.156	500	251.197968	1.990	100	50.9184875	1.964
2,6-Dinitrotoluene	1000			500	121.976257	4.099	100	24.9163990	4.013
2-Amino-4,6-Dinitrotoluene	1000	238.729309	4.189	500	152.127487	3.287	100	30.7204628	3.255
2-Nitrotoluene	1000			500	101.645988	4.919	100	20.3516426	4.914
3-Nitrotoluene	1000			500	115.008423	4.348	100	22.9069786	4.365
4-Amino-2,6-Dinitrotoluene	1000			500	121.125664	4.128	100	24.4640102	4.088
4-Nitrotoluene	1000			500	84.9606018	5.885	100	17.0263252	5.873
HMX	1000	169.042252	5.916	500	90.1942596	5.544	100	16.3395462	6.120
Nitrobenzene	1000	354.979858	2.817	500	179.311600	2.788	100	36.4564056	2.743
RDX	1000	182.905731	5.467	500	92.5733414	5.401	100	18.2953339	5.466
Tetryl	1000	295.412659	3.385	500	149.222870	3.351	100	30.2906513	3.301

INITIAL CALIBRATION DATA

Login Number:L0609004

Analytical Method:8330

Instrument ID: HPLC4 00091762 Initial Calibration Date: 10-AUG-06 19:30

Column ID:F

		WG219506-0	4		WG219506-0	5		WG219506-0	6
Analyte	CONC	RESP	RF	CONC	RESP	RF	CONC	RESP	RF
1,3,5-Trinitrobenzene	50.0	19.1474266	2.611	25.0	9.62814522	2.597	10.0	3.86683512	2.586
1,3-Dinitrobenzene	50.0	25.9892025	1.924	25.0	13.0911617	1.910	10.0	5.28941250	1.891
2,4,6-Trinitrotoluene	50.0	18.2330532	2.742	25.0	9.31017685	2.685	10.0	3.66835594	2.726
2,4-Dinitrotoluene	50.0	23.2483425	2.151	25.0	11.9094486	2.099	10.0	4.65987062	2.146
2,6-Dinitrotoluene	50.0	11.3105459	4.421	25.0	5.74631023	4.351	10.0	1.93934882	5.156
2-Amino-4,6-Dinitrotoluene	50.0	14.0588083	3.556	25.0	7.13465643	3.504	10.0	3.03034019	3.300
2-Nitrotoluene	50.0	9.48513603	5.271	25.0	4.91147327	5.090	10.0	1.76889133	5.653
3-Nitrotoluene	50.0	10.7789402	4.639	25.0	5.51862288	4.530	10.0	2.09677839	4.769
4-Amino-2,6-Dinitrotoluene	50.0	11.2209272	4.456	25.0	5.79186916	4.316	10.0	2.26526356	4.414
4-Nitrotoluene	50.0	7.76470518	6.439	25.0	4.07508135	6.135	10.0	1.37910843	7.251
HMX	50.0	7.68003368	6.510	25.0	3.77735090	6.618	10.0	1.60739887	6.221
Nitrobenzene	50.0	16.7608624	2.983	25.0	8.35599613	2.992	10.0	3.30798101	3.023
RDX	50.0	7.96912861	6.274	25.0	3.91651797	6.383	10.0	1.23154259	8.120
Tetryl	50.0	13.8570604	3.608	25.0	7.04509830	3.549	10.0	2.74744797	3.640

ALTERNATE SOURCE CALIBRATION REPORT

Login Number: L0609004 Run Date: 08/10/2006 Sample ID: WG219506 91763

Run Time: 20:07 Method: 8330

File ID: 4L008953.F Analyst: JLS

ICal Workgroup: WG219506 Cal ID: HPLC4 - 10-AUG-06

Analyte	Expected	Found	RF	%D	UNITS	Q
1,3,5-Trinitrobenzene	50	49.0	2.49	2.1	ug/L	
1,3-Dinitrobenzene	50	48.1	1.88	3.8	ug/L	
2,4,6-Trinitrotoluene	50	48.7	2.65	2.5	ug/L	
2,4-Dinitrotoluene	50	48.1	2.08	3.9	ug/L	
2,6-Dinitrotoluene	50	51.0	4.07	1.9	ug/L	
2-Amino-4,6-Dinitrotoluene	50	53.4	3.11	6.9	ug/L	
2-Nitrotoluene	50	51.2	4.86	2.4	ug/L	
3-Nitrotoluene	50	50.2	4.37	.4	ug/L	
4-Nitrotoluene	50	51.9	5.78	3.8	ug/L	
4-Amino-2,6-Dinitrotoluene	50	49.3	4.23	1.5	ug/L	
нмх	50	43.9	6.61	12.1	ug/L	
Nitrobenzene	50	48.7	2.89	2.5	ug/L	
RDX	50	49.2	5.86	1.6	ug/L	
Tetryl	50	48.1	3.53	3.9	ug/L	

^{*} Exceeds %D Limit

CONTINUING CALIBRATION VERIFICATION (CCV)

Login Number: L0609004 Run Date: 09/08/2006 Sample ID: WG2 10091764

Instrument ID: HPLC4 Run Time: 15:57 Method: 8330

File ID: 4L009137.F Analyst: JLS

Analyte	Expected	Found	RF	%D	UNITS	Q
Sym-Trinitrobenzene	50.0	47.8	2.55	4.30	ug/L	
1,3-Dinitrobenzene	50.0	48.0	1.88	3.90	ug/L	
2,4,6-Trinitrotoluene	50.0	47.4	2.72	5.10	ug/L	
2,4-Dinitrotoluene	50.0	47.6	2.10	4.80	ug/L	
2,6-Dinitrotoluene	50.0	49.0	4.24	2.00	ug/L	
2-Amino-4,6-Dinitrotoluene	50.0	48.5	3.43	3.00	ug/L	
2-Nitrotoluene	50.0	49.1	5.08	1.90	ug/L	
3-Nitrotoluene	50.0	48.5	4.52	3.00	ug/L	
4-Nitrotoluene	50.0	62.9	4.76	25.8	ug/L	*
4-Amino-2,6-Dinitrotoluene	50.0	48.9	4.26	2.20	ug/L	
нмх	50.0	43.1	6.74	13.8	ug/L	
Nitrobenzene	50.0	47.6	2.96	4.90	ug/L	
RDX	50.0	46.5	6.23	7.10	ug/L	
Tetryl	50.0	50.7	3.34	1.40	ug/L	

^{*} Exceeds %D Criteria

CONTINUING CALIBRATION VERIFICATION (CCV)

Login Number: L0609004 Run Date: 09/08/2006 Sample ID: WG2202091765

Instrument ID: HPLC4 Run Time: 22:09 Method: 8330

File ID:4L009147.F Analyst:JLS

Workgroup (AAB#):WG221826_____ Cal ID: <u>HPLC4 - 10-AUG-06</u>

Analyte	Expected	Found	RF	%D	UNITS	Q
Sym-Trinitrobenzene	50.0	47.6	2.57	4.90	ug/L	
1,3-Dinitrobenzene	50.0	47.9	1.89	4.20	ug/L	
2,4,6-Trinitrotoluene	50.0	47.2	2.73	5.60	ug/L	
2,4-Dinitrotoluene	50.0	48.2	2.08	3.50	ug/L	
2,6-Dinitrotoluene	50.0	50.7	4.10	1.40	ug/L	
2-Amino-4,6-Dinitrotoluene	50.0	49.5	3.36	1.10	ug/L	
2-Nitrotoluene	50.0	48.1	5.18	3.70	ug/L	
3-Nitrotoluene	50.0	48.0	4.58	4.10	ug/L	
4-Nitrotoluene	50.0	59.1	5.07	18.1	ug/L	*
4-Amino-2,6-Dinitrotoluene	50.0	48.5	4.29	2.90	ug/L	
нмх	50.0	42.7	6.81	14.7	ug/L	
Nitrobenzene	50.0	47.1	2.99	5.80	ug/L	
RDX	50.0	43.0	6.77	14.1	ug/L	
Tetryl	50.0	50.1	3.39	0.200	ug/L	

^{*} Exceeds %D Criteria

CONTINUING CALIBRATION VERIFICATION (CCV)

Login Number:L0609004 Run Date:09/11/2006 Sample ID:WG2**100091766**Instrument ID:HPLC4 Run Time:15:40 Method:8330

File ID:4L009150.F Analyst:JLS

Workgroup (AAB#):WG221826 Cal ID: HPLC4 - 10-AUG-06

Analyte	Expected	Found	RF	%D	UNITS	Q
Sym-Trinitrobenzene	50.0	49.3	2.48	1.30	ug/L	
1,3-Dinitrobenzene	50.0	49.1	1.84	1.80	ug/L	
2,4,6-Trinitrotoluene	50.0	48.3	2.67	3.50	ug/L	
2,4-Dinitrotoluene	50.0	47.3	2.12	5.40	ug/L	
2,6-Dinitrotoluene	50.0	48.7	4.27	2.70	ug/L	
2-Amino-4,6-Dinitrotoluene	50.0	48.7	3.41	2.60	ug/L	
2-Nitrotoluene	50.0	50.1	4.97	0.200	ug/L	
3-Nitrotoluene	50.0	52.0	4.22	4.00	ug/L	
4-Nitrotoluene	50.0	52.7	5.69	5.40	ug/L	
4-Amino-2,6-Dinitrotoluene	50.0	49.0	4.25	2.00	ug/L	
нмх	50.0	45.1	6.44	9.80	ug/L	
Nitrobenzene	50.0	48.9	2.88	2.20	ug/L	
RDX	50.0	46.6	6.20	6.70	ug/L	
Tetryl	50.0	51.5	3.29	3.00	ug/L	

^{*} Exceeds %D Criteria

CONTINUING CALIBRATION VERIFICATION (CCV)

Login Number:L0609004 Run Date:09/11/2006 Sample ID:WG2**09091767**Instrument ID:HPLC4 Run Time:18:11 Method:8330

File ID:4L009154.F Analyst:JLS

Workgroup (AAB#):WG221826 Cal ID: HPLC4 - 10-AUG-06

Analyte	Expected	Found	RF	%D	UNITS	Q
Sym-Trinitrobenzene	50.0	48.9	2.50	2.20	ug/L	
1,3-Dinitrobenzene	50.0	52.6	1.72	5.20	ug/L	
2,4,6-Trinitrotoluene	50.0	47.0	2.74	5.90	ug/L	
2,4-Dinitrotoluene	50.0	49.7	2.02	0.700	ug/L	
2,6-Dinitrotoluene	50.0	52.0	4.00	3.90	ug/L	
2-Amino-4,6-Dinitrotoluene	50.0	49.8	3.33	0.400	ug/L	
2-Nitrotoluene	50.0	52.1	4.78	4.20	ug/L	
3-Nitrotoluene	50.0	51.3	4.28	2.50	ug/L	
4-Nitrotoluene	50.0	54.7	5.48	9.40	ug/L	
4-Amino-2,6-Dinitrotoluene	50.0	48.0	4.33	3.90	ug/L	
нмх	50.0	44.1	6.59	11.8	ug/L	
Nitrobenzene	50.0	47.8	2.95	4.30	ug/L	
RDX	50.0	47.6	6.06	4.70	ug/L	
Tetryl	50.0	54.0	3.14	8.00	ug/L	

^{*} Exceeds %D Criteria

KEMRON Environmental Services Data Checklist

00091768

Date: <u>08-SEP-2006</u>	
Analyst: TMM	
Analyst: NA	
Method: PCT-S	
Instrument: OVEN	
Curve Workgroup: NA	
Runlog ID:	
nalytical Workgroups: WC221770	

Calibration/Linearity	09/08/06
Second Source Check	
CV/CCV (std)	
CB/CCB	
Blank	
LCS/LCS Dup	
MS/MSD	
Duplicate	Х
Upload Results	Х
Client Forms	X
QC Violation Sheet	
Case Narratives	
Signed Raw Data	Х
STD/LCS on benchsheet	
Check for compliance with method and project specific requirements	X
Check the completeness of reported information	X
Check the information for the report narrative	Х
Primary Reviewer	TMM
Secondary Reviewer	DIH
Comments	

Primary Reviewer: 11-SEP-2006 Secondary Reviewer: 13-SEP-2006

Jammy morris Dannalpsson

Generated: SEP-13-2006 07:55:53

B2452

00091769

	Houston, TX 77042 (713) 996-4400 CHAIN-OF-CUSTODY Translite fine # Ditch No. 10407														
L	aboratory Name:	von			Add	raca:	Marvetta, Ob	_	Conta						
'roje	ct Name LHAAP			Proje	ct Loca	ition 7	varsif ine/Kamuck	7			and Metho separate o				Remarks
roje	ct No.		Project	Contac	t .		Project Telephone No.) jers	8						
	of contact: hone No.					Projec	t Manager/Supervisor:	Number of Containers	165/cm						
Š.	Sample Number	Date	Time	Comp	Grab	Matrix	Sample Description, Location		EN	 		-			
1	29-WL-12	8/31	1/30		X	5		- 1	入						
2	29-WL-12 32-WL-05		1050		Х	3		١	X						X Place grake Very good MIX
3	29-517-48		915		Х	3		١	X						
	29-SD-49		930		X	3		1	X						
5	29-SD-47		900		አ	5		1	X						
6	29-5D-49-QC		930		X	5		1)	X						
7															
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9															
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	Transfers Relinquished By (Signat	ture)	<u> </u>	ite/Tim		Tr	ansfers Accepted By (Signature)	Date	/Time	Special Ins	tructions	•			le sealed to what only semp
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,			<u> </u>				EmaCregory		01	Sampler	Signature		<u>All</u> z	/	
	TAT: Standard Rust	Due:		Se	eals inta	ict?	YN Received G	ood Condition	<u>'</u>	N_	% fd	_/_			

White - Lab Copy Canary - Field Copy Pink - File Copy

SAMPLE RECEIPT FORM

00091770

Date: 9-01-06 Client: Shaus	• · ·
Shipped By: () Fed-Ex (+OPS ()DHL () KEMRON () Client () Other	er 9 130
Opened By:	
Logged By: Login # L06_09004	
IR Temp Gun: () D S	

156 STARLITE DRIVE MARIETTA, OH 45750 (740) 373-4071

Revised 8/22/03

COOLER INFORMATION

Comments:_

Number	Cooler ID	Temp °C	Airbill#	COC#	Other
· 1	1462	3	124016632210054751		
2					
3					
4					
. 5					
6					

6					<u> </u>								
Were all	l coolers seale	ed?		(Ø	N	N/A						
Were cu	ustody seals u	(0	N	N/A								
Were cu	ustody seals ir	itact?			Ø	N	N/A						
Was vis	ible ice preser	nt?		(\bigcirc	N	N/A						
Were all	l coolers in the	e tempera	ture range of 2-6C? (>6	SC*) (3	N	N/A	-					
Were th	e samples fro	zen?*			Y	N	N/A						
Were Co	OC papers pro	ovided?		(4	N	_N/A		-				_
Were all	l sample conta	ainers inta	ct?*	. 6	\bigcirc	N	N/A						
Were all	l sample label	s intact?		۷	D	N	N/A			. ~			
Were all	l sample label	s legible?	•	(\mathcal{L}	N	N/A						
Did all s	ample labels	match the	COC?*	(\bigcirc	N	N/A		•	•			
Was the	a label informa	tion comp	lete?*	4	\mathcal{L}	Ν	N/A						
Were th	e correct cont	ainers use	ed?*	C	\bigcirc	Ν	N/A						
Were th	e correct pres	ervatives	added to water sample	s?*	Υ	N	MA.	7					
Was the	pH tested on	preserve	d water samples?		Υ	N	/N/A	()					
Were pl	H ranges acce	ptable?*			Y	N	N/A	/					
Was sut	fficient amoun	t of sampl	e provided?*		Y	N	N/A						
Were bu	ubbles presen	t in VOA s	amples?*		Y	N	(N/A	\geq					
Were C	OC's signed a	nd dated?	-	(Y	Ŋ	N/A				•		
Did sam	nples arrive be	fore hold	time expired?*	(D	Ν	N/A						
	crepancy forma res a discrepa		?		Υ	N	N/A)					
												CDE #1	

Internal Chain of Custody Report

Login: L0609004 Account: 2773 Project: 2773.025

Samples: 6

Due Date: 12-SEP-2006

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0609004-01</u> 270773 PCT-S 8330

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:56	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

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<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0609004-02</u> 270774 8330 PCT-S

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:57	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0609004-03</u> 270775 8330 PCT-S

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:57	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0609004-04</u> 270776 8330 PCT-S

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:57	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

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Internal Chain of Custody Report

Login: L0609004
Account: 2773
Project: 2773.025

Samples: 6

Due Date: 12-SEP-2006

 Samplenum
 Container ID
 Products

 L0609004-05
 270777
 8330 PCT-S

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:57	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

<u>Samplenum</u> <u>Container ID</u> <u>Products</u> <u>L0609004-06</u> 270778 8330 PCT-S

Bottle: 1

Seq.	Purpose	From	То	Date/Time	Accept	Relinquish
1	LOGIN			01-SEP-2006 10:23	BRG	
2	PREP	W1	EXT	05-SEP-2006 13:57	CEB	BRG
3	PREP	W1	EXT	05-SEP-2006 14:05	BRG	CEB
4	ANALYZ	W1	WET	07-SEP-2006 08:03	FJB	JKT
5	STORE	WET	A1	09-SEP-2006 10:27	BRG	TMM

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